

# **CARBON NANOTUBE BASED THIN FILM TRANSISTORS FOR GAS-SENSING AND ELECTRONIC APPLICATIONS**

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by

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# **CARBON NANOTUBE BASED THIN FILM TRANSISTORS FOR GAS-SENSING AND ELECTRONIC APPLICATIONS**

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## LIST OF SYMBOLS AND ABBREVIATIONS

### *Abbreviations*

abs	Absolute value
AFM	Atomic force microscope
AJ200	The aerosol jet 200 system
AJP	Aerosol jet printing
ALD	Atomic layer deposition
AMECD	Active-matrix electrochromic display
AMOLED	Active matrix organic light-emitting diode
$A_{s\_white}$	White pixel area in the sample binary image
$A_t$	Total area of the target SEM image
$A_{t\_white}$	White pixel area in the target binary image
ChemFET	Chemical field-effect transistor
CMOS	Complementary metal–oxide–semiconductor
CNT	Carbon nanotube

CNT-FET	Carbon nanotube field-effect transistor
CNT-TFT	Carbon nanotube thin film transistor
cP	Unit of centipoise
CVD	Chemical vapor deposition
DI	Deionized (water)
$D_{s\_CNT}$	Average CNT diameter in the sample binary image
$D_{t\_CNT}$	Average CNT diameter in the target binary image
FET	Field-effect transistor
G	Gate electrodes
GND	Grounded
h	Height of the pulse signal in a sensing cycle
IC	Integrated circuit
$I_d$	Drain current
$I_{d(sat)}$	Saturated drain current
IEN	Institute for Electronics and Nanotechnology
IJP	Inkjet printing
IPA	Isopropyl alcohol

L	Channel length
LCP	Liquid crystal polymer
Ls	The mean length of CNTs
L <sub>s_CNT</sub>	Total CNT length in the sample binary image
L <sub>t_CNT</sub>	Total CNT length in the target binary image
m	A universal exponent of CNT percolating system
MOS	Metal-oxide-semiconductor
MOSFET	Metal-oxide-semiconductor field-effect transistor
MWCNT	Multi-walled carbon nanotube
M-CNT	Metallic carbon nanotube
NAND	A digital logic NAND gate
nIR	Near-infrared
NOR	A digital logic NOR gate
PDF	Probability distribution function
PDMS	Polydimethylsiloxane
PEI	Poly (ethylene imine)
PET	Poly(ethylene terephthalate)

PL	Photolithography
PR	Photoresist
PS	Printing speed
PVD	Physical vapor deposition
PVP/PMSSQ	Poly(vinylphenol)/poly(methyl silsesquioxane)
R	Resistance of a CNT device over time
R <sub>c</sub>	Contact resistance between CNTs and electrodes
RF	Radio frequency
RFID	Radiofrequency identification
RIE	Reactive-ion etching
R <sub>m</sub>	Maximum or minimum resistance of a sensor in a sensing cycle
R <sub>o</sub>	Stable resistance of a CNT device before gas spray
R <sub>SD</sub>	Total resistance of random CNT network in the channel
S	Sensitivity of a sensor
SEM	Scanning electron microscope
SG	Sheath gas flow rate
SMUs	Source measurement units

SRAM	Static random-access memory
SWCNT	Single-walled carbon nanotube
S/D	Source and drain electrodes
S-CNT	Semiconducting carbon nanotube
t	Time
TEM	Transmission electron microscope
TFT	Thin film transistor
TLM	Transfer length method
$t_o$	Time of onset point in a sensing cycle
UA	Ultrasonic atomizer flow rate
UHV	Ultrahigh vacuum
$V_{dd}$	Supply voltage
$V_{ds}$	Drain voltage
$V_{gs}$	Gate voltage
$V_{th}$	Threshold voltage
W	Channel width
xdi-dcs	Dielectric ink: a blend of PVP/PMSSQ solution

$\xi$	A function of the geometrical parameters and bias conditions
$\lambda$	Standard deviation in a distribution function
$\sigma$	Volumetric dilute ratio
$\rho$	CNT network density
$\tau_a$	Time constant in a convolution model
$\tau_b$	Time constant in a convolution model
$\mu$	Statistical mean value in a distribution function
$v$	Standard deviation for error evaluation

## SUMMARY

Single-walled carbon nanotubes (CNTs) are promising candidates for future electronic devices because of their excellent electrical, mechanical, optical and chemical properties. CNT based sensors have high potential for large scale adaptation because of its high sensitivity, fast response, and physical/chemical stability. Fabrication of CNT based devices such as thin film transistors (TFTs) by photolithography (PL) can reach high resolution, and meet the requirements of aggressive scaling of physical dimensions like Si-based metal-oxide-semiconductor field-effect transistors (MOSFETs). However, the complicated processes and need of expensive equipment of PL become a major drawback and severely limits its application in various fields. Fully printed CNT-TFTs, using inkjet (IJP) or aerosol jet (AJP) printing, possess tremendous advantages in design versatility and operational customization for sensing devices. They are also very promising for cost-effective and scalable production of flexible/wearable devices. However, the performance of CNT-TFTs and their usage as CNT sensors need to be significantly improved.

For CNT-TFTs fabricated by PL, device-to-device performance variability can pose challenging problems for its practical applications. To address this issue, both experimental and theoretical methods were employed to analyze the variability in I–V characteristics in a statistical framework. For the experimental analysis, array of CNT-TFTs were fabricated with high-k dielectric  $\text{HfO}_2$  as gate oxide layer to achieve high performance. For the theoretical part, the current scaling relationship was applied to analyze variation sources such as % of metallic CNTs (M-CNTs), threshold voltage, CNT mean length, etc. Results show that a better consistency in performance can be guaranteed for TFTs with larger channel area, which ensures a smaller variation in CNT network density and CNT mean length. The fabricated CNT-TFTs can be used

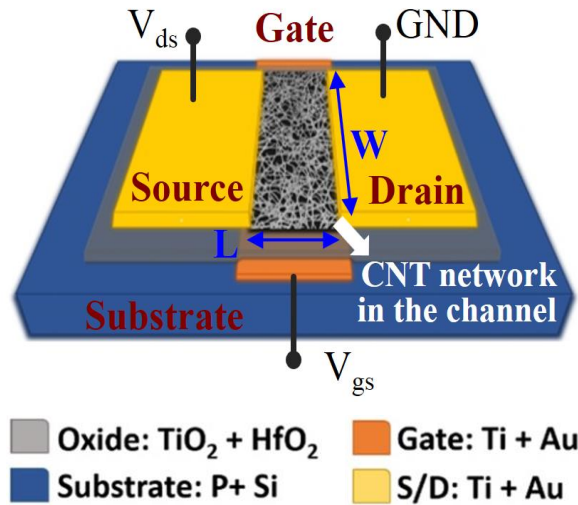


as gas sensors for ammonia and nitrogen dioxide detection at low ppm concentrations. To improve the selectivity of CNT sensors, a double exponential-convolution model was developed to decipher sensor response as well as to explore its application in gas identification. The uniqueness of time constants of the model can work as identity verification for different sensing gases, which demonstrates that the sensor response is a distinctive behavior determined by the unique channel structure of each TFT.

For fully printed CNT-TFTs, the performance is mainly limited by the printed gate dielectric. Its relatively large thickness can result in high gate voltage to switch on and off the transistors, which will cause high power dissipation for printed devices. In response to address this challenge, fully printed CNT-TFTs have been fabricated on flexible substrates using AJP. The devices show very stable performance including high on/off ratio, high mobility, negligible hysteresis, and good uniformity. More importantly, these devices can be operated using bias voltages as small as  $\pm 5\text{V}$ , which is much smaller than the previously reported values and is a consequence of the improvement in printing both CNT network and gate dielectric layer. The fully printed CNT sensors are also fabricated using AJP or IJP separately. Compared to PL, printed sensors show no degradation with respect to sensitivity and stability, but can be fabricated at much lower cost. Besides, the sensitivity of printed CNT sensors can be highly improved using post drop-cast CNT deposition without any surface functionalization. This work provides key insights for the fabrication and usage of extremely low-cost CNT gas sensors, which has immense potential in flexible and wearable devices as well as air quality detection and industrial emission control.

## CHAPTER 1. INTRODUCTION

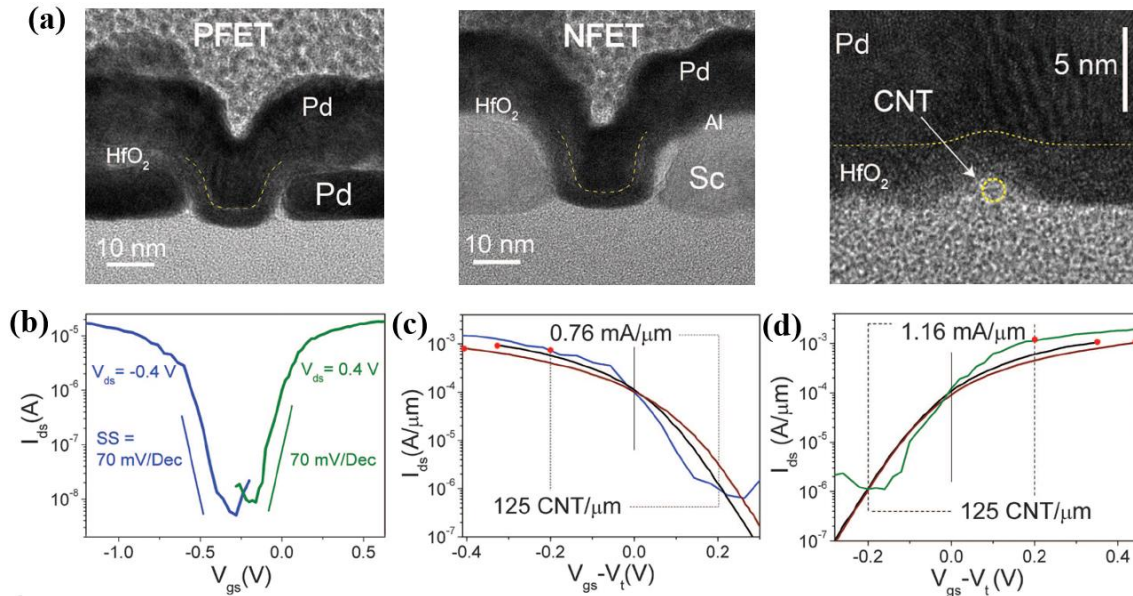
Carbon nanotubes (CNTs) are one-dimensional cylinders of monolayer graphene which is made of carbon atoms arranged in a hexagonal / honeycomb structure with open or close ends. It is a promising candidate for future nanoscale devices[1]. Diameters of CNTs can range between 0.8 nm to 20 nm and their lengths can be as large as several centimeters. The advantages of the CNT mainly lie in its remarkable properties such as high carrier mobility, excellent thermal conductivity, high mechanical flexibility, and high photo transparency, etc. Field-effect transistors (FETs) are the most common type of transistors, which are the basic building blocks used in amplifiers, switches as well as logic, memory, and sensors [2-4]. The structure of a typical CNT-FET with randomly distributed CNT network is illustrated in Figure 1.1. Other CNT-FETs with single CNT and aligned CNT network in the channel are also extensively used in different applications. The unique properties make CNTs, especially single-wall carbon nanotubes (SWCNTs) a perfect material for transistors.



**Figure 1.1** Schematic of a CNT-TFT with randomly distributed CNT network. W is channel width, L is channel length, V<sub>ds</sub> is drain voltage, V<sub>gs</sub> is gate voltage, and GND is grounded.

## 1.1 Progress in CNT based Devices

Ever since Gordon E. Moore made a prediction on doubling the number of transistors on IC every two years, the semiconductor industry has been driven to reach this goal mostly by scaling down the size of transistors [5]. The projection has been achieved when the device dimension was reduced to sub-22nm. At this level, the steady growth of transistor numbers started to slow down due to limitations from both miniaturization and device performance. The decreased size problems will cause short channel effect, current leakage, and power dissipation[6-8].



**Figure 1.2 Structure and performance of 10-nm CNT based complementary metal-oxide semiconductor (CMOS) FETs [9]. (a) The cross sections of a p-type FET, n-type FET, and gate stack; gate length 10 nm, channel length 20 nm. (b) Transfer characteristics of typical CMOS FETs fabricated on a s-SWCNT with a diameter of 1.3 nm at a drain bias  $V_{ds} = \pm 0.4$  V. The solid blue and green curves represent CNT p-type and n-type FETs, respectively. (c and d) Comparison of 10-nm CNT CMOS FETs and commercial Si CMOS transistors of Intel's 14-nm (22) (solid black curve) and 22-nm nodes (23) (solid maroon curve). The on currents of n-FETs for CNT, Si 14-nm node, and Si 22-nm node are 1.16 mA/mm (supply voltage  $V_{dd} = 0.4$  V, 125 CNTs/mm), 1.1 mA/mm ( $V_{dd} = 0.7$  V), and 1.03mA/mm ( $V_{dd} = 0.8$  V), respectively. The on-currents of p-FETs for CNT, Si 14-nm node, and Si 22-nm node are 0.76 mA/mm ( $V_{dd} = 0.4$  V, 125 CNTs/mm), 0.96 mA/mm ( $V_{dd} = 0.7$  V), and 0.83mA/mm ( $V_{dd} = 0.8$  V), respectively. CNT CMOS FETs and 14- and 22-nm Si CMOS FETs have gate lengths of 10 nm, 20 nm, and 26 to 30 nm, respectively. Copyright (2017) American Association for the Advancement of Science.**

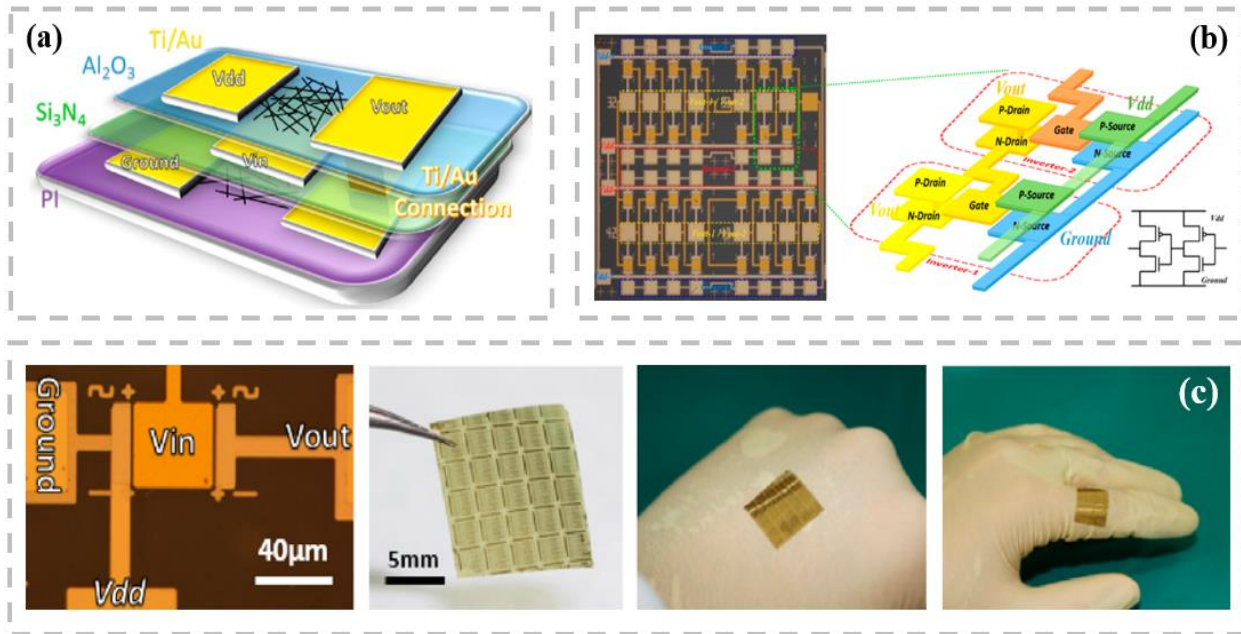
CNT-FETs are one of the promising alternatives for further miniaturization and they have been widely researched. Even though good progresses have been made, their high application potential still needs to be exploited to take the place of conventional metal-oxide-semiconductor field-effect transistors (MOSFETs) in the future. As a new generation of transistors, CNT-FETs have significant advantages such as low power consumption, high flexibility, and high operation speed [9, 10]. CNT-TFTs are also promising for flexible microelectronic applications because of their high mobility, substrate-neutrality, and low-temperature fabrication process. These capabilities enable a wide range of applications such as wearable/flexible e-displays, disposable electronics, chemical/biological sensors, etc. [3, 11-19]

Figure 1.2 shows the transmission electron microscope (TEM) images of the cross sections of CNT-FETs (with gate length 10 nm and channel length 20 nm; the smallest size can reach 5 nm) and the performance comparison with transistors fabricated by Intel. It turned out that the performance of CNT-FETs is better than silicon complementary metal-oxide semiconductor (CMOS) FETs at the same scale. The 5 nm CNT-FETs actually approached the quantum limit of FETs by using only one electron per switching operation.

Most of these advantages root in the excellent performance of CNTs, which can be classified as either single-walled (SWCNT) or multi-walled carbon nanotube (MWCNT). As a one-dimensional nanoscale material, individual CNTs exhibit exceptional electrical, mechanical, chemical, thermal, and optical properties. SWCNTs have exceptional high current carrying capacity as its mobility can reach as high as  $100,000 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  [10, 20]. Extraordinary flexibility and elasticity can also be expected when it undergoes high strain and bending. Aligned SWCNT based thin film transistors (TFTs) have certain advantages such as small TFT dimensions, high mobility, and only few CNTs are needed per channel. The CNT network based TFT is also of high

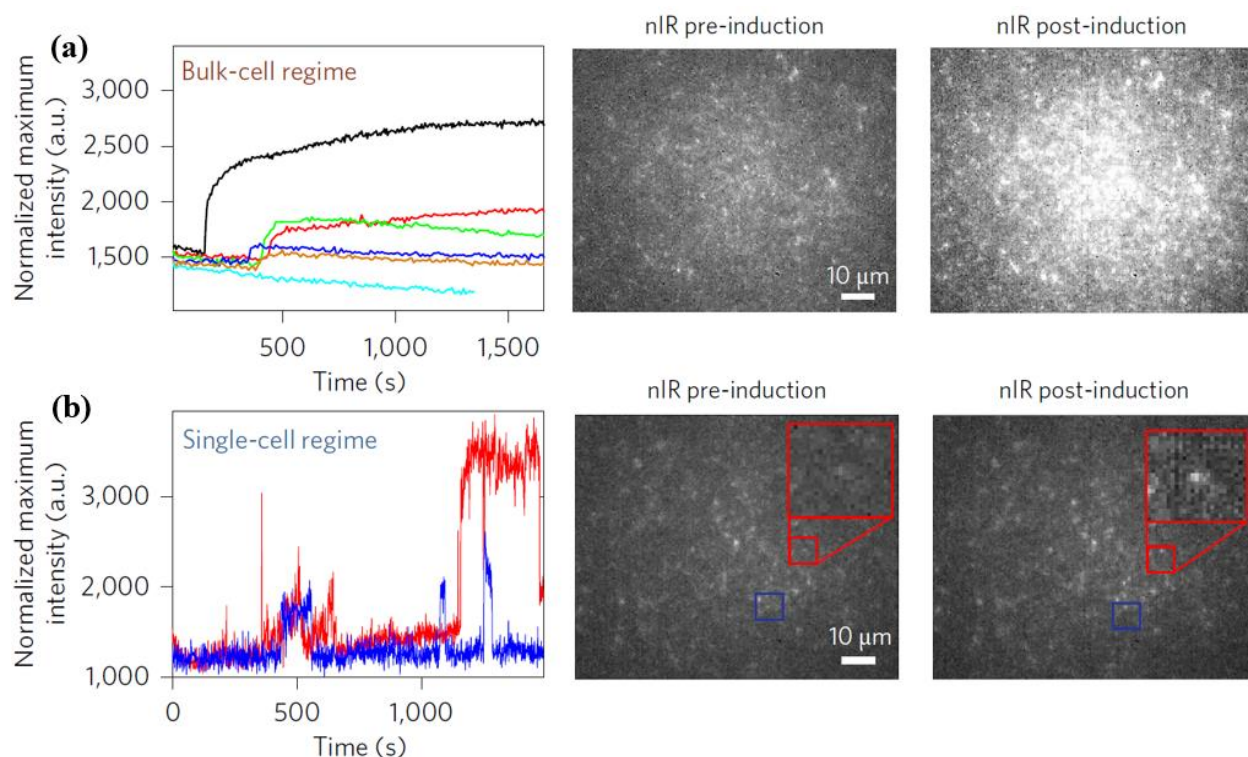
interest for low-cost and large area electronic applications such as antennae, RF tags, sensors, etc. as it is much easier to fabricate on both flexible and hard substrates [21, 22]. In recent years, the cost of CNTs has significantly dropped and the large amount of CNT usage per TFT is not necessarily a major concern from a cost standpoint.

Figure 1.3 presents one of the applications in three-dimensional flexible CMOS logic circuits [22]. These flexible SWCNT-TFT CMOS circuits have a 3D structure based on a two-layer stack of SWCNT networks. Other 3D flexible circuits such as CMOS NOR, NAND logic gates, and 15-stage ring oscillators were fabricated on the same polyimide substrates with high performance as well, which also showed stable electrical properties with bending radii as small as 3.16mm. It demonstrates this 3D structure is a reliable architecture and suitable for carbon nanotube electrical applications in complex flexible and wearable electronic devices.



**Figure 1.3 (a) Schematic of 3D flexible CMOS CNT-TFT inverter. (b) Optical microscope photo of the two nested 3D CMOS ring oscillators. (c) Optical images of 3D flexible CMOS inverter arrays based on CNT-TFTs formed on polyimide substrate [22]. Copyright (2016) ACS Publications.**

The sensitivity of CNTs has been utilized in sensor applications because of its unique structure for high sensitivity. As sensor material, CNTs have large surface area and exhibit charge-sensitive conductance, which attributes to the carbon atoms and C-C bonds on the tube surface [23]. The conductance of CNTs is known to be sensitive to ambient environment, especially to oxygen and oxygen-containing gaseous species [24, 25]. In addition, CNT sensors can also work for the detection of hydrogen ( $H_2$ ) [26, 27], organic vapors [28], alcohols [29], protein [30], etc. which has huge practical significance for disease and health diagnosis [31-33]. CNT based sensors can also benefit from their low cost, room temperature operation, and nanoscale and microelectronics applications [10, 34, 35].



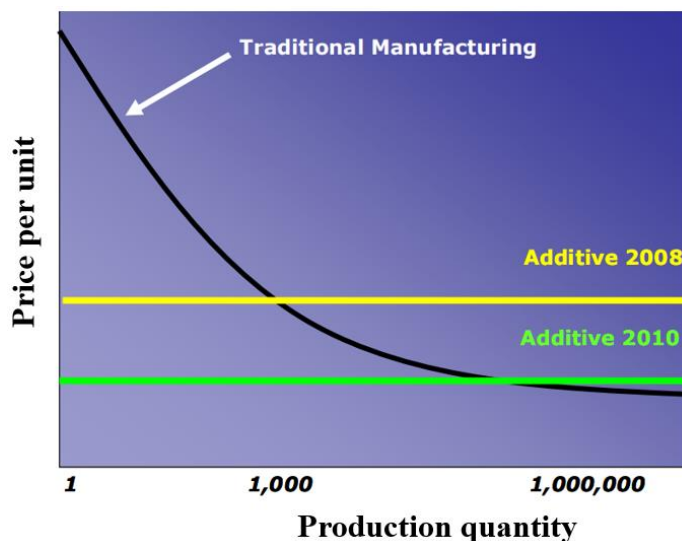
**Figure 1.4** Detection of protein from *crude cell lysate* and from *Escherichia coli* (*E. coli*) (bacteria) engineered to secrete target protein [30]. (a) Concentration–response curves for 0 (cyan),  $1 \times 10^8$  (orange),  $4 \times 10^8$  (blue),  $7 \times 10^8$  (red),  $1 \times 10^9$  (green) and  $1.6 \times 10^9$  (black) c.f.u. ml<sup>-1</sup> *E. coli*. (b) Two representative single-sensor fluorescence intensity traces (red and blue) for an agarose gel-immobilized *E. coli* bacterium. Copyright (2017) Nature Publishing Group.



Figure 1.4 plots the detection of protein efflux from microorganisms using fluorescent SWCNT based sensor arrays. Protein binding to aptamer targets on SWCNTs subsequently relays an optical signal in the near-infrared (nIR) optical window. And SWCNTs are the only fluorophores to date that have essentially infinite lifetimes and are not susceptible to on–off blinking, as quantum dots are. Therefore, the signal produced by SWCNTs, combined with the selectivity provided by aptamers, provides much promise for the long-term optical monitoring of specific protein targets from within crude biological samples over long timescales [30]. As nanosensor arrays, which can provide a distinct way to achieve ultralow detection limits in solution by proximity placement to an analyte, they enable real-time, single-cell analysis of different protein products from various cells.

## 1.2 Motivation and Challenges

### 1.2.1 Fabrication



**Figure 1.5** The aerosol jet process provides a cost-effective solution for low to moderate volume production runs or where mass customization is required. The cost per unit for printing techniques is flat regardless of volume (copyright belongs to Optomec Inc).

Even though advances in high resolution lithography process (and other traditional fabrication methods) have achieved smallest features of several nanometers for CNT based devices which almost approaches the quantum limit, the corresponding high cost has severely limited their further applications. The improvement of printing techniques, synthesis, and processing of nanomaterials has brought fresh impetus to the development of printed flexible devices[36]. First, printing techniques such as AJP and IJP can reach spatial resolution as small as  $\sim 20\text{ }\mu\text{m}$  and this spatial resolution can be further decreased in the near future. Even though they cannot compete with traditional fabrication methods in resolution, they are good enough for applications in most flexible and wearable electronics. Secondly, printing techniques have much simpler fabrication process, which do not involve too many other high-cost equipment or complicated procedures. Thus, the overall cost is much lower and it can save time when making a prototype. Moreover, incredibly resource-efficiency is also one of their major advantages because printing techniques apply the so-called “additive” process instead of a traditional “subtractive” process, which produces much less waste than traditional fabrication methods. Besides, printing techniques are also very suitable for large-scale production, etc. Figure 1.5 compares the cost between AJP printing and typical traditional fabrication methods.

However, the tradeoff between cost and performance is still an urgent problem to be solved because of the huge gap between printing techniques and traditional fabrication methods. It is becoming quite critical to fabricate microelectronics using printing techniques for cost consideration while maintain the relatively high performance and stability at the same time, which has significant potential in applications of flexible electronics.



### 1.2.2 Performance Variability

Even for devices fabricated using the PL process, device-to-device performance variation of CNT-TFTs is becoming a critical problem while trying to harvest the exceptional properties of CNTs. Performance variations of TFTs can be reflected in the variability in I-V characteristics, including output and transfer characteristics. It results from the multiple sources. The atomic structure of CNT is a source of large variation, which includes variations in diameter, defects, doping, length, etc. A CNT of similar diameter can be either metallic or semiconducting depending on its chirality, leading to significant variability in I-V characteristics. The CNT network distribution and morphology in its channel area, e.g., CNT network density, channel length, and orientation, are very different from one TFT to another because of the randomness induced during deposition. Fabrication process, especially fabrication imperfections, further affects the variability. Even though the CNTs are grown by the same method and the devices are fabricated under the same processing conditions, the I-V characteristics of TFTs can still vary.

In the previous studies, performance variation of CNT-FETs had been discussed with respect to the CNT diameter, CNT density fluctuation, CNT growth and manufacturing process. Cao et al. studied variability in threshold voltage ( $V_{th}$ ) of CNT-FETs. It showed that variability in  $V_{th}$  mainly results from the random fluctuation of fixed charges on the oxide/air interface [37, 38]. Franklin et al. analyzed the origin of variability in  $V_{th}$  and hysteresis of CNT-FETs, and tried to improve the device-to-device consistency through optimized gate dielectric and passivation layer [39]. However, most of the studies only focused on the devices using single or aligned nanotubes as channel. Performance variability of FETs with aligned CNTs [40-42] is of high interest because of large variation in FET performance with small changes in CNT structure, which had been studied to achieve better consistency. None of the previous studies reported the variability analysis

of CNT-TFTs using random CNT networks as channel. For CNT networks, the variability analysis becomes more complicated due to randomness in the network structure and CNT distribution, which varies with respect to CNT network density, deposition methods, surface condition before CNT deposition, etc. Undoubtedly, these further increase performance uncertainty which need to be analyzed and understood thoroughly.

### *1.2.3 Chemical Sensors*

SWCNT based chemiresistor gas sensors have been widely studied due to their significant advantages in monitoring different gases in low ppm and ppb level. The first CNT gas sensor was reported in 2000 by Kong et al. [43] Since then, many research groups have worked on the sensor application and enormous progress has been achieved. Reports on the sensing mechanism have been discussed and argued still today. Early discussions mainly focused on the adsorption of gas molecules at CNT junction area [44], indirect interaction through pre-adsorbed water layer or the hydroxyl group from SiO<sub>2</sub> substrate [45, 46], direct charge transfer between gas molecules and CNT [47], and Schottky barrier modulation at the CNT/metal contacts [23], etc. Battie et al. performed an experiment based on CNT network and suggested gas molecules mainly attach to CNT network, not CNT/metal contacts [48]. Later, Boyd et al. pointed out the gas sensitivity is due to both the CNT/metal contacts and the CNT junctions [49], and the network effects are dominated by gas-induced changes in CNT junctions. As for sensitivity, a detection limit of 3ppb ammonia (NH<sub>3</sub>) was demonstrated by Rigoni et al [50].

Functionalization strategies, including polymers coating or CNT decoration with different metal nanoparticle, were performed and yielded good results. But these methods degraded the overall performance of the sensors in terms of response rate and long-term stability. Random CNT

network and aligned CNT network in sensors were also investigated with single decorated molecules and nanoparticles, either in chambers or in air. However, few researches focused on the selectivity of CNT based gas sensors, and no publication has been reported on gas identification study without functionalization or coating or using array of CNTs. More work needs to be done to explore the selectivity of CNT sensors.

#### *1.2.4 Flexible Electronics and Sensors*

Printed microelectronics on flexible substrates has attracted significant attentions in recent years because of the high potential in wearable and bendable devices[21]. Its applications include flexible displays[51], radiofrequency identification (RFID) antennae/tags[52, 53], sensors[54, 55], artificial skins[56], etc[57]. As for printing techniques, AJP has been proven to be capable of printing microelectronic devices and relevant circuits with low-cost, repeatability, scalability, and relatively high precision compared to other printing techniques[58]. AJP has been utilized to deposit a wide range of materials because it can handle inks viscosities in the range of 1-1000 Cp[59] Printed CNT-TFTs have significant potential with improved carrier mobility, device stability, variability, dissipation power, and other operation performance[60-62].

Even though advances in printing techniques, synthesis and processing of nanomaterials have promoted the development of printed flexible devices[36], the tradeoff between cost and performance still limits their further applications in various fields. On the one hand, fully printed CNT-TFTs are crucial for low-cost consideration. Procedures such as atomic layer deposition (ALD) will complicate the process and increase the cost at the same time. On the other hand, high performance is hard to achieve for fully printed CNT-TFTs. The causes are different, such as imperfections in electrode patterns, contact interfaces, uniformity of CNT network, thickness of

dielectric layer, etc[11]. Most of them are being addressed properly with the improvement of nanomaterial inks, including nanoparticle silver (Ag) inks [63], highly purified semiconducting CNT (S-CNT) inks [64], ion-gels [65, 66], dielectric inks such as barium titanate ( $\text{BaTiO}_3$ ) nanoparticles[67] and xdi-dcs [68], which is a blend of poly(vinylphenol)/poly(methyl silsesquioxane) (PVP/pMSSQ). However, printable dielectric layer is still one of the major obstacles because its relatively large thickness can result in very high gate voltage to fully switch on and off the transistors, which will cause high power dissipation for printed devices on flexible substrates. For example, the high  $V_{th}$  in some fully printed TFTs highly limited their performance because the gate bias has to be as large as  $\pm 40\text{V}$  to fully switch on/off the transistors. Ion gel could be an alternative solution to address the specific problem of high  $V_{th}$  [65, 66, 69], but it is temperature sensitive, very fragile and unstable compared to other dielectric materials. In this context, the optimization of fully printed CNT-TFTs, especially the printed CNT network and dielectric layers, is becoming more and more indispensable to make full use of its high potential in many practical applications.

### **1.3 Scope of Current Work**

The proposed research tasks are organized in the following sequence. Chapter 2 summarizes the literature for CNT-TFTs, including their excellent properties, fabrication processes, and various applications. It also lists the important contributions of the present work. Chapter 3 concentrates on the fabrication of CNT-TFTs by typical PL process and discusses the performance variability in output characteristics of the fabricated CNT-TFTs. Chapter 4 presents CNT-TFTs' application as selective chemiresistor sensors for gas identification by putting forward a convolution model to characterize the corresponding sensor responses. Chapter 5 discusses the improvement in device performance after the optimization of fully printed CNT-TFTs using AJP,

including the printed CNT network and dielectric thin film. Chapter 6 characterizes the sensor responses of fully printed CNT sensors fabricated by different printing techniques as well as puts forward an efficient strategy to improve the sensitivity. Chapter 7 summarizes the current work and introduces the scope of future work.

## CHAPTER 2.BACKGROUND

### 2.1 CNTs and CNT Based Devices

#### 2.1.1 *Properties of CNTs*

Since their discovery in 1991, CNTs have become one of the most highly researched materials in the areas of science and engineering due to their superior electrical, mechanical, chemical, thermal, and optical properties[70]. CNTs can be classified as either MWCNTs or SWCNTs. SWCNTs can be further classified as either metallic (M-CNTs) or S-CNTs[71].

#### Electrical Properties

For a SWCNT, the mobility and current carrying capacity can be exceptionally high [72]. Nevertheless, large difference exists between properties of M-CNTs and S-CNTs. Because 1/3<sup>rd</sup> of SWCNTs are metallic in a grown CNT network, a significant variation in property among CNTs is not unexpected. S-CNTs show stronger temperature dependence than M-CNTs in conductivity due to the thermal excitation of carriers[73]. For CNT thin film, which contains both M-CNTs and S-CNTs, carrier transport includes travelling across tube-tube junction in addition to merely along the tube. The M-M or S-S CNT junctions have 20k $\Omega$ ~400k $\Omega$  contact resistance, but M-S contact resistance is found to be as high as 1M $\Omega$ ~5M $\Omega$ . Hence, the CNT-CNT contact resistance is one of the main contributions to the film resistance and network transport properties.

#### Mechanical Properties

CNTs show extraordinary mechanical flexibility and elasticity when they undergo large strain and bending [74, 75]. This can be credited to the large aspect ratio and strong internal

bonding within CNTs. Defects may be introduced upon deformation, and they will affect both electrical and thermal transport properties. Therefore, the superior mechanical property of individual CNTs is an important figure of merit. Moreover, because of the strong interaction between substrate and CNTs, CNT thin films are amazingly flexible, stretchable, and foldable without causing significant reliability problem. Typically, a CNT thin film can be bent down to radius of 2 mm without causing damage to network.

### Chemical Properties

Because of the special structure of CNT where all carbon atom and C-C bonds are on the tube surface, the chemical sensitivity of CNTs can be utilized in sensing applications [76]. After absorbing chemicals, two resulting effects may be observed. One is the change in carrier concentration due to charge transfer between CNTs and incoming chemicals. The other is the induced potential energy barrier that affects carrier mobility along the tube. CNT thin films are required to have an acceptable chemical stability after exposure, especially to those chemicals that will be employed in fabrication and regular usage.

### Thermal Properties

The thermal conductivity of a SWCNT can reach  $3500\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$  along its axis at room temperature, which is much higher than the widely used high conductivity metal copper ( $385\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ ). CNTs can also bear high temperature in practice. The temperature stability of CNTs is estimated to be up to  $750^{\circ}\text{C}$  in air and about  $2800^{\circ}\text{C}$  in vacuum [75]. Crystallographic defects strongly affect CNTs' thermal properties, which leads to phonon scattering and in turn increases the relaxation rate of the phonons, thus reducing the thermal conductivity. Besides that, CNTs also

show superior optical properties and CNT network is relatively easy to deposit by multiple methods for the fabrication of TFTs.

### *2.1.2 CNT Network*

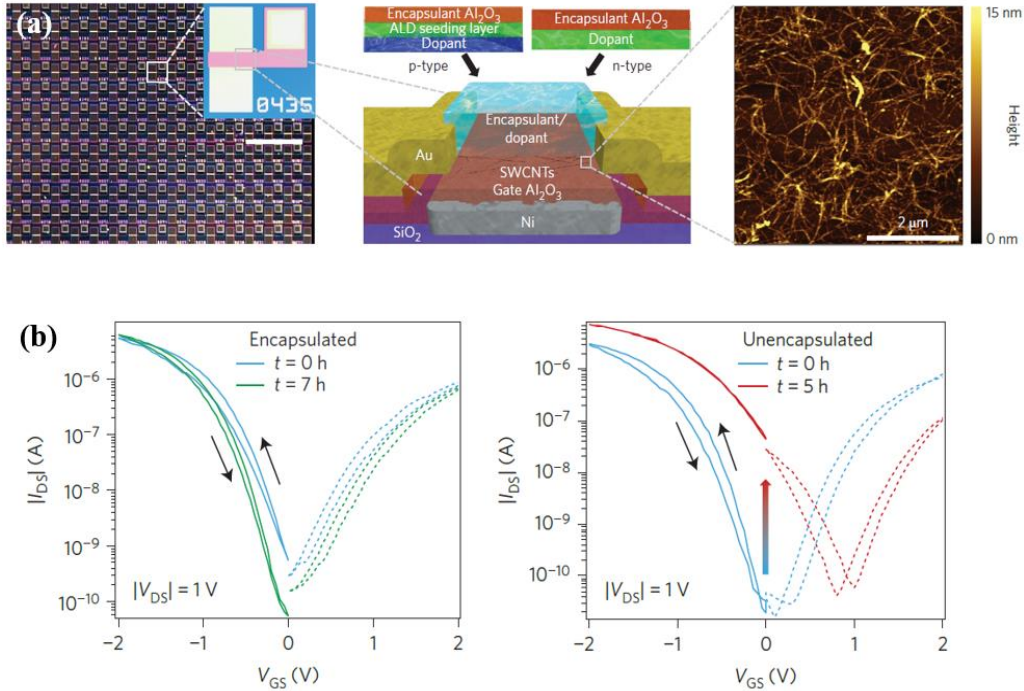
The most common technique to grow CNT network or CNT thin films is chemical vapor deposition (CVD) [77]. CVD has a great advance in density control by tuning the catalyst density and growth time. It also gives a better tube-tube contact and fewer defects that result in higher conductance. However, solution-based deposition is more suitable for pressure and temperature sensitive electronics [78]. It is also more compatible for fabrication of plastic/flexible electronic devices. Compared to CVD, the cost of solution-based deposition is much lower since it operates at low temperature and no vacuum system is needed. The highly purified S-CNT solution are commercially available nowadays, which are typically either water based or solvent based. Solution-based deposition further increases the design flexibility and makes it more accessible for mass production of CNT based microelectronics/circuits.

Uniformity of CNT thin films is very important to obtain high performance [21, 79]. To achieve this, the quality of CNT solution and coating methods are crucial. For example, the “Langmuir-Blodgett” method spreads CNT solution over a substrate surface covered by a water layer. Self-assembly method enhances the interaction between CNTs and deposition surface by chemical treatment, local surface charge, or microfluidic guidance. For electrophoretic deposition, a metallic layer is added on top of the substrate and CNTs are locally charged and polarized by an electric field. After deposition, the conductive layer will be etched away, leaving only the transparent CNT thin films. All these deposition methods can accommodate to various objectives.

### *2.1.3 CNT Based Thin Film Transistors*



CNT-TFTs can withstand high degree of strain, exhibit excellent electrical performance due to their high mobility, on/off ratio [80-82]. Even though individual CNT based FETs can meet the requirements of aggressive scaling down of physical dimensions, they have been deemed impractical for commercialization due to the difficulty of pinpointing individual CNTs at desired locations and the performance variability depending on the chirality and diameter of individual CNTs. CNT network based TFTs are more practical due to the ease of fabrication using either conventional lithography or printing techniques, and their relatively high device-to-device performance uniformity which is vital for scalable production.



**Figure 2.1 Complementary SWCNT-TFT structures and performance. (a) Micrographs of the fabricated SWCNT-TFT device with a channel width of 150 μm and length of 50 μm (inset) and an array of SWCNT TFTs. (b) Time stability of SWCNT-TFT electrical properties. Left: Log-linear transfer curves for encapsulated p-type (solid lines) and n-type (dashed lines) SWCNT-TFTs measured after initial exposure to atmosphere (blue) and after 7 h of ambient exposure (green); Right: Log-linear transfer curves for unencapsulated p-type (solid lines) and n-type (dashed lines) SWCNT TFTs measured after initial exposure to atmosphere (blue) and after 5 h of atmospheric exposure (red), with the change in I<sub>off</sub> indicated by the arrow (red/blue). Copyright (2015) Nature Publishing Group. [83]**

Geier et al. fabricated both p-type and n-type SWCNT-TFTs using methods similar to a previous work[84]; they modified the structure to encapsulate the doped SWCNT channel networks. The schematic structure and corresponding performance are shown in Figure 2.1. Based on these transistors, SWCNT CMOS static random-access memory (SRAM) cells and corresponding circuits were also fabricated. Read, write, and hold noise margin stability testing was obtained for these SWCNT CMOS SRAM cells over 40 h (4,000 cycles) of ambient testing with high temporal stability and spatial uniformity. Overall, their work provides an approach for the design and fabrication of complex solution-processable, large-area, energy-efficient CMOS logic devices. These features have potentially wide-ranging implications for high-performance wearable and bendable electronics when combined with recent advances in flexible and printed electronics. [83]

CNT-TFTs on bendable substrate have attracted major interests because of their wide range of applications in flexible electronics such as transparent displays, chemical/biological sensors, RFIDs, logic circuits, oscillators, etc. [10]. The main advantages of the flexible TFTs lie in their potential to enable low-cost, and high throughput manufacturing in practice. To further realize the cost-effective and scalable production of flexible TFTs, printing techniques have been introduced as a viable solution. Printable TFTs do not require fabrication masks or templates, which provide significant design flexibility compared to the conventional photolithography (PL) process.

Feng et al. proposed artificial synapses based on dual-gate SWCNT-TFTs which are fabricated by printing techniques[85]. High field-effect mobility was demonstrated for those printed low-voltage synaptic devices. Some key synaptic behaviors were emulated including paired-pulse facilitation and filtering characteristics. They presented a printable method to fabricate synaptic devices for a neuromorphic system.

#### 2.1.4 Hysteresis of CNT-TFTs

Hysteresis of transistors is highly undesirable in practice[86, 87]. Hysteresis can result from various factors such as trap states in the dielectric or semiconductor/dielectric interface, trap charges induced by water molecules absorbed onto or in the vicinity of the semiconductor channel. Hysteresis can lead to a shift in  $V_{th}$  as a function of the voltage sweeping speed, sweeping direction, and sweeping range. Instability and reliability problems can result from hysteresis during transistor operation and logic circuit design [88-90].

Lee et al. studied gate hysteresis of CNT-FETs on silicon oxide substrates in an ultrahigh vacuum (UHV) at low temperatures[87]. Results showed the hysteresis decreases greatly upon co-adsorption of water and ammonia below condensation temperatures. But it is neither reduced by thermal annealing over 300°C under UHV nor significantly affected by independent adsorption of ammonia or water at 56 K. Yu et al. demonstrated transparent and flexible transistors and logic gates using a monolayer graphene electrode and CNT network in the channel. Small hysteresis was observed for the nanocarbon based integrated circuits (ICs) [91]. Because of the defect-free graphene surface, the hysteresis of the devices was independent of the gate voltage sweeping range.

Ha et al. applied fluorocarbon polymer (Teflon-AF) in CNT-TFTs and obtained hysteresis-free performance in the transfer characteristics[92]. This fluorocarbon encapsulation method provides a promising approach for enhanced device stability and reliability, which is critical for future CNT based system-level electronics. Cao et al. also reported hysteresis-free CNT-TFTs using AJP techniques[68]. They fabricated fully printed transistors on flexible substrate (Kapton), which includes the printing of all layers: S-CNTs, metallic electrodes, and insulating gate dielectrics. Other hysteresis-free devices can be seen in [86, 93-98].

### 2.1.5 Variability Analysis of CNT-TFTs

Performance variability of transistors increases with the decrease of the smallest feature size, resulting in large challenges in device reliability and stability. The challenges include the unpredictability of delay to increasing leakage current, as well as the inherent unreliability of the components, posing design, and test challenges[99].

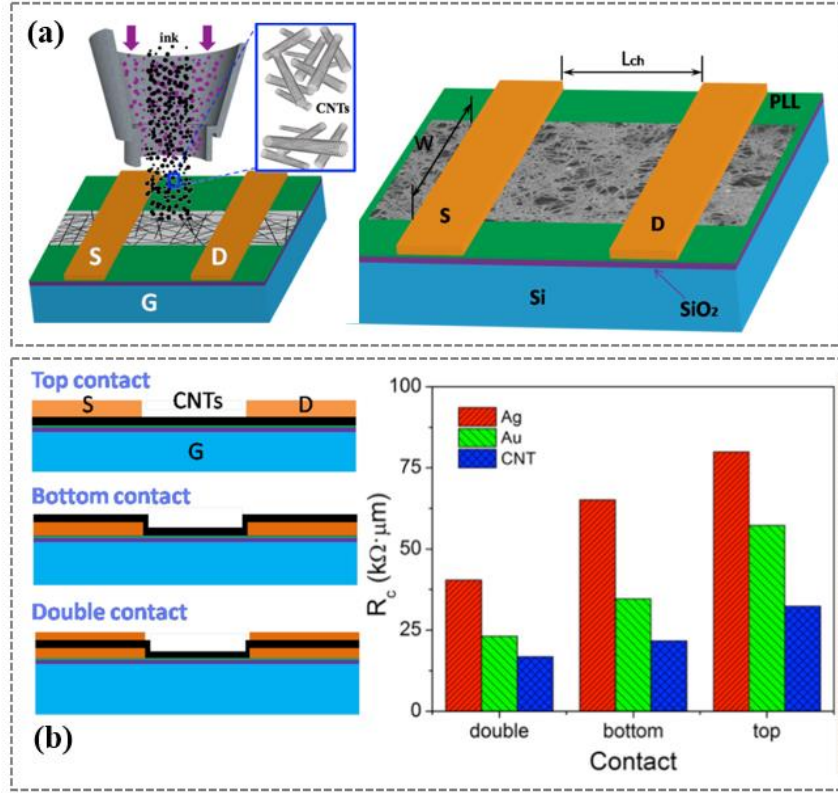
Islam et al. discussed the variability and reliability of SWCNT-FETs in different aspects[100]. They pointed out that performance variability of SWCNT-FETs is mainly attributed to both the distributions of SWCNTs' diameter and the interface defects caused by hydroxyl-group. Besides, oxide defects also play a dominant role in controlling reliability parameters, like low-frequency noise, radiation damage, and long-term performance degradation. Salamat et al. explored the origin of large device-to-device fluctuation in aligned array transistors[101]. They developed numerical simulations using measured diameter distribution of CNTs to demonstrate that the diameter distribution had significant impacts on the variability. Results showed the control over diameter distribution is vital for attaining high-performance transistors and circuits with characteristics rivaling those of the state-of-the-art Si technology. Hu et al. presents variability and reliability analysis of self-assembled CNT-FETs based on thousands (~3000) of multichannel CNT-FETs [102]. By increasing the number of channels in CNT-FETs, the on-state current was increased and the  $V_{th}$  was reduced. Moreover, the major failure mode in the scaled multichannel CNT-FETs may be the “shorts” caused by M-CNTs. Almudéver et al. studied the variability and reliability of CNT-FETs due to the density variations [39] and manufacturing imperfections[103], including the presence of M-CNTs, imperfect M-CNT removal processes, chirality variations, CNT doping variations, and density fluctuations. Other work concentrating on the variability analysis of transistors can be found in [37-39, 104, 105]. However, none of the studies reported

the variability analysis of CNT-TFTs using random CNT networks as channel. For CNT networks, it becomes more complicated due to randomness in the network structure and CNT distribution, which need to be analyzed and understood thoroughly.

#### *2.1.6 Contact Analysis of CNT-TFTs*

Franklin et al. defined various contact resistances in CNT-FETs and explained how they related to the technology-relevant device-level resistance in the context of a high-performance scaled transistors at the sub-10 nm technology nodes[106]. They presented the impact of the scaling of contact resistances versus contact length using different source/drain contact metals (Pd, Pt, Au, Rh, Ni, and Ti), which enhanced the understanding and engineering of transport at the metal-CNT interface in CNT-FETs and other CNT related devices. Shahrjerdi et al. conducted a thorough experimental study of device yield and performance for several low work function metal contacts such as erbium, lanthanum, and Yttrium for high-performance air-stable n-type CNT-FETs[107]. They found that the lower yield and large variation in performance of n-type CNT devices with low work function metal contacts are mainly caused by high oxidation rates and sensitivity to deposition conditions. Device yield was improved by using erbium contacts evaporated at high deposition rates. Chai et al. introduced low-resistance electrical contact using a graphitic carbon (G-C) interfacial layer which is introduced with different capping metals[108]. Electrical contact to the CNT was improved using the G-C interfacial layer catalyzed by a Ni layer, which is attributed to the improved wetting and the formation of chemical bonding with the CNTs. Cao et al. evaluated contact resistance and field-effect mobility of transistors fabricated using solution-processed SWCNTs; they used both the transmission line method and the Y function method[109]. Results indicated solution-processed SWCNTs can offer performance comparable

to that of CVD based CNTs in ultimately scaled FETs, where contacts could dominate electron transport instead of electron scattering in the channel region.



**Figure 2.2 Fully printed CNT-TFTs and analysis of different CNT-metal contact interfaces[61]. (a) Schematic diagram of a printed, back-gated CNT-TFT with indication of key dimensions using AJP techniques. (b) Schematic structures of the three different contact configurations studied in this work: top, bottom, and double contacts, as well as comparison of contact resistance for printed CNT-TFTs having different printed electrode materials (Ag, Au, and M-CNTs) and contact geometries (top, bottom, and double). Copyright (2016) ACS Publications.**

Cao et al. analyzed different contact resistance in fully printed CNT-TFTs fabricated using AJP techniques[61]. Three different contact geometries including top, bottom and double (a sandwich-like structure combining contacts below (bottom) and above (top) the printed CNTs) are illustrated in Figure 2.2. They demonstrated that double contacts offered a significant decrease in contact resistance in CNT-TFTs for different electrode materials compared to top and bottom

contact geometries. Besides, using M-CNTs as contacts were proved to be one of the best options for enhancing performance of the CNT-TFTs. The bottom contacts were able to boost the on current by up to 50% compared to the top contacts. Similar work can be found in [110-115].

### *2.1.7 Performance Analysis of CNT-TFTs*

Kim et al. fabricated high-performance transparent electrodes and FETs using SWCNT and graphene hybrid thin film. The high-performance was achieved by controlling the density and alignment of pre-coated SWCNTs at the optimized spin-coating speed. Compared to the previous work, they improved the on/off ratio and on-state current with respect to pristine graphene, and the hybrid film possessed a sheet resistance of 300  $\Omega/\text{sq}$  with 96.4% transparency.[116]

It is well known that n-type SWCNT transistors are much difficult to achieve because of various issues related with n-type doping strategies, e.g., limited carrier concentration modulation, environmental instability, undesirable  $V_{\text{th}}$  control, and/or poor morphology. Geier et al. reported controlled n-type doping of SWCNT thin-film transistors with a solution-processed pentamethylrhodocene dimer. Consistent n-type behavior was observed for the charge transport properties of organorhodium-treated SWCNT thin films when characterized in both Hall effect and thin-film transistor geometries. Their work can facilitate ongoing efforts to realize high-density SWCNT based ICs.[117]

Ha et al. also studied air-stable n-doping of CNT-TFTs by utilizing SiNx thin films deposited by plasma enhanced CVD. Different from commonly used methods in the past, the fixed positive charges within SiNx act to n-dope the underlying nanotubes via field-effect, which presented a reliable and easy process route toward obtaining high performance SWCNT n-type transistors. Moreover, excellent device-to-device uniformity was also achieved for these n-type CNT-TFTs

with comparable electrical characteristics to their p-type counterparts. Their work is significant toward realization of CMOS circuitry based on CNT-TFTs for large-area electronic applications.[118]

Jeon et al. demonstrated high-performance SWCNT-TFTs by reducing the charge transfer using an interacting fluoropolymer encapsulation with thermal annealing in vacuum. As results, the on-current increased, the off-current reduced, the  $V_{th}$  shifted toward 0 V, and the subthreshold swing improved. Those improvement are the crucial to realize high-performance microelectronics with low power consumption. They also investigated the instability characteristics of the SWCNT-TFTs during the prolonged electrical bias-stress. The drop in drain current of the SWCNT-TFTs was partially recovered with a second phenomenon that increases the drain current after a certain time.[119]

Choi et al. reported TFTs with highly uniform SWCNT nanomesh network fabricated from a pre-separated semiconducting nanotube solution. The nanomesh structure can be formed using oxygen plasma with etched nanoscale holes over the entire CNT network channel. These devices could achieve on/off ratio as high as  $10^6$  (or even higher), which was superior for application in large-scale ICs. The on/off ratio increased with the decreasing distance between the nanoscale holes in the nanomesh network while maintaining a high degree of uniformity, which attributed to the effective elimination of metallic paths across the source/drain electrodes by forming the nanomesh structure in the high-density SWCNT network channel.[120]

Thermal issues also can be critical to the realization of high performance of CNT based devices[121, 122]. Lee et al. investigated the coupling between thermal and electrical effects of SWCNT based devices using an atomic force microscope (AFM) cantilever that is capable of



applying local electric and temperature fields in both contact and amplitude modulation modes. They found tip-CNT thermal resistance was estimated at  $1.6 \times 10^7$  K/W and decreased with increasing temperature. The ability to measure thermal coupling to a single-molecule electronic device could offer new insights into CNT based devices in micro and nano scale.[123]

## **2.2 Fabrication of CNT-TFTs**

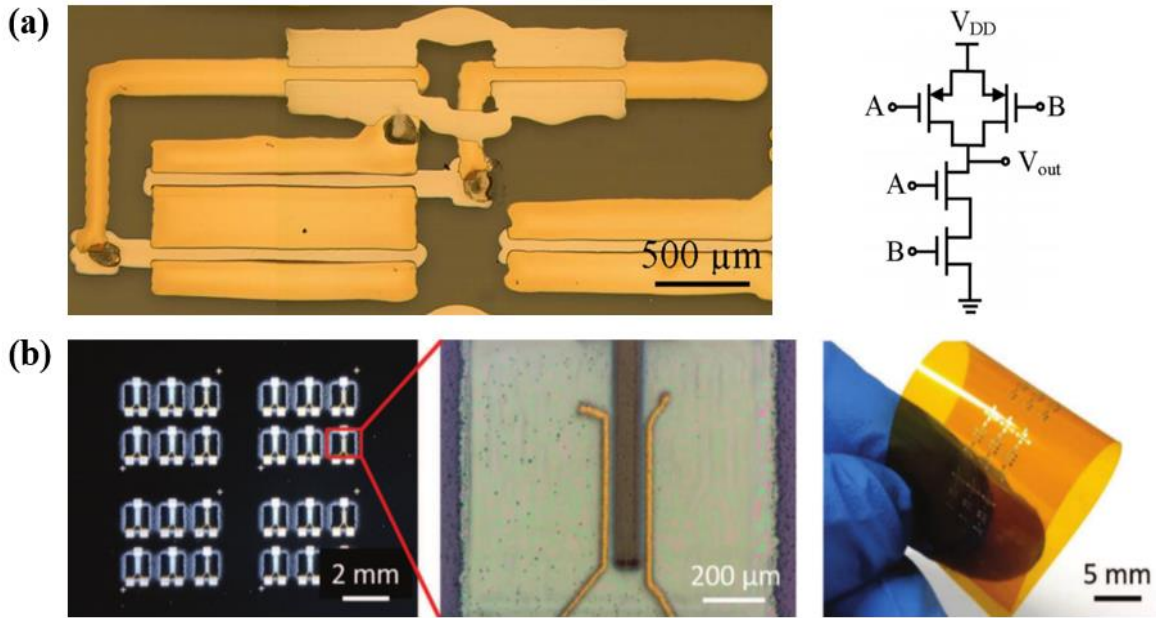
### *2.2.1 Photolithography*

PL is one of the most important methods for ICs fabrication [124]. Compared to printing techniques, CNT-TFTs fabricated from PL exhibit much better electrical performance such as higher carrier mobility and lower operation voltage [21]. More importantly, it can well control the exact size/shape of the designed features and ensure resolution  $< 100\text{nm}$ , especially when using electron-beam lithography the resolution can reach sub-10nm level. However, multiple photolithographic processes are indispensable for different patterns or layers. Typically, more than 10 masks might be needed for certain ICs fabrication, and each requires an extremely clean condition in order to avoid possible contamination and environmental hazards. In general, conventional lithographic patterning and vacuum processes will result in high-cost and low-throughput processing.

### *2.2.2 Inkjet Printing*

IJP has been widely used as a free-form fabrication technology for building three dimensional layer-by-layer patterns and an effective way to fabricate flexible microelectronic devices [34, 125, 126]. Typically, inkjet printers are able to handle inks with viscosities less than 20 centipoise (cP) and achieve resolution as small as  $20\text{ }\mu\text{m}$ . Compared to conventional

lithography, low-cost is one of its greatest advantages. Another tremendous advantage lies in its design versatility and operational flexibility. Due to the drop-by-drop printing method, inkjet printers are capable of printing any desired features on demand within its resolution limits, which makes it an efficient solution for cost-effective and scalable production.



**Figure 2.3 Printed CNT based transistors using different printing techniques. (a) Micrograph of the inkjet printed NAND gate based on SWCNT-TFTs[127]. (b) Fully-printed, flexible, and hysteresis-free CNT-TFTs using aerosol jet printing (AJP)[68]. Copyright (2017) Nature Publishing Group and (2017) Wiley-VCH Verlag.**

Vaillancourt et al. reported all inkjet printed CNT-TFTs on flexible substrates. The entire fabrication was free from PL [128]. In Figure 2.3(a), Kim et al. fabricated ambipolar CNT-TFTs mainly by IJP, which can be used for complementary circuits for sensor applications in ambient conditions [127]. In this work, ALD was applied for dielectric layer because dielectric printing is quite challenging for inkjet printers when considering its thickness and uniformity. Grubb et al. reported 100% inkjet printed transistors with channel length as short as 0.3-2 μm, which was accomplished by using silver inks with different chemical properties to prevent mixing [129]. Cao

et al. also obtained fully printed CNT-TFTs using IJP with dramatically enhanced on-state current density to  $\sim 4.5 \mu\text{A}/\mu\text{m}$ [130]. Surprisingly, their CNT-TFTs actually achieved a sub-micron channel length with top-contact self-aligned printing and employing high capacitance ion gel as the gate dielectric, which may pave the way for future high-definition printed displays, sensing systems, and low-power consumer electronics[131-133]. Other important publications focusing on IJP based fabrication can be seen from [134-140].

### 2.2.3 *Aerosol Jet Printing*

AJP begins with atomization of liquid ink, producing droplets ranging 1-5 $\mu\text{m}$  in diameter. The atomized droplets are delivered to the print head with an annular flow of clean nitrogen ( $\text{N}_2$ ) gas wrapped around in order to focus the droplets into a tightly collimated beam of material. Then this printable stream exits a converging nozzle at a controllable flow rate and then can be deposited onto the target surface with relatively high velocity[58, 59, 141-146]. AJP has been proven to be capable of printing microelectronic devices and relevant circuits with relatively high precision, which is noncontact injection with high repeatability and scalability. AJP is also low in cost compared to PL process. Like IJP, it has the ability to print fine and easily controllable patterns or layers but with higher resolution ( $<10\mu\text{m}$ ). The most significant advantage of AJP is that it can deal with a much wider range of inks with viscosities  $>1000 \text{ cP}$ .

AJP has also been successfully used for CNT-FET fabrication. Rother et al. investigated the suitability of AJP of polymer-sorted (6,5) SWCNTs for top-gate FETs[147]. No impact was found on the quality of the SWCNTs in terms of defects and length after sonication during the printing process. Reproducible device performance was guaranteed over extended printing periods and for different ink batches with constant printing parameters. Ha et al. fabricated sub-3V digital circuits

on plastic by AJP of CNT network, ion gel dielectric, and conducting polymer gate electrode sequentially from liquid inks [65]. Cardenas et al. reported in-place printing of CNT-FETs with Ag-CNT contacts at low temperature using AJP[148]. No external baking, coating, or other treatments were involved during fabrication after the substrate was loaded, which ensured entirely in-place, from first step to last, without removal of the substrate from the printer. In Cao et al.'s work, they explored the printing of hydrophobic dielectric layer (xdi-dcs) based on AJP for their hysteresis-free CNT-TFTs, depicted in Figure 2.3(b) [68]. Another work from Cao et al. focused on improving the contact interfaces in AJP printed CNT-TFTs, where contact resistance dominates the performance and degree of variability in these TFTs [61]. Similar work can be found in [58, 149-152]. However, the thick printed dielectric layer highly limits the performance of printed CNT-TFTs because high gate bias is required to switch on/off the devices. More work needs to be done considering the quality of printed dielectric layer in order to improve the overall performance.

#### 2.2.4 *Screen Printing*

Screen printing, also known as serigraphy or screen process, is a printing technique whereby a thick paste ink is forced through a stencil attached to a finely-woven mesh screen, transferring ink to the desired substrate except in areas made impermeable to the ink by a blocking stencil[153]. Similar as IJP and AJP techniques, it is also a relatively simple and inexpensive way to make detailed prints on a diverse set of substrates including paper, polyimide, bumper stickers, posters, cloth, etc.[154, 155]

Cao et al. utilized screen printing as simple, scalable, and cost-effective approach for both rigid and flexible SWCNT-TFTs[156]. The fully printed transistors exhibited decent performance, with mobility up to  $7.67 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , on/off ratio of  $10^4 \sim 10^5$ , minimal hysteresis, and low

operation voltage ( $<10$  V). They also demonstrated outstanding mechanical flexibility of the CNT-TFTs bent with radius of curvature down to 3 mm. Another work from Cao et al. focused on CNT-TFT based large-area and flexible active-matrix electrochromic displays (AMECD), which were also fabricated by screen printing[157]. This fully printed backplane showed high electrical performance with mobility of  $3.92 \pm 1.08 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , on/off ratio  $\sim 10^4$ , and good uniformity. To obtain an entirely screen-printed AMECD, they monolithically integrated the printed backplane with an array of printed electrochromic pixels, which resulted in devices with good switching characteristics, facile manufacturing, and long-term stability. Bandodkar et al. reported fully printed CNT-based electrochemical sensors and biofuel cells using screen printing technique for large-scale fabrication[158]. These devices were highly stretchable and could withstand strains as high as 500% with very limited effect on their structural integrity and electrochemical performance. This work lays the foundation for scalable, low-cost, and highly stretchable CNT based devices for wide range of applications in healthcare, consumer electronics etc.

### 2.2.5 *Roll-to-roll Gravure Printing*

During roll-to-roll gravure printing, the ink or paste is rolled over the engraved cylinder first and then wiped to remove excess ink from the non-image areas of the gravure roll using a doctor blade. The ink is compressed, stretched, sheared, fractured, and then transferred to the substrate. During the printing process, the effectiveness of excess ink removal from the non-image areas highly depends on two major factors: (1) the viscosity of the ink under a given roll speed, and (2) the doctor blade angle. [159]

Koo et al. demonstrated roll-to-roll gravure printing as a suitable manufacturing technique for flexible CNT-TFT based electronic circuits[160, 161]. Fully printed SWCNT-TFTs with

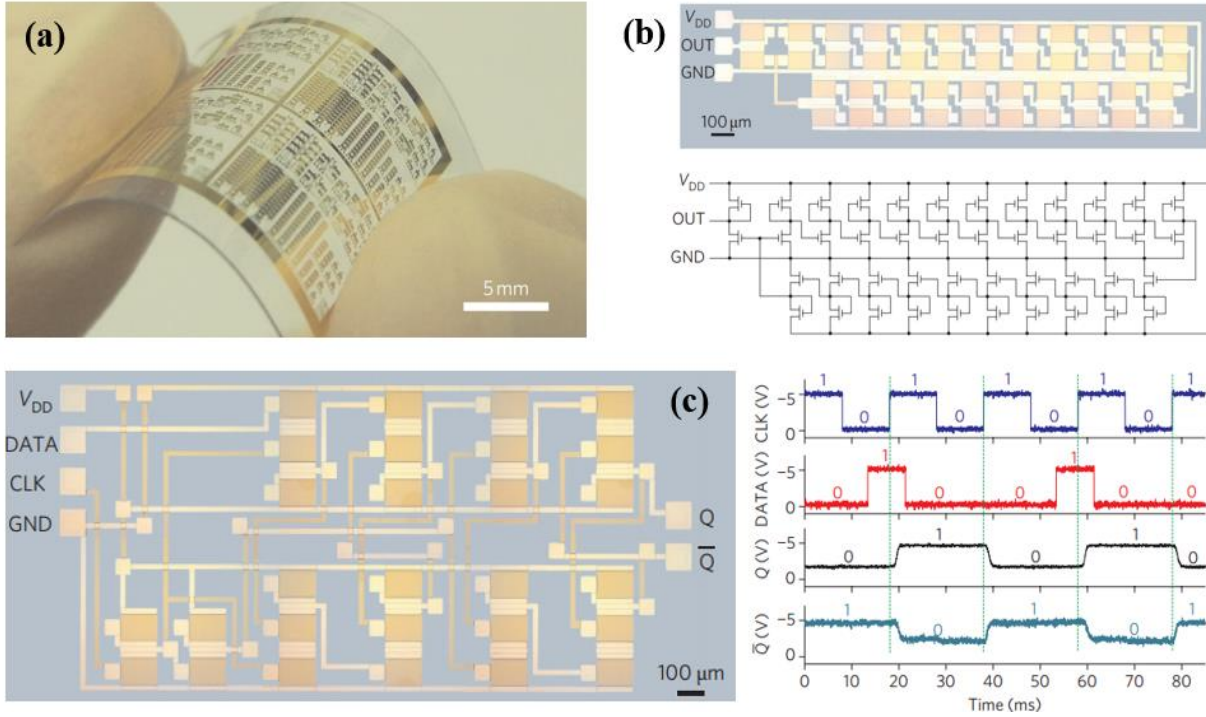
different channel sizes were fabricated on 150-m-long rolls of 0.25-m-wide poly(ethylene terephthalate) (PET) using silver nanoparticles, BaTiO<sub>3</sub> nanoparticles, and SWCNTs ink. A Monte Carlo simulation for a 1-bit adder circuit was conducted to demonstrate the feasibility of roll-to-roll gravure printing for functional circuits with reasonable complexity. Noh et al. fabricated fully roll-to-roll gravure printed D flip-flop on flexible plastic foils using p-channel SWCNT-TFTs for the first time, which shows a clock-to-output delay of 23 ms for 20-Hz clock signal[162]. Combined printing methods are also of large interest. Fully printed CNT-TFTs were fabricated by Homenick et al. [126]. This printing process combined roll-to-roll gravure for gate/dielectric and IJP for CNTs/source/drain, which yielded CNT-TFTs with good operational stability.

## **2.3 Applications**

### *2.3.1 Flexible Electronics*

Due to the excellent properties of CNTs such as high conductivity, intrinsic carrier mobility, mechanical flexibility, stability and reliability, they have been widely used as material for flexible electronics. In most of the cases, CNTs are the semiconducting material (either single CNT or CNT thin film) in the channel of FETs, which are the elemental building blocks for flexible electronics. They also can be applied as transparent electrodes, sensor materials, etc. in other applications. Two major processing methods have been extensively utilized for CNT film fabrication, which are CVD based and solution/ink based method. One of the biggest advantages of CVD based CNTs is that they can be highly aligned for better performance. However, solution/ink based CNTs is more convenient for large-scale fabrication and especially compatible for printed flexible electronics, which is beyond the capability of CVD based method. Besides, the

low cost of solution based CNT film deposition make them suitable for the development of future flexible and wearable devices.



**Figure 2.4 (a) Devices on PEN substrate. (b) Optical micrograph and circuit diagram of a 21-stage ring oscillator. (c) Optical micrograph and input–output characteristics master–slave delay flip-flop[164]. Copyright (2011) Nature Publishing Group.**

Wang et al. fabricated extremely bendable devices using SWCNT-TFTs on a flexible substrate, which offers high performance, low cost, ambient stability, and significantly outruns the organic semiconductor materials [21]. Such devices are proven to be practical for digital, analog and radio frequency (RF) applications. Cao et al. reported medium-scale CNT thin-film devices on plastic substrates using sub-monolayer SWCNT networks to yield small to medium-scale integrated digital circuits, composed of up to nearly 100 transistors [163]. The sub-monolayer films are superior materials for flexible ICs, with potential applications in consumer and other areas of electronics. Sun et al. investigated high performance flexible devices using CNT-TFTs exhibited

in Figure 2.4 [164]. They not only demonstrated flexible ICs, including a 21-stage ring oscillator and master–slave delay flip-flops that are capable of sequential logic, but also pointed out the lithographic techniques can be replaced with printing techniques in order to develop large-scale, low-cost and flexible electronics. Other similar applications include flexible circuits[163-166], flexible displays[167-169], flexible sensors[170-174], flexible solar cells[175-177], artificial skin[56, 178], and conformable RFID tags[14, 124], etc.

**Table 2.1 Summary of selected sensing performance (N/S = Not-stated) [25]**

<b>CNT type</b>	<b>Sensor configuration</b>	<b>Targeted analytes</b>	<b>Detection limit</b>	<b>Response time (s)</b>	<b>Reversibility</b>
Single SWCNT	ChemFET	NO <sub>2</sub> , NH <sub>3</sub>	2 ppm (NO <sub>2</sub> ) 0.1% (NH <sub>3</sub> )	<600	Irreversible
SWCNTs	ChemFET	Alcoholic vapors	N/S	5-150	Reversible
SWCNTs	Chemiresistor	O <sub>2</sub>	N/S	N/S	Reversible
SWCNTs	ChemFET	DMMP	<1 ppb	1000	Reversible
MWCNTs	Chemiresistor	NO <sub>2</sub>	10 ppb	N/S	Reversible (165°C)
SWCNTs	Chemiresistor	NO <sub>2</sub> , Nitrotoluene	44 ppb (NO <sub>2</sub> ), 262 ppb (Nitrotoluene)	600	Reversible (UV)
MWCNTs	Chemiresistor	NH <sub>3</sub>	10 ppm	~ 100	Reversible
SWCNTs	Chemiresistor	SOCl <sub>2</sub> , DMMP	100 ppm	10	Irreversible
SWCNTs	Chemiresistor	O <sub>3</sub>	6 ppb	<600	Reversible
MWCNTs	Chemiresistor	NO <sub>2</sub>	5-10 ppb	~ 600 (165°C)	Reversible (165°C)
SWCNTs	Chemiresistor	methanol, acetone	N/S	~ 100	N/S
SWCNTs	Chemiresistor	H <sub>2</sub> O	N/S	10-100	Reversible
Carboxylated SWCNT	Chemiresistor	CO	1 ppm	~ 100	Reversible

### 2.3.2 Sensors and Actuators

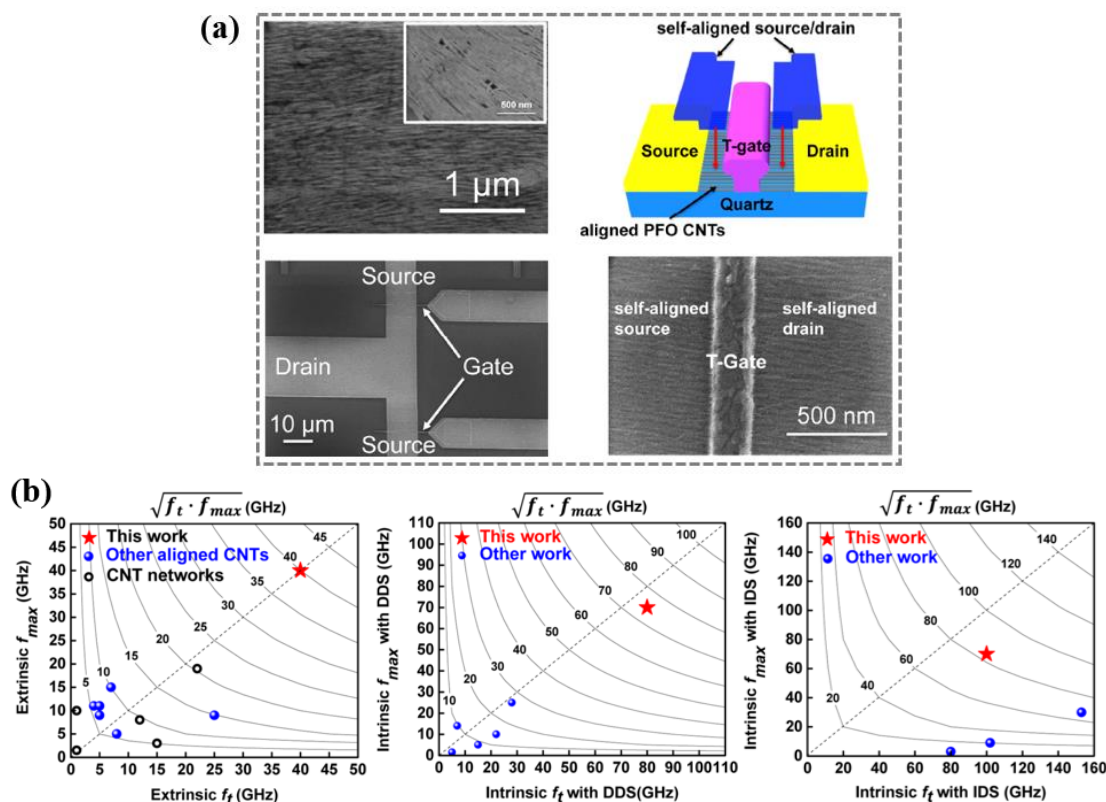
The special structure of being composed entirely of surface atoms makes CNTs an ideal material to detect electrical signals resulting from interaction with different gas molecules.



Generally, chemical field-effect transistors (ChemFET) and chemiresistors are two typical gas sensors. Table 2.1 summarizes the sensing performance of some pristine CNT gas sensors from previous work. Snow et al. demonstrated that the capacitance of SWCNTs is highly sensitive for both polar and non-polar gas molecules at room temperature [179]. MWCNTs were used in gas sensors by Ong et al. for the detection of CO<sub>2</sub>, O<sub>2</sub>, and NH<sub>3</sub> [180]. They developed a wireless, passive MWCNT-SiO<sub>2</sub> sensors based on changes of relative permittivity and conductivity of the material. Functionalization of CNTs can not only increase the sensitivity, but also well address the potential drawbacks: lack of selectivity to different gaseous analytes. Kuzmych et al. functionalized the SWCNT networks with poly (ethylene imine) (PEI) non-covalently to detect NO in exhaled breath, which reached detection limit ~5ppb in air [181]. Guerin et al. fabricated different electrode metals on top of horizontal CNT arrays [182]. These structures can take advantage of the specific interaction for each metal/CNTs/gas case to discriminate different gases at room temperature. Abdelhalim et al. utilized different metals to alter the response of each sensing element towards different gases, which can discriminate four gases: NH<sub>3</sub>, CO, CO<sub>2</sub>, and ethanol [183].

CNTs can be also used as material for other different types of sensors. Lipomi et al. fabricated skin-like pressure and strain sensors based on transparent elastic CNT films[173]. Even though the sensors showed less sensitivity compared to previously reported work, ~~but~~ they were the first transparent and stretchable devices which could detect both pressure and strain. Besides, those devices were monolithically integrated, extremely mechanically compliant, physically robust and easily fabricated. Liu et al. applied synergistic CNTs and graphene bifillers in strain sensors[184]. The dispersion of CNTs and formation of effective conductive paths were strengthened when graphene acted as a ‘spacer’ to separate the entangled CNTs from each other.

The sensors showed good reversibility and reproducibility under cyclic extension. As biosensors, CNTs can be modified with suitable groups capable of recognizing biomolecules (e.g., proteins such as enzymes and antibodies) and also can be modified with a biological sensing element (e.g., nucleic acids and peptides)[33]. Shah et al. reported electrochemical sensors based on SWCNT-modified glassy carbon electrodes for the sensitive detection of valacyclovir[185]. The electrochemical oxidation of valacyclovir was investigated using cyclic voltammetry and differential pulse voltammetry. Results revealed the proposed sensors had a lower detection limit compared to the previously reported instrumental analysis.



**Figure 2.5 (a) Characterization of the self-aligned T-shape gate transistors based on aligned polyfluorene-sorted CNTs. (b) Comparison of the RF performance between different CNT based transistors. The extrinsic frequency response (left). The intrinsic frequency response with the device de-embedding structure (middle). The intrinsic frequency response with the intrinsic de-embedding structure (right) [186]. Copyright (2016) ACS Publications.**

### 2.3.3 Radio Frequency Applications

Cao et al. reported RF transistors using well-aligned S-CNTs with current-gain cutoff frequency and maximum oscillation frequency simultaneously greater than 70GHz[186]. As shown in Figure 2.5, these transistors showed outstanding direct current performance with on current density of 350  $\mu\text{A}/\mu\text{m}$ , transconductance of 310  $\mu\text{S}/\mu\text{m}$ , and superior current saturation with normalized output resistance greater than 100  $\text{k}\Omega\cdot\mu\text{m}$ , and also exhibited good linearity performance with 1 dB gain compression point of 14 dBm and input third-order intercept point of 22 dBm. Their contribution in CNT based RF electronics will broaden the applications for signal amplification, wireless communication, and wearable/flexible electronics. Wang et al. studied RF and linearity performance of CNT-FETs using high-density, uniform S-CNT networks[187]. The channel length of the RF transistors was fabricated as small as 500nm, exhibiting a cutoff frequency of 5 GHz and with maximum oscillation frequency of 1.5 GHz, with linearity metrics up to 1 GHz. Those RF transistors are promising building blocks for highly linear RF electronics and circuit applications. Vincent et al. performed a systematic study of the use of resonating nanotubes in a field emission configuration to demodulate RF signals and explored the use of CNTs undergoing field emission as nanoantennae and the different geometries that could be used for optimization and implementation[188].

### 2.3.4 Batteries and Energy Devices

Yu et al. described a hierarchically structured carbon microfibre made of an interconnected network of aligned SWCNT with interposed nitrogen-doped reduced graphene oxide sheets[189]. They fabricated capacitor electrodes using these fibres, which showed a specific volumetric capacity of 305  $\text{F cm}^{-3}$  in  $\text{H}_2\text{SO}_4$  and 300  $\text{F cm}^{-3}$  in polyvinyl alcohol (PVA)/ $\text{H}_3\text{PO}_4$ . They also

fabricated a full micro-supercapacitor with PVA/H<sub>3</sub>PO<sub>4</sub> gel electrolyte, which has a volumetric energy density of  $\sim 6.3 \text{ m Wh cm}^{-3}$  while maintaining a power density more than two orders of magnitude higher than that of batteries. Their device could bridge the energy density gap between microbatteries and micro-supercapacitors for miniaturized portable electronics. Lee et al. used layer-by-layer techniques to assemble an electrode with MWCNTs, which was an alternative approach based on the redox reactions of functional groups on the surfaces of CNTs[190]. A gravimetric energy  $\sim 5$  times higher than conventional electrochemical capacitors and power delivery  $\sim 10$  times higher than conventional lithium-ion batteries were achieved by using the CNT electrode as the positive electrode and lithium titanium oxide as a negative electrode. Kim et al. electrodeposited MnOx nanoparticles onto CNT sheets for high-performance energy storage devices, which can be used as electrodes for lithium batteries and supercapacitors[191].

### 2.3.5 *Other Applications*

CNT-TFTs are promising for optically transparent and flexible display electronics. Zhang et al. reported separated CNT macro-electronics for a monolithically integrated active matrix organic light-emitting diode (AMOLED) displays on glass substrates [192]. It exhibits huge advantages for the next generation visual technologies due to its high light efficiency, flexibility, lightweight, and low-temperature processing. High performance ICs is another important application of CNT-TFTs. Chen et al. built medium scale ICs using CNT-TFTs [35]. Logical/arithmetical gates, shifters, and d-latch circuits were designed and demonstrated with rail-to-rail output with superior performance. Besides, as the maturity of printing techniques, many wearable devices have been put into use with outstanding flexibility and stability, such as artificial electronic skin, chemical/biological sensors, solar cells, and stretchable electrode for actuators [20, 80, 124].

However, significant challenges still exist in many aspects, e.g., (a) device-to-device performance variation is becoming a critical problem for reliability and stability consideration as well as circuit design; (b) the lack of selectivity of CNT based gas sensors can severely limit their applications in gas detection and gas identification; (c) for printed TFTs, the uniformity of printed CNT network and roughness/thickness of dielectric layer will be a major obstacle to achieve higher device performance; and (d) the application of flexible sensors is the trend in the future. It is critical to make best of the tradeoff between high sensitivity and low cost, which needs further studies, etc. Undoubtedly, all of these need to be analyzed and understood thoroughly.

## **2.4 Contributions of Current Work**

The important findings and the major contributions of the current work are listed below

- (1) A systematic study of variability in I-V characteristics has been performed in a statistical framework through a combination of experimental and theoretical analysis of the major sources which cause performance variation. For the experimental analysis, array of CNT-TFTs are fabricated using high-k dielectric  $\text{HfO}_2$  as gate oxide layer to achieve high performance (PL fabrication). For the theoretical part, we apply the current scaling relationship developed by Pimparkar et al.[193] and analyze each variable used in the relationship, which can be a major source of variability. The sources of variation including % of M-CNTs,  $V_{th}$ , CNT mean length and CNT network density have been studied separately. The analysis shows that the presence of m-CNT is a major source contributing to the performance variation for short channel TFTs, but its effect reduces for large channel length transistors.  $V_{th}$  is found to be the major source of variation for long channel TFTs. A better consistency in performance can be guaranteed for TFTs

with larger channel area, which ensures a smaller variation in CNT network density and CNT mean length. These results provide key insights into the variability estimation of I-V characteristics of CNT based devices which is vital for reliability studies of CNT-TFTs based circuits for different electronic applications.

- (2) CNT-TFTs have been fabricated using randomly distributed CNT network (PL fabrication) and they are investigated for  $\text{NH}_3$  and  $\text{NO}_2$  detection at low ppm concentrations. Sensor response from  $\text{NH}_3$  and  $\text{NO}_2$  spray at 2ppm-40ppm has been measured in air at room temperature. A sensing mechanism is proposed based on the interaction between gas molecules and different types of dwelling spots inside the channel area of a TFT. We present double exponential-convolution model to decipher sensor response as well as to explore its application in gas identification. In this context, the consistency in time constants is recognized, which is independent of gas concentration. More importantly, the time constants vary with respect to different gas types and TFTs. The uniqueness of time constants can work as identity verification for different sensing gases, which demonstrates that the sensor response is a distinctive behavior determined by the unique channel structure of each TFT. It provides a general strategy for gas identification in ppm level and a practical path to realize the advantages of CNT gas sensors in air quality detection as well as the industrial emission control.
- (3) Fully printed CNT-TFTs have been fabricated (AJP fabrication) on Kapton and PET substrates with high on/off ratio, high mobility, negligible hysteresis, and good uniformity. More importantly, the fully printed CNT-TFTs can be operated using bias voltages  $\sim \pm 5\text{V}$ , which is much smaller than the previously reported values because of the improvement in both CNT network and dielectric layer. Multiple layer by layer CNT

network deposition is applied for density control and high uniformity, and xdi-dcs is diluted and optimized with natural  $\geq 99.5\%$  butyl alcohol to reach thinner printing for better gate dielectric quality. The performance was highly improved by optimization of xdi-dcs layer for the first time, which is key for CNT-TFTs based flexible electronics to achieve lower voltage operation and power dissipation. This paves the path for applications of CNT-FETs in wearable and bendable devices such as flexible displays, RFID antennae/tags, sensors, artificial skins, etc.

- (4) CNT networked gas sensors are fabricated base on printing techniques (AJP and IJP fabrication). The fully printed CNT sensors are applied for  $\text{NH}_3$  and  $\text{NO}_2$  detection in air at low ppm concentration. Through comparison with CNT sensors fabricated by PL, printed sensors show no degradation with respect to sensitivity and stability, but much lower in cost. Especially for sensors using extremely low-cost IJP (with the printer price only US \$108), the corresponding sensor responses still show excellent performance. The sensitivity was surprisingly high for some printed CNT sensors with drop-casted CNT network. Moreover, the post drop-casted deposition (without any surface functionalization) could help improve the sensitivity efficiently by rebuilding the CNT network of low sensitivity sensors, which implies the extremely low-cost potential of CNT gas sensors using IJP and drop-cast method. It provides key insights for the application of extremely low-cost CNT gas sensors.

## CHAPTER 3. PERFORMANCE VARIABILITY OF CNT-TFTS

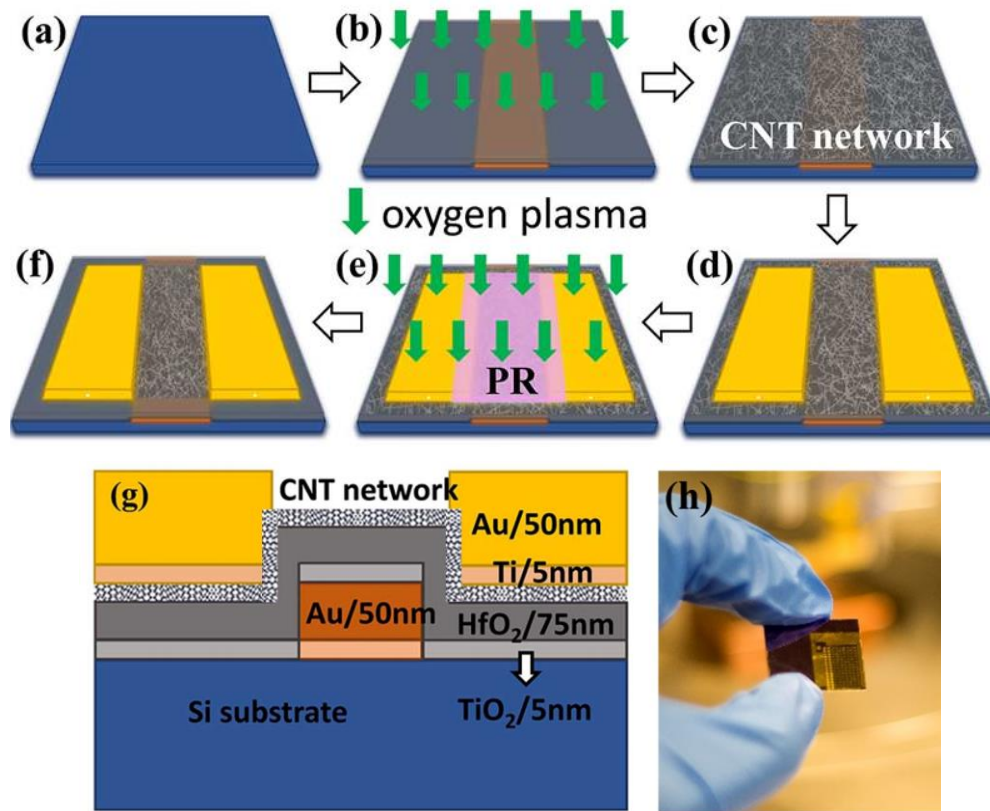
In this Chapter, both experimental and theoretical methods were employed to analyze the variability in I-V characteristics in a statistical framework. For the experimental analysis, array of CNT-TFTs were fabricated using high-k dielectric  $\text{HfO}_2$  as gate dielectric to achieve high performance. 40~50 devices of each series (same channel dimensions) were fabricated on a Si wafer for the statistical study. For the theoretical part, the current scaling relationship [193] was applied and each variable used in the relationship was analyzed, which can be a major source of variability. To be specific, each variable was treated as a distribution function while keeping others as constants. Variation sources such as % of M-CNTs,  $V_{th}$ , CNT mean length, and CNT network density were studied statistically for different channel dimensions. For the first time, the variability analysis of random CNT network based TFTs has been studied systematically. This analysis presents an effective way of the variability estimation of CNT network based TFTs. Such analysis of CNT-TFTs is crucial to explore the reliability and stability of CNT network based circuits and to devise techniques which can help reduce variability in circuit performance for various electronic applications.

### 3.1 Fabrication of CNT-TFTs

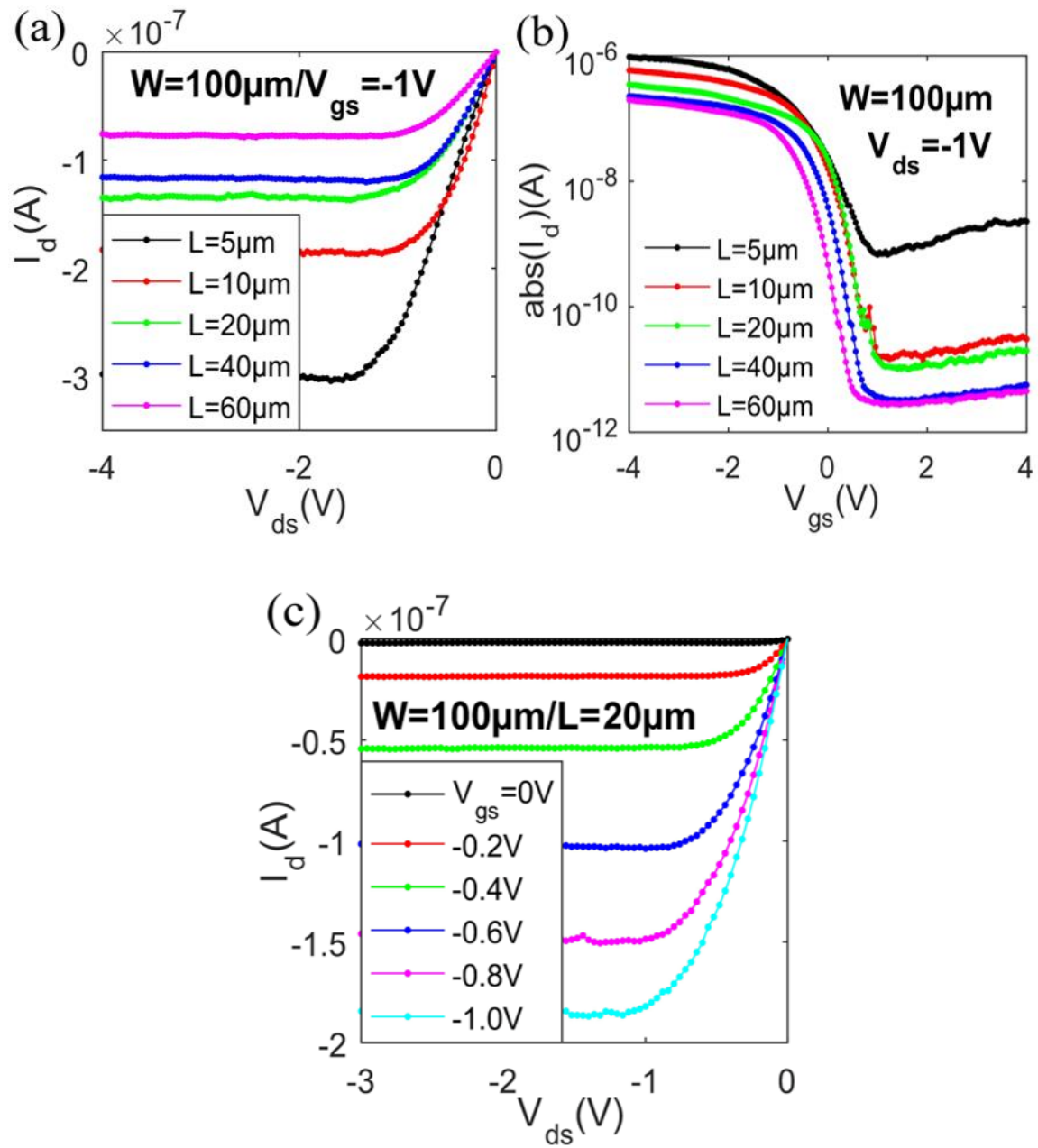
CNT-TFTs were fabricated at the Institute for Electronics and Nanotechnology (IEN) cleanroom of Georgia Tech. The structure and fabrication process of a typical TFT are illustrated in Figure 3.1. First, Ti/Au (5nm/50nm) layers as back gate were deposited on top of a Si wafer by e-beam evaporation at deposit rate of  $0.2\text{\AA}/\text{s}$  and  $1\text{\AA}/\text{s}$  respectively. The gate contacts were patterned between the source/drain (S/D, deposited later) electrodes. Following this, ALD was used to deposit  $\text{TiO}_2$  (1.5 nm/15 cycles) and  $\text{HfO}_2$  (75nm/600 cycles), covering the entire wafer



surface as a global gate-dielectric layer. Ti and TiO<sub>2</sub> work as adhesion layers for the gate and gate dielectric. Then, 15~30s oxygen plasma treatment was indispensable to make the surface hydrophilic[81]. After this, CNT network was deposited by immersing the wafer into 0.005-0.01g/L toluene-based CNT solution for 5-15 minutes (CNT source: >99% purity polymer-wrapped CNT solution from NanoIntegris). The resulting density of the CNT network is a function of both deposition time and concentration of the CNT solution. Ti/Au (5nm/50nm) layers as S/D electrodes are patterned by PL and lift-off process. This step was followed by another PL and 30s oxygen plasma treatment to form channel area by etching away unwanted part of the CNT network. At last, vacuum annealing at 250°C for 2 hours was performed to get rid of the surface residue on the wafer.



**Figure 3.1 Fabrication of CNT-TFTs. (a) ~ (f) Fabrication process. (g) The sectional view of the CNT-TFT. (h) CNT-TFTs fabricated in IEN cleanroom.**



**Figure 3.2 I-V characteristics. The overall I-V characteristics shows good performance of the p-type CNT-TFTs with on/off ratio as high as  $10^5$  and mobility around  $1\text{-}4\text{ cm}^2\text{ V}^{-1}\text{ s}^{-1}$ .**

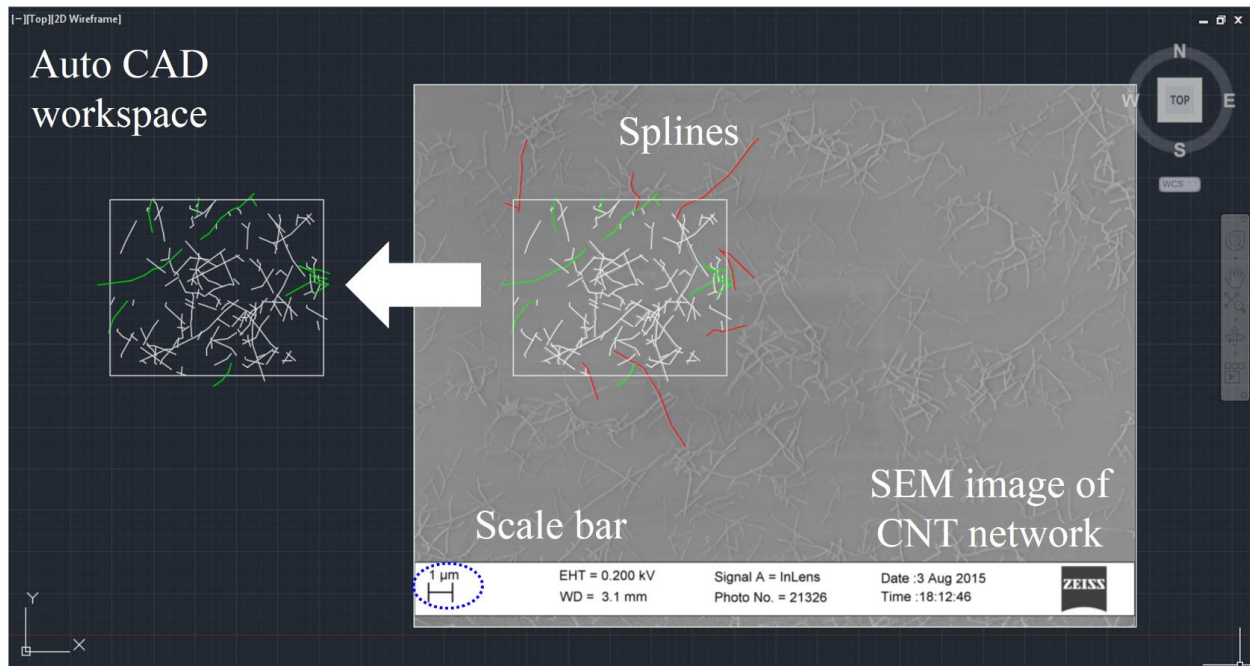
### 3.2 I-V Characteristics of CNT-TFTs

After the fabrication, I-V characteristics of the CNT-TFTs had been measured using Microtech Summit 11k probe station and Keithley 4200-SCS. The I-V of the CNT-TFTs is plotted

in Figure 3.2. The output characteristics ( $I_d$ - $V_{ds}$  curves) of the CNT-TFTs is depicted in Figure 3.2(a) for different channel lengths with drain voltage ( $V_{ds}$ ) swept from 0 to -4V at  $V_{gs}=-1$  V, where  $I_d$  is the drain current and  $V_{gs}$  is the gate voltage. For the transfer characteristics ( $I_d$ - $V_{gs}$  curves),  $V_{gs}$  was swept from -4~4V (forward sweeping) while keeping  $V_{ds} = -1$  V. Semi-log plots are shown in Figure 3.2(b) for each channel length. The on/off ratio increases from  $10^3$  to as high as  $10^5$  when the channel length increases from 5 $\mu$ m to 60 $\mu$ m, which can be expected since the CNT networks still contain M-CNTs even though it is purified for 99% semiconducting tubes. The on/off ratio is a function of the channel length as the TFTs with smaller channel length have much higher possibility to bridge the channel by M-CNTs. In Figure 3.2(c), the output characteristics at different  $V_{gs}$  is plotted for a specific device. The overall I-V characteristics shows good performance of the p-type CNT-TFTs with on/off ratio as high as  $10^5$  and mobility around 1-4  $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$

### 3.3 CNT Statistics

CNT network as well as individual CNTs play an important role for the fabricated CNT-TFTs with respect to mobility, on/off ratio,  $V_{th}$ , etc. Before variability analysis, CNT length distribution has been obtained using Auto CAD sampling and statistics based on the scanning electron microscope (SEM) images of CNT network. Besides, CNT network density can be estimated based on both Auto CAD sampling and image processing technique.



**Figure 3.3 Statistics of CNT length distribution using Auto CAD software and a SEM image of low-density CNT network. The white frame is selected randomly. The green splines denote CNTs that will be recorded (the red ones will not be recorded). The scale bar is used as calibration standard in order to calculate the real lengths of all the target CNTs.**

### 3.3.1 Statistics of CNT Length Distribution

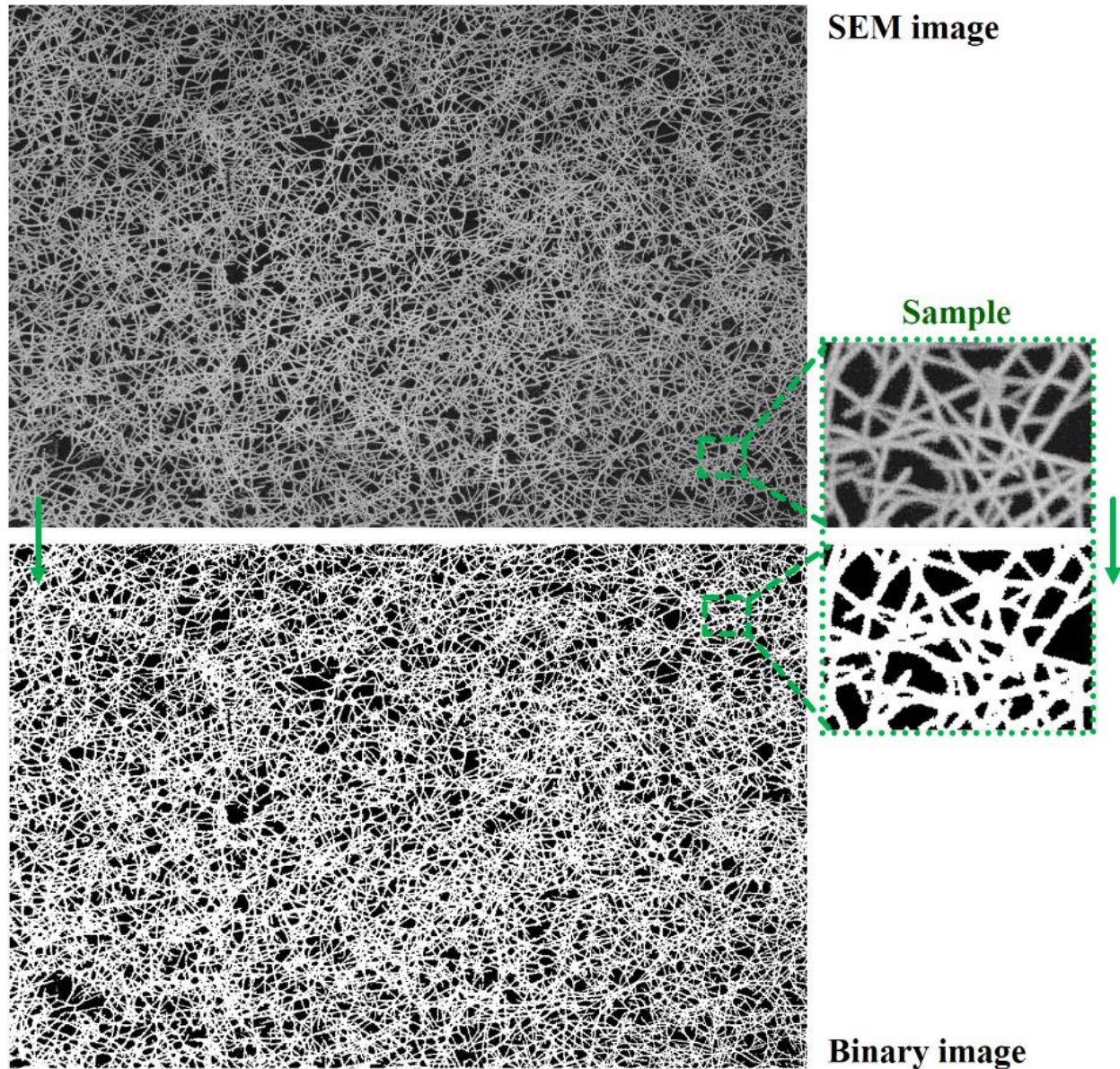
To obtain the CNT length distribution, we measure CNT length one by one from a much lower density network using the same CNT solution. In this way, the overlapping between CNTs can be avoided and each of them can be located individually. Then ‘spline’ of Auto CAD is used to draw each CNT separately while setting the SEM image as background in Auto CAD workspace as shown in Figure 3.3. After that, the length information of CNTs can be obtained by recording the length of each ‘spline’. At last, calibration is performed by utilizing the scale bar in the SEM image to calculate the real length information of the target CNTs.

In order to get accurate length distribution, different area is selected randomly (using multiple white frames to repeat the described process) from different CNT network samples. And



for each target area (each white frame), only CNTs with  $>50\%$  of its length inside the frame are recorded, which can guarantee that all the CNTs will have the equal probability to be recorded no matter what length it is. Considering hundreds of CNTs, the CNT mean length is measured to be  $1.08\mu\text{m}$  (the suggested value from the vendor is  $\sim 1\mu\text{m}$ ).

### Target image of CNT network



**Figure 3.4** Estimation of CNT network density based on image processing by converting the SEM image into a binary image. The inset of the sample image is used to estimate the average diameter of all the CNTs in the target image.

### 3.3.2 Estimation of CNT Network Density

The CNT network density ( $\rho$ ) is defined as the number of CNTs per unit area. To estimate CNT network density in the channel of CNT-TFTs, an image processing technique is put forward to convert the target SEM image of CNT network into the corresponding binary image by using Matlab. Then the relationship between CNT network density and the white pixel of the binary image can be established for the density estimation.

As shown in Figure 3.4, the target SEM image can be acquired through Zeiss Ultra60 FE-SEM. To calculate the CNT network density of the target image, the corresponding binary image can be generated to obtain the white pixel area ( $A_{t\_white}$ ), which denotes all the CNTs in the target image. Then  $A_{t\_white}$  can be expressed as

$$A_{t\_white} = D_{t\_CNT} \times L_{t\_CNT} \quad (3.1)$$

where  $D_{t\_CNT}$  is the average diameter of CNTs in the target binary image, and  $L_{t\_CNT}$  is the total length of all the CNTs in the target binary image. It is worth noting that the real diameter of SWCNT is as small as 1-3nm, which cannot be used as  $D_{t\_CNT}$  in equation (3.1).  $D_{t\_CNT}$  will be much larger because of the optical effect during SEM imaging. To estimate the value of  $D_{t\_CNT}$ , a sample area is selected and similar expression can be obtain for this sample binary image

$$A_{s\_white} = D_{s\_CNT} \times L_{s\_CNT} \quad (3.2)$$

where  $D_{s\_CNT}$  is the average diameter of CNTs in the sample binary image, and  $L_{s\_CNT}$  is the total length of all the CNTs in the sample binary image. To obtain the value of  $L_{s\_CNT}$ , Auto CAD sampling and statistics strategy has been used again as described in Figure 3.3.  $A_{t\_white}$  and  $A_{s\_white}$  can be obtained from the corresponding binary images. Then assume

$$D_{t\_CNT} = D_{s\_CNT} \quad (3.3)$$

Based on equation 3.1 – 3.3,  $L_{t\_CNT}$  can be calculated as

$$L_{t\_CNT} = L_{s\_CNT} \times A_{t\_white} / A_{s\_white} \quad (3.4)$$

At last, the CNT network density ( $\rho$ ) can be calculated as

$$\rho = L_{t\_CNT} / A_t / L_s \quad (3.5)$$

where  $A_t$  is the total area of the target image, and  $L_s$  is the CNT mean length ( $1.08\mu\text{m}$ ) which has been obtained in section 3.3.1. As a result, the CNT network density is calculated as  $11.718 / \mu\text{m}^2$  in the target image. Clearly, the assumption of equation 3.3 is the key during the calculation, which depends on the selection of the sample area. As a matter of fact, the value of  $D_{s\_CNT}$  is very stable in most of situation when the SEM image is taken properly. If  $D_{s\_CNT}$  depends much on the selection of sample area, multiple sample area should be selected in order to satisfy the assumption of equation 3.3. This method is proved to be very reliable for the estimation of CNT network density.

### 3.4 Source of Variation and Variability Analysis

This study focuses on the variability analysis of I-V characteristics of CNT-TFTs. The performance variation results from multiple sources, described below:

#### On the level of individual CNTs

One of the major sources of variability lies in the large difference of electronic properties between M-CNTs and semiconducting S-CNTs. Generally, as-grown CNT networks contains 33% M-CNTs, which largely limit the function of gate to achieve high on/off ratio[1]. In Figure 3.2, the

on/off ratio varies from  $10^3$  to  $10^5$  for different channel lengths even though 99% purified CNT solution (i.e., 99% S-CNT and 1% M-CNT) were used. The length distribution of CNT is another source of variability. In our CNT networks, the average length of CNT is  $\sim 1\mu\text{m}$ . However, some CNTs can be  $> 5\mu\text{m}$  while some other CNTs can be as short as  $0.1\mu\text{m}$ . The performance variations for the short channel TFTs will be much higher since longer CNTs can directly bridge the source and drain with much higher probabilities[193]. Besides, difference in diameter, morphology, doping of individual CNTs may also contribute to the variability in I-V characteristics[194, 195].

#### On the level of the CNT networks

On the one hand, CNT network density has a significant effect on the drain current, which has been studied intensively in the recent years. The significant performance variations can result from the density variation since it cannot be controlled perfectly in practice. No matter how a CNT network is fabricated in a TFT, density will vary from region to region. On the other hand, CNT network structure can be another reason for variability. For TFTs with the same channel length and the same network density, performance variations still exist because the randomly distributed CNTs make each network structure different from each other. Although each TFT has different network structure, variability can be deciphered in a statistical framework by studying TFTs with a range of channel dimensions and network densities.

#### On the level of the device

The variation in  $V_{th}$  can lead to significant variation in I-V characteristics and device performance.  $V_{th}$  can be obtained for each TFT and its effect on the variability can be quantified[72, 196, 197]. Many imperfections may exist during the fabrication process which can be significant sources of variation, e.g., variations in oxide layer thickness, contact patterns,

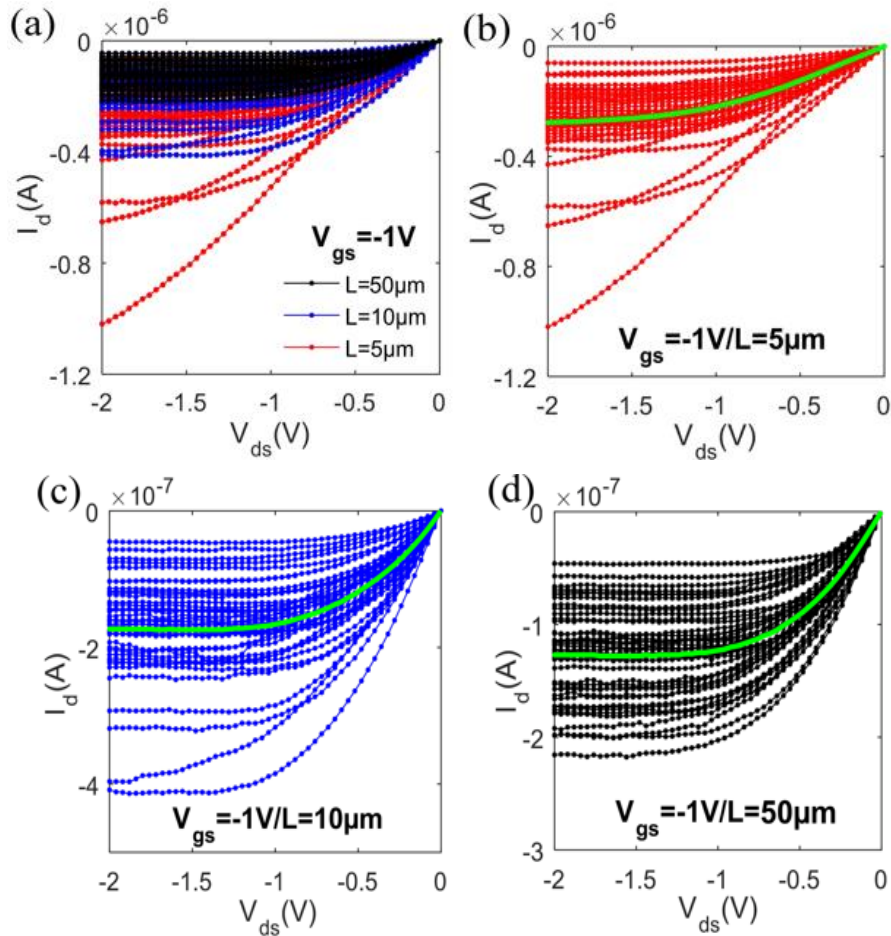


contamination region by region etc.

In general, the sources described above at different levels can contribute to the final performance variation. It is impossible and needless to analyze each cause one by one. But capturing the effect of most important sources is rather reasonable and feasible. Contact resistance ( $R_c$ ) between CNTs and electrodes has been ignored because  $R_c$  is small compared to the total resistance ( $R_{SD}$ ) of the random CNT networks considered. Using a transfer length method (TLM),  $R_c$  is estimated to be  $\sim 6.8\text{k}\Omega$  which is less than 1% of the average total resistance ( $R_{SD}$ ) of the smallest channel length considered ( $\sim 5\mu\text{m}$ ). The reason for high  $R_{SD}$  is rooted in the large number of CNT-CNT junctions inside a randomly generated CNT network, which dominates the total resistance. In the following discussion, variation in I-V characteristics of TFTs were analyzed and compared by both experimental and theoretical means. Experimental data corresponds to the I-V characteristics measured for the TFTs fabricated at Georgia Tech's IEN. Theoretical data were obtained using the empirical formula developed by Pimparkar et al. [193].

CNT-TFTs with three different channel length series ( $L=5\mu\text{m}$ ,  $10\mu\text{m}$ , and  $50\mu\text{m}$ ) were considered and referred as  $5\mu\text{m}$  series,  $10\mu\text{m}$  series, and  $50\mu\text{m}$  series, respectively. For each series, we fabricated 45 CNT-TFTs and analyzed the variability of I-V. The transfer and output characteristics was measured for CNT-TFTs with  $5\mu\text{m}$ ,  $10\mu\text{m}$ , and  $50\mu\text{m}$  series. For output characteristics,  $V_{ds}$  was swept from 0 to  $-2\text{V}$  at  $V_{gs} = -1\text{V}$ . From Figure 3.5(a)~(d), it is obvious that TFTs with longer channel lengths have smaller current magnitude. It can be also noted that the longer channel TFTs have a smaller range of variation in the saturated current, referred as  $I_{d(sat)}$ . From the experimental data, the range of variation in  $I_{d(sat)}$  of  $L=5\mu\text{m}$ ,  $10\mu\text{m}$ , and  $50\mu\text{m}$  series are  $(-1\times 10^{-6}, -0.6\times 10^{-7})$ ,  $(-4\times 10^{-7}, -0.5\times 10^{-7})$ , and  $(-2.1\times 10^{-7}, -0.4\times 10^{-7})$ . Their mean values are  $-2.8\times 10^{-7}$ ,  $-1.7\times 10^{-7}$ , and  $-1.3\times 10^{-7}$  respectively. Here the unit of current is A by default unless stated

otherwise. For the TFTs whose current does not saturate in the range of sweep voltage considered, the  $I_{d(sat)}$  corresponds to the maximum magnitude of the measured current. The average  $I_d$ - $V_{ds}$  curves for each series are illustrated in Figure 3.5(b)~(d) by green curves. The  $I_{d(sat)}$  distribution can be found in Figure 3.6. The standard deviations for 5 $\mu$ m, 10 $\mu$ m, and 50 $\mu$ m series are  $1.7 \times 10^{-7}$ ,  $7.7 \times 10^{-8}$ , and  $4.1 \times 10^{-8}$ , respectively. And the corresponding standard deviation normalized by mean are 0.61, 0.45, and 0.32 respectively. From the experimental data, it can be deciphered that the longer channel length TFTs are more stable and have less variations in performance.



**Figure 3.5 Measured output characteristics of fabricated CNT-TFTs. All devices are shown together in (a), and shown separately for 5 $\mu$ m series (b), 10 $\mu$ m series (c), and 50 $\mu$ m series (d). Green curves in (b)~(d) denote average output characteristics.**

### 3.4.1 M-CNT and S-CNT

In experiments, the variability of I-V characteristics is a combined result of all the possible sources. It is difficult to separate the influence of each source. However, the influence of some variables can be easily deciphered, e.g., M-CNTs and S-CNTs. As depicted in Figure 3.7, the I-V curves are significantly different for TFTs with only M-CNTs or only S-CNTs. The presence of M-CNTs makes the curves unsaturated since M-CNTs form a percolating path through source and drain (the M-CNT effect). It will be difficult to switch on or switch off such transistors by gating. Considering this fact, we further inspected the curves in Figure 3.5. Clearly, the M-CNT effect is significant only for 5 $\mu$ m and 10 $\mu$ m series, and insignificant for 50 $\mu$ m series. As we used 99% purified CNT solution, it is very less likely that M-CNTs bridge source and drain with distance of 50 $\mu$ m when the average length of CNTs is only 1  $\mu$ m and the CNT network density is around 13/ $\mu$ m<sup>2</sup>. However, the probability is much higher for M-CNTs to bridge source and drain for 5 $\mu$ m series TFTs. Moreover, there are some longer CNTs (3-5 $\mu$ m, some even >5 $\mu$ m) which will make bridging much easier for 5 $\mu$ m series. In Figure 3.8, CNT length distribution was investigated. The average length is 1.08 $\mu$ m, which is consistent with the reference value  $\sim$ 1 $\mu$ m. That is why we have relatively large % of TFTs experiencing the M-CNT effect for 5 $\mu$ m series, less for 10 $\mu$ m series, none for 50 $\mu$ m series. After ruling out the M-CNT effect (discard unsaturated curves), the variation range for 5 $\mu$ m series is narrowed down from  $(-10 \times 10^{-7}, -0.6 \times 10^{-7})$  to  $(-4.3 \times 10^{-7}, -0.6 \times 10^{-7})$ . While 10 $\mu$ m and 50 $\mu$ m series stay the same. Therefore, the M-CNT effect dominates performance variations for short channel TFTs but not for the long channel TFTs. Even though the M-CNT effect exists for 10 $\mu$ m series, its variation range does not change.

To analyze other potential variation sources, we resort to the current scaling relationship[193], which does not include the effect of M-CNTs.

$$I_d = \frac{A}{L_s} \xi\left(\frac{L_s}{L}, \rho L_s^2\right) \times f(V_{gs}, V_{ds}) \quad (3.6)$$

Here,  $I_d$  is the drain current and the proportionally constant  $A$  depends on the oxide capacitance, CNT diameter and CNT-CNT interaction parameter[72].  $L_s$  is CNT mean length.  $\xi$  and  $f$  are functions of the geometrical parameters ( $L_s$ ,  $L$  and  $\rho$ ) and bias conditions ( $V_{gs}$  and  $V_{ds}$ ), where  $L$  is channel length,  $\rho$  is CNT network density,  $V_{gs}$  is gate bias voltage, and  $V_{ds}$  is drain bias voltage.  $\xi$  can be expressed as

$$\xi\left(\frac{L_s}{L}, \rho L_s^2\right) = \left(\frac{L_s}{L}\right)^{m(\rho L_s^2)} \quad (3.7)$$

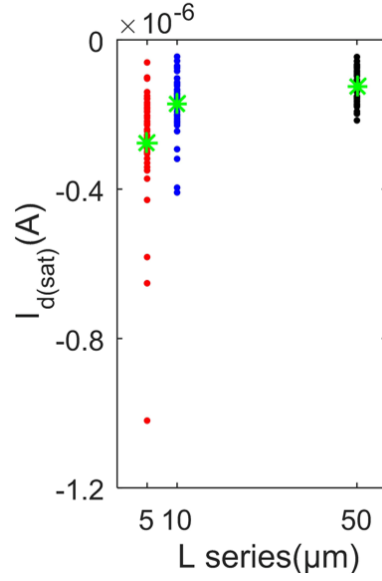
Here,  $m$  is a universal exponent of CNT percolating system, which is a function of  $\rho$  and  $L_s$ . This relation is derived and analyzed in [193]. The bias-dependent scaling function

$$f(V_{gs}, V_{ds}) = [(V_{gs} - V_{th})V_{ds} - \frac{1}{2}V_{ds}^2] \quad (3.8)$$

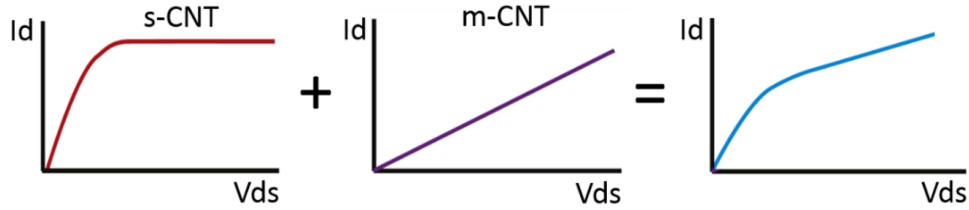
is independent of the geometrical parameters, where  $V_{th}$  is threshold voltage. Plugging (3.7) and (3.8) into (3.6), the current scaling relationship can be expressed as

$$I_d = \frac{A}{L_s} \left(\frac{L_s}{L}\right)^m [(V_{gs} - V_{th})V_{ds} - \frac{1}{2}V_{ds}^2] \quad (3.9)$$

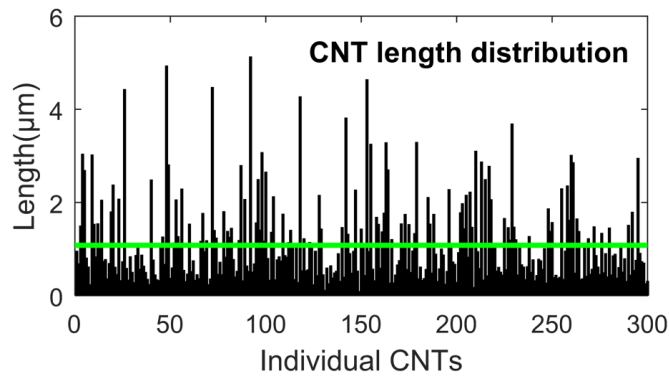
Theoretically, all the listing variables will have effects on the variation of  $I_d$ . By considering each variable as a statistical distribution such as normal or lognormal distribution, the corresponding distribution for  $I_d$  can be obtained.



**Figure 3.6  $I_{d(sat)}$  distribution for various channel lengths. L series: red=5 $\mu\text{m}$  series; blue=10 $\mu\text{m}$  series, black=50 $\mu\text{m}$  series. Green stars denote average values for each series.**



**Figure 3.7 Schematic of output characteristics for S-CNT, M-CNT, and considering mutual influence from both.**

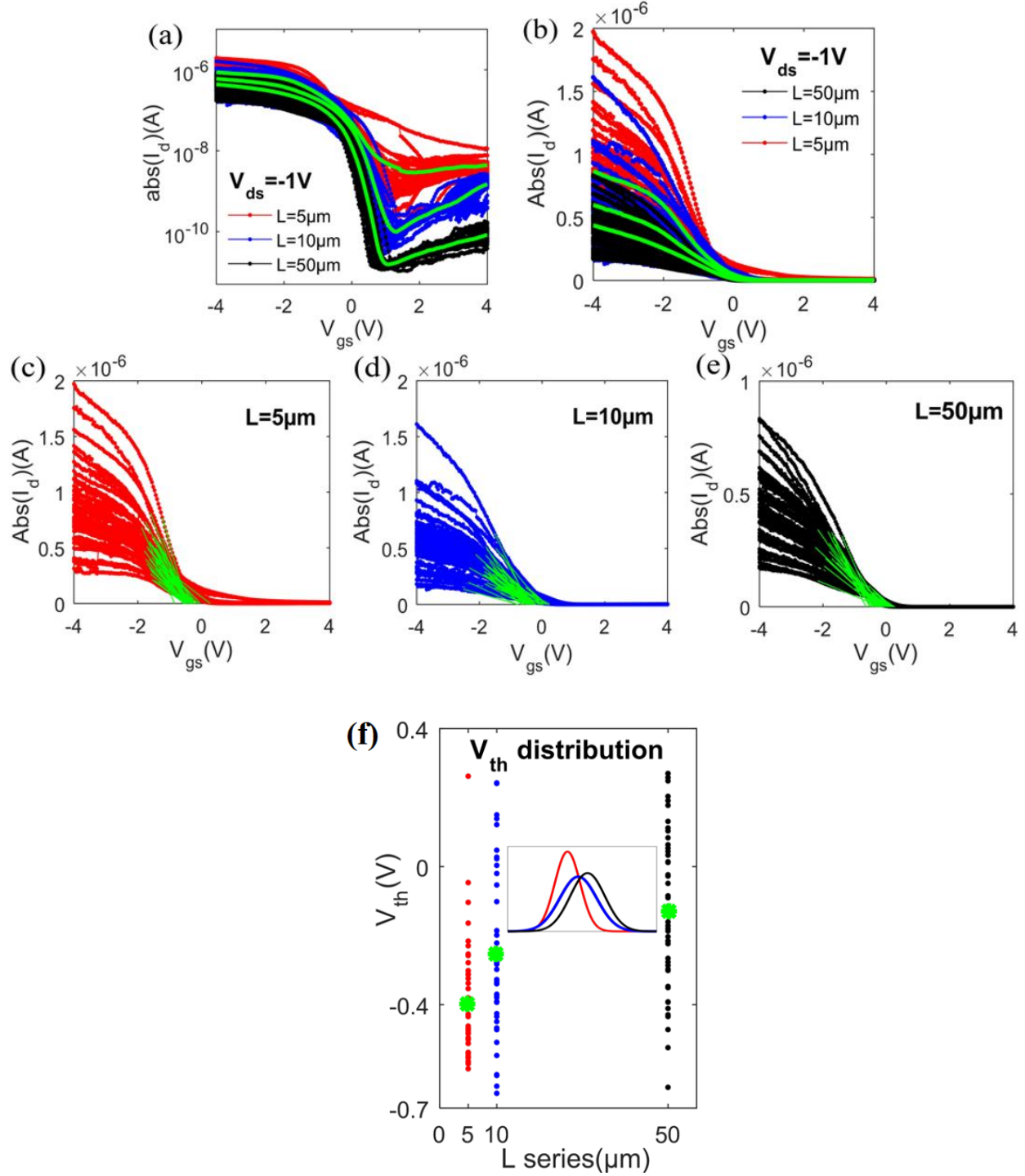


**Figure 3.8 CNT length distribution from measurement. A sample of 300 CNTs was chosen for statistics (x-axis). Green line denotes the average length (1.08 $\mu\text{m}$ ) of the 300 CNTs (reference average length  $\sim 1\mu\text{m}$ ).**

### 3.4.2 Threshold Voltage

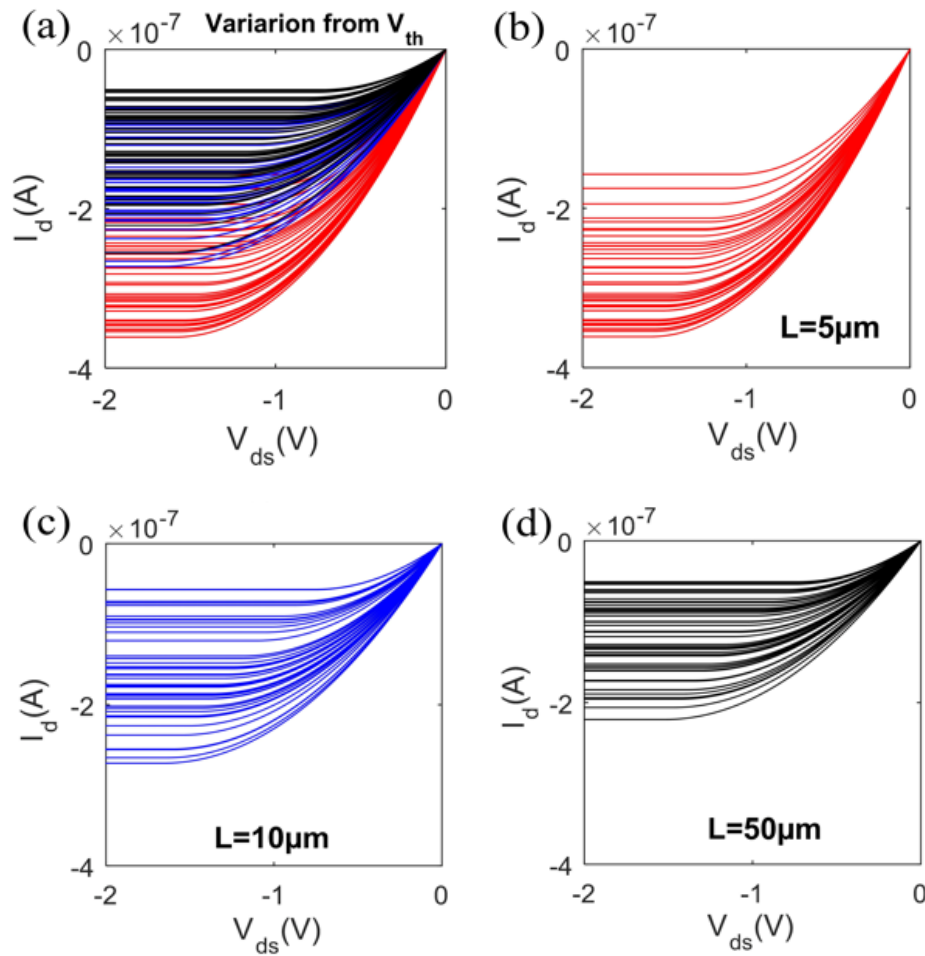
The  $V_{th}$  distribution was considered as a source of variability in the I-V characteristics. Ortiz-Conde et al. studied multiple methods to obtain  $V_{th}$  from the transfer characteristics [197], e.g., by linear extrapolation of the  $I_d$ - $V_{gs}$  curve at its maximum first derivative point and finding the intercept of the gate bias axis. Using this method,  $V_{th}$  was extracted from the measured  $I_d$ - $V_{gs}$  curves where  $V_{gs}$  was swept from -4~4V at  $V_{ds} = -1V$ .  $I_d$ - $V_{gs}$  curves are shown in Figure 3.9(a)~(b) under both linear and semi-log axes for  $V_{gs}$ . The results for  $V_{th}$  are presented in Figure 3.9(c)~(e) for 5 $\mu m$ , 10 $\mu m$ , and 50 $\mu m$  series separately. The corresponding distribution of  $V_{th}$  can be found in Figure 3.9(f). Average  $V_{th}$  equals to -0.39V, -0.25V, and -0.13V, and standard deviation of  $V_{th}$  equals to 0.17, 0.25, and 0.23 for 5 $\mu m$ , 10 $\mu m$ , and 50 $\mu m$  series, respectively. Even though  $V_{th}$  shows increasing trend with increasing channel length, such trend should not be generalized for other TFTs. We do not have experimental data and evidences to accurately explain the physics behind this observation.  $V_{th}$  can be affected by many factors such as random dopant fluctuation, different types of oxide charges, body effect, etc. and the observed trend can be a combined influence of these parameters.  $V_{th}$  can be represented as a normal distribution, which is shown in inset of Figure 3.9(f).

Using the  $V_{th}$  distribution estimated from the experimental data, we obtained series of output characteristics from equation 3.9 by setting the rest of variables constants ( $L_s = 1.08\mu m$ ,  $V_{gs} = -1V$ ,  $m = 1.05$ ,  $L = 5\mu m$ , 10 $\mu m$ , and 50 $\mu m$  for each series).  $L_s = 1.08\mu m$  is CNT mean length, and  $m = 1.05$  is determined by average CNT network density, which is  $\rho = 13/\mu m^2$ . The value of  $A$  in equation 3.9 was determined by making the calculated average  $I_{d(sat)}$  from equation 3.9 equals the experimental average  $I_{d(sat)}$ .



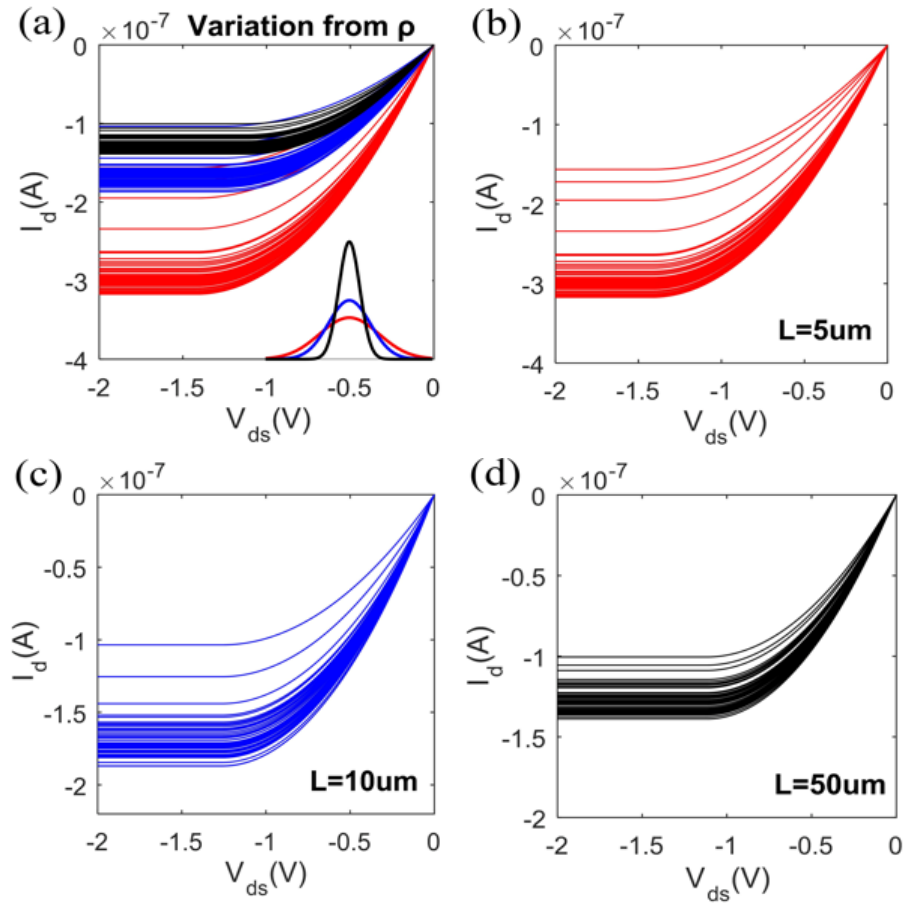
**Figure 3.9** Measured transfer characteristics using semi-log scale (a) and linear scale (b). of CNT-TFTs for  $5\mu\text{m}$  series (c),  $10\mu\text{m}$  series (d), and  $50\mu\text{m}$  series (e). Green curves in (a)~(b) denote the average transfer characteristics. Green lines in (c)~(e) denote  $V_{th}$  extrapolation. The resulting  $V_{th}$  distribution is shown in (f) for different  $L$  series.

Therefore,  $V_{th}$  is the only source of variation in equation 3.9. The corresponding variability in output characteristics is shown in Figure 3.10. The variation range of calculated  $I_{d(sat)}$  for 5 $\mu\text{m}$ , 10 $\mu\text{m}$  and 50 $\mu\text{m}$  series are  $(-3.61 \times 10^{-7}, -1.57 \times 10^{-7})$ ,  $(-2.73 \times 10^{-7}, -5.69 \times 10^{-8})$  and  $(-2.21 \times 10^{-7}, -5.23 \times 10^{-8})$ . Analyzing the measured  $I_{d(sat)}$  in Figure 3.6, the variation caused by  $V_{th}$  account for 16%, 61%, and 99% of the range of variation in  $I_{d(sat)}$  for 5 $\mu\text{m}$ , 10 $\mu\text{m}$ , and 50 $\mu\text{m}$  series, respectively. Therefore,  $V_{th}$  is a main source that contributes to variability in  $I_{d(sat)}$  for long channel TFTs ( $L \geq 10\mu\text{m}$ ). While for short channel TFTs ( $L \leq 5\mu\text{m}$ ),  $V_{th}$  only accounts for a small part of the entire variation.



**Figure 3.10** The variability based on the normal distributions of  $V_{th}$





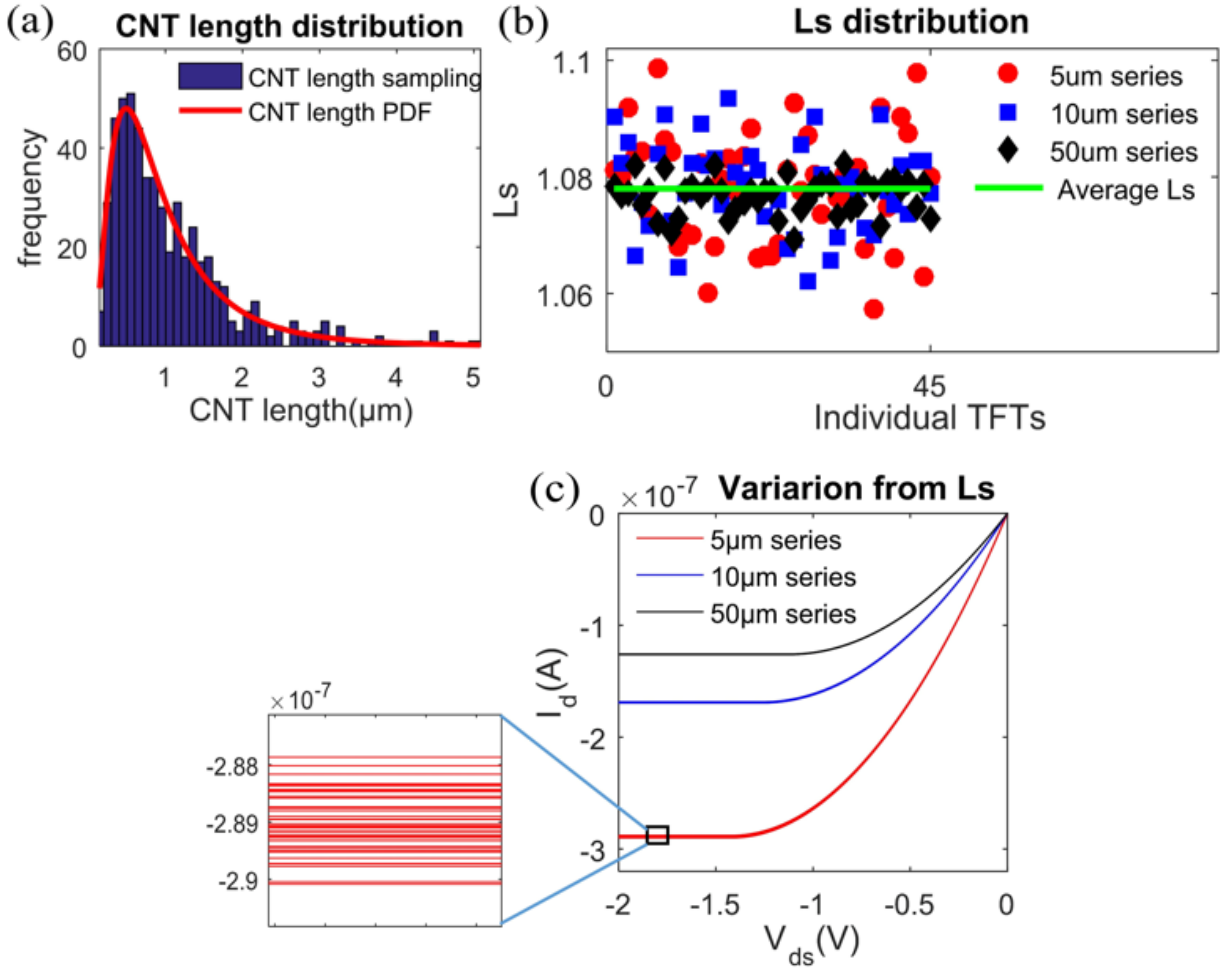
**Figure 3.11 The variability based on the normal distributions of CNT network density.**

### 3.4.3 CNT Network Density

The effect of CNT density ( $\rho$ ) distribution in the TFT channel was analyzed using the same method as for  $V_{th}$ . The variation in  $\rho$  will result in the variation in ‘m’ parameter in equation 3.9, which in turn affects the variability in output characteristics. The relationship between  $\rho$  and m can be found in [193]. From this relationship, we incorporated the distribution of  $\rho$  for each channel length series. Assume  $\rho$  obeys normal distribution with mean value  $\mu$  and standard deviation  $\sigma$ , we measured  $\rho$  from SEM images by sampling multiple regions inside TFT channels. This measurement was performed only for 5 $\mu$ m series TFTs; we obtained statistical mean  $\mu=13/\mu\text{m}^2$

and standard deviation  $\lambda=2.45$ . Based on this normal distribution, density values for all 5  $\mu\text{m}$  TFTs were generated. This normal distribution for 5 $\mu\text{m}$  series was then used for density value generation for 10 $\mu\text{m}$  and 50 $\mu\text{m}$  series. The only difference is, a 10 $\mu\text{m}$  channel can be treated as two 5 $\mu\text{m}$ -channels combined together and a 50 $\mu\text{m}$  channel can be treated as ten 5 $\mu\text{m}$ -channels combined together, with each element (a 5 $\mu\text{m}$ -channel) obeys the same normal distribution with  $\mu=13$  and  $\lambda=2.45$ . In this way, we can expect that the density for 10 $\mu\text{m}$  and 50 $\mu\text{m}$  series will stay the same ( $13/\mu\text{m}^2$ ) as for 5 $\mu\text{m}$  series while the standard deviation will be smaller. Both theoretical method and numerical sampling verified that the resulting standard deviations are  $\lambda=1.73$  for 10 $\mu\text{m}$  series and  $\lambda=0.77$  for 50 $\mu\text{m}$  series. Using the corresponding density distributions for 5 $\mu\text{m}$ , 10 $\mu\text{m}$ , and 50 $\mu\text{m}$  series (Figure 3.11 inset), the variability in output characteristics for each series was calculated and is presented in Figure 3.11(a)~(d).

Apparently, the range of variation for 5 $\mu\text{m}$ , 10 $\mu\text{m}$ , and 50 $\mu\text{m}$  series decreases with the increasing channel length, which is in agreement with the experimental trends depicted in Figure 3.5. This is because TFTs with larger channel area (longer channel lengths) are likely to have smaller standard deviation in density. Consequently, for 10 $\mu\text{m}$  and 50 $\mu\text{m}$  series, the range of variation caused by  $\rho$  are comparably smaller than that caused by  $V_{\text{th}}$ . But the range of variation for 5 $\mu\text{m}$  series is at the same level. Therefore, the influence on the output characteristics variability from  $\rho$  is more prevalent for small channel length TFTs. But for long channel length TFTs, such influence is a secondary consideration.



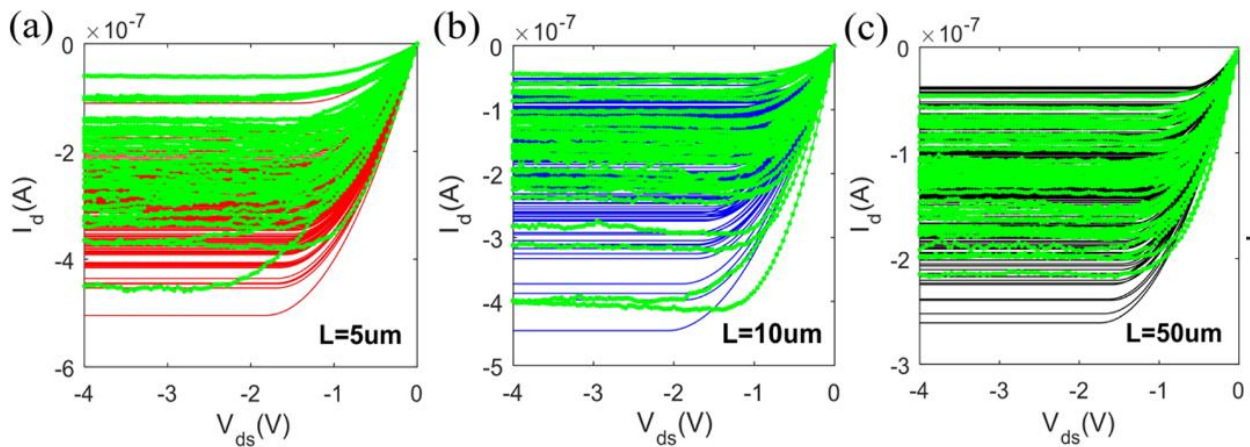
**Figure 3.12 (a) CNT length distribution. (b)  $L_s$  distribution for individual TFTs of each series. The green line denotes the average  $L_s$  of all series. (c) The variability based on  $L_s$ .**

#### 3.4.4 CNT Mean Length

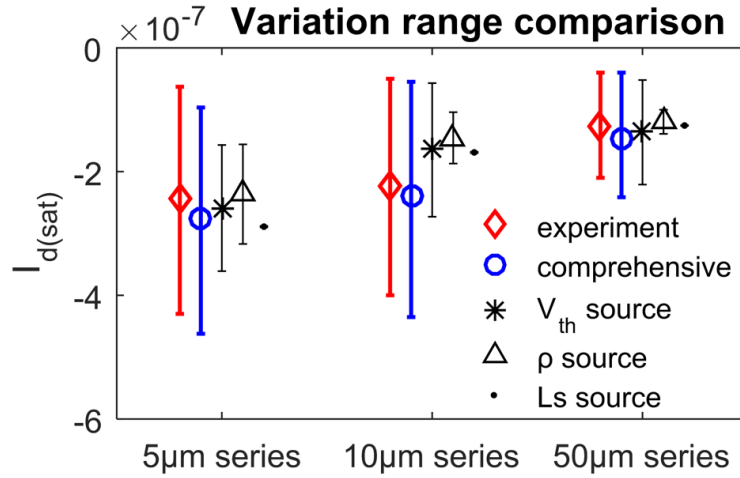
Using the similar method as for  $V_{th}$ , we considered the distribution of CNT mean length ( $L_s$ ) in the channel area of TFTs.  $V_{th}$  can be extracted from  $I_d$ - $V_{gs}$  curves while it is very difficult to obtain the length information of all CNTs in the TFT channel, especially when CNT network density is as large as  $13/\mu\text{m}^2$ . There will be a large number of CNTs in the channel and some CNTs may bundle with each other. So, a low-density network was fabricated and the lengths of all CNTs

in the network were recorded. We fitted the probability distribution function (PDF) to the measured CNT lengths, shown in Figure 3.12(a). This was found to be a log-normal distribution as observed in some previous studies[198]. Based on this PDF, CNT networks were generated using a computational model for TFT series with different channel lengths at a given density. Then  $L_s$  was determined by averaging the CNT lengths for each TFT channel. This simulation method is statistically reasonable because the CNT networks in the fabricated TFTs were also randomly generated during deposition.  $L_s$  distributions for  $5\mu\text{m}$ ,  $10\mu\text{m}$  and  $50\mu\text{m}$  series are plotted in Figure 3.12(b), which clearly shows that the standard deviation is larger for shorter channels. As more CNTs exist in the longer channel TFTs at a given density, the mean CNT length ( $L_s$ ) has a smaller range of variation than the channel with less CNTs.

Based on the  $L_s$  distributions, the corresponding output characteristics were obtained and shown in Figure 3.12(c). Results shows that  $L_s$  has very limited influence on the variability due to the large number of CNTs in the channel. However, the influence from  $L_s$  will be much larger when density goes down in small channels, i.e., when the variation range of  $L_s$  will be much larger.



**Figure 3.13** The variability after considering comprehensive effect of  $V_{th}$ ,  $\rho$ , and  $L_s$ .



**Figure 3.14 Comparison of variation range of different sources ( $V_{th}$ ,  $\rho$ , and  $L_s$ ) individually, comprehensive effect of the three sources, and experimental measurement (without M-CNT effect) for three different series ( $L=5\mu m$ ,  $10\mu m$ , and  $50\mu m$ ) analyzed in previous sections.**

### 3.4.5 Comprehensive Effects

Up to now, each important parameter of equation 3.9 has been considered individually. In practice, I-V characteristics variability is a comprehensive effect caused by all the parameters. Therefore, we considered the comprehensive variations from  $V_{th}$ , network density ( $\rho$ ), and CNT mean length ( $L_s$ ) all together in equation 3.9. To calculate the overall variability in  $I_d$ ,  $V_{th}$ ,  $\rho$ , and  $L_s$  were assigned values following their distribution functions ( $V_{th}$  and  $\rho$  satisfy normal distribution;  $L_s$  is based on the lognormal distribution of CNT length). We considered 200 samples in order to obtain a general variability of the output characteristics. Results are shown in Figure 3.13 (a)~(c). We observed that  $I_{d(sat)}$  of more than 90% of samples fall into the variation range of  $(-4.5 \times 10^{-7}, -1 \times 10^{-7})$ ,  $(-4 \times 10^{-7}, -0.5 \times 10^{-7})$ , and  $(-2.5 \times 10^{-7}, -0.4 \times 10^{-7})$  for  $5\mu m$ ,  $10\mu m$ , and  $50\mu m$  series respectively, compared with the experimental data in Figure 3.5 (after removal of the curves with the M-CNT effect). Variation range comparison analyzed in section III is illustrated in Figure 3.14. It can be concluded that more than 90% of the variation range of simulation data overlap

with the experimental data for each series. Therefore, the method applied here for variability analysis is reliable. It is an important tool to capture the overall variability of CNT-TFTs, which can be further used in the design of relevant microelectronics.

### **3.5 Closure**

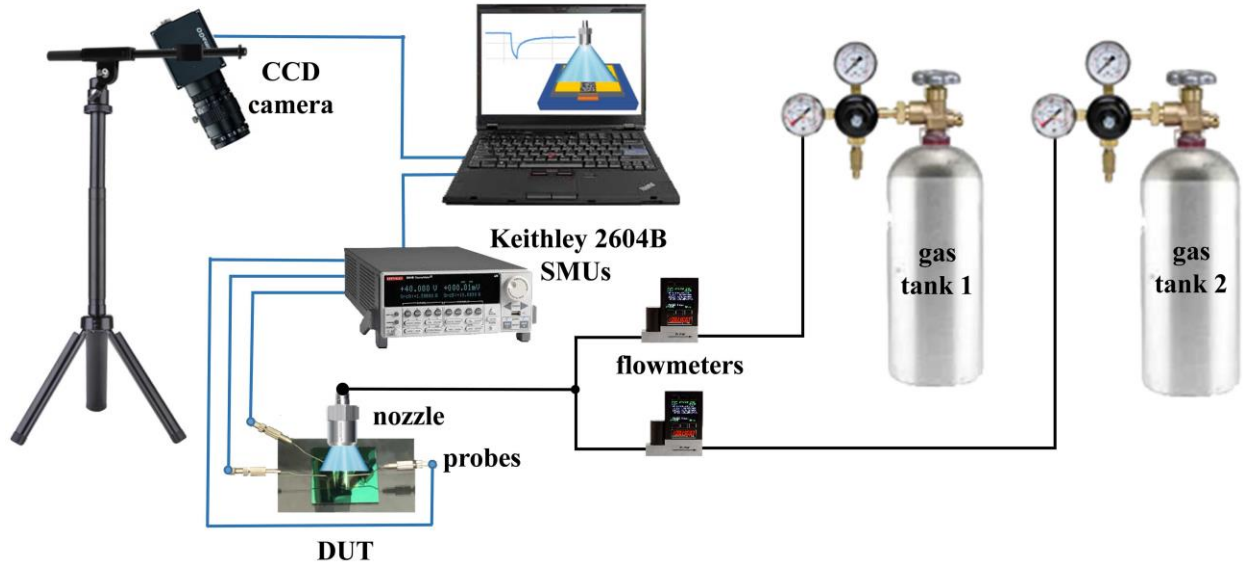
We fabricated array of CNT-TFTs of different channel lengths and analyzed variability in the output characteristics through a combination of experimental and computational methods. We obtained distribution functions for different sources of variation such as  $V_{th}$ , CNT network density and CNT mean length. The variability in I-V characteristics resulting from each source were analyzed individually and combined. The M-CNT is found to be a major source contributing to variability in I-V characteristics for short channel TFTs.  $V_{th}$  is the major source of variation for long channel TFTs. The effect of variation in the CNT mean length can be ignored unless CNT network density is very low and channel is short. A better consistency in performance can be reached for TFTs with larger channel area, which ensure smaller variations in the CNT network density and the CNT mean length. More importantly, the variability of I-V characteristics for CNT-TFTs can be reconstructed from the distribution functions of the relevant parameters, which will be helpful for the reliability analysis and testing of CNT-TFT based devices and circuits.

## CHAPTER 4. CNT-TFTS AS GAS SENSORS

In this chapter, CNT-TFTs as gas sensors were fabricated using randomly distributed CNT network as described in Chapter 3. Sensor response from  $\text{NH}_3$  and  $\text{NO}_2$  spray at 2ppm-40ppm were measured in air at room temperature. A convolution based model was developed and demonstrated to be a perfect match to the response curves. For a given CNT-TFT, the time constants of double exponential function were found to be independent of gas concentration while vary with respect to different gas types. More importantly, this uniqueness in time constants can be considered as its inherent identity with respect to different sensing gases, which can be used for gas identity verification. The verification process is proved to be very reliable when using single TFT, which is ultimately rooted in the randomness of CNT network. The verification can be applied to other gases such as  $\text{H}_2$  and its accuracy can be further guaranteed when using multiple TFTs in parallel.

### 4.1 Experiment Setup and Sensing Characteristics

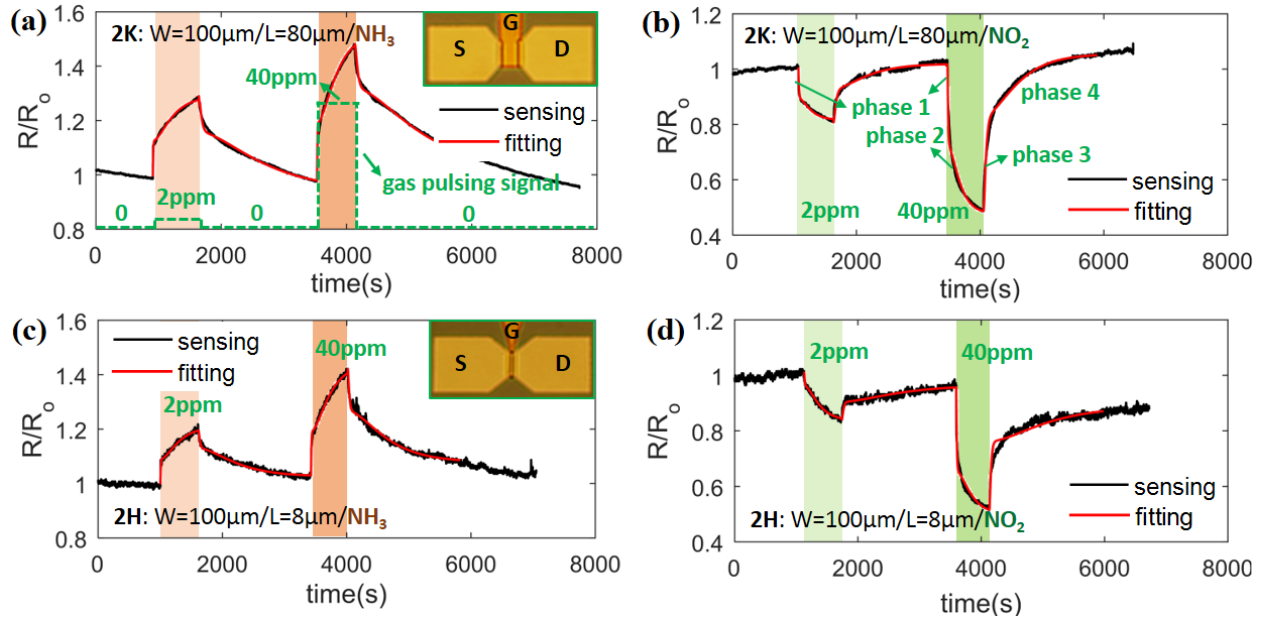
The experiment setup for CNT-TFT based gas sensing measurement is depicted in Figure 4.1. Gas spray was applied directly to the channel area of a TFT with Keithley 2604B source measurement units (SMUs) recording the current change over time. The nozzle, with inner diameter of 5mm, was large enough to generate stable gas flow to cover the entire surface of target TFT ( $0.25\text{mm} \times 0.75\text{mm}$ ). Only one TFT was tested each time. The applied gas was nitrogen ( $\text{N}_2$ , gas tank 1) mixed with either  $\text{NH}_3$  (gas tank 2) or  $\text{NO}_2$  (gas tank 2) at different ppm concentrate level (2ppm, 10ppm, 20ppm, 40ppm) controlled by ALICAT flowmeters. The CCD camera helped probe the target TFT before sensing. The whole setup was located inside fume hood under atmosphere pressure and stable room temperature.



**Figure 4.1 Schematic diagram of the experiment setup for gas sensing**

During measurement, the target TFT was biased with  $V_{ds} = -0.5V$  and  $V_{gs} = -1V$ . We first apply this bias to the TFT for more than 20 minutes in order to stabilize the drain current ( $I_d$ ). Then, we open the valves to release the gas mixture (either  $N_2 + NH_3$  or  $N_2 + NO_2$ ) while keep the mass flowrate constant at 1000 sccm all the time. After 10 minutes of gas spray (gas on state), we close the valves (gas off state) and keep the gas off state for 20~30 minutes before another sensing cycle began at a higher ppm level. The lowest concentrate we used was 2ppm for both  $NH_3$  and  $NO_2$  sensing, which is higher enough to get rid of the possible noise effect since the CNT-TFTs might also detect interfering gases (such as  $NH_3$ ,  $NO_2$ ,  $H_2$ , etc.) at ppb level from the environment.





**Figure 4.2** 2-cycle (2ppm and 40ppm) sensor response under  $\text{NH}_3$  or  $\text{NO}_2$  spray for a long channel TFT (2K:  $W=100\mu\text{m}/L=80\mu\text{m}$ ) and a short-channel TFT (2H:  $W=100\mu\text{m}/L=8\mu\text{m}$ ).  $R_0$  is the stable device resistance before gas spray. (a)-(b) Sensor response of 2K under  $\text{NH}_3$  or  $\text{NO}_2$  spray respectively. (c)-(d) Sensor response of 2H under  $\text{NH}_3$  or  $\text{NO}_2$  spray respectively. Inset figures are the corresponding TFTs. Red curves are the fitting results using common time constants of double exponential-convolution model.

## 4.2 Sample Characteristics and the Sensing Mechanism

The sensor response under 2-cycle (2ppm and 40ppm) of  $\text{NH}_3$  or  $\text{NO}_2$  pulsing is shown in Figure 4.2 for a long-channel CNT-TFT with  $L=80\mu\text{m}/W=100\mu\text{m}$  (2K) and a short-channel CNT-TFT with  $L=8\mu\text{m}/W=100\mu\text{m}$  (2H). They all show stable sensor response to either  $\text{NH}_3$  or  $\text{NO}_2$  sensing. For each gas sensing process, the gas pulsing signal stayed for 10 minutes in ‘on state’ (shown as orange stripes for  $\text{NH}_3$  or green stripes for  $\text{NO}_2$  in figures) and 30 minutes in ‘off state’ (no stripe in figures) between each cycle. When  $\text{NH}_3$  molecules interact with the CNT network in the channel area, they work as electron source which decreases the current by consuming the holes in the channel of the p-type CNT-TFT. Thus, the resistance will increase during on state and

decrease during off state.  $\text{NO}_2$  affects the resistance in an opposite way by providing more holes to the channel. For 2ppm concentration, both TFTs have more than 20% increase or decrease in resistance when exposed to  $\text{NH}_3$  and  $\text{NO}_2$ . While for 40ppm concentration, both TFTs show more than 50% resistance decrease under  $\text{NO}_2$  spray and more than 40% resistance increase under  $\text{NH}_3$  spray.

From the sensor response curves, it is easy to find 4 phases within each gas spray cycle, described in Figure 4.2(b) in bold green, which is vital to understand the sensing mechanism for CNT-TFT based sensors. We define the interactive units between gas molecules and the device as dwelling spots, which largely exist in CNT-CNT junctions, CNT-metal area, and other locations such as defects on CNTs. A dwelling spot can either capture or release a gas molecule depending on it is taken already or not.

For a gas spray cycle, phase 1 is the beginning of gas on state, where the resistance experiences an abrupt change when large number of empty dwelling spots are being taken by the gas molecules. Phase 1 only lasts for several seconds when all gas molecules can unlimitedly take the empty spots, which counts for a significant proportion of the resistance change during the entire on state. Even though gas molecules can escape their dwelling spots all the time, it can be ignored compared to the amount of gas molecules that take the empty spots.

Phase 2 starts when a large number of the empty spots have already been taken. In this phase, endless gas molecules reach the channel surface continuously like phase 1, but only part of them can be taken by the dwelling spots because only some of them will reach unavailable spots, which slows down the rate of change in resistance compared to phase 1. Another cause is, more and more trapped molecules can escape their spots than phase 1. Even after saturation, the target TFT is in a

dynamic equilibrium with the escaping molecules cancelling out the molecules being taken by the dwelling spots.

Phase 3 begins when gas spray comes to an end and no molecule reaches the channel surface (gas off state). Conversely, there are a large number of gas molecules escaping their spots, resulting in the abrupt change in resistance which is similar to phase 1 but in an opposite manner. In phase 4, the change rate slows down because it is more difficult for the remaining trapped molecules to escape their spots. It is commonly known that the dwelling spots near CNT junctions and CNT-metal region are much easier to capture gas molecules (gas molecules are relatively stable and harder to escape in those spots) than CNT itself and other region of the channel. Therefore, the slowness in phase 4 mainly results from the difficulty of gas molecules escaping from CNT junctions and CNT-metal region, while the sudden change in resistance of phase 3 mainly attributes to the rapid escape of gas molecules from CNT itself and other similar unstable gas-dwelling spots.

### 4.3 Sensor Response Fitting

Enlightened by the two phases during gas on or gas off state, it is natural to resort to double exponential function for fitting purpose. There are two formats related to double exponential function

$$f_1(t) = a \cdot \exp(-t / \tau_a) + b \cdot \exp(-t / \tau_b) \quad (4.1)$$

$$f_2(t) = a \cdot t \cdot \exp(-t / \tau_a) + b \cdot t \cdot \exp(-t / \tau_b) \quad (4.2)$$

where  $\tau_a$  and  $\tau_b$  are time constants,  $t$  is time,  $a$  and  $b$  are constants. To distinguish these two formats, we define equation 4.1 as double exponential function, equation 4.2 as double t exponential function. The gas pulsing signal can be expressed as

$$g(t) = \begin{cases} h & \text{gas on} \\ 0 & \text{gas off} \end{cases} \quad (4.3)$$

where the constant  $h$  is the height of the pulse signal.

Rigoni et al. used convolution between double t exponential function and gas pulsing signal to fit the sensor response curves of a whole cycle using the same time constants [50]. However, we found convolution between double exponential function and gas pulsing signal is a better match for our sensor response curves. To be specific, let  $D(t)$  be the original sensor response data, e.g., the sensor response curves in Figure 4.2. To fit  $D(t)$  separately for gas on state and gas off state in each case, linear transformation was applied to move both gas on state and gas off state to the origin from the onset point, exhibited in Figure 4.3(a). Obviously linear actions will not change the time constants. Then we resorted to double exponential-convolution model to fit the sensor response curves separately. That is

$$D_{f1}(t) = f_1(t) \otimes g(t) \quad (4.4)$$

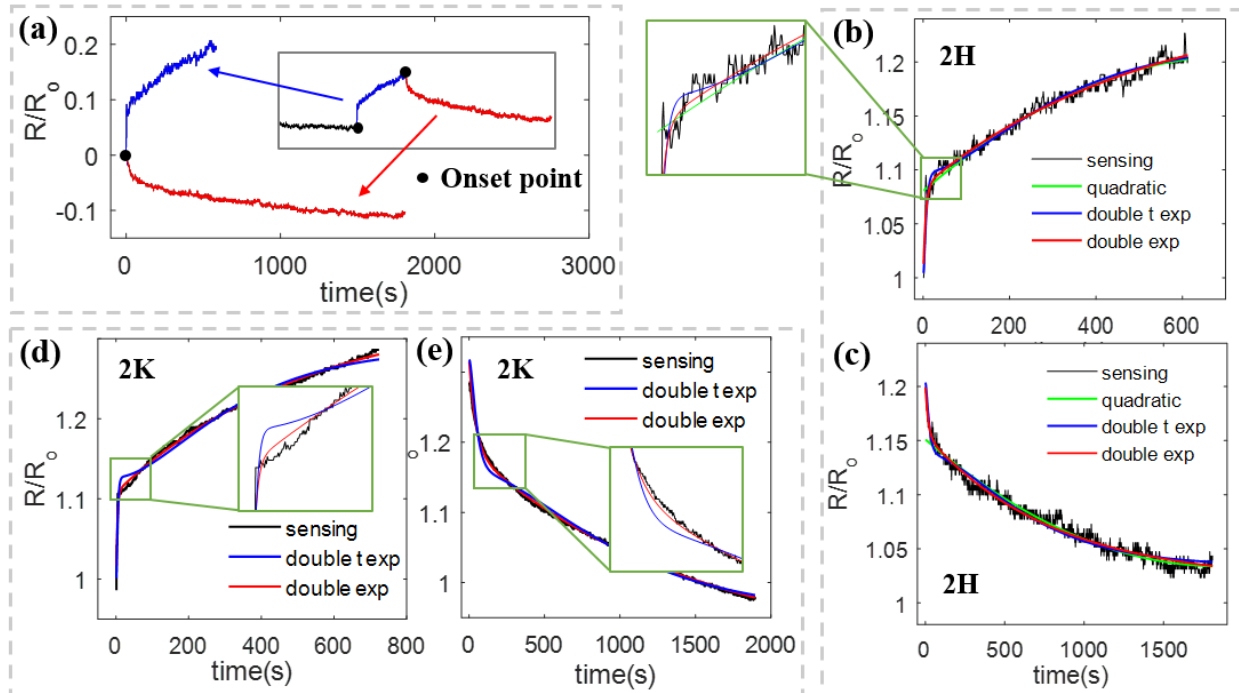
where  $D_{f1}(t)$  is the fitting results from convolution between double exponential function and gas pulsing signal. We consider  $a=1$  to eliminate a redundant variable during fitting. Then apply linear transformation for  $D_{f1}(t)$  in order to restore the real time fitting

$$D_f(t) = D_{f1}(t - t_o) + D(t_o) \quad (4.5)$$

Where  $D(t)$  is the original sensor response data,  $t_o$  is the time at the onset point. The standard deviation

$$v = \|D_f(t) - D(t)\| = \sqrt{\frac{1}{N} \sum_{i=1}^N (D_f(t_i) - D(t_i))^2} \quad (4.6)$$

is defined for error evaluation. Same process is applied for double t exponential-convolution model by using  $f2$  instead of  $f1$ .

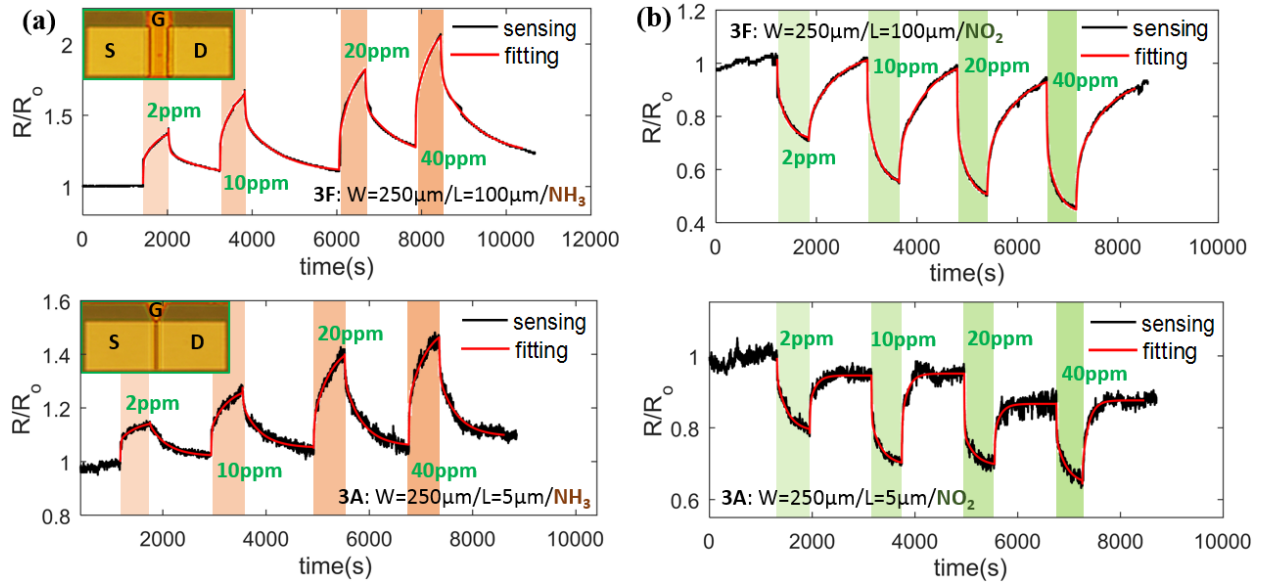


**Figure 4.3 Fitting for sensor response curves. (a) Linear transformation before fitting to standardize the fitting process for different sensing gas. (b)-(c) Fitting result comparison of device 2H in gas on and off state between double exponential-convolution (double exp) model, double t exponential-convolution (double t exp) model, and quadratic model. (d)-(e) Fitting result comparison of device 2K in gas on and off state between double exponential and double t exponential models.**

Device	State	$(\tau_a, \tau_b)$	$\nu$
2K	NH <sub>3</sub> on	(471, 5.0)	$3.22 \times 10^{-5}$
	NH <sub>3</sub> off	(1879, 38.6)	$1.88 \times 10^{-5}$
	NO <sub>2</sub> on	(227, 10.9)	$12.2 \times 10^{-5}$
	NO <sub>2</sub> off	(843, 51.0)	$6.37 \times 10^{-5}$
2H	NH <sub>3</sub> on	(514, 5.7)	$3.85 \times 10^{-5}$
	NH <sub>3</sub> off	(801, 17.3)	$4.85 \times 10^{-5}$
	NO <sub>2</sub> on	(328, 10.3)	$8.26 \times 10^{-5}$
	NO <sub>2</sub> off	(1723, 30.3)	$15.9 \times 10^{-5}$

**Table 4.1 Common time constants at different gas concentration in each state and the corresponding fitting errors**

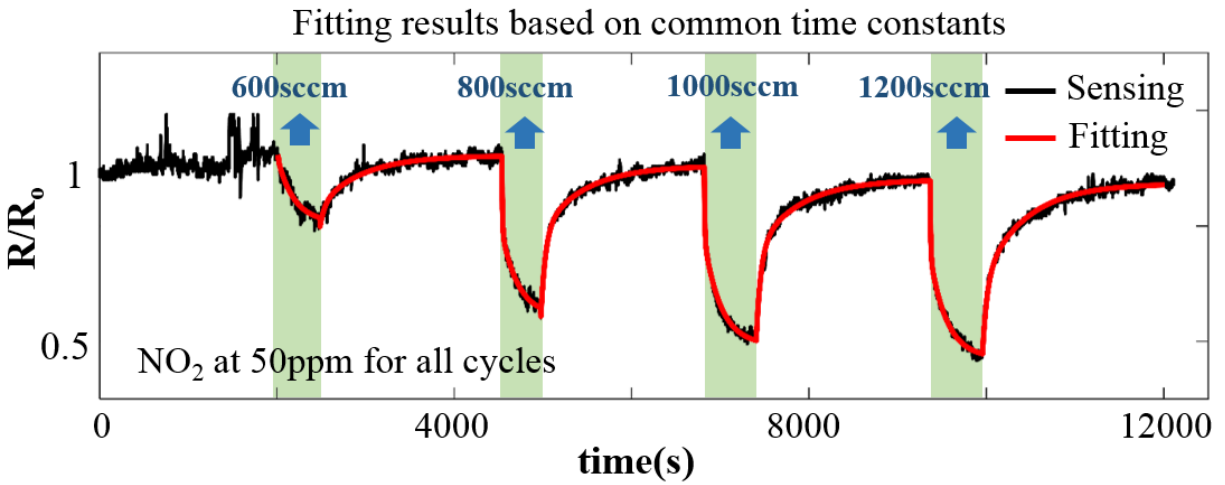
Figure 4.3(b)-(c) compares the fitting results of 2H between double exponential-convolution model, double t exponential-convolution model, and quadratic model. From the fitting curves, double exponential-convolution model matches the original sensor response data the best in both states. It is quite clear that the quadratic model is unable to depict the sudden change at the beginning of each state (phase 1 and phase 3). While for double t exponential-convolution model, the fitting is distorted during the transition period between each phase. Quantitatively, the standard deviations ( $\nu$ ) for double exponential-convolution model, double t exponential-convolution model, and quadratic model during gas on state are  $3.65 \times 10^{-5}$ ,  $4.24 \times 10^{-5}$ , and  $6.68 \times 10^{-5}$  respectively. And for gas off state, the corresponding standard deviations are  $3.15 \times 10^{-5}$ ,  $4.31 \times 10^{-5}$ , and  $4.55 \times 10^{-5}$ . Therefore, double exponential-convolution model can best fit the sensor response curves. Figure 4.3(d)-(e) further confirm the superior of double exponential-convolution model. Other fitting cases also support the same conclusion.



**Figure 4.4** 4-cycle (2ppm, 10ppm, 20ppm, 40ppm) sensor response and the corresponding fitting, using common time constants of double exponential-convolution model at different gas concentration. (a)-(b) Results for a long channel device 3F. (c)-(d) Results for a short channel device 3A.

#### 4.4 Consistency of Time Constants for Different Concentration

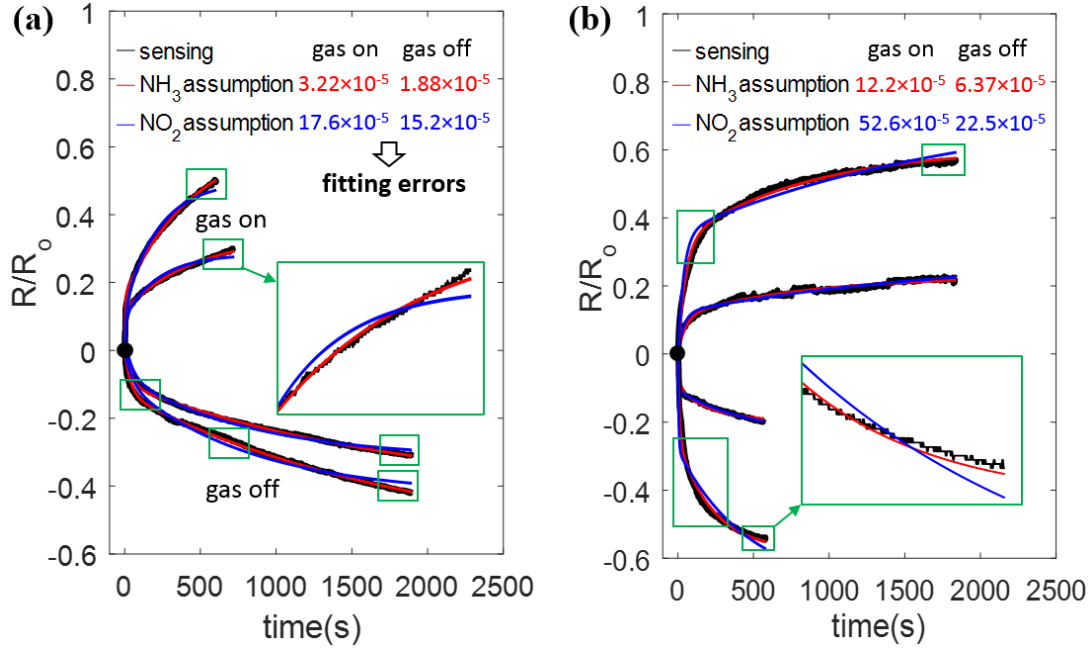
During sensor response fitting from double exponential-convolution model, we noticed the two time constants ( $\tau_a$  and  $\tau_b$ ) in equation 4.1 are quite stable for sensing at different gas concentrations. Based on that observation, we assumed the same  $\tau_a$  and  $\tau_b$  (common time constants) while fitting response of the same TFT during gas sensing at different concentrations. The fitting results are shown in Figure 4.2. The common time constants and the corresponding fitting errors are listed in Table 4.1. Surprisingly, the fitting are excellent for both  $\text{NH}_3$  and  $\text{NO}_2$  spray in either gas on state or gas off state. Figure 4.4 shows the fitting results for another TFT at 4 different gas concentrations, which are 2ppm, 10ppm, 20ppm, and 40ppm. The excellence in sensor response fitting from both Figure 4.2 and Figure 4.4 demonstrates the consistency of the common time constants with respect to different gas concentration.



**Figure 4.5 4-cycle sensor response under NO<sub>2</sub> spray and the corresponding fitting using common time constants of double exponential-convolution model with different flowrates (600sccm, 800sccm, 1000sccm, 1200sccm) but at the same concentration of 50ppm.**

Using the same fitting strategy based on common time constants, 4-cycle gas sensing of NO<sub>2</sub> spray were applied with different flowrates (600sccm, 800sccm, 1000sccm, and 1200sccm) but at the same concentration of 50ppm. This 4-cycle gas sensing is used to justify the impacts from nozzle pressure, which is a function of the flowrate. The sensor response and corresponding fitting results are plotted in Figure 4.5. It is easy to observe that the nozzle pressure has significant impact on sensitivity. That is, the resistance ( $R/R_0$ ) increases with increasing flowrate/pressure. The corresponding values of  $R/R_0$  are 0.83 (600sccm), 0.62 (800sccm), 0.55 (1000sccm), and 0.52 (1200sccm). However, the sensor responses can still be well described with low fitting errors by common time constants obtained from the double exponential-convolution model in this 4-cycle sensing test, which is similar in Figure 4.4. Therefore, the two time constants, which mainly depends on the device morphology (CNT network structure, CNT-metal contacts, etc.), are very stable under the change of nozzle pressure.





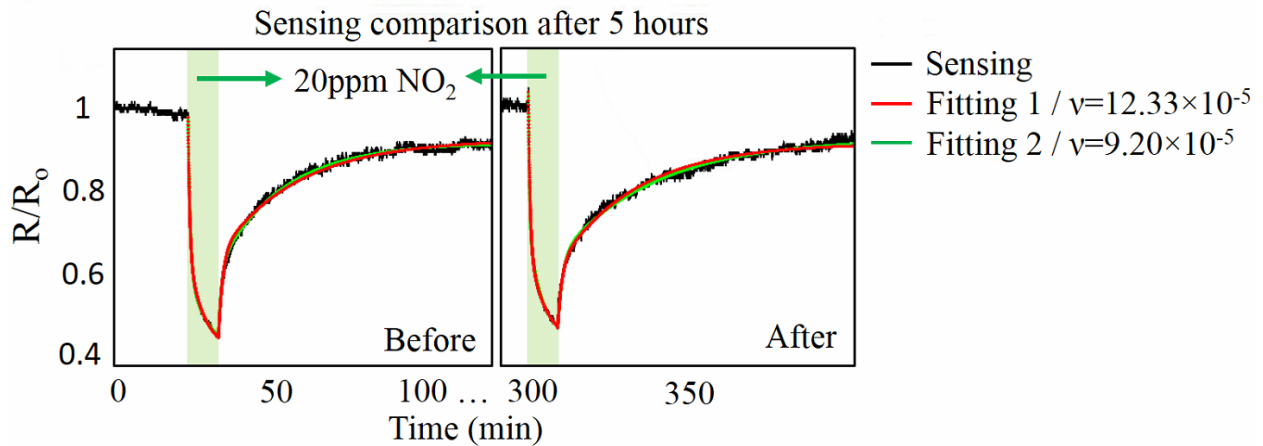
**Figure 4.6 Gas identification based on common time constant and the corresponding error difference. (a) Fitting results from different gas assumptions (time constant pairs) for device 2K in gas on state. (b) Same strategy as (a) for device 2K in gas off state.**

#### 4.5 Gas Identification

For a given CNT-TFT, the two time constants,  $(\tau_a, \tau_b)$  pair, are unique for either gas on state or gas off state and do not depend on the gas concentration. More importantly,  $(\tau_a, \tau_b)$  pair changes with respect to different gas types. Therefore, the one-to-one mapping between time constants and gas types can be regarded as the inherent properties for a given TFT, which can be used for gas identity verification depend on the corresponding error difference.

Take the device 2K in Figure 4.2(a) as an example,  $(\tau_a, \tau_b)$  pair for different gas sensing in different states can be determined easily from tentative testing for calibration purpose, shown in Table 4.1. For an unknown sensing gas (e.g., either NH<sub>3</sub> or NO<sub>2</sub>), let 2K record the sensor response for a cycle. Based on  $(\tau_a, \tau_b)$  pairs from different assumptions, the corresponding fitting errors can

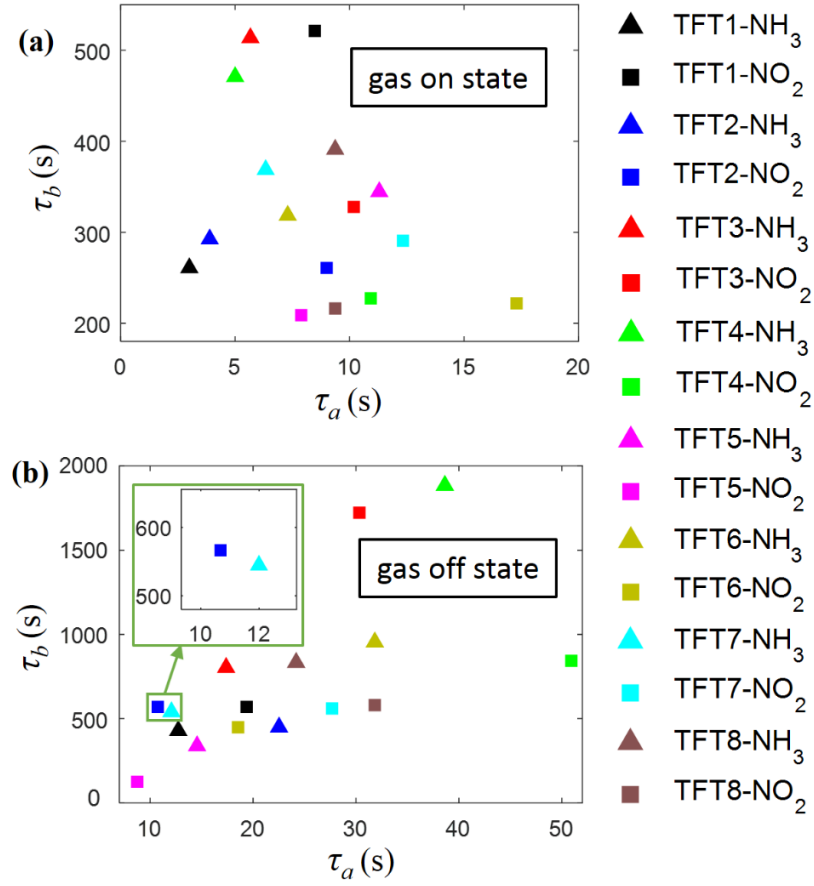
be obtained, shown in Figure 4.6. It is clear that  $(\tau_a, \tau_b)=(471, 5.0)$  from  $\text{NH}_3$  assumption can perfectly fit the sensor response curve while the fitting is distorted when  $(\tau_a, \tau_b)=(227, 10.9)$  from  $\text{NO}_2$  assumption. Quantitatively, the fitting error is  $\nu=3.22\times 10^{-5}$  when  $(\tau_a, \tau_b)=(471, 5.0)$  during gas on state, while  $\nu=17.57\times 10^{-5}$  when  $(\tau_a, \tau_b)=(227, 10.9)$ . That means the fitting error from  $\text{NO}_2$  assumption is more than 5 times larger than  $\text{NH}_3$  assumption. Therefore, we can safely conclude the unknown gas is  $\text{NH}_3$ , not  $\text{NO}_2$ . Same conclusion can be drawn from the corresponding error difference during gas off state, shown in Figure 4.6. Without any doubt, this is actually a general strategy that can be easily applied for identity verification for more gases. Moreover, this gas identification strategy is proved to be valid for gas sensing with different flowrates (different nozzle pressure), which is confirmed by conducting sensing test with different flowrates ranging from 600sccm to 1200sccm.



**Figure 4.7** The cycling sensing experiment and comparison of the corresponding sensor responses under  $\text{NO}_2$  spray at the same concentration (20ppm) for the same device at 5 hours' time period. Fitting 1 is based on common time constants and fitting 2 is based on separate time constants.

The cycling experiment has been conducted under NO<sub>2</sub> spray at the same concentration considering possible external influence (e.g., humidity, temperature fluctuation, other possible sensing noise) during sensing test at different time. The corresponding sensor responses are plotted in Figure 4.7 at 5 hours' time difference. During this period, the target sensor is put in air in order to ensure the full interaction with surrounding environment for enough time. Fitting 1 is based on common time constants and fitting 2 is based on separate time constants (performed separately for each cycle, which is the best fitting from the convolution model). As shown in Figure 4.7, the overall errors from fitting 2 are  $2.26 \times 10^{-5}$  and  $6.94 \times 10^{-5}$  in gas on and gas off state respectively. As for fitting 1, those values are  $3.11 \times 10^{-5}$  and  $9.22 \times 10^{-5}$ , which means the changes are only 138% and 132% between fitting 1 and fitting 2. However, the error difference between different gas assumptions (NH<sub>3</sub> and NO<sub>2</sub>) is as large as 10 times (1000%) for gas identification. Therefore, the external influence is very limited, which will not affect the accuracy of gas identification.

Theoretically, this identification process can be conducted through only one state from a single sensing cycle because of the uniqueness of  $(\tau_a, \tau_b)$  pair. Figure 4.8 maps the  $(\tau_a, \tau_b)$  pairs for more TFTs under NH<sub>3</sub> and NO<sub>2</sub> spray. The scattered marks reveal the uniqueness of  $(\tau_a, \tau_b)$  pair with respect to different gas types for different TFTs. On the one hand, for a given TFT, there is no overlapped or even close  $(\tau_a, \tau_b)$  pairs with respect to different gases. On the other hand, for a given sensing gas, there is no overlapped or even close  $(\tau_a, \tau_b)$  pairs with respect to different TFTs either. This uniqueness mainly roots in the randomness of CNT network inside the channel area, which is different with respect to CNT network density, CNT network structure, and channel dimensions, etc.



**Figure 4.8 One-to-one mapping for time constant pairs ( $\tau_a, \tau_b$ ) in gas on state (a) and gas off state (b). The same marks denote the same gas type, and the same colors represent the same device.**

However, in practice, some ( $\tau_a, \tau_b$ ) pairs might be very close to each other and cause interference when considering sensing cases for more possible gases. Many causes contribute to this such as ambience noise, unstable gas spray, experimental errors, etc. To address this problem, more tentative testing for a better calibration is vital in order to obtain the authentic time constant pairs for each gas sensing case. Similarly, performing multiple sensing cycles are also crucial during identity verification process. More efficiently, different TFTs can be used in parallel for gas identification instead of using just one, which helps avoid the possibility that the difference in fitting errors might be on the same level. Generally, the smoother sensor response from longer

channel TFTs are more reliable for gas identification because of the larger difference in fitting errors. From most cases we experienced, one TFT is enough for the verification process.

#### **4.6 Closure**

CNT-TFT based gas sensors have been fabricated with randomly distributed CNT network and sensor response under  $\text{NH}_3$  and  $\text{NO}_2$  spray at low ppm level have been tested. The different phases for gas response within each cycle suggest the sensing mechanism is based on the interaction between gas molecules and different types of dwelling spots inside the device. We developed double exponential-convolution model to fit the sensor response. The two time constants of double exponential function are found to be independent of gas concentration, but vary with respect to different gas types and different TFTs. This can be used for gas identification because of the uniqueness of the time constants for different gas types. We ascribe this uniqueness to the randomness of CNT network in channel area, which help build a unique channel structure for each TFT and thus create the diversity in dwelling spots for gas molecules during sensing process. By comparing the large difference in fitting errors, this one-to-one dependence between time constants and the sensing gases is successfully used for gas identity verification between  $\text{NH}_3$  and  $\text{NO}_2$ . More significantly, it actually provides a general and practical strategy for identity verification over more gases without distinction. In perspective, this analysis manages to create the selectivity of SWCNT based sensors with respect to different gases, which will largely broaden their applications in practice.

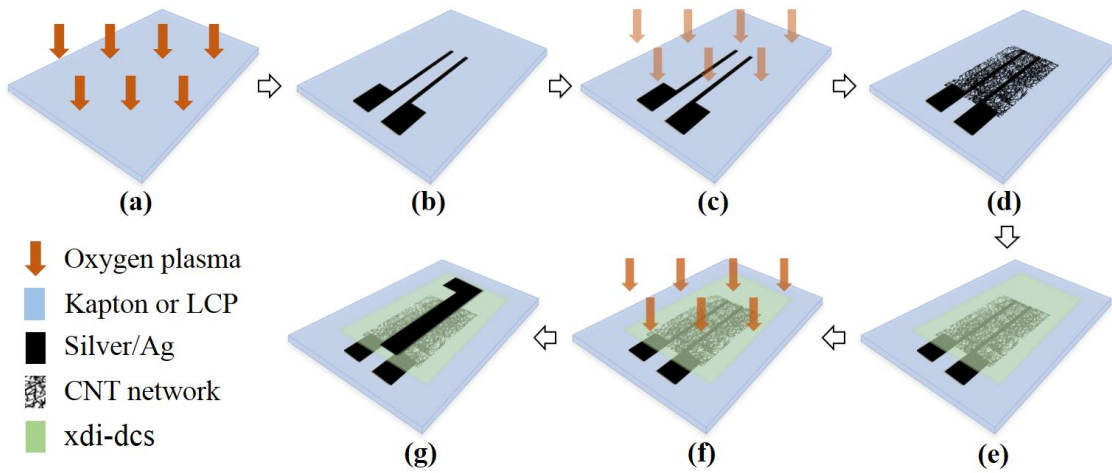
## CHAPTER 5. FULLY PRINTED CNT-TFTS

In this chapter, fully printed CNT-TFTs were fabricated on both Kapton and liquid crystal polymer (LCP) substrates utilizing only AJP technique. The performance was highly improved by optimization of xdi-dcs layer for the first time. During fabrication, CNT network was printed as channel material of TFTs using toluene based >99% highly purified semiconducting single-walled CNT ink. Highly uniform CNT network film was achieved by performing a multiple layer by layer deposition method, which largely decreases the CNT bundling effect and provides an effective way for density control. The printing of xdi-dcs thin film as gate dielectric was realized by diluting and optimizing with natural  $\geq 99.5\%$  butyl alcohol in appropriate %, and applying plasma treatment for better surface wetting. The fabricated CNT-TFTs shown very stable performance with on/off current ratio as high as  $\sim 10^6$ , mobility around  $5 \text{ cm}^2\text{V}^{-1}\text{s}^{-1}$ , negligible hysteresis, and good uniformity. More importantly, these TFTs can be operated under gate voltages as small as  $\pm 5\text{V}$ . This improvement is key for the applications of printed microelectronics and CNT-TFTs based circuits on flexible substrates because of the lower voltage operation and power dissipation.

### 5.1 Fabrication

The fully printed CNT-TFTs were fabricated based on a single printing system, the aerosol jet 200 system (AJ200). AJ200 is capable of printing fine-feature electronic, structural, and biological patterns, which can be used for noncontact and conformal printing onto almost any surface[59]. It begins with atomization of liquid ink, producing droplets ranging  $1\sim 5\mu\text{m}$  in diameter. The atomized droplets are delivered to the print head with an annular flow of clean  $\text{N}_2$  gas wrapped around in order to focus the droplets into a tightly collimated beam of material. Then this printable stream exits a converging nozzle at controllable flow rate and it can be deposited

onto the target surface with relatively high velocity. The printed features can reach small width around 10 $\mu$ m and thickness of submicron level, which are also determined by the ink properties and surface conditions. The whole printing process needs no vacuum or pressure chambers and it can operate under room temperature. Generally, no substrate damage will occur despite the high velocity of the stream.



**Figure 5.1** Schematic of fabrication process of fully printed CNT-TFTs on flexible substrates using AJP. (a) A well prepared flexible substrate (either Kapton or LCP) which is cleaned by 3-5min oxygen plasma before printing. (b) Ag printing as S/D electrodes. (c) 1min oxygen plasma before CNT printing for better wetting. (d) CNT network printing using a multiple layer by layer printing method. (e) Dielectric layer/xdi-dcs printing. (f) 2-3min oxygen plasma treatment before Ag printing. (g) Ag printing as a top gate electrode. A fully printed CNT-TFT is fabricated by this process. Note: Ag is cured at 150°C for 15~25min. Dielectric layer/xdi-dcs is cured at 140°C for 20min.

### 5.1.1 Fabrication Process

The fabrication process of the fully printed CNT-TFTs using AJP technique is shown in Figure 5.1. During fabrication, Kapton (DuPont, USA) and LCP (Rogers, USA) films were used as the flexible substrates. They were rinsed by acetone, IPA, and DI water successively, then blown dry by N<sub>2</sub> gun. Next, 5min oxygen plasma was applied for better surface preparation. Followed by

Ag printing (Ag ink: UTD Ag Conductive Silver Nanoinks, UT Dot) as source and drain (S/D) electrodes using AJ200. Then Ag patterns are cured at 150°C for 15~25min in an oven. Before CNT printing (CNT ink: IsoSol-S100® Polymer-Wrapped Nanotubes, NanoIntegris), 30s quick oxygen plasma was applied to functionalize the surface which could help achieve uniformly distributed CNT network. A thorough cleaning of AJ200 would be indispensable when changing from Ag to CNT ink (2~3hours ultrasonic, then acetone, IPA, DI water, and toluene rinse successively). After CNT printing, toluene rinse was used to wash away the excess surfactant and polymers on the surface, followed by thermal annealing at 120°C for >1hour in the oven. After that, xdi-dcs thin layer was printed (with sheath gas flow rate of 40CCM and printing speed of 10mm/s for all as default setting) as gate dielectric (xdi-dcs ink: Xerox Research Center Canada), which was diluted and optimized with butyl alcohol (Sigma Aldrich), cured by thermal annealing at 140°C for 20min in the oven. Then 2-3min oxygen plasma was performed to make the surface of the xdi-dcs layer hydrophilic before Ag printing again as gate electrodes on top, followed by Ag cure at 150°C for 15~25min. Ultrasonic atomizer is good enough for the printing of all inks involved. The sheath gas flow rate (SG), ultrasonic atomizer flow rate (UA), and printing speed (PS) are chosen differently to control the printing quality with respect to different inks.

### *5.1.2 Fabrication Details*

#### Printing Ag Electrodes:

The Ag ink is based on silver nanoparticles with average size around 10 nm and dispersed in a liquid vehicle. Since they are surface stabilized, UTD's Ag inks are highly soluble in nonpolar organic solvents and stable under atmospheric conditions at room temperature. The ink is tuned



by using xylene as solvent for better printing quality. The prepared ink was printed on flexible substrate such as Kapton and LCP.

A 100 $\mu$ m diameter nozzle was used for Ag printing. SG, UA, and PS were set to 25CCM, 18CCM, 10mm/s respectively in most of the cases (PS=10mm/s was set as default value for all Ag, CNT, and xdi-dcs printing unless stated otherwise). SG and UA changes in the range of 15-30CCM and 15-25CCM accordingly for Ag printing, depending on the tuning degree by using xylene as solvent. SG and UA also affect the printing quality of Ag. Generally, the increase of SG will decrease the width and increase the height of each printed Ag line. Ag can be cured at 150°C for 30min or 180°C for 10min in ambient. One-layer printing is enough for all the Ag patterns of the CNT-TFTs. The thickness of printed Ag patterns changes between 0.6-1.5 $\mu$ m with average of  $\sim$ 0.8 $\mu$ m, measured by Tencor P15 profilometer.

The temperature of chilling water bath and the platen was maintained at 25 °C and 75 °C respectively (for the printing of Ag, CNT, and xdi-dcs). 3-5min oxygen plasma before Ag printing will be very helpful to clean the surface of the substrates and ensure better wetting during printing.

#### Printing CNT Network:

Highly purified (>99% semiconducting) single-walled CNT solution are used as printable inks for CNT network. The initial concentration of the solution is 0.05 mg/mL and was further diluted with toluene at volumetric ratio of 1:1 before printing.

A 150 $\mu$ m diameter nozzle was used for CNT printing with SG=40CCM, UA=40CCM, and PS=10mm/s in most of the cases. UA changes between 30-45CCM based on the dilute ratio as well as the stability of the AJP system (CNT and xdi-dcs printing is more sensitive than Ag

printing). After printing, the samples were rinsed with toluene to remove excess surfactant, followed by thermal annealing in air at 140 °C for an hour. For multiple layer by layer deposition of CNT network, the processes of CNT printing, toluene rinse, and thermal annealing were performed 2-4 times under same conditions for both network density control and better uniformity.

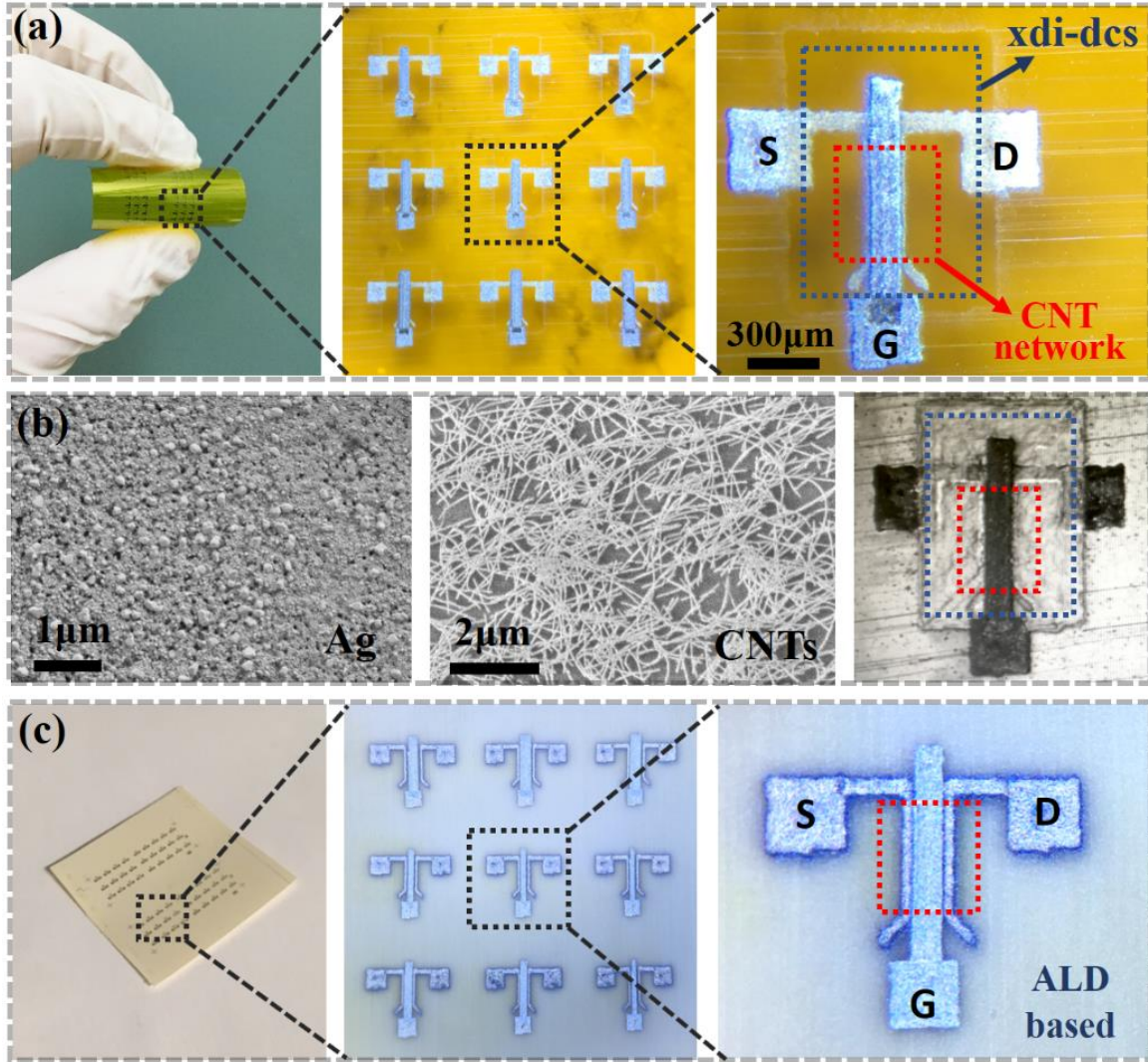
Before CNT printing, the system needs to be cleaned thoroughly by using 2 hours ultrasonic bath, followed by acetone, IPA, and DI water rinse successively. It can avoid contamination of CNT ink because it is very sensitive to the tube and assembly system. Again, 1min oxygen plasma will be helpful before CNT printing in order to reduce the bundling effect of CNTs. However, oxygen plasma can partially oxidize the previously printed Ag pattern, which will darken the overall color conspicuous. But result shows this oxidization only has limited influence on the conductivity of Ag patterns. No extra plasma should be applied during multiple layer by layer CNT network deposition because it can easily etch away CNTs.

#### Printing xdi-dcs:

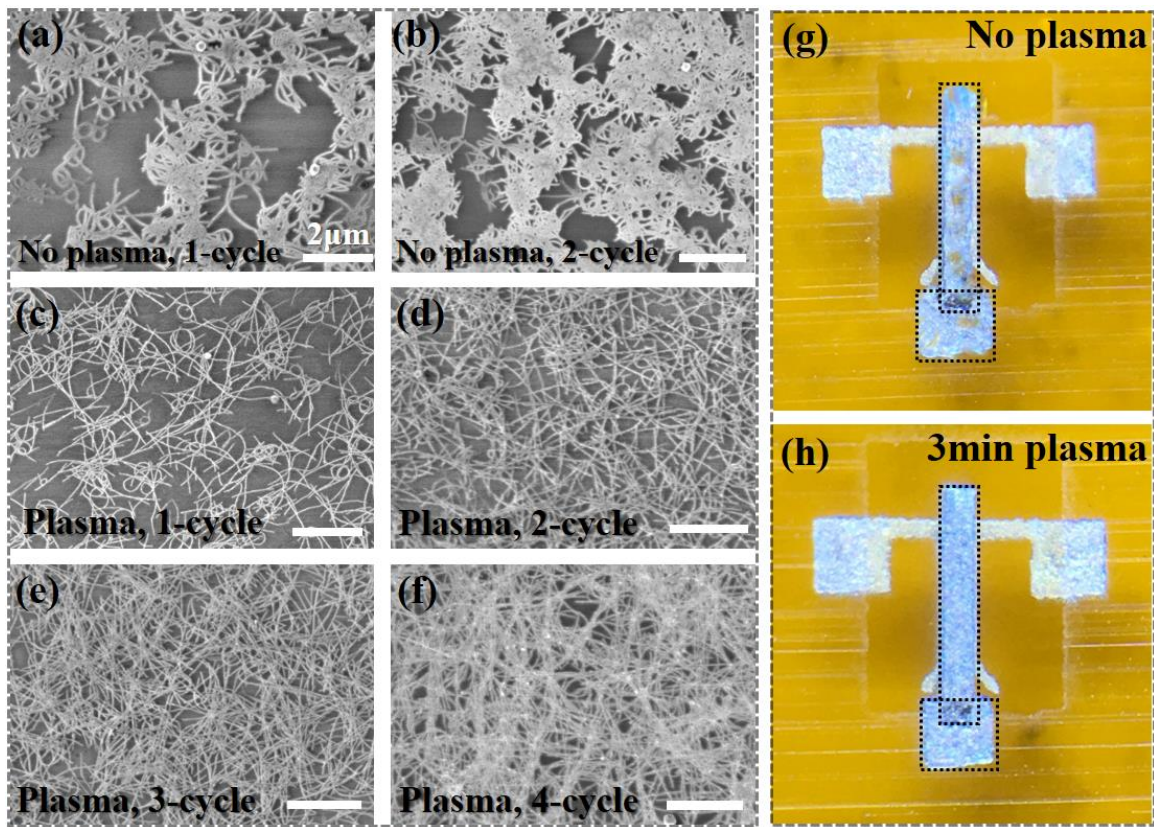
The original dielectric ink, xdi-dcs, is formed by mixing poly(vinylphenol) and poly(methyl silsesquioxane) in a ratio of 10:1. It is diluted and well optimized by using natural  $\geq 99.5\%$  butyl alcohol (Sigma Aldrich Inc.) to reach thinner printing for better quality with volumetric dilute ratio  $\sigma$  around 1:2.5 (xdi-dcs : butyl alcohol).

A 150 $\mu\text{m}$  diameter nozzle was used for xdi-dcs printing with SG=18CCM, UA=30CCM, PS=10mm/s in order to achieve thickness of  $\sim 0.3\mu\text{m}$ . The value of UA can be adjusted between 30CCM and 38CCM to control the thickness of xdi-dcs thin film ranging from 0.3-0.8 $\mu\text{m}$  accordingly. After printing, xdi-dcs is cured at 140 °C for 30min.

Again, the system needs to be cleaned thoroughly before xdi-dcs printing using the same way as for CNT printing. More importantly, 2min oxygen plasma is indispensable for the following Ag printing on top of the xdi-dcs layer. Without oxygen plasma, Ag cannot be printed continuous because of the hydrophobic property of as-printed xdi-dcs thin film.



**Figure 5.2 Features and morphology of printed CNT-TFTs. (a) Fully printed CNT-TFTs on Kapton substrate based on xdi-dcs layer. xdi-dcs layer is a transparent thin film under microscope where CNT network (denoted by red dash box) is almost invisible in the channel. (b) Morphology of Ag, CNT network, and a CNT-TFT using SEM. (c) Printed CNT-TFTs on LCP substrate based on ALD dielectric layer.**



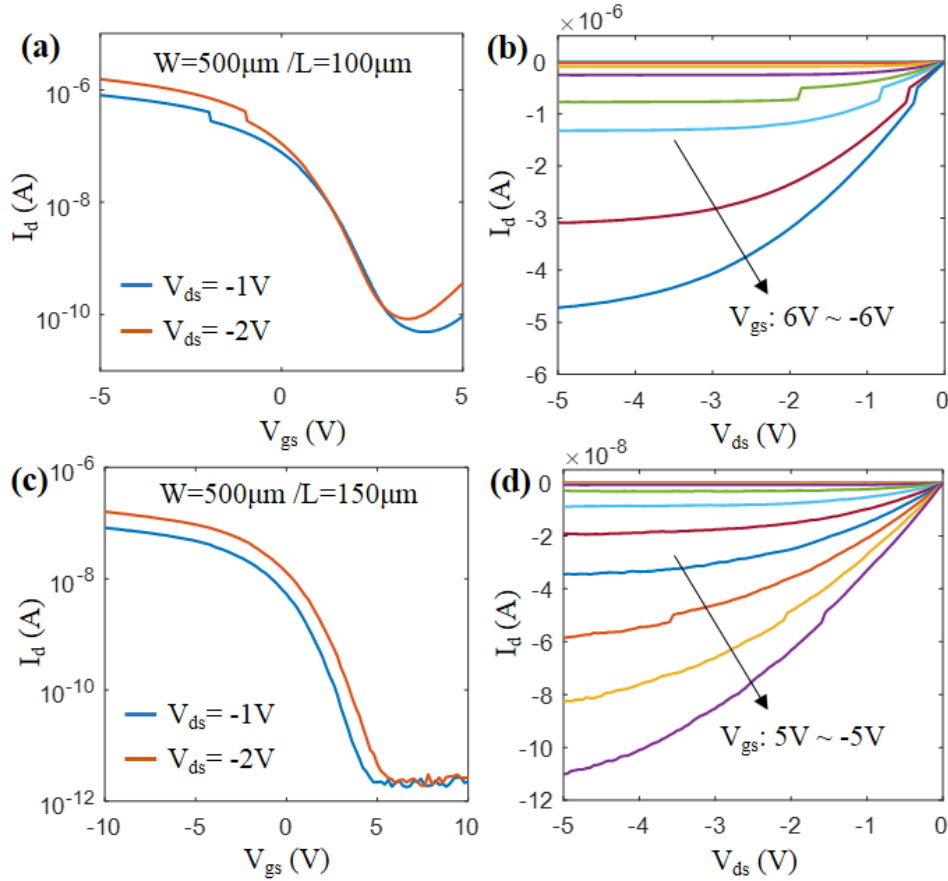
**Figure 5.3** The effects of oxygen plasma treatment before CNT network printing (a)-(f) and Ag printing on top of xdi-dcs thin film (g)-(h). Without plasma treatment, CNTs bundle together easily (a)-(b) and Ag thin film is uneven with huge pinholes everywhere (g). CNT network density can be well controlled by multiple layer by layer deposition after plasma treatment (c)-(f). Scale bar is 2 μm in each figure.

## 5.2 Morphologies and Performance

Figure 5.2 describes the structure and SEM images of the printed CNT-TFTs. Figure 5.2(a) displays fully printed CNT-TFTs using xdi-dcs as gate dielectric. For comparison, CNT-TFTs with ~80nm aluminum oxide ( $\text{Al}_2\text{O}_3$ ) layer as gate dielectric were fabricated using ALD at 100°C, replacing the xdi-dcs layer for new CNT-TFTs (ALD based CNT-TFTs), depicted in Figure 5.2(c) (the rest fabrication steps are the same). CNT network is printed on top of S/D electrodes, which is proved to have better contact than S/D on top of CNT network[61]. Top gate is used in the CNT-



TFTs to achieve lower hysteresis of the devices, where CNT network is not in direct contact with the environment. The morphology of the CNT-TFTs (as-printed Ag, CNT network, and xdi-dcs) on flexible substrates can be seen in Figure 5.2(b). CNT network is only visible by using SEM. Figure 5.2(b)-middle shows uniform CNT network resulting from multiple layer by layer deposition method. In order to acquire highly uniform CNT network, CNT printing, toluene rinsing, and blown dry processes (1 cycle altogether) are performed repeatedly for density control (normally 2-4 cycles).



**Figure 5.4 I-V characteristics of CNT-TFTs. Transfer curve (a) and output curve (b) of printed CNT-TFTs where gate dielectric were fabricated using ALD ( $\sim 80\text{nm}$   $\text{Al}_2\text{O}_3$ ,  $W=500\mu\text{m}$ ,  $L=100\mu\text{m}$ , 1-cycle CNT network deposition). Transfer curve (c) and output curve (d) of a fully printed CNT-TFTs based on printed dielectric layer with thickness as small as  $0.3\mu\text{m}$  ( $W=500\mu\text{m}$ ,  $L=100\mu\text{m}$ , 3-cycle CNT network deposition).**

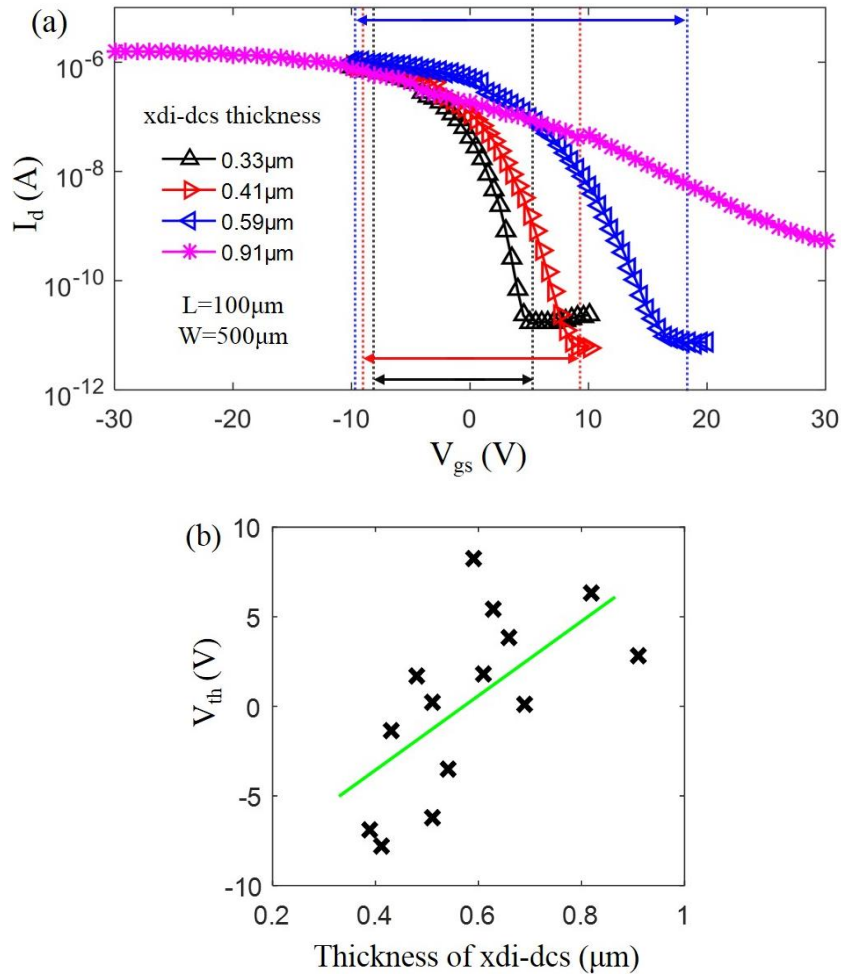
The significance of oxygen plasma treatment and multiple layer by layer deposition of CNT network can be seen in Figure 5.3. Without oxygen plasma treatment, CNTs bundle together easily as shown in Figure 5.3(a) and 5.3(b). And multiple layer by layer deposition cannot result in uniform CNT network because CNTs tend to entangle to the previously printed CNTs which makes the bundling effect even worse. Multiple layer by layer deposition works very well after 1min plasma treatment before printing as observed in Figure 5.3(c)-5.3(f), where CNT network density can be controlled by performing multiple cycles as needed. Similar effect can be expected for Ag printing on top of xdi-dcs thin film because of the hydrophobic property of the as-printed xdi-dcs layer, shown in Figure 5.3(g) and 5.3(h).

The I-V characteristics of the CNT-TFTs was measured using Microtech Summit 11 k probe station and Keithley 4200 SCS. We fabricated series of devices with the same channel width ( $W=500\mu\text{m}$ ), but different channel lengths ( $L=50\sim 250\mu\text{m}$ ). The output characteristics ( $I_d-V_{ds}$  curves) and transfer characteristics ( $I_d-V_{gs}$  curves) of the CNT-TFTs are plotted in Figure 5.4. Figure 5.4(a) and 5.4(b) are ALD based CNT-TFTs, Figure 5.4(c) and 5.4(d) are fully printed CNT-TFTs. The on/off ratio of the fully printed CNT-TFTs ranges from  $10^3$  to  $10^6$ , which increases with increasing channel length. The overall I-V characteristics shows good p-type performance with mobility ranging from 2 to  $8\text{ cm}^2\text{V}^{-1}\text{s}^{-1}$ .

### 5.3 Optimization of Printed xdi-dcs Thin Film

The performance of fully printed CNT-TFTs is mainly limited by the gate dielectric. The printing of xdi-dcs thin film is critical to obtain relatively high-performance CNT-TFTs. During AJP printing, the thickness of xdi-dcs can vary in large range based on the dilute ratio of xdi-dcs as well as the printing parameters such as SG, UA, and PS. The thinnest xdi-dcs film we achieved

for a CNT-TFT is  $\sim 0.3\mu\text{m}$  (SG=18CCM and PS=10mm/s as default setting unless stated otherwise, UA=30CCM in this case), and the thickest could be larger than  $1\mu\text{m}$  (measured by Tencor P15 profilometer). Figure 5.5 displays the difference in transfer characteristics caused by the thickness of xdi-dcs thin film. The difference in thickness is controlled by the values of UA, which are 30CCM, 32CCM, 36CCM, and 40CCM for  $0.33\mu\text{m}$ ,  $0.41\mu\text{m}$ ,  $0.59\mu\text{m}$ , and  $0.91\mu\text{m}$  respectively. Except for the values of UA, the fabrication process and other parameters/dimension are exactly same for the CNT-TFTs ( $W=500\mu\text{m}$ ,  $L=100\mu\text{m}$ , 2-cycle CNT network deposition).

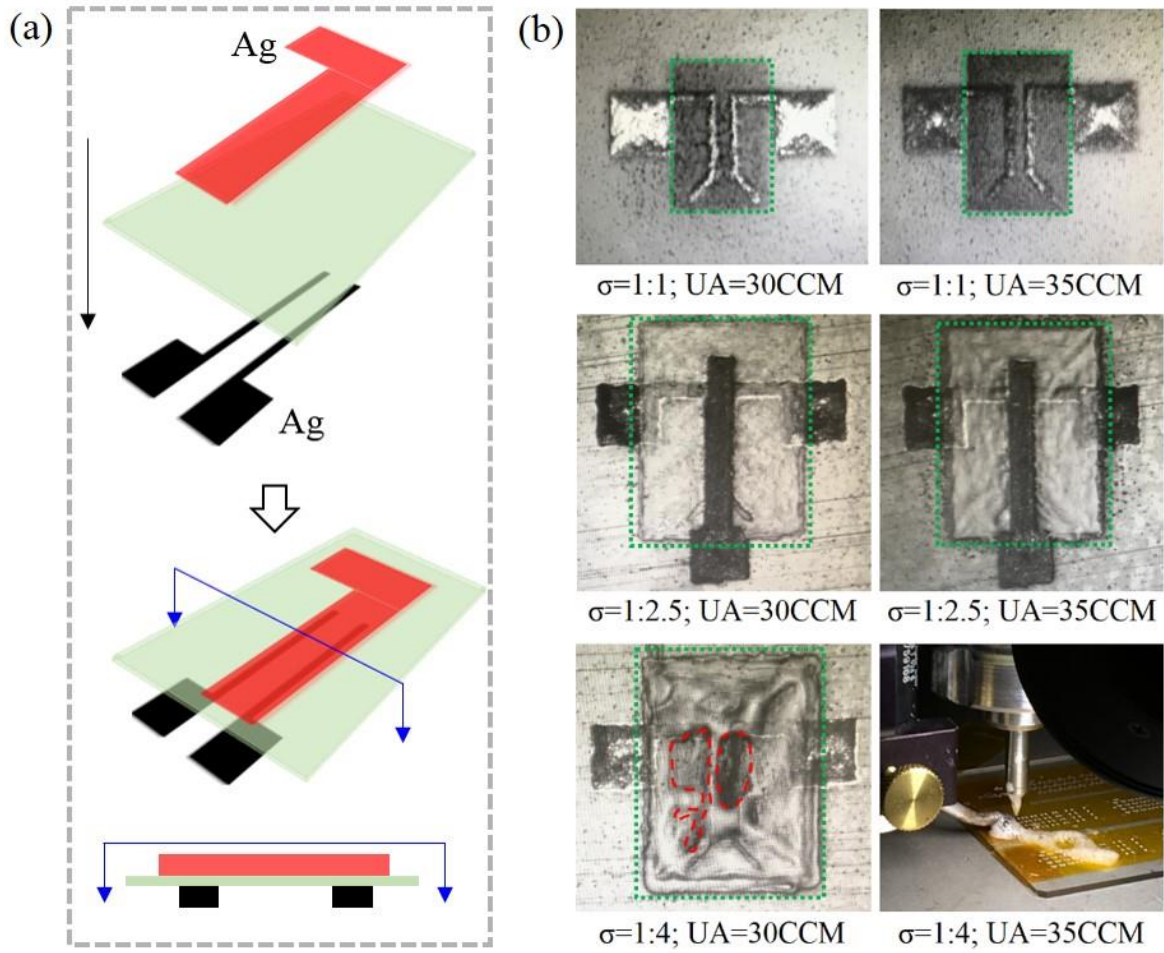


**Figure 5.5** The impact of the printed xdi-dcs layer on the performance of fully printed CNT-TFTs. (a) Comparison of transfer curves of four fully printed CNT-TFTs with different thickness of dielectric layers. (b) The dependence of  $V_{th}$  on the thickness of printed xdi-dcs thin films for fully printed CNT-TFTs.

Figure 5.5(a) compares the transfer curves of four fully printed CNT-TFTs with different thickness of dielectric layers. The thickness of printed xdi-dcs of the CNT-TFTs are 0.33 $\mu\text{m}$ , 0.41 $\mu\text{m}$ , 0.59 $\mu\text{m}$ , and 0.91 $\mu\text{m}$ . Obviously, the range of  $V_g$  needed to fully switch on and off the devices has direct dependence on the thickness of printed xdi-dcs layer. As observed from the figure, for the device with thickness of 0.33 $\mu\text{m}$ ,  $V_g$  has to be swept between -8V ~ 6V in order to reach on/off ratio of  $10^5$ . However,  $V_g$  has to be swept more than the range of -10V ~ 30V in order to switch on and off the device with thickness of 0.91 $\mu\text{m}$ . Clearly, the thicker of the printed dielectric layer, the larger  $V_g$  needed for the transistor to operate at its highest on/off ratio. Figure 5.5(b) plots the dependence between the thickness of printed xdi-dcs layer and  $V_{th}$  for a set of fully printed CNT-TFTs (each triangle denotes a different CNT-TFT). These CNT-TFTs were fabricated using the same process and parameters except that the PS value is different in order to control the thickness of the xdi-dcs layers. Generally, positive correlation can be seen from the plotting. That is, the thicker of printed dielectric layer, the transistor tend to have higher value of  $V_{th}$ . However, it is very difficult to obtain closer relationship between the thickness of printed xdi-dcs layer and  $V_{th}$  because  $V_{th}$  also depends much on other factors such as body effect, temperature, etc. (which is hard to control for state-of-art printed CNT-TFTs even though they are fabricated exactly the same way).

During fabrication, the xdi-dcs thin film with thickness less than 0.3 $\mu\text{m}$  can easily cause short between gate and S/D electrodes. But an overprinting can appear with ink spill outside the designed feature when the thickness is larger than 1 $\mu\text{m}$ , which should be avoided.





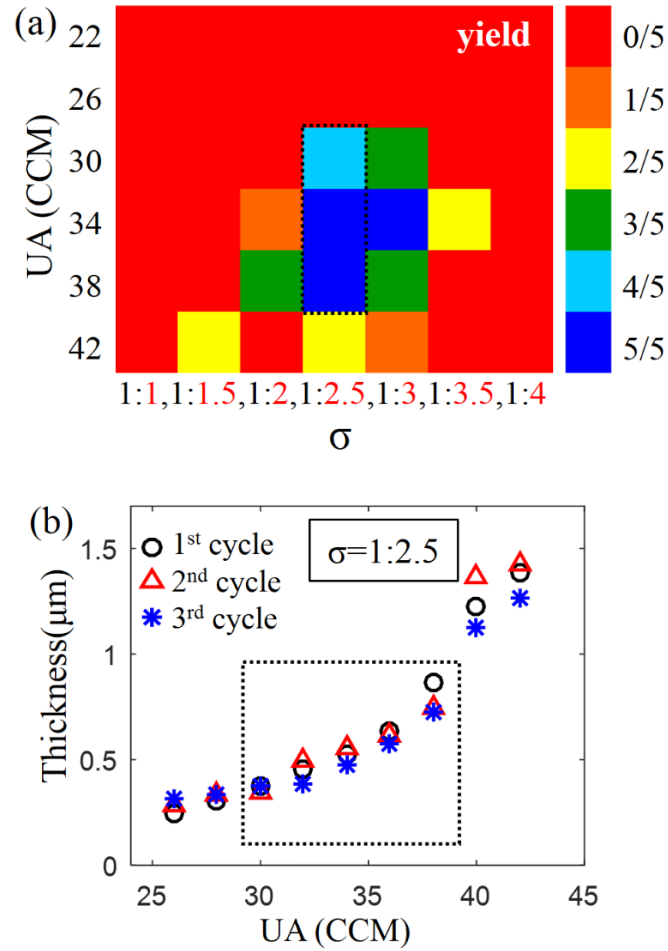
**Figure 5.6 (a) Schematic structure (layer by layer structure and the sectional view) used to test the insulation quality of printed xdi-dcs thin films. (b) Visualization of printed xdi-dcs thin film at different dilute ratio  $\sigma$  and UA. The devices in upper figures will not work as numerous pinholes created during xdi-dcs printing. The middle figures show well printed xdi-dcs thin films. The lower figures will not work either because of the over printing, which can result in several big pinholes (denoted by red dash area, left) and even ruin the substrate (right).**

Even though thin xdi-dcs layer is the key for fully printed CNT-TFTs, it can hardly go thinner than  $0.3\mu\text{m}$  because the existence of pinholes in an extremely thin film ( $<0.3\mu\text{m}$ ) can easily cause short circuit (pinhole effect, which fails to provide good insulation between gate and S/D electrodes).

Figure 5.6(a) illustrates the structure we used to test the insulation quality of printed xdi-dcs thin film, which is similar to the structure of fully printed CNT-TFTs. Undoubtedly, good insulation of printed dielectric is the precondition for fully printed CNT-TFTs. The measured capacitance of printed xdi-dcs thin film is 6-8 nF/cm<sup>2</sup> with thickness between 0.3-0.8μm. Generally, bad quality of xdi-dcs layer results from severe pinhole effect when current can flow directly from the red Ag electrode (gate) to the black Ag electrodes (S/D) of Figure 5.6(a).

To optimize the printing quality of xdi-dcs layer, natural  $\geq 99.5\%$  butyl alcohol is used to dilute the xdi-dcs ink with dilute ratio  $\sigma$  (defined as volumetric ratio of xdi-dcs : butyl alcohol) ranging from 1:1 to 1:4. Figure 5.6(b) shows the printed xdi-dcs layers at different  $\sigma$  and UA, which are the two most important parameters for printed xdi-dcs thin film. As shown in the figures, when  $\sigma$  is 1:1 or less dilution, no continuous thin layer can form. Instead, the printed features show particle-like morphology with numerous small pinholes. When  $\sigma$  is 1:4 (or further dilution), the morphology of printed features is severely uneven with several large pinholes (red dash area). Worse still, when UA is as large as 35CCM, over spill of the ink from the nozzle will ruin the substrate badly (over printing). Clearly, over printing of xdi-dcs can cause troubles too. In general, good morphology of printed features can be achieved with  $\sigma$  around 1:2.5, which results in very uniform and continuous xdi-dcs thin film and the thickness can be well controlled by changing UA accordingly.

Based on the structure displayed in Figure 5.6(a), 5 samples are fabricated for each combination of  $\sigma$  and UA, with  $\sigma$  varying from 1:1 to 1:4 and UA varying from 22CCM to 42CCM. The yield counts the number of samples without short between the red Ag electrode and the two black Ag electrodes while using printed xdi-dcs thin film.



**Figure 5.7 Optimization of printed xdi-dcs thin film. (a) Yield rate (number of samples with good insulation quality) under different  $\sigma$  and UA combinations. (b) Thickness dependence of xdi-dcs thin film on UA when  $\sigma$  equals to 1:2.5, which is the best  $\sigma$  from (a). The black dash box in (a) and (b) denotes UA range of 30-38CCM at best  $\sigma$ .**

The results can be seen in Figure 5.7(a). The samples with good insulation quality are 0/30, 2/30, 4/30, 16/30, 12/30, 2/30, 0/30 when  $\sigma$  equals to 1:1, 1:1.5, 1:2, 1:2.5, 1:3, 1:3.5, 1:4 respectively with UA changing from 22 to 42CCM for each  $\sigma$ . Similarly, those values are 0/30, 0/30, 7/30, 13/30, 11/30, 5/30 when UA equals to 22, 26, 30, 34, 38, 42CCM respectively with  $\sigma$  changing from 1:1 to 1:4 for each UA. Therefore,  $(\sigma, UA) = (1:2.5, 34)$ , would be one of the best

combinations for the printing of xdi-dcs thin film. Other combinations such as  $(\sigma, UA) = (1:2.5, 38)$  and  $(\sigma, UA) = (1:3, 34)$  are also very reliable in the test.

The value of  $\sigma$  is more important because it cannot be adjusted freely during printing, which should be determined before printing. Figure 5.7(b) plots the thickness dependence on UA of printed xdi-dcs thin film when  $\sigma$  is determined as 1:2.5 in advance. UA can be changed freely as needed during printing. To guarantee the stability of the ink mist of xdi-dcs, the printing is performed 2min after the changing of UA value. The time interval for each printing cycle (1<sup>st</sup> cycle, 2<sup>nd</sup> cycle, and 3<sup>rd</sup> cycle) is roughly 1 hour. Generally, the dependence in Figure 5.7(b) should be linear because of mass conservation. However, the printing becomes unstable when  $UA > 40\text{CCM}$  ( $\sigma=1:2.5$ ). Worse still, over printing can happen when UA is close to 50CCM, which is similar as depicted in Figure 5.6(b) when  $(\sigma, UA)=(1:4, 35)$ . The instability and over printing ( $UA > 40\text{CCM}$  at  $\sigma=1:2.5$ ) make the curve deviate from linear dependence, which should be avoided for better printing quality. Therefore, the data inside the black dash box of Figure 5.7(b) has more significance because of the high reliability and the high yield rate which can be seen from Figure 5.7(a). Collectively, the printing of xdi-dcs thin film can be well optimized to achieve thickness as thin as  $\sim 0.3\mu\text{m}$  by using AJP and the corresponding devices can be operated using gate voltages as small as  $\pm 5\text{V}$ . High printing quality of the dielectric layer is the key for fully printed CNT-TFTs with much lower power dissipation.

## 5.4 Closure

Using only AJP, fully printed CNT-TFTs have been fabricated on flexible substrates. The fabricated devices can be fully switched on and off by using  $V_g$  as small as  $\pm 5\text{V}$  to reach on/off ratio as high as  $\sim 10^6$ . During printing, multiple layer by layer deposition method is applied for

CNT network. The advantages lie in the density control as well as highly uniform CNT network structure. By diluting xdi-dcs with natural  $\geq 99.5\%$  butyl alcohol in appropriate volumetric ratio ( $\sigma=1:2.5$ ), printed dielectric thin film with thickness of  $\sim 0.3\mu\text{m}$  can be achieved with high yield rate for fully printed CNT-TFTs. The high quality of printed dielectric layer free of pinhole effect can be achieved by controlling the UA. The improvement in printed dielectric layer is crucial for flexible transistors with lower voltage operation and power dissipation, which paves the path for applications of CNT-FETs as building blocks in wearable and bendable devices such as flexible displays, RFID antennae/tags, sensors, artificial skins, etc.

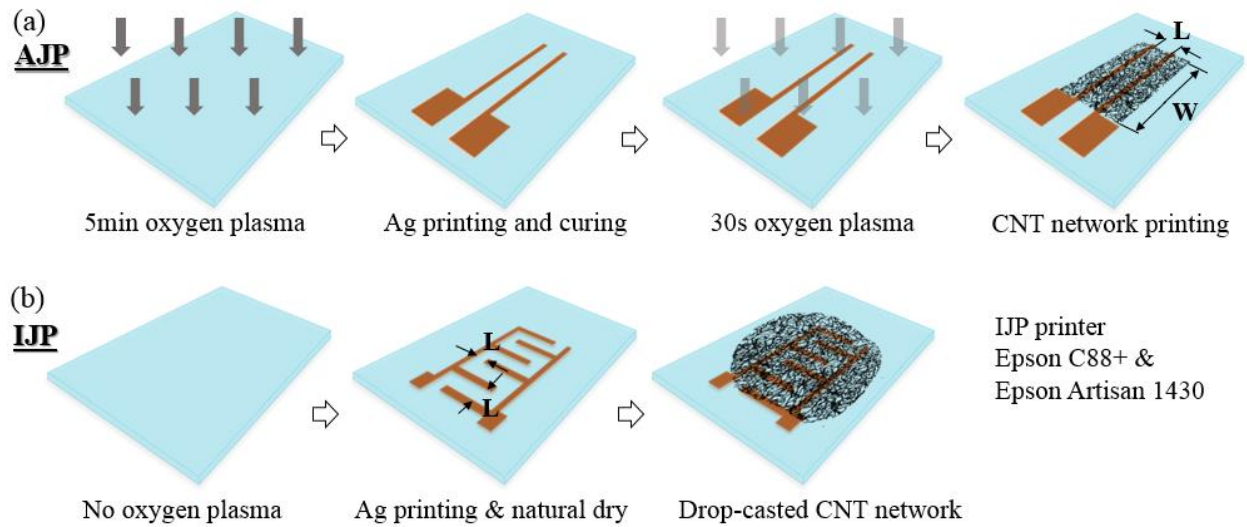
## CHAPTER 6. FULLY PRINTED GAS SENSORS

In this chapter, CNT gas sensors were fabricated using three different methods: photolithography (PL), aerosol jet printing (AJP), and low-cost inkjet printing (IJP) (Epson C88+ and Epson Artisan 1430) and compare their performance in context of sensitivity and variability. The latter two were fully printed sensors on flexible substrates (Kapton or PET). The sensor responses of all the CNT sensors (referred as PL sensors, AJP sensors, IJP sensors respectively) were obtained for the detection of reducing gas  $\text{NH}_3$  and oxidative gas  $\text{NO}_2$ . The measurement was conducted at low ppm level in air at room temperature. AJP sensors and IJP sensors showed high sensitivity and stability in performance, with no obvious disadvantages compared to PL sensors. During fabrication, both drop-cast and printed CNT network were patterned for the sensors, resulting in bundled CNT network and highly uniform CNT network, respectively. The sensitivity was surprisingly high for some printed CNT sensors with drop-cast CNT network. Moreover, the post drop-cast deposition could help improve the sensitivity by rebuilding the CNT network of low sensitivity sensors, which implies the potential of fabrication of extremely low-cost CNT gas sensors using IJP with drop-cast method.

### 6.1 Fabrication

Fully printed AJP sensors, using CNT networks as sensing element, were fabricated using Optomec Aerosol Jet 200 system (AJ200). The fabrication process is illustrated in Figure 6.1(a). A flexible substrate of Kapton (DuPont) was cleaned by acetone, IPA, and DI water, and then blown dry by nitrogen gun. After that, a surface treatment was performed using oxygen plasma, which ensured better wetting between Ag and the substrate. For printing Ag, 100 $\mu\text{m}$  size nozzle was utilized to pattern the electrodes with channel width (W) of 500 $\mu\text{m}$  and channel length (L) in

the range of 100~250 $\mu\text{m}$ . Ag was cured by thermal annealing at 150°C for ~20min in an oven. Next, 30s oxygen plasma was applied to functionalize the surface, followed by CNT printing using 150 $\mu\text{m}$  size nozzle. In order to acquire highly uniform CNT network, after each layer of CNT printing, toluene rinsing, and blown dry processes (1 cycle) were performed; this process is repeated for CNT density control (normally 2~4 cycles, the multiple layer by layer deposition method). At last, the entire device was put in the oven at 120°C for 30min.



**Figure 6.1** Fabrication steps of AJP sensors (a) and highly simplified fabrication steps of IJP sensors (b). For IJP, extremely low-cost daily-used printers (Epson C88+ or Artisan 1430) were utilized without any controllable stage.

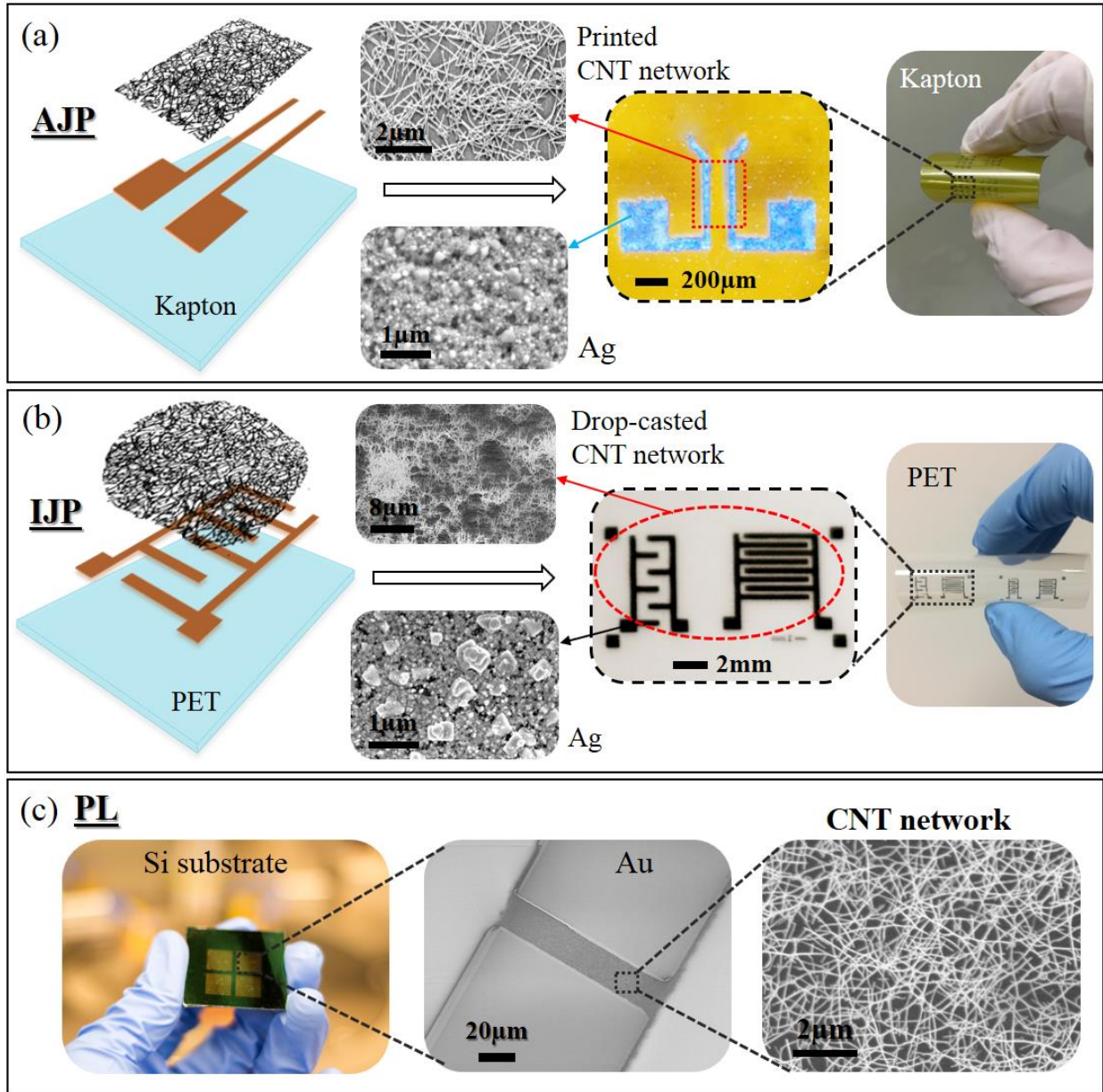
For fully printed IJP sensors, the process was highly simplified in order to demonstrate a very low-cost fabrication process. As shown in Figure 6.1(b), flexible mesoporous PET substrates were prepared the same way as for AJP. Then, Ag electrodes with  $L=500\sim1000\mu\text{m}$  and effective  $W > 10\text{mm}$  were printed using very low-cost printer Epson C88+ (\$108) or Artisan 1430 (~\$300) without oxygen plasma treatment. These printers have  $< 1\%$  price of frequently used Dimatix inkjet printer[127, 199, 200] and other inkjet printers for the printing of flexible devices. The Ag

features were almost instant dry in air after being printed onto the mesoporous substrates, which makes this a cure-free low-temperature process. Then, CNT network was deposited by drop-cast method. This IJP fabrication process used only basic materials (CNT, Ag, PET) and a very cheap Epson printer. No other equipment, chemicals or process was involved, which ensures the lowest cost of the CNT sensors that have ever been reported. For comparison, PL sensors were also fabricated. Gold (Au) electrodes with  $L=10\sim50\mu\text{m}$  and  $W=100\mu\text{m}$  were patterned on hard Si wafer using physical vapor deposition (PVD) since it can bear high temperature. Then 3 min oxygen plasma was applied before CNT deposition. Then, PL was used to pattern the CNT network in the channel, i.e., 30s oxygen plasma to etch away CNT network outside the channel. At last, thermal annealing was performed for the devices.

Details of fully printed flexible AJP sensors and IJP sensors are displayed in Figure 6.2(a) and 2(b) respectively. PL sensors on hard substrates are displayed in Figure 6.2(c). The smallest features of PL, AJP, and IJP are close to  $1\mu\text{m}$ ,  $10\mu\text{m}$ , and  $20\mu\text{m}$  respectively (around  $80\mu\text{m}$  for the low-cost Epson printers). Specifically, the smallest channel size of the fabricated AJP sensors, IJP sensors, and PL sensors are  $\sim50\mu\text{m}\times500\mu\text{m}$ , and  $\sim2000\mu\text{m}\times5000\mu\text{m}$ ,  $\sim10\mu\text{m}\times100\mu\text{m}$ , respectively. From the SEM images of Ag electrodes shown in Figure 6.2, it is obvious AJP printed Ag is better than IJP printed Ag because the cure-free low-temperature process of IJP printed Ag preserved large particles with radius as large as  $400\text{nm}$ . For CNT deposition, the CNT network fabricated by PL is more uniform than CNT network from AJP, because oxygen plasma treatment functions better on Si wafer than the flexible substrates of Kapton. CNT bundling effect is obvious in CNT network from IJP because no surface treatment was performed. Table 6.1 summaries the comparison among AJP sensors, IJP sensors, and PL sensors. Even though PL has unique advantages in miniaturizing sensors, the overall cost will be much higher than printing techniques



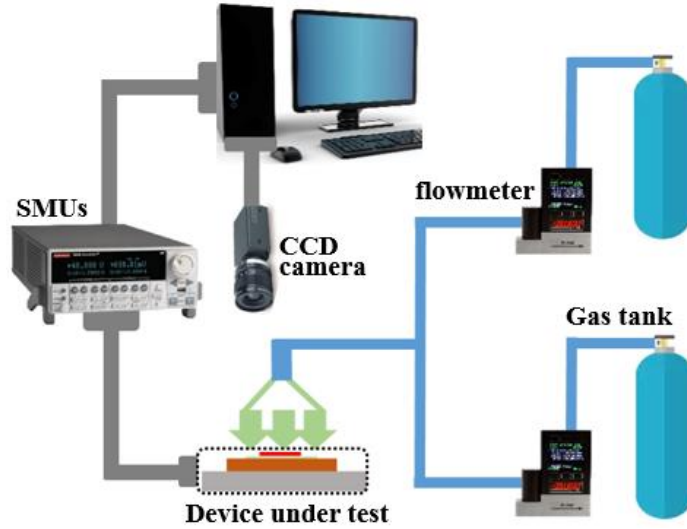
such as AJP and IJP, which limits its applications in various fields especially where large number of sensors need to be employed at low cost.



**Figure 6.2 Morphology and comparison of CNT sensors fabricated by AJP on Kapton substrate (a), IJP on PET substrate (b), and PL on Si wafer (c). SEM was used for the imaging of CNT network and Ag electrodes. Uniform CNT network was obtained in both PL and AJP process, but severe CNT bundling effect was observed in IJP process. CNT network is invisible under low resolution microscope.**

PL						
AJP						
IJP						
	Size	Ag	CNT	Cost		
					Good	
					Medium	
					Bad	
					Worse	

**Table 6.1 Fabrication comparison among PL, AJP, and IJP**

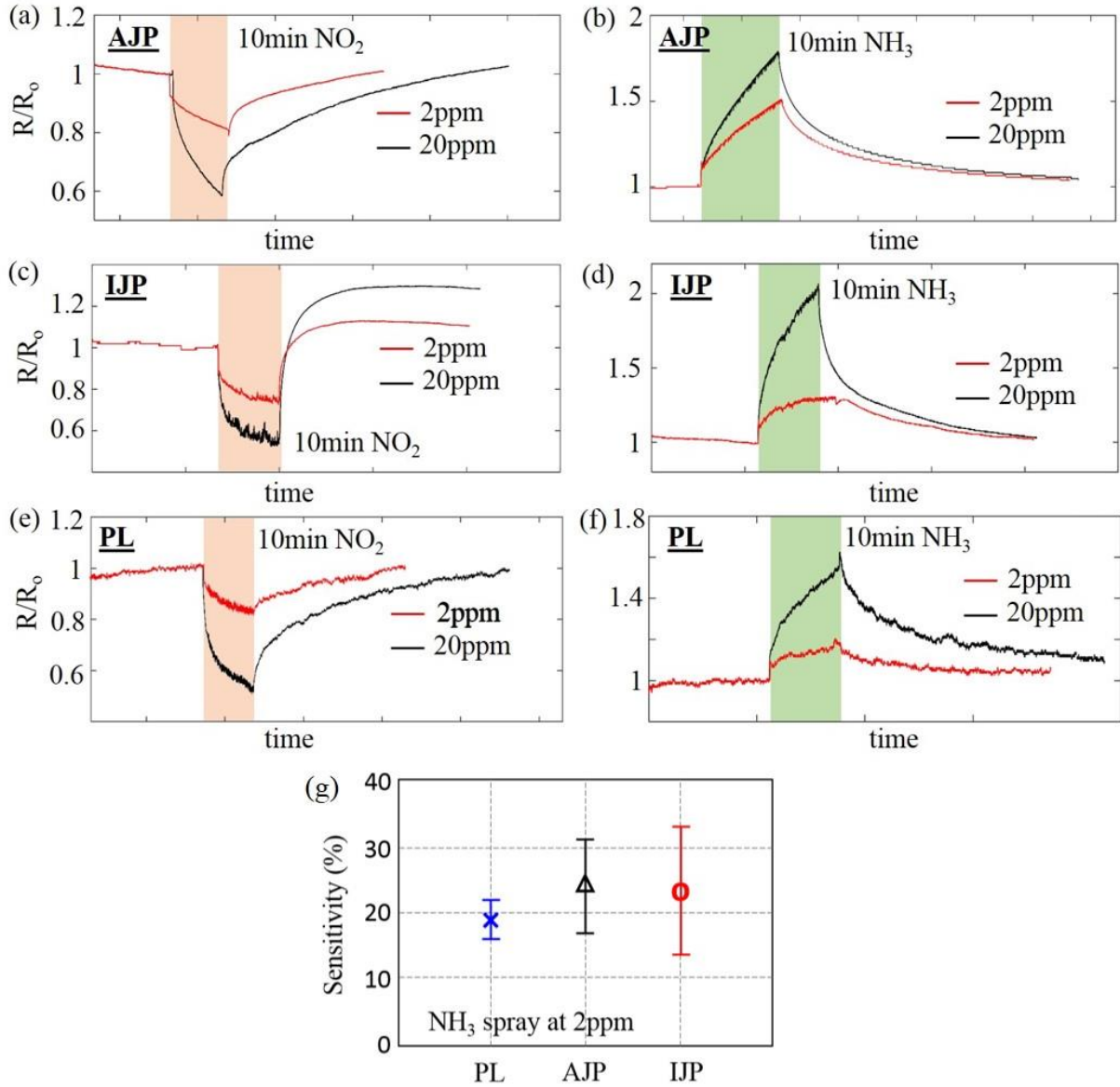


**Figure 6.3 Schematic of the experimental setup for gas sensing**

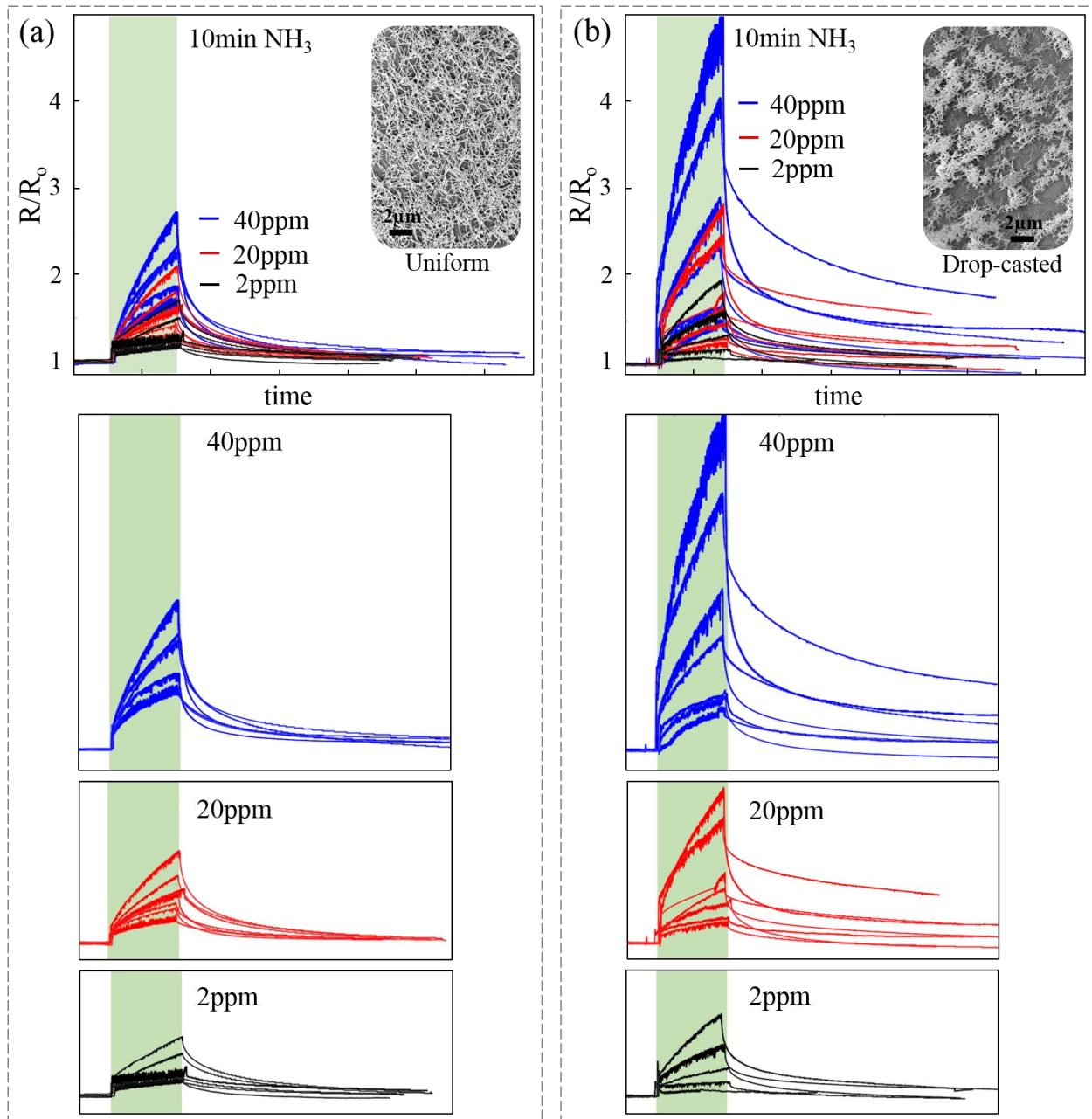
## 6.2 Experimental Setup

The sensing setup is described in Figure 6.3. Mixed gas spray with  $N_2$  as the carrier gas (either  $N_2+NO_2$  or  $N_2+NH_3$ ) is applied directly to the channel area of a CNT sensors from the nozzle at low ppm concentrate level (2ppm, 20ppm, and 40ppm) controlled by ALICAT flowmeters. The bias between sensor electrodes is set to -1V with Keithley 2604B SMUs recording the current change over time. The CCD camera helps visualize the device from laptop and probe the device under test. The whole setup is located inside fume hood under atmosphere pressure and stable room temperature. During measurement, the gas spray opens for ~10min after the current

becomes stable, then closes for ~30mins, which is referred as one cycle all together for certain concentration. The mass flowrate keeps the same (1000sccm) at different gas concentration. 2ppm as the lowest concentration applied during sensing test, which is high enough to get rid of the possible noise effect from the environment, e.g.,  $\text{NH}_3$ ,  $\text{NO}_2$ ,  $\text{H}_2$ , etc. at ppb level in air.



**Figure 6.4** Sensor responses of AJP sensors (a-b), IJP sensors (c-d), and PL sensors (e-f) under ~10min  $\text{NO}_2$  spray (orange strips) and 10min  $\text{NH}_3$  spray (green strips) at 2ppm and 20ppm concentration. Color strips denote gas on states (orange for  $\text{NO}_2$  and green for  $\text{NH}_3$ ), no strip denotes gas off state. The width of each color strip denotes the length of 10min. (g) sensitivity error bars of the PL, AJP, and IJP sensors.



**Figure 6.5 Variabilities in response of sensors, printed by AJP, with respect to different CNT network: layer by layer printed uniform CNT network (with oxygen plasma treatment) (a), drop-cast CNT network with CNT bundling effect (no surface treatment involved) (b). The inset figures are SEM imaging of CNT network patterned by the two different methods.**

### 6.3 Sensor Responses

The response of different CNT sensors (AJP sensors, IJP sensors, and PL sensors) were measured under either NO<sub>2</sub> or NH<sub>3</sub> spray at different concentrations. The results are shown in Figure 6.4. Again, R is the resistance of CNT sensors which changes over time. R<sub>o</sub> is the stable resistance before gas spray begins which is constant during the sensing test. R<sub>m</sub> is the maximum (for NH<sub>3</sub> sensing) or minimum (for NO<sub>2</sub> sensing) resistance under certain gas spray. Then the sensitivity can be defined as[201]

$$S(\%) = \frac{R_m - R_o}{R_o} \quad (6.1)$$

From the sensor responses of Figure 6.4(a)-(f), the sensitivity of all the CNT sensors change between 18%-25% and 38%-45% under 2ppm and 20ppm NO<sub>2</sub> gas spray, respectively. For NH<sub>3</sub> gas spray, the values are 20%-50% (2ppm) and 60%-100% (20ppm) correspondingly. There is no obvious trend that which type of CNT sensors have higher sensitivity with respect to the different fabrication methods (AJP, IJP, and PL), e.g., the PL sensor has the lowest sensitivity under 2ppm NO<sub>2</sub> gas spray but the highest sensitivity under 20ppm while the IJP sensor is the opposite. For NH<sub>3</sub> gas spray, the sensitivity also varies for different sensors at different concentrations as expected. As mentioned earlier, the smallest channel sizes of AJP sensors, IJP sensors, and PL sensors are nearly in the level of 50μm×500μm, 2000μm×5000μm, and 10μm×100μm, respectively. The electrodes materials are also different for PL sensors (Au) and printed sensors (Ag for both AJP sensors and IJP sensors). Moreover, the printing quality of Ag also varies between AJP and IJP as observed in the SEM images of Figure 6.2. However, qualitatively all the sensor responses are similar with respect to 4 different response phases within a cycle. As depicted

in Figure 6.4(a)-(f), when gas molecules (either  $\text{NH}_3$  or  $\text{NO}_2$ ) reach the surface of the CNT sensors (gas on state), there is a sudden change in resistance (phase 1) which lasts for only several seconds, followed by a gradual change in resistance (phase 2) which lasts till gas spray stops (gas off state begins). As for gas off state, there are also a sudden change (phase 3) and a gradual change (phase 4) in resistance but in the opposite way. Surprisingly, all the sensing curves of individual cycles can be well characterized by the convolution model described in Chapter 4. Considering all these distinctions during fabrication, the sensor responses of all the CNT sensors (AJP, IJP, and PL sensors) do not show very large differences qualitatively. And the printed CNT sensors do not show conspicuous lower sensitivity compared to PL sensors. The error bars displayed in Figure 6.4(g) reveal the variability of sensitivity of the PL, AJP, and IJP sensors. The average sensitivity is close to 20% for all the sensors, and the printed sensors even have higher sensitivity. However, the standard error of the mean shows that the variability of sensitivity changes significantly among them. For PL sensors, the standard error of the mean is only 2.6% because of much smaller fabrication difference between individual PL sensors, e.g. more uniformed CNT networks. But for printed sensors, they are 6.9% (AJP sensors) and 9.3% (IJP sensors).

#### **6.4 Variability of Sensor Responses**

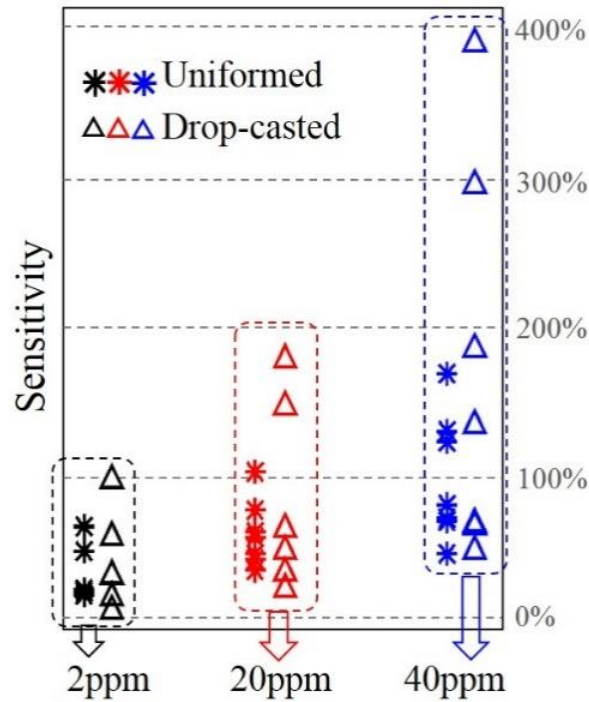
The CNTs in the channel are the ultimate gas sensing source, which have significant impact on the sensitivity. To study the impact of CNT network quality, two types of AJP sensors were fabricated, i.e., CNT network patterned by two different methods. One is the multiple layer by layer deposition after treating surface by oxygen plasma (described before in AJP fabrication section), which ends up with a uniform CNT network. The other one is drop-cast CNT network without oxygen plasma treatment (mentioned in the IJP fabrication section), which ends up with severe CNT bundling effect in the network. The rest of fabrication steps are exactly same for these

two types of AJP sensors. IJP printed CNT sensors are not utilized here for the comparison because the yield of printed CNT network is bad using low-cost IJP printers such as Epson C88+ and Artisan 1430. After fabrication, sensor responses were measured for ~10min  $\text{NH}_3$  spray at three different concentrations (2ppm, 20ppm, and 40ppm). The different in results can be observed in Figure 6.5(a) and 6.5(b), which are under the same coordinates scale. It is quite clear that AJP sensors with drop-cast CNT network have much larger variability in sensor response than AJP sensors with uniform CNT network. That is, for all the three different concentrations (2ppm, 20ppm, and 40ppm), the overall resistance change is much larger for AJP sensors with drop-cast CNT network. Figure 6.6 plots the sensitivity distribution based on the results in Figure 6.5. For AJP sensors with uniform CNT network (stars), the sensitivity changes in the range of 22%-68%, 38%-105%, and 50%-173% at 2ppm, 20ppm, and 40ppm respectively. But for AJP sensors with drop-cast CNT network, the corresponding ranges are as large as 10%-99% (2ppm), 25%-182% (20ppm), and 51%-400% (40ppm).

To explain this significant difference in sensitivity, CNT network is analyzed because the other processing steps remain same during fabrication. From previous studies, it is known that gas sensitivity of CNT network based sensors is mainly caused by the CNT/metal contacts and the CNT junctions[49]. Boyd et al. further pointed out that CNT network effects are dominated by gas-induced changes at CNT junctions for CNT network based sensors[49]. As shown in the inset figures of Figure 6.5, the two sets of CNT network are distinct in morphology. That is, the CNT network in Figure 6.5(a) is highly uniform while severe CNT bundling effect exists almost everywhere in channel in Figure 6.5(b). Specifically, regional CNT network density, CNT network structure, CNT-CNT contacts, CNT-metal contacts will vary significantly by the two different deposition methods. In other words, much higher uncertainty exists for drop-cast CNT network

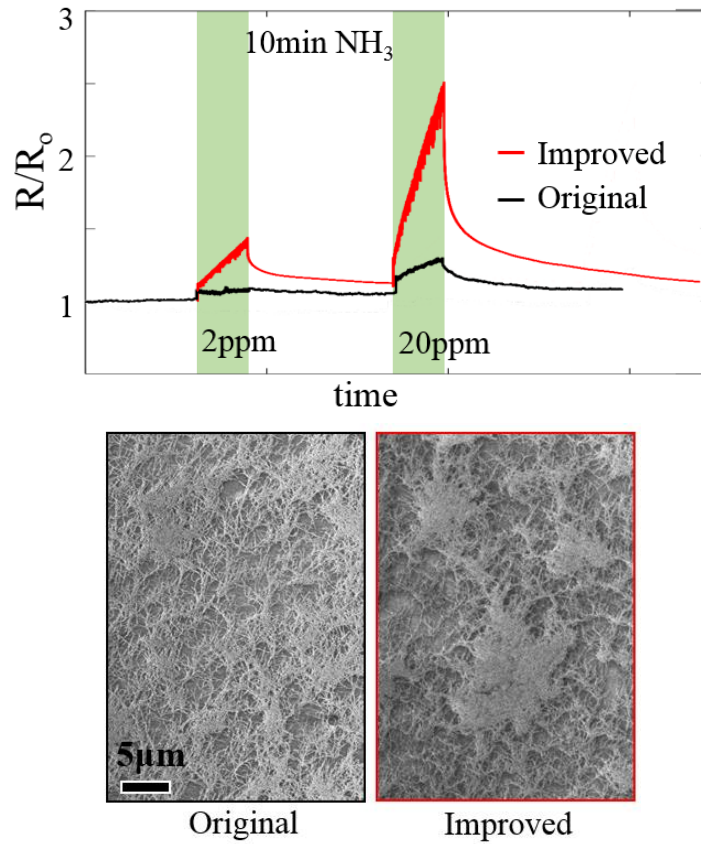


with respect to CNT/metal contacts and the CNT-CNT junctions, which are the main causes for gas sensitivity. The low quality (CNT bundling effect) CNT network from drop-cast method will not necessarily lower the sensitivity for CNT sensors, even though it could be one of the major issues for low sensitivity of CNT based thin film transistors. On the contrary, as the result shows in Figure 6.6, it can actually improve the sensitivity significantly in some of the cases with the highest sensitivity exceeding 400% at 40ppm gas spray. This high sensitivity is more than twice compared to AJP sensors with uniform CNT network (173%) under the same conditions. Similar conclusions can be drawn at other concentrations.



**Figure 6.6 Comparison of sensitivity distribution of AJP sensors with respect to different CNT network: printed uniform CNT network (with oxygen plasma treatment, stars), drop-cast CNT network with severe CNT bundling effect (no surface treatment involved, triangles).**





**Figure 6.7 Sensitivity improvement of an IJP sensor under  $\text{NH}_3$  spray at 2ppm and 20ppm. Black curve is the sensor response from the original IJP sensor with relatively low sensitivity. Red curve is the improved sensor response of the IJP sensor with post drop-cast CNT deposition. The SEM images show the change of CNT network after post drop-cast deposition.**

In some cases, sensitivity could be extremely low for sensors with drop-cast CNT network because of its high uncertainty compared to uniform CNT network formed by layer by layer deposition by AJP, e.g., the lowest sensitivity is only 10% for drop-cast CNT network but it is 22% for uniform CNT network at 2ppm concentration, as shown in Figure 6.6. To address this issue, the unique advantage of drop-cast deposition becomes very beneficial. Unlike uniform CNT network printed by multiple layer by layer deposition, drop-cast deposition involves no extra equipment at all and it can be conducted anywhere anytime. Therefore, drop-cast deposition of

CNT network can be easily performed after the completion of IJP sensor fabrication (referred as post drop-cast deposition), in order to improve the low sensitivity of certain IJP sensors. On the one hand, post drop-cast deposition will neither increase the cost nor complicate the process, which are the main considerations of the IJP sensors. On the other hand, it can actually rebuild the CNT network easily and repeatedly to achieve high sensitivity. Figure 6.7 plots the change in sensitivity before and after the application of post drop-cast CNT network. This improvement is significant. For the original IJP sensor, the sensitivity is as low as ~6% at 2ppm and ~25% at 20ppm. After post drop-cast deposition, its sensitivity jumps to ~50% (2ppm) and 150% (20ppm) respectively. As observed from the SEM images, the CNT network structure is rebuilt (with respect to both local density and CNT bundling effect) after post drop-cast deposition. This result demonstrates that post drop-cast deposition can provide an efficient strategy to improve the sensitivity of printed CNT sensors while maintaining the low-cost, especially for IJP sensors which can be fabricated outside the cleanroom or even outside the lab because of the simplified steps with cure-free low-temperature process.

## **6.5 Closure**

Single-walled CNT network based gas sensors have been fabricated using AJP, IJP, and PL separately. Their sensor responses behave similarly under gas spray of  $\text{NH}_3$  and  $\text{NO}_2$  even though these CNT sensors are different in size, electrodes, and CNT network structure. For fully printed CNT sensors (either AJP or IJP sensors), no performance degradation has been observed with respect to sensitivity and stability in response. The significance of CNT network in sensor response has been demonstrated by comparison of two types AJP sensors with CNT network patterned by either multiple layer by layer printing (with highly uniform CNT network) or drop-cast method (with severe CNT bundling effect). Sensors with drop-cast CNT network have much larger

variability in sensor response than those with layer by layer printing uniform CNT network. However, fully printed sensors with very high sensitivity can be fabricated using drop-cast CNT network. And a post drop-cast deposition can provide an efficient strategy to improve the sensitivity of printed CNT sensors while maintaining the low-cost nature, which paves the way for extensive applications of low-cost CNT sensors in flexible and wearable electronics and devices.

## CHAPTER 7. SUMMARY AND FUTURE WORK

### 7.1 Summary of Current Work

In this work, randomly distributed CNT network based devices, such as CNT-TFTs and CNT chemiresistor sensors, have been fabricated on both hard (Si substrate) and flexible substrates (Kapton, LCP, PET) using PL, AJP, and IJP separately. The performance of CNT-TFTs have been studied thoroughly and the sensor response of CNT sensors have been improved, which will have wide range applications in the areas of flexible and wearable electronics, artificial skins, low-cost CNT sensors, etc.

First, CNT-TFTs on hard Si substrate are fabricated by using PL. To achieve high performance, >99% highly purified semiconducting single-walled CNT solution is utilized as the semiconductor material in the channel. However, device-to-device performance variability of TFTs can pose challenging problems for the fabricated CNT-TFTs. One of the major problems is the variability in performance, which is mainly rooted in the randomness of CNT networks, the variation in individual CNT properties due to change in chirality, and the fabrication imperfections. To address this issue, both experimental and theoretical methods are employed to analyze the variability in I-V characteristics in a statistical framework. To be specific, the sources of variation including % of M-CNTs,  $V_{th}$ , CNT mean length, and CNT network density have been studied separately. The analysis shows that the presence of M-CNTs is a major source contributing to the performance variation for short channel TFTs, but its effect reduces for large channel length transistors.  $V_{th}$  is found to be the major source of variation for long channel TFTs. A better consistency in performance can be guaranteed for TFTs with larger channel area, which ensures a smaller variation in CNT network density and CNT mean length. These results provide key

insights into the variability estimation of I-V characteristics of CNT based devices which is vital for reliability studies of CNT-TFTs based circuits for different electronic applications.

Secondly, the fabricated CNT-TFTs have been used as sensors for gas detection. It is well known that the lack of selectivity has been a major drawback of CNT sensors for the wide range of applications in air quality detection and the industrial emission control. In order to create the selectivity of CNT sensors with respect to different sensing gases, cycling test of the CNT sensors have been recorded for  $\text{NH}_3$  and  $\text{NO}_2$  detection in air at low ppm concentrations. A sensing mechanism is proposed based on the interaction between gas molecules and different types of dwelling spots inside the channel area of a TFT. Moreover, a double exponential-convolution model is put forward to decipher sensor response as well as to explore its application in gas identification. In this context, the consistency in time constants is recognized, which is independent of gas concentration. More importantly, the time constants vary with respect to different gas types and TFTs. The uniqueness of time constants can work as identity verification for different sensing gases, which demonstrates that the sensor response is a distinctive behavior determined by the unique channel structure of each TFT. This work provides us a general strategy for gas identification and a practical path to realize the advantages of CNT gas sensors in pollution monitoring in low concentration level.

Then, we concentrate on the fabrication of fully printed CNT-TFTs because of their significant potential in flexible and wearable devices with huge advantages in the low cost, high repeatability and scalability. However, quality of printable dielectric layer has become one of the major obstacles. Its relatively large thickness can result in very high gate voltage to fully switch on and switch off the transistors, which will cause high power dissipation for printed devices. In response to this challenge, fully printed CNT-TFTs have been fabricated on Kapton and LCP

substrates using single printing technique of AJP. The printed CNT-TFTs show very stable performance including high on/off ratio, high mobility, negligible hysteresis, and good uniformity. More importantly, these devices can be operated using bias voltages as small as  $\pm 5\text{V}$ , which is much smaller than the previously reported values because of the improvement in both printed CNT network and dielectric layer. Multiple layer by layer CNT network deposition is applied for density control and high uniformity, and xdi-dcs is diluted and optimized with natural  $\geq 99.5\%$  butyl alcohol to reach thinner printing for better quality. This work paves the path for applications of CNT-FETs in wearable and bendable devices such as flexible displays, RFID antennae/tags, sensors, artificial skins, etc.

Finally, fully printed CNT sensors have also been fabricated using AJP and IJP separately because of the promise for cost-effective and scalable production, which provides high design flexibility compared to conventional PL process. The fully printed CNT devices are tested for  $\text{NH}_3$  and  $\text{NO}_2$  detection in air at low ppm concentration based on cycling gas sensing. Through comparison with CNT sensors fabricated by PL, printed sensors show no degradation with respect to sensitivity and stability, but they are much lower in cost. Especially for sensors using extremely low-cost IJP (with the printer price only US \$108), the corresponding sensor responses still show excellent performance. During fabrication, both drop-cast CNT network and printed CNT network were patterned for the sensors, resulting in bundled CNT network and highly uniform CNT network respectively. The sensitivity is surprisingly high for some printed CNT sensors with drop-cast CNT network. Moreover, the low sensitivity of some printed CNT sensors can be highly improved using post drop-cast CNT deposition without any surface functionalization. This work provides key insights for the fabrication and performance improvement of extremely low-cost CNT gas sensors.

## 7.2 Future Work

The work in present thesis can be extended and continued in several topics as suggested below.

### 7.2.1 *Optimization and Improvement of Fully Printed CNT-TFTs*

Even though the printed dielectric layer has been highly improved, the overall performance of fully printed CNT-TFTs are still relatively low considering their high potential. Various aspects can be further improved and optimized for fully printed CNT-TFTs. The CNT/metal contact is one of them, which will have significant impact on the overall resistance in printed CNT devices. The high resistance of CNT/metal contact also can be seen in devices fabricated by PL process, and it is even worse in printed ones. To address this issue, printed M-CNT layer, as well as graphene layer, can be a feasible solution. It actually avoids direct CNT/metal contact by introducing contacts such as S-CNT/M-CNT, M-CNT/metal, S-CNT /graphene, graphene/metal, etc. The improvement in contact can reduce the performance variability of fully printed CNT-TFTs. Moreover, the much superior bending and stretching capability of M-CNT layer can also improve the mechanical performance of printed CNT devices at the same time, e.g., the printed Ag layer (one-time single printing of AJP) can only survive 20%-30% stretching, but printed CNT layer (both M-CNT and S-CNT layer) can bear much higher stretching strength (sometimes even higher than the stretching limit of some flexible substrates such as Kapton with a stretching limit around 60%) because of the excellent mechanical properties of CNTs. Besides, the M-CNTs have the potential to take the place of printed metal as electrodes of CNT-TFTs, which will have high potential in transparent electronics. The improvement of fully printed CNT-TFTs can be also be performed with respect to the dimensions, stability, and reliability of the fabrication process, etc.

### 7.2.2 *Mechanical Test of Flexible CNT-TFTs*

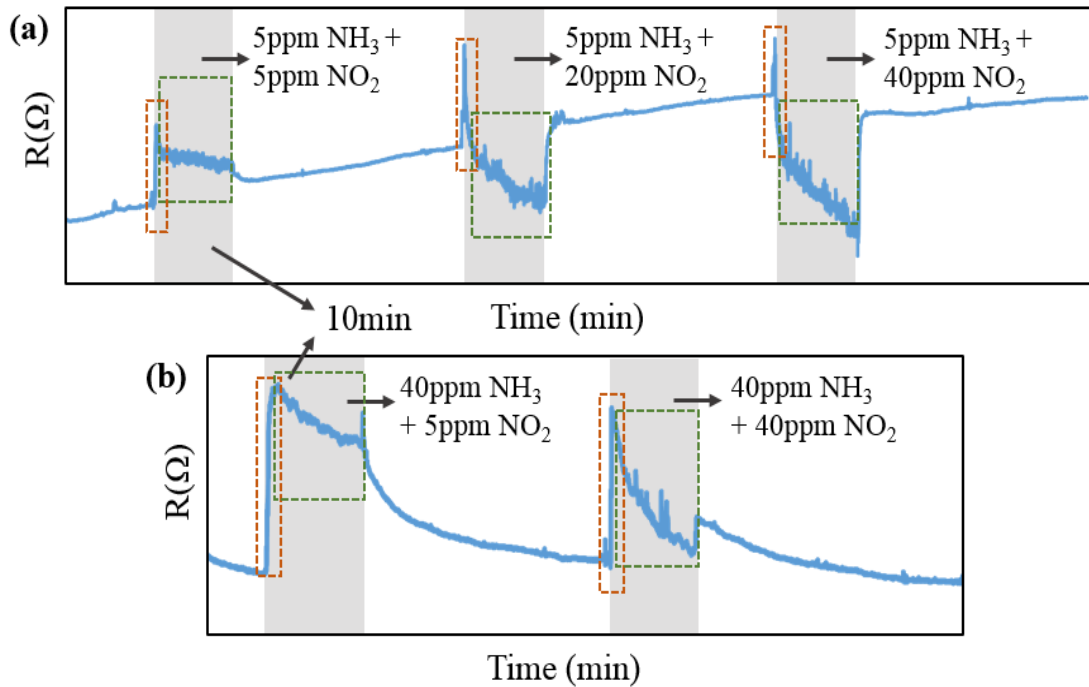
CNT network based flexible electronics are most commonly used for TFTs as building blocks for ICs and active-matrix displays, which have great significance in future wearable devices. The major advantages of flexible CNT-TFTs lie in the excellent mechanical properties under stress. Generally, there are two types of flexible electronics, stretchable and non-stretchable (bendable) [202]. Stretchable electronics are usually made of elastomeric substrates such as rubber, polydimethylsiloxane (PDMS), or polyurethane. Bendable (non-stretchable) electronics usually use flexible substrates such as thin glass sheets, polyimide, polyethylene terephthalate, or polyethylene naphthalate. As described earlier, the mechanical test of flexible electronics is of great significance for various applications. Up to now, most of the researches concentrate on the bending test of CNT-TFTs. However, flexible CNT-TFTs on non-stretchable substrates can actually survive from stretching test after improvement during fabrication. This is also very important for non-stretchable electronics because of the ever-increasing demands in practice. On the one hand, how the performance changes during stretching test is crucial for the reliability and stability of the CNT-TFTs. On the other hand, the stretching limit is also the key factor for the applications of flexible devices. Besides, the mechanical test of flexible CNT-TFTs will give us feedback on insights about performance improvement of the devices in various ways.

### 7.2.3 *Gas Sensing of Flexible CNT Sensors under Stress*

The mechanical test of flexible CNT sensors during gas sensing has attracted more interests in recent years. As is well-known, gas adsorption in CNTs (including CNT/CNT junctions, CNT/metal contact, etc.) is an important issue for both fundamental research and technical application. Both bending test and stretching test need to be performed in order to better understand



the sensing mechanism during gas sensing. When gas molecules interact with the CNT network in channel area, they will work as either electron source or hole source which can either decrease or increase the current of the sensor depending on the existing current type (either n-type or p-type). During this process, the CNT/CNT junctions and CNT/metal contact area are the major dwelling spots for gas molecules. Generally, the dwelling spots stay the same during the gas sensing process. However, it will be a different situation when CNT sensors are under stress resulting from either bending or stretching. To be specific, the bending and stretching can change the CNT network structure more or less because of the deformation in certain area, e.g., the movement of CNTs or the slide of CNT/CNT junctions in small range. Especially with the increase of stretching strength, the resistance of the device itself will change significantly because of the change in overall morphology of the device, which will have significant impact on the sensing performance, such as the sensitivity, stability, etc.



**Figure 7.1** Sensor responses of mixed gases. Same concentration of  $\text{NH}_3$  at 5ppm (a) and 40ppm (b) with increasing concentration of  $\text{NO}_2$  for each cycle.

#### 7.2.4 Mixed Gas Sensing

Even though it has been proven that CNT sensors are able to detect various gases such as  $\text{NH}_3$ ,  $\text{NO}_2$ ,  $\text{H}_2$ , etc., there is very limited work concentrating on the sensing test of mixed gases. And the corresponding sensor responses have not been fully understood for mixed gas sensing because of the complicated sensing mechanism. Similarly, cycling tests have been performed with gas mixture on for  $\sim 10$ min and gas mixture off for  $>20$ min (gas mixture: mix  $\text{NO}_2$  with  $\text{NH}_3$  at different concentrations). The results are plotted in Figure 7.1. In Figure 7.1(a),  $\text{NH}_3$  is maintained at 5ppm with increasing concentration of  $\text{NO}_2$  from 5ppm, 20ppm to 40ppm. In Figure 7.1(b),  $\text{NH}_3$  is maintained at 40ppm with increasing concentration of  $\text{NO}_2$  from 5ppm to 40ppm. In both figures, it is observable that all the sensors first experience rapid resistance jump caused by  $\text{NH}_3$  for a very short time (dash orange box), then the resistance decreases slowly for the rest of gas on state caused by  $\text{NO}_2$  (dash green box). The increasing concentration of  $\text{NO}_2$  affects the final resistance at the end of gas on state, while the concentration of  $\text{NH}_3$  affects the highest resistance at the beginning of gas on state. Compared to single gas sensing, the sensor responses of gas mixture are less stable during gas on state. Undoubtedly, further exploration is indispensable because none of the sensor responses can be well described using any of the previously mentioned models. Clearly, the sensing mechanism of gas mixture is more complicated than single gas sensing and it has not been fully understood. More work needs to be done in this area.

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