PROJECT ADMINISTRATION DATA SHEET

		X ORIGINAL	REVISION NO.	
Project No. E-16-692 (R6213-0)AO)	GTRC/Ğǐ华		
Project Director: D.P. Schrage		School/Lab	made and a second secon	
Sponsor: _U.S. Army Research	Office			
Type Agreement: DAA103-86-K-0			10/21/87	
Award Period: From 9/1/86	То8/31/88	(Performance)	10/31/87 (Reports)	
Sponsor Amount:	This Change		Total to Date	
Estimated: \$		<u>\$ 228,4</u>	39 (including Options)	
Funded: \$		s <u>68.7</u>	07 (1st year)	
Cost Sharing Amount: \$ 8,807		Cost Sharing No:	E-16-392	
Title: A Systems Approach to	Rotocraft Stabilit	y and Control Res	earch	
				
ADMINISTE ATIVE DATA		John D. Cah	onk X-4820	
ADMINISTRATIVE DATA 1) Sponsor Technical Contact:	OCA Contact _	John B. Sch 2) Sponsor Admin/Co		
Robert E. Singleton			I. Calder	
Army Research Office		ONR RR		
P.O. Box 12211		Georgia	Tech	
Research Triangle Park, NO	27709-2211			
				
				
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GEORGIA INSTITUTE OF TECHNOLOGY OFFICE OF CONTRACT ADMINISTRATION

NOTICE OF PROJECT CLOSEOUT

S S	Date 2/21/89
Froject No. E-16-692	Center No. R6213-0A0
Project Director D.P. Schrage	School/LabAE
Sponsor ARMY	<u> </u>
Contract/Grant No. DAAL03-86-K-0160	GTRC XX GIT
Prime Contract No	
Title <u>Turbulence Model Development for Rot</u>	ocraft Stability and Control Specification
Effective Completion Date 8/31/88	(Performance) 10/31/88 (Reports)
Closeout Actions Required:	
None X Final Invoice or Copy of Last I X Final Report of Inventions and/ X Government Property Inventory & Classified Material Certificate X Release and Assignment Other	nvoice or Subcontracts- Patent Questionnaire sent to P/I Related Certificate
Includes Subproject No(s). E-25-M17/ B.	H. Tongue/ME (In DB)
Subproject Under Main Project No	
Continues Project No.	_ Continued by Project No
Distribution:	
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E-16-670

GEORGIA INSTITUTE OF TECHNOLOGY

ATLANTA, GEORGIA 30332

SCHOOL OF AEROSPACE ENGINEERING

404-894-3000

DANIEL GUGGENHEIM SCHOOL OF AERONAUTICS

May 3, 1987

Dr. Robert E. Singleton
Director, Engineering Sciences Division
U.S. Army Research Office
Box 12211
Research Triangle Park, NC 27709-2211

Dear Dr. Singleton:

Sorry for the late submittal of this initial progress report. The original was misplaced. We are beginning to make good progress after spending considerable time working with NASA Ames obtaining and understanding the UH-60A Black Hawk Flight Test data. We should have some results as well as a planned paper in our next progress submittal at the end of June.

Sincerely,

Daniel P. Schräge

Co-Principal Investigation

DPS/1p Attachments

PROGRESS REPORT

ARO PROPOSAL NUMBER:

23246-EG

PERIOD COVERED BY REPORT:

1 July 1986 - 31 December 1986

3. TITLE OF PROPOSAL:

A Systems Approach to Rotorcraft Stability & Control Research

4. CONTRACT OR GRANT NUMBER:

DAAL0-3-86-K-0160

5. NAME OF INSTITUTION:

Georgia Institute of Technology

AUTHORS OF REPORT:

D. P. Schrage and B. H. Tongue

7. LIST OF MANUSCRIPTS SUBMITTED OR PUBLISHED UNDER ARO SPONSORSHIP DURING THIS REPORTING PERIOD, INCLUDING JOURNAL REFERENCES:

NONE

8. SCIENTIFIC PERSONNEL SUPPORTED BY THIS PROJECT AND DEGREES AWARDED DURING THIS REPORTING PERIOD:

Arran en la companya de la companya

D. P. Schrage

V. R. P. Jonnalagadda

Department of Aerospace Engineering Georgia Institute of Technology Atlanta, GA 30332-0150

B. H. Tongue

Department of Mechanical Engineering Georgia Institute of Technology Atlanta, GA 30332

BRIEF OUTLINE OF RESEARCH FINDINGS

This research project entails extensive interaction with the U.S. Army Aviation Aeroflightdynamics Directorate at NASA Ames Research Center, as well as the rotorcraft industry. The genesis of this research project was based on the "Topics for Helicopter Stability and Control Research" identified by Mr. David L. Key, Chief, Aircrew-Aircraft Systems Division, Aeroflightdynamics Directorate in his 26 November 1984 memorandum (Enclosure 1). During the first year this research project is addressing rotorcraft modeling and is applying parameter identification techniques and a generic NASA/Army developed flight dynamics mathematical model, ARMCOP, to try and shed light on the number of degrees of freedom required in linear models, as well as demonstrate techniques for math model verification and updating from flight test.

The three tasks included in the first year are well underway. The ARMCOP model of the UH-60A Black Hawk has been obtained and installed on the GIT computer system. The UH-60A Black Hawk helicopter flight test data base has been obtained and installed on the GIT computer system. We have completed initial least squares parameter identification assessment of the flight test data in forward flight and have shown poor correlation with the ARMCOP results, as expected, due to the measurement noise in the flight test data and the number of degrees of freedom in the linear model of ARMCOP. We are completing the least squares identification at the hover condition and then will proceed to apply more sophisticated identification techniques, such as extended Kalman Filter and modified Newton-Raphson techniques which can account for the measurement noise.

The work being accomplished under this research project and its relationship to other Georgia Tech rotorcraft flight mechanics and controls research projects is illustrated in Enclosure 2. As can be seen this research project is the centerpiece which allows a systems approach to rotorcraft stability and control research.

Visits have been made to NASA Ames Research Center in September 1986 and again in March 1987 to discuss this work as well as obtain the necessary flight test and modelling information to conduct this research.



DEPARTMENT OF THE ARMY AEROMECHANICS LABORATORY US ARMY RESEARCH & TECHNOLOGY LABORATORIES-AVSCOM AMES RESEARCH CENTER MOFFETT FIELD, CALIFORNIA 94035

SAVDL-AL-C

26 November 1984

MEMORANDUM FOR RECORD

SUBJECT: Topics for Helicopter Stability and Control Research

1. The ongoing efforts at the Aeromechanics Laboratory in stability, control, handling qualities and pilot aircraft interface are generally at the 6.2 Exploratory Development level and involve use of sophisticated experimental facilities. However, there are many topics related to this program that could be considered 6.1 Basic Research that are essentially analytical and require primarily computational support; such topics could usefully be addressed by universities and small analytical research companies and perhaps supported through the U.S. Army Research Office. The following is a brief listing of some such topics:

a. Rotorcraft Modeling

- (1) The degrees of freedom required in linear models.
- (2) Techniques for math model verification and updating from flight test.

b. Modern Control Theory Applications

(1) Use of optimal and modal control law implementation approaches, i.e., both time and frequency domain approaches. We particularly need to assess methods that can minimize feedback gain levels.

c. Digital Flight Control System Effects

- (1) Study the effects of digital computation delays and interaction with rotor and structural dynamics on the performance of highgain digital flight control systems.
- (2) Methods for direct digital design—rather than converting from continuous system designs.

SAVDL-AL-C 26 Novem SUBJECT: Topics for Helicopter Stability and Control Research

e. Active Control Applications

- (1) Techniques for applying active horizontal stabilizer, higher harmonic control, integration of the propulsion and flight control system, and relaxed static stability configurations.

f. Real-Time Expert Systems Development

(1) Applications of expert systems to flight path management, could include functions such as automation of NOE navigation, terrain avoidance, terrain following, threat avoidance, failure sensing and recovery:

g. Simulation Technology

- (1) Quantification of visual and motion cue effects.
- (2) Math modeling techniques to minimize computation times.
- (3) Air combat simulation requirements.

h. Effects of Outside Visual Cue Quality

(1) Relate the characteristics of both outside visual scene and sensor/display quality to human perceptual capabilities and flight path control limitations.

i. Turbulence Model

(1) There is a need for development of a low-altitude turbulence model for incorporation into the updated handling qualities Spec 8501.

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j. Maneuvering Envelope Limiting and Cueing

(1) Need to understand fundamental envelope maneuver limitations and how these can be cued to the pilot to inhibit him from violating these limits but allowing him to exceed them in emergency situations.

k. Energy Management Techniques

(1) Apply optimization methods to air combat, autorotation, and engine-out operations.

SAVDL-AL-C 26 November 1984 SUBJECT: Topics for Helicopter Stability and Control Research

1. Interactional Aerodynamics

- (1) Better techniques for developing stability and control predictions especially applied to empennage design.
- 2. If further explanation or discussion of potential responses to these topics is required, please contact the undersigned (415) 694-5839 or Ed Aiken (415) 694-5362.

DAVID L. REY!

Chief, Aircrew-Aircraft Systems Division

CF: I. Statler

E. Aiken

R. Stapleton

D. Schrage

A. Gessow

G. Loey

H. Curtiss

D. Schmidt

A. Bryson

E. Laitone

R. Hess

D. McRuer

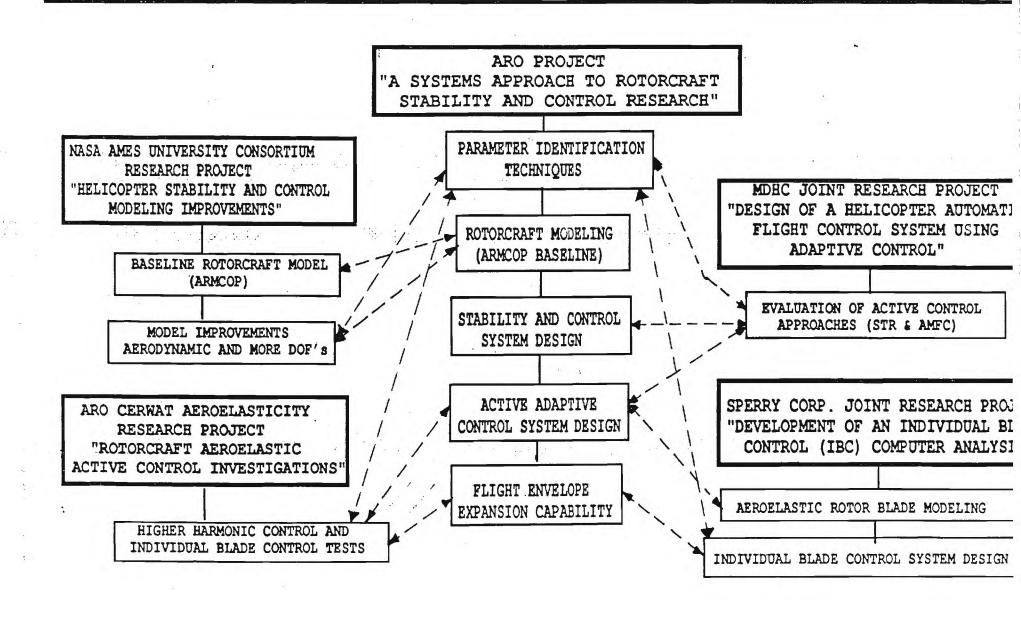
R. Harper

R. Heffley

N. Ham

S. Miley

ROTORCRAFT FLIGHT MECHANICS AND CONTROLS RESEARCH PROJECTS



 G_{Γ}

Georgia Institute of Technology

SCHOOL OF MECHANICAL ENGINEERING

Dynamics and Vibrations Laboratory

BENSON H. TONGUE DIRECTOR, DYNAMICS AND VIBRATIONS LAB [404] 894-3298

ATLANTA, GA 30332

July 28, 1987

Dr. Robert E. Singleton Director, Engineering Sciences Division U.S. Army Research Office Box 12211 Research Triangle Park, NC 27709-2211

Dear Dr. Singleton:

I have enclosed the bi-yearly update on the research that Dan and I are involved in. If anything else is needed, please let me know.

Best Regards

Benson H. Tongue

PROGRESS REPORT

TWENTY COPIES REQUIRED

- 1. ARO PROPOSAL NUMBER: 23246-EG
- 2. PERIOD COVERED BY REPORT: 1 January 1987 30 June 1987
- 3. TITLE OF PROPOSAL: A Systems Approach to Rotocraft Stability & Control Research
- 4. CONTRACT OR GRANT NUMBER: DAALO3-86-K-0160
- 5. NAME OF INSTITUTION: Georgia Institute of Technology
- G. AUTHORS OF REPORT: Benson H. Tongue, Daniel P. Schrage
- 7. LIST OF MANUSCRIPTS SUBMITTED OR PUBLISHED UNDER ARO SPONSORSHIP DURING THIS REPORTING PERIOD. INCLUDING JOURNAL REFERENCES:

Abstract submitted to the Second International Conference on Rotorcraft Basic Research, 16-18 February, 1988, College Park, Maryland

Preliminary results to presented at the AGARD panel meeting on Helicopter System Identification to be held on September 7-11, 1987 at Arles, France

8. SCIENTIFIC PERSONNEL SUPPORTED BY THIS PROJECT AND DEGREES AWARDED DURING THIS REPORTING PERIOD:

Benson H. Tongue Daniel P. Schrage Prasad Jonnalagadda

Daniel P. Schrage Department of Aerospace Engineering Georgia Institute of Technology Atlanta. GA 30332 GENHEL has been installed on the school's VAX computer. After extensive investigation, it has become clear that the UH-60A flight test data that was obtained from NASA earlier this year was strongly flawed. The first problem was that no documentation was available for the data. The second problem was that the results of preliminary estimation runs indicated physically unrealistic results. The trouble was thought to have been produced by sign convention irregularities and physical units problems. Upon discussion with both Sikorsky and NASA, these speculations proved to be correct. At the present time it is believed that the sign conventions and units used are now correct.

Identification runs were then made which indicated a strong variation in the response as a function of noise in the data. In order to address this points, a program was laid out in which a known mathematical model was used to generate numerical data. This data was then contaminated with a given amount of noise and used in a Recursive Least Squares identification scheme. The model used was a fourth order (longitudinal) one. Results showed that the technique did well in the face of zero noise but poorly for even very small amounts of noise.

An Extended Kalman Filter was then implemented to compare to the previous results. This technique showed a strong tendency to divergence and was judged unsuitable for rotorcraft identification purposes. A relatively new technique, the Statistically Linearized Filter, was then utilized. This method worked very well with the zero and small noise cases but appeared to give incorrect results with moderate noise levels. This technique is still under investigation. An investigation into the advantages of the Maximum Likelihood method is currently underway.

A global characterization of the methods under consideration is being prepared in which the effect of varying models is investigated. For instance, the techniques will be applied to linear and nonlinear, stable and unstable, well behaved and ill conditioned, etc. systems. In this way an envelope of applicability can be constructed for the different techniques.

System identification data on the UH-60A has turned out to be unusable in its present form. The problem is in the format of the tapes. This problem is currently being addressed. STEP and STEPSL have been obtained from NASA Lewis. These are linear regression packages that were developed for fixed wing applications. This material is now being tailored for use with rotorcraft.

(Abstract submitted for the 2nd International Conference on Rotorcraft Basic Research, 16 – 18 February, 1988, College Park, Maryland)

SOME BASIC ISSUES IN HELICOPTER SYSTEM IDENTIFICATION

Daniel P. Schrage, V.R.P. Johnalagadda School of Aerospace Engineering

and

Benson H. Tongue, Philip M. Fitzsimons, David Teare
School of Mechanical Engineering
Georgia Institute of Technology
Atlanta, Georgia 30332

Rotorcraft modeling poses a far more difficult problem than fixed-wing aircraft due to both the large number of degrees of freedom that occur in the nonrotating and rotating axes and the complexity of the aerodynamics. In the recent past, helicopter mathematical model extraction from flight test data using identification techniques has received a great deal of attention by various researchers. Though the theory is well developed, the application of system identification techniques to helicopter problems is still essentially an art rather than a science. Central to the issues of helicopter system identification are the short record lengths and noisy measurements. In addition to these issues, the question of input type and appropriate amplitudes needs to be well established prior to actual flight testing. The input amplitude should be limited for linear model extraction and at the same time it should have enough spectral content to excite all the dynamic modes of the helicopter. This paper addresses the first two issues using simulated as well as flight test data of the UH-60A Black Hawk helicopter. The issue of model identifiability in the presence of noise in the measurements is examined in detail for different levels of noise content. Also, the minimum data record length required for obtaining various order models of the helicopter for stability and control analysis is investigated. The helicopter simulated response data is generated using the ARMCOP flight simulation program and the resulting response is corrupted with different levels of zero-mean Gaussian noise. Two representative identification techniques - the maximum likelihood method and the stochastic linear filter method- are used and the results are compared. Conclusions and recommendations are presented.

This work is sponsored by a research grant from the Army Research Office (ARO) under the contract No. DAALO-3-86-K-0160.

PROGRESS REPORT

ARO PROPOSAL NUMBER: 1.

23246-EG

2. PERIOD COVERED BY REPORT: 1 July 1987 - 31 December 1987

3. TITLE OF PROPOSAL: A Systems Approach to Rotorcraft

Stability and Control Research

4. CONTRACT OR GRANT NUMBER: DAAL03-86-K-0160

NAME OF INSTITUTION: 5.

Georgia Institute of Technology

6. AUTHORS OF REPORT: D.P. Schrage and B.H. Tongue

- 7. LIST OF MANUSCRIPTS SUBMITTED OR PUBLISHED UNDER ARO SPONSORSHIP AWARDED DURING THIS REPORTING PERIOD:
 - A. Fitzsimons, P.M., Teare, D., Prasad, J.V.R., Schrage, D.P., and Tongue, B.H., "Some Basic Issues in Helicopter System Identification." Paper to be presented at 2nd International Conference on Basic Rotorcraft Research, University of Maryland, Feb. 16-18, 1988.
 - В. The following presentations were made at The Second Technical Workshop on Dynamics and Aeroelastic Stability Modeling of Rotorcraft Systems, Sponsored by the ARO and Florida Atlantic University in Boca Raton, Florida, on Nov. 18-20, 1987:
 - Calise, A.J. and Jonnalagadda, V.R.P., "Compensator Based 1) Controller Design for Helicopters," Georgia Institute of Technology.

Schrage, D.P., Oakes, G., and Jonnalagadda, V.R.P., "Develop-2) ment of an Individual Blade Control Computer Analysis."

Georgia Institute of Technology.

- Schrage, D.P., Jonnalagadda, V.R.P., and Wasikowski, M.E., 3) "Active Vibration Control Using Reduced Order Models," Georgia Institute of Technology.
- Calise, A.J. and Prasad, J.V.R., "An Approximate Loop Transfer Recovery Method for Designing Fixed-Order Compensators," Paper to be presented at AIAA Guidance, Navigation and Control Conference, August 1988.
- D. Schrage, D.P., Tongue, B.H., Prasad, J.V.R., Fitzsimons, P.M., and Teare, D., "Time Domain Parameter Identification Techniques Applied to the UH-60A Black Hawk Helicopter Flight Test Data," Paper to be included in special edition of Vertica Magazine on Helicopter System Identification, December 1988.
- SCIENTIFIC PERSONNEL SUPPORTED BY THIS PROJECT AND DEGREES AWARDED 8. DURING THIS REPORTING PERIOD:

D.P. Schrage V.R.P. Jonnalagadda (corrected to J.V.R. Prasad)

School of Aerospace Engineering Georgia Institute of Technology Atlanta, GA 30332-0150

B.H. Tongue

School of Mechanical Engineering Georgia Institute of Technology Atlanta, GA 30332-0405

BRIEF OUTLINE OF RESEARCH FINDINGS

Substantial progress has been made during this period in applying various parameter identification (PID) techniques to the UH-60A Black Hawk Helicopter, using both ARMCOP simulated response and actual flight test data. In addition, several modern control techniques have been developed for usage on the updated UH-60A math model extracted from the simulated response and flight test data. The time domain identification techniques that have proven to be most useful are the Recursive Least Squares and Maximum Likelihood Methods. Results using these PID techniques are being reported in the 7A and 7D papers. Another opportunity to use these PID techniques will be in conjunction with AGARD Flight Mechanics Panel (FMP) Working Group 18 (WG-18), "Rotorcraft System Identification." Georgia Tech is the only university involved in this effort and is receiving flight test data on the AH-64 Apache Helicopter from McDonnell Douglas Helicopter Company (MDHC), on the BO-105 Helicopter from DFVLR, GERMANY, and the Puma Helicopter from RAE, UNITED KINGDOM.

Modern control techniques have been developed along several paths as reported in the 7B presentations and the 7C paper. These techniques along with classical techniques will now be applied and compared using the UH-60A Black Hawk Helicopter model to design a stability and control augmentation system. This research has provided substantive interaction with Army and NASA laboratory personnel at the NASA - Ames Research Center, with the AGARD community, and with the rotorcraft industry. Due to this systems approach to rotorcraft stability and control research, parallel joint research efforts have been established through the NASA - Ames University Consortium, and through industry IRAD Programs. These interactions are extensive and additional material, if desired, can be provided.

(sch.047/2)

A SYSTEMS APPROACH

TO

ROTORCRAFT STABILITY AND CONTROL RESEARCH

FINAL REPORT

AUTHORS: D.P. Schrage J.V.R. Prasad C.M. McKeithan B.H. Tongue P. Fitzsimmons D. Teare

24 October 1988

U.S. ARMY RESEARCH OFFICE CONTRACT DAAL03-86-K-0160

GEORGIA INSTITUTE OF TECHNOLOGY SCHOOL OF AEROSPACE ENGINEERING

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66. NAME OF PERFORMING ORGANIZATION 68. OFFICE SYMBOL School of Aerospace Engineering (# applicable) Georgia Institute of Technology 66. ADDRSSS (Gry, State, and ZiP Code) Atlanta, Georgia, 30332-0150 88. NAME OF FUNDING/ISONSORING ORGANIZATION U. S. Army Research Office 89. OFFICE SYMBOL (# applicable) 80. ADDRSSS (Gry, State, and ZiP Code) Pr. O. Box 12211 Research Triangle Park, NC 27709-2211 80. ADDRSSS (Gry, State, and ZiP Code) Pr. O. Box 12211 Research Triangle Park, NC 27709-2211 80. ADDRSSS (Gry, State, and ZiP Code) Pr. O. Box 12211 Research Triangle Park, NC 27709-2211 80. ADDRSSS (Gry, State, and ZiP Code) Pr. O. Box 12211 Research Triangle Park, NC 27709-2211 81. TITLE (Include Security Classification) A Systems Approach to Rotorcraft Stability and Control Research (Unclassified) 12. PERSONAL AUTHORIS) D. P. Schrage, J. V. R. Prasad, C.M. McKeithan, B. H. Tongue, P. Fitzsimmons, D. Teare 13a. TYPE OF REPORT 13b. THE COVERED ROOMS 15 SUPPLEMENTARY NOTATION The View, Opinions and/or findings contained in this report are those of the author(s) and should not be construed as an official Department of the Army position, policy, or decision, unless so designated by other documentation. 17. COSAIL COOSS 18. SUBSCT TERMS (Continue on reverse if necessary and identify by block number) FIELD GROUP SUB-GROUP SLESSION and Identify by block number) Research Triangle Park, NC 27709-2211 18. DATE OF REDORT (Vear, Month, Day) 19. ABSTRACT (Continue on reverse if necessary and identify by block number) Research Triangle Park, NC 27709-2211 19. ABSTRACT (Continue on reverse if necessary and identify by block number) Research Triangle Park, NC 27709-2211 19. ABSTRACT (Continue on reverse if necessary and identify by block number) 19. ABSTRACT (Continue on reverse if necessary and identify by block number) Research Triangle Park, NC 27709-2211 10. TITLE (Include Security Classification) 10. Decided Park 10. The Security Classification of the Army position, policy or decided and		OCE				
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1. FOREWORD

The overall objective of this research has been to apply a systems approach to rotorcraft stability and control research as illustrated in Figure 1. When this research was first proposed in May 1985, it was becoming more and more evident that this approach was the key to expanding rotary wing aircraft capability through expanded flight envelopes. With respect to basic research areas, two separate sources were utilized to establish the methodology in Figure 1. The first source (Ref. 1) was a document prepared by Mr. David L. Key of the U.S. Army Aeromechanics Laboratory which outlined "Topics for Helicopter Stability and Control Research." The second source (Ref. 2) was the results of an independent assessment of helicopter stability and control for ARO by Dr. Frederick O. Smetana. Both of these source documents have been included in Appendix A of this final report for completeness.

A SYSTEMS APPROACH TO ROTORCRAFT STABILITY AND CONTROL RESEARCH

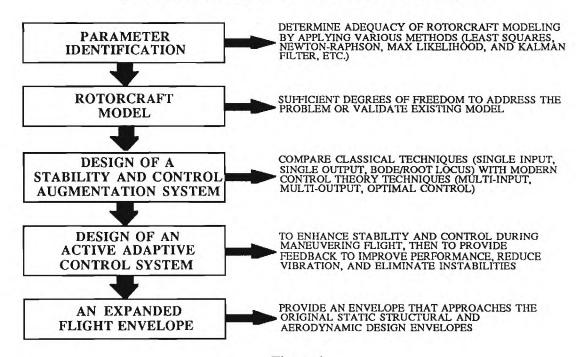


Figure 1

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4. Body of Report

A. Statement of the Problem Studied

Before applying sophisticated modern and active flight control design techniques to rotorcraft, a better understanding of the required mathematical model structure is necessary. Still unanswered questions in rotorcraft stability and control mathematical modeling are the degrees of greedom required in linear models and the proper use of techniques for mathematical model verification and updating from flight test. Therefore, a systems approach to rotorcraft stability and control research is required as illustrated in Figure 1. A systems approach, including parameter identification, rotorcraft modeling, and flight control system design was proposed because these areas address the necessary aspects of stability and control research and are essential to the interaction of the pilot with the vehicle dynamics through the control system. This work was to be accomplished over a three-year period as described in the year-by-year breakout of Statement of Work (SOW) tasks. Unfortunately, this research is being terminated after two years due to ARO funding contraints and the comphrehensive documentation required in the third year will not be accomplished. Considerable progress has been accomplished over the first two years and the research has generated extensive interaction with the U.S. Army, the rotorcraft industry, and NASA. An example of this interaction is provided in Figure 2 which illustrates how this ARO project has generated considerable involvement of the resarchers with other organizations.

The proposed year-by-year breakout of the Statement of Work (SOW) tasks were:

1) Year One:

- Task 1: Obtain UH-60A Black Hawk Helicopter Flight Test Data Base, General Helicopter (GEN HEL) Flight Dynamics Simulation Program, NASA AMES Army Copter (ARMCOP) Flight Simulation program, and install on the GIT computer system.
- <u>Task 2</u>: Use Black Hawk ARMCOP Model and flight test data to estimate stability and control derivatives in hover and cruise speed. Correlate computed response to actual measured response.
- <u>Task 3</u>: Apply parameter identification methods such as least squares, and Modified Newton-Raphson Techniques for the derivative extraction and modify ARMCOP if necessary to meet performance criteria.

2) Year Two:

- <u>Task 1</u>: Develop a stablity augmentation system for the Black Hawk Helicopter using both classical and modern control techniques based on the updated math model extracted from flight test data.
- <u>Task 2</u>: Repeat Task 1 for the design of a control augmentation system. Investigate a direct method for the selection of the weighting matrices to reduce the trial and error required in the analysis.
- <u>Task 3</u>: Generate an adaptive controller from the improved math model to address stability and control effectiveness for varying flight conditions.

3) Year Three:

- <u>Task 1</u>: Investigate nonlinear effects, such as actuator dynamics and control authority, and their impact on the flight control system design.
- <u>Task 2</u>: Include in the flight control system design the provisions for a higher harmonic controller to provide further envelope expansion.
- <u>Task 3</u>: Generate a comprehensive documentation of the methodology used in applying a Systems Approach to Rotorcraft Stability and Control Research and the design of a flight control system.

B. Summary of the Most Important Results

1. Year One:

All three tasks identified were accomplished, although it became clear after extensive investigation that the UH-60A flight test data obtained (Ref. 3) was strongly flawed. The first problem was that no complete documentation was available for the data. The second problem was that the results of preliminary estimation runs indicated physically unrealistic results. The trouble was thought to have been produced by sign convention irregularities and physical units problems. Upon discussion with Sikorsky, the Army, and NASA, these speculations proved to be correct. Similar problems have been found in analyzing flight test data of the AH-64 as part of the AGARD Flight Mechanics Panel (FMP) Working Group (WG) 18 identified in Figure 2. This illustrates the level of immaturity and difficulty in working with rotorcraft flight test data.

Once an understanding of the errors in the UH-60A flight test data was achieved, parameter identification runs were made which indicated a strong variation in the response as a function of noise in the data. In order to address these points, a program was laid out in which a known mathematical model, derived as a reduced order model from the UH-60A ARMCOP model, was used to generate numerical data. This data was then contaminated with a given amount of noise and used in a Recursive Least Squares identification scheme. The model used was a fourth order (longitudinal) one. Results showed that the technique did well in the face of zero noise but poorly for even small amounts of noise.

An Extended Kalman Filter was then implemented to compare to the previous results. This technique showed a strong tendency to diverge and was judged unsuitable for rotorcraft identification purposes at this time. A relatively new technique, the Statistically Linearized Filter, was then utilized. This method worked very well with the zero and small noise cases, but appeared to give incorrect results with moderate noise levels. Finally, the Maximum Likelihood method was investigated to determine its advantages.

The UH-60A ARMCOP model was obtained and used to estimate stability and control derivatives in hover and cruise speed. Correlations of computed response to actual measured response were also obtained. Results of the efforts conducted during the first year have been reported and will be reported in References 4 and 5.

2. Year Two:

Helicopters exhibit undesirable dynamic characteristics due to the strong coupling that exists between longitudinal and lateral modes. In addition to being unstable at hover and low forward flight speeds, the helicopter has significantly different dynamic modal characteristics in hover and low speeds as compared to forward flight. For example, in hover, the body translational motion and pitching motion are decoupled from the heaving motion. Whereas in forward flight, the pitching motion and the vertical motion are strongly coupled. These dissimilar characteristics in hover and forward flight make the piloting technique much more difficult and thus increase the pilot work load resulting in degraded handling qualities. These undesirable characteristics may be substantially reduced by using feedback control for modal decoupling and stability augmentation.

It has been a common practice to use classical techniques such as the root locus technique for the design of helicopter flight control systems. This calls for considerable amount of trial-and-error and experience for a successful design. Because of its time consuming nature, the use of classical techniques, though simple, often result in an

adequate design rather than the best design. Thus, although these techniques have resulted in satisfactory designs in the past, they may not prove adequate for future high performance helicopters. In particular, classical techniques are difficult to use in the design of controllers for systems in which there are several coupled inputs and outputs. However, the use of modern control theory permits the use of multi-variable feedback without much complexity.

There are various methods that are commonly used for multi-variable feedback controller design. A few of the modern control theory techniques that can be used for helicopter flight control system design are

a) Linear Quadratic Regulator Design (LQR)

b) Optimal Output Feedback Design

c) Constrained Optimal Output Feedback Design

d) Model Following

e) Eigenstructure Assignment

All these design procedures except the eigenstructure assignment technique are based on optimal control theory involving the design of the feedback controller based on minimization of a chosen quadratic performance index.

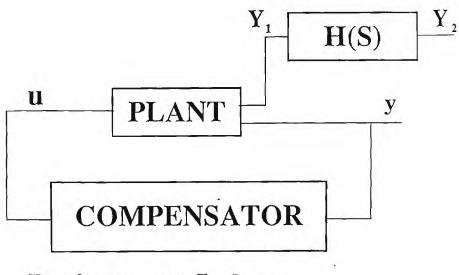
It is well known that Linear Quadratic Regulator (LQR) synthesis methods have guaranteed stability margins in terms of phase and gain margins. Unfortunately, these properties hold only in the case of full state feedback. Observer based compensator design techniques exist to estimate the unavailable plant states, and make the LQR design viable. However, this combination of state estimation and regulation may result in a compensator design with poor stability margins, even though the separate designs are robust. The LQR design for minimum phase plants can be recovered via an asymptotic method called Loop Transfer Recovery (LTR). The LTR method relies on a cheap control formulation with a subset of the compensator dynamics becoming infinitely fast. It is often stated that the order of the compensator can later be reduced by discarding the fast modes; however, it is not clear how this can be accomplished without introducing direct feedthrough of the measured variables. It is generally a good practice to avoid having direct feedthrough of sensor outputs to improve robustness and reduce the effect of sensor noise at high frequency. Aside from robustness issues, the order of the resulting compensator when designed for large order systems may prove unwarranted.

Optimal output feedback design of fixed-order compensators introduced in the early seventies has received limited attention due to numerous difficulties associated with the design approach. Part of the difficulty lies in the fact that the compensator representation initially proposed was overparameterized. That is, the compensator formulation lacked a predefined structure, which invariably results in convergence problems when attempting to numerically optimize the design. Since that time, several people have adopted canonical structure which results in a minimal parameterization. In spite of the simplification achieved through canonical structure of the compensator, the optimal output feedback design approach lacks the ability to characterize the stability margin properties.

As part of the second year effort, the optimal output feedback with fixed order compensator design approach has been investigated for improvements. On the outset, the optimal output feedback design approach is well suited for helicopter flight control system design as compared to other multi-variable feedback control design techniques. This is due to the fact that the output feedback controller is easy to realize in terms of required hardware. Because of very high vibratory environment, only certain states of the helicopter can be measured accurately and inexpensively, e.g., body attitudes, body angular rates. Thus output feedback design approach offers a direct advantage in terms of its ability to

make use of available measurements for feedback. The modifications made to the output feedback design approach as part of this study are presented in the following paragraphs.

One of the major objections to optimal output feedback design are that there are no guarantees on stability margins, and there are few guidelines for penalizing the plant states and compensator states to improve either performance or robustness. In order to address these issues, the use of frequency shaped cost functionals in an optimal output feedback setting was considered based on the work by Mehra (Ref. 6) wherein the concept of frequency shaped cost functionals was first introduced in a full-state feedback design. This method is a result of embedding classical design concepts within LQ optimal design and it is well suited for damping of widely separated structural modes and disturbance rejection over a narrow frequency range. However, in the design approach followed in Ref. 6, the frequency shaper (filter) is part of the feedback controller and it has to be physically realized for actual implementation of the design. Whereas in the present work, the output of the frequency shaper (filter tuned to a particular frequency) is used only in the performance index and hence, the filter need not be realized as part of the compensator (see Figure 3).



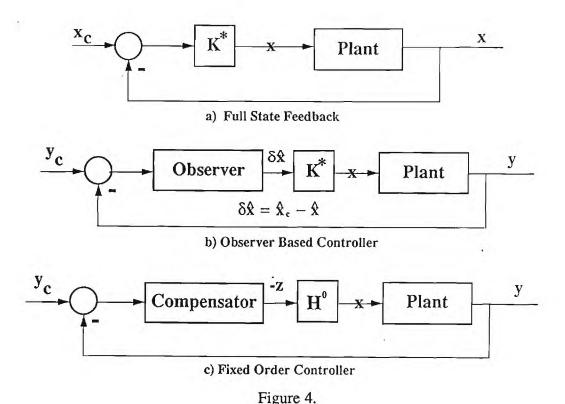
Performance Index:

$$\mathbf{J} = \mathbf{E}_{xo} \left\{ \int \left[\mathbf{y}_{2}^{t} \mathbf{Q} \mathbf{y}_{2} + \mathbf{u}_{c}^{t} \mathbf{R} \mathbf{u}_{c} \right] dt \right\}$$

Figure 3

This method was successfully implemented on two example design problems. The first example deals with helicopter active vibration control (Ref. 7) and the second example deals with improvement of damping of the structural modes (Ref. 8). Though this method is well suited for active control of helicopter vibration, the procedure becomes complicated when this method is used for helicopter flight control system design.

Another way of achieving robustness is the approximate loop transfer recover procedure developed as part of the ARO Center of Excellence for Rotary Wing Aircraft Technology (CERWAT) contract. The full-state and output feedback structures are illustrated in the Figure 4.



The objective in observer-based controller design is to estimate the plant states, and to use the estimated states in place of the actual states. This results in a higher order system where closed-loop eigenvalues and eigenvectors of the full-state design are preserved, and the compensator merely adds its own dynamics to the response. When the compensator is designed based on loop transfer recovery, it is also possible to recover the gain and phase margin properties of the full-state design. This amounts to suitably choosing the weighting matrices in a dual LQR formulation for the observer design. Both full-state and observer design problems are decoupled. In fixed-order compensator design using output feedback, the notion of state estimation is not present. However, it should be recognized that, so long as the loop transfer properties of a full-state design can be recovered to a sufficient degree of accuracy, then the closed loop eigenvalues should contain a set of eigenvalues and eigenvectors that approximate those of the full-state design. Most importantly, the multivariable gain and phase margin properties should also be approximated, With this in mind, consider the loops broken at the points marked x in Figure 4. The loop transfer properties of both loops are nearly equal when the time response of the signals at the the return of the loop are approximately equal for a set of identically chosen input signals, with zero initial conditions on all states in the two feedback systems. This recovery procedure can be viewed as a rationale for properly selecting the plant and compensator state weighting, and the initial condition distribution matrix. This design procedure was successfully used in the design of a tight attitude control system for the Sikorsky S-61 helicopter in hover flight condition (Ref. 9). Also, the same design approach is used for the Black Hawk helicopter flight control system design in satisfying the updated helicopter handling qualities specifications and the results will be presented at the upcoming International Conference on Helicopter Handling Qualities (Ref. 10).

Also, as part of this study, the approximate loop transfer recovery procedure described in the previous paragraph is implemented in a two-time scale controller design and the results are submitted for publication to the ASME Journal of Dynamic Systems (Ref. 11). The two-time scale controller design is particularly well suited for active control of rotor dynamic characteristics. In this method, the overall design is simplified in terms of design of a slow controller for slow dynamics and a fast controller for the fast dynamics. The procedure of designing individual controllers becomes decoupled when the fast subsytem design is carried out with certain constraints placed on it and the composite controller is obtained by adding the fast controller and the slow controller.

Based on the results obtained as part of this study, it is concluded that optimal output feedback approach offers a great potential in the design of very tight controllers for envelope expansion and hence, this design procedure is very useful in designing flight control systems for future high performance rotorcraft.

C. List of All Publications Produced under this Research Contract

- 1) Fitzsimons, P.M., Teare, D., Prasad, J.V.R., Schrage, D.P. and Tongue, B.H., "Some Basic Issues in Helicopter System Identification," presented at the 2nd International Conference on Basic Rotorcraft Research, University of Maryland, February 16-18, 1988.
- 2) The following presentations were made at <u>The Second Technical Workshop on Dynamics and Aeroelastic Stability Modeling of Rotorcraft Systems</u>, Sponsored by the ARO and Florida Atlantic University in Boca Raton, Florida, on November 18-20, 1987:
 - a) Calise, A.J. and Jonnalagadda, V.R.P., "Compensator Based Controller Design for Helicopters," Georgia Institute of Technology.
 - b) Schrage, D.P., Oakes, G., and Jonnalagadda, V.R.P., "Development of an Individual Blade Control Computer Analysis," Georgia Institute of Technology.
 - c) Schrage, D.P., Jonnalagadda, V.R.P., and Wasikowski, M.E., "Active Vibration Control Using Reduced Order Models," Georgia Institute of Technology.
- 3) Calise, A.J. and Prasad, J.V.R., "An Approximate Loop Transfer Recovery Method for Designing Fixed-Order Compensators," Presented at the <u>AIAA Guidance</u>, Navigation and Control Conference, August 1988.
- 4) Schrage, D.P., Tongue, B.H., Prasad, J.V.R., Fitzsimons, P.M., and Teare, D., "Time Domain Parameter Identification Techniques Applied to the UH-60A Black Hawk Helicopter Flight Test Data," Paper to be included in special edition of Vertica Magazine on Helicopter System Identification, December 1988. (Abstract in Appendix B)

- 5) Prasad, J.V.R. and Schrage, D.P., "Comparison of Helicopter Flight Control System Design Techniques," to be presented at the International Conference on Helicopter Handling Qualities and Control, London, England, November 16, 1988. (Abstract in Appendix B)
- 6) Calise, A.J., and Prasad, J.V.R., "Fixed-order Compensator Design Based on Frequency Shaped Cost Functionals," to appear in the <u>Journal of Guidance and Control</u>.
- 7) Siciliano, B., Calise, A.J. and Prasad, J.V.R., "Two-Time Scale Stabilization of a Flexible ???? with Output Feedback," submitted for publication to the ASME Journal of Dynamic Systems, Measurement and Control, 1988.

D. List of All Participating Scientific Personnel

<u>Name</u>	Organization	Advanced Degree Earned
D. P. Schrage	School of Aerospace Engineering	N/A
J.V. R. Prasad	School of Aerospace Engineering	N/A
B.H. Tongue	School of Mechanical Engineering	N/A
P.M. Fitzsimmons	School of Mechanical Engineering	N/A
D. Teare	School of Mechanical Engineering	M.S., March 1988

5. References

The following are publications referenced in the body of this report:

- Key, D.L., Memorandum for Record, 26 November 1984, Subject: <u>Topics for Helicopter Stability and Control Research</u>, Aeromechanics Laboratory, U.S. Army Research and Technology Laboratories AVSCOM, Ames Research Center, Moffett Field, CA 94035
- 2. Smetana, F.O., Letter, received 24 September 1984, Subject: <u>Helicopter Stability and Control Research Needs</u>, Engineering Sciences Division, U.S. Army Research Office
- 3. Abbott, W.Y., et al., USAAEFA Project No. 79-24, <u>Validation Flight Test of UH-60A for Rotorcraft Systems Integration Simulator (RSIS)</u>, September 1982
- 4. Fitzsimons, P.M., Teare, D., Prasad, J.V.R., Schrage, D.P. and Tongue, B.H., "Some Basic Issues in Helicopter System Identification," presented at the 2nd International Conference on Basic Rotorcraft Research, University of Maryland, February 16-18, 1988.
- Schrage, D.P., Tongue, B.H., Prasad, J.V.R., Fitzsimons, P.M., and Teare, D., "Time Domain Parameter Identification Techniques Applied to the UH-60A Black Hawk Helicopter Flight Test Data," Paper to be included in special edition of <u>Vertica</u> Magazine on Helicopter System Identification, December 1988.
- 6. Gupta, N.K., "Frequency-Shaped Cost Functionals: Extension of Linear Quadratic-Gaussian Methods," <u>Journal of Guidance and Control</u>, Vol. 3, Nov.-Dec., 1980, pp. 529-535.
- 7. Schrage, D.P., Jonnalagadda, V.R.P., and Wasikowski, M.E., "Active Vibration Control Using Reduced Order Models," presented at Technical Workshop on Dynamics and Aeroelastic Stability Modeling of Rotorcraft Systems, Sponsored by the ARO and Florida Atlantic University in Boca Raton, Florida, on November 18-20, 1987.
- 8. Calise, A.J., and Prasad, J.V.R., "Fixed-order Compensator Design Based on Frequency Shaped Cost Functionals," to appear in the <u>Journal of Guidance and Control</u>.
- 9. Calise, A.J. and Prasad, J.V.R., "An Approximate Loop Transfer Recovery Method for Designing Fixed-Order Compensators," Presented at the <u>AIAA Guidance, Navigation and Control Conference</u>, August 1988.
- 10. Prasad, J.V.R. and Schrage, D.P., "Comparison of Helicopter Flight Control System Design Techniques," to be presented at the International Conference on Helicopter Handling Qualities and Control, London, England, November 16, 1988. (Abstract in Appendix B)

11. Siciliano, B., Calise, A.J. and Prasad, J.V.R., "Two-Time Scale Stabilization of a Flexible Arm with Output Feedback," submitted for publication to the ASME <u>Journal of Dynamic Systems</u>, <u>Measurement and Control</u>, 1988.

6. Appendicies

Appendix A. Source Documentation on Rotorcraft Documentation of Rotorcraft Stability and Control Research Needs

Appendix B. Abstracts for Forthcoming Publications



DEPARTMENT OF THE ARMY AEROMECHANICS LABORATORY US ARMY RESEARCH & TECHNOLOGY LABORATORIES-AVSCOM AMES RESEARCH CENTER MOFFETT FIELD, CALIFORNIA 94035

SAVDL-AL-C

26 November 1984

MEMORANDUM FOR RECORD

SUBJECT: Topics for Helicopter Stability and Control Research

1. The ongoing efforts at the Aeromechanics Laboratory in stability, control, handling qualities and pilot aircraft interface are generally at the 6.2 Exploratory Development level and involve use of sophisticated experimental facilities. However, there are many topics related to this program that could be considered 6.1 Basic Research that are essentially analytical and require primarily computational support; such topics could usefully be addressed by universities and small analytical research companies and perhaps supported through the U.S. Army Research Office. The following is a brief listing of some such topics:

a. Rotorcraft Modeling

- (1) The degrees of freedom required in linear models.
- (2) Techniques for math model verification and updating from flight test.

b. Modern Control Theory Applications

(1) Use of optimal and modal control law implementation approaches, i.e., both time and frequency domain approaches. We particularly need to assess methods that can minimize feedback gain levels.

c. Digital Flight Control System Effects

- (1) Study the effects of digital computation delays and interaction with rotor and structural dynamics on the performance of high-gain digital flight control systems.
- (2) Methods for direct digital design—rather than converting from continuous system designs.

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e. Active Control Applications

• (1) Techniques for applying active horizontal stabilizer, higher harmonic control, integration of the propulsion and flight control system, and relaxed static stability configurations.

f. Real-Time Expert Systems Development

(1) Applications of expert systems to flight path management, could include functions such as automation of NOE navigation, terrain avoidance, terrain following, threat avoidance, failure sensing and recovery.

g. Simulation Technology

- (1) Quantification of visual and motion cue effects.
- (2) Math modeling techniques to minimize computation times.
- (3) Air combat simulation requirements.

h. Effects of Outside Visual Cue Quality

(1) Relate the characteristics of both outside visual scene and sensor/display quality to human perceptual capabilities and flight path control limitations.

i. Turbulence Model

(1) There is a need for development of a low-altitude turbulence model for incorporation into the updated handling qualities Spec 8501.

j. Maneuvering Envelope Limiting and Cueing

(1) Need to understand fundamental envelope maneuver limitations and how these can be cued to the pilot to inhibit him from violating these limits but allowing him to exceed them in emergency situations.

k. Energy Management Techniques

(1) Apply optimization methods to air combat, autorotation, and engine-out operations.

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1. Interactional Aerodynamics

- (1) Better techniques for developing stability and control predictions especially applied to empennage design.
- 2. If further explanation or discussion of potential responses to these topics is required, please contact the undersigned (415) 694-5839 or Ed Aiken (415) 694-5362.

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CHELICOPTER STABILITY AND CONTROL RESEARCH NEEDS

by
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Engineering Sciences Division
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COPY TO:

I. Introduction

The Army Research Office currently supports no research directed specifically toward improved methods for controlling the response of a helicopter to pilot commands or gust excitations. Given this knowledge, members of the Army research community have expressed concern that new helicopter designs will place such severe demands on the pilot for flight path management that he will be unable to carry out his mission successfully. These researchers are further concerned that the technology base for alleviating these demands on the pilot does not now appear to exist within the Army laboratories or its helicopter contractors. The writer was asked to investigate the situation and to recommend a suitable research program in the event that these concerns were justified.

Visits were made to the Aeromechanics Laboratory and to Bell, Vertol, and Sikorsky to attempt to obtain a feel for the level of technical sophistication available or in use at these installations and for the management philosophy regarding the employment of sophisticated technology. The Aeromechanics Laboratory has a major program underway to procure an integrated collection of computer programs which calculate such things as vehicle aerodynamics, structural dynamics, flight dynamics, and performance given the vehicle configuration, power plant, and structural layout. The design for the executive program of the collection has been fixed and the desired capabilities of most of the modules in the collection seem to have been established. The writer received the impression that these modules would be provided with numerous switches to enable various options. The sophisticated user would be able to vary the complexity of the calculations considerably to permit a variety of accuracy/cost needs to be satisified. It will, however, require someone with a good feeling for what is needed in a particular circumstance to take advantage of these features.

The basic technological sophistication of the individual modules seems to be restricted by two considerations: (1) a recognition that each module is part of a larger whole and must run in a reasonable period of time, and (2) the methods programmed must be well-accepted. This effectively locks them to the present state of helicopter aerodynamic computation and control system technology. However, because of the modular design of the overall program, individual sections can be replaced as more effective methods become available.

Perhaps because the helicopter is a more complex flying machine than are fixed-wing craft, engineers in the helicopter industry have tended to use empirical data correlations and cut-and-try approaches more than have engineers in the fixed-wing industry. As a result, they appear, on the basis of the writers' interviews, to be less well-informed on the subtleties of new analysis methods and less able to take advantage of them than are their brothers in the fixed-wing industry. The cash flow generated by current low

production rates in the helicopter industry may also have something to do with this situation though it appears to be a result of a long-term mindset.

The writer did not attempt to compare the requirements of an LHX mission with currently available technology to determine the extent to which concerns voiced by Army laboratory personnel are valid. He observes only that the following situation exists:

- (1) The helicopter industry is generally behind the fixed-wing industry in the employment of sophisticated aerodynamics and flight control analysis tools.
- (2) Mission success is inversely related to the severity and complexity of pilot workload.
- (3) Current helicopters are more demanding and less forgiving of errors than current fixed-wing craft.

Given this situation, a research program such as that described below is justified. Sections II and III provide some additional detail on the relationship between five suggested research tasks outlined in Section IV and current practice in aerodynamics and control system design.

II. Aerodynamics

The determination of the motion of a helicopter as a result of a control input or excitation by a gust requires a knowledge of the aerodynamic forces acting on the craft during its response. For fixed-wing aircraft undergoing relatively small displacements from equilibrium, these forces are usually represented by the first terms of Taylor series expansions in the linear and angular velocity components of the vehicle motion, accelerations, and aerodynamic and/or inertial angles, e.g.,

$$\mathsf{L} = \mathsf{L}_0 + \frac{\partial \mathsf{U}}{\partial \mathsf{L}} \left(\mathsf{U}_1 - \mathsf{U}_0 \right) + \frac{\partial \mathsf{U}}{\partial \mathsf{L}} \left(\mathsf{v}_1 - \mathsf{v}_0 \right) + \frac{\partial \mathsf{W}}{\partial \mathsf{L}} \left(\mathsf{w}_1 - \mathsf{w}_0 \right) + \frac{\partial \mathsf{L}}{\partial \mathsf{L}} \left(\mathsf{q}_1 - \mathsf{q}_0 \right) + \cdots$$

The partial derivatives in such expressions are taken to be constants and must be evaluated a priori from wind tunnel or flight test data or by suitable theoretical computation. The more accurately these values are known, the more accurately the vehicle motion can be determined and the more easily the need for installing or retaining non-linear terms in the equations of motion can be ascertained.

Conversations with engineers in the helicopter manufacturing industry have revealed that their knowledge of the values of these "stability derivatives" for specific configurations is relatively crude or even non-existent, particularly when the vehicle is in vertical or sidewise motion. There apparently has not yet been a concentrated national effort (as there was for fixedwing vehicles) to develop a comprehensive and generally-accepted set of evaluation procedures for these derivative values. It would appear that development of at least some of these procedures must await the results of tests now being conducted or planned for the near future and the completion of large computer codes which are capable of accurately modeling rotor-fuselage

interactions, rotor-tail rotor interactions, and fuselage wakes in vertical and sidewise motion. While the knowledge to prepare such codes is thought to exist, they apparently have not as yet been contracted for.

III. Flight Dynamics and Control System Design

Oral queries of engineers in the helicopter manufacturing industry have led the writer to the conclusion that current flight path management and mission management systems do not take full advantage of modern digital control design methodology and hardware implementation or of recent research results on means of reducing the pilot workload and enhancing his performance. It is the writer's impression that current design methodology proceeds more or less along the following path:

- 1. Review design requirements; formulate an optimal control problem which models the proposed system in a fairly crude fashion; solve this problem to determine control laws which offer the better opportunities to produce the desired result.
- 2. Model the vehicle plus the proposed control laws in a linear fashion; using classical linear control theory, perform design analyses to estimate the system gains required.
- 3. Construct actual system hardware; connect to simulator of vehicle; adjust system gains or modify control laws to give desired result.
- 4. Fine tune control system gains or modify control laws as a result of flight tests.

There is considerable cut-and-try to this process that probably achieves suboptimal results in a longer-than-necessary time span.

IV. Research Needs

- (1) Determination of Aerodynamic Stability Derivative Values. A two-phase research effort is envisioned to provide more accurate aerodynamic data for use in flight path determinations: (a) Comprehensive, rigorous analysis of the flow field around specific, complete helicopter configurations in (i) hover, (ii) forward flight—at both low and high advance ratios, (iii) vertical flight, (iv) sidewise flight, and (v) rearward flight leading to determinations of the lift, drag, side force, pitching moment, rolling moment, and yawing moment as functions of angle of attack, angle of sideslip, pitch angle, yaw angle, roll angle, flight path velocity, rotor RPM, cyclic pitch, collective pitch, tail rotor RPM, and their first and possibly second derivatives with respect to time. (b) Correlation of the foregoing theoretical results with wind tunnel and flight results to develop simplified—possibly semiempirical—methods to predict the values of all significant derivatives, these methods to be suitable for preliminary design and some detail design in the manner of the DATCOM for fixed wing aircraft.
- (2) Develop the Control Laws, Control Means, and Sensor Requirements for Decoupling the Three Components of Linear Velocity as well as the Three Components of Vehicle Attitude. Much of the pilot workload in flight path management is as a result of the need to coordinate the various controls avail-

able to him. Decoupling removes the need for such coordination and frees the pilot to undertake mission management functions. An integral part of the control law and associated display development should be a consideration of the requirements and abilities of the pilot. A second phase of the investigation should be a handling qualities evaluation (and refinement if necessary) of the resulting control laws and displays in a simulator.

- (3) Determine the Effects of an Elastic Vehicle Structure on the Performance of a High-Gain Flight Path Management System and Methods to Suppress Undesirable Coupling. A simulator study of which coupling effects are undesirable also seems indicated.
- (4) Determine the Most Suitable Applications for Digital Control Technology to Helicopters. Considerations in this study should include availability of suitable hardware or its potential for development and any improvements in handling qualities which can be anticipated from the implementation of digital control technology. Suitable should be interpreted in terms of size, weight, cost, reliability, and maintainability.
- (5) Determine a Proper Role for "Modern Control" Analysis in Helicopter Control Systems Design. The modern control approach seeks to maximize or minimize some performance function by varying the gains in the vehicle control laws. Classical approaches consider the various control loops separately and seek only to vary the gains sufficiently to satisfy preset specifications. By choosing weights in the performance function or adding additional terms to it, considerations of size, cost, and accuracy can be included in the global maximization or minimization. Construction of a suitable performance criterion, however, is perhaps still an art. A study of how one should proceed to do this in a systematic way would be very much in order.

The foregoing research needs can be investigated in parallel efforts. Task #1 is by far the most difficult, requiring perhaps three times the effort of one of the others. Tasks 2 and 3 should be conducted in-conjunction with an existing simulator to save time and money.

It is probable that satisfactory results can be obtained from tasks 4 and 5 over a 3-year period at a level of about \$115,000/year each. Tasks 2 and 3 can be anticipated to require the same resources exclusive of the costs associated with the operation of the simulator.

Task 1, which should be given the highest priority, can be expected to require funding at the level of \$180,000/year for five to six years.

Appendix B Abstracts of Papers to be Presented

Time Domain Parameter IdentificationTechniques Applied to the UH-60A Black Hawk Helicopter

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Abstract

This study is directed towards the modeling and system identification of rotorcraft. The assumed models are Linear Time Invariant (LTI) perturbation models about the helicopters "trimmed" flight condition. Parameter identification is applied to the assumed models using flight test data from Sikorsky's UH-60A Black Hawk Helicopter. The parameter identification techniques used are Least-Squares and Maximum-Likelihood. The "trimmed" flight conditions are forward flight at 100 knots and hover.

Comparison of Helicopter Flight Control System Design Techniques

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Abstract

The revised handling quality specifications (ADS 33) will have an impact on the techniques used for helicopter flgiht control system design. Traditionally, classical control methods have been used in the determination of the control law and a matrix of control gains involving a trial and error application of analysis procedures until the presified performance criteria are satisfies. The prodedures are larely a graphical portrayal of Bode, Nyquist, and root locus techniques for the analysis of open loop and closed loop systems. In modern control theory, synthesis of a flight control system proceeds more directly than in classical control theory. It allows the designer more freedom to work directly with the system eigenvalues and eigenvectors. Of course, an iterative procedure must still be performed to meet specified time domain specifications. The advantages of optimal control theory are substantial since a stable, multiple-input/multiple-output flight control system can be designed directly in an optimal sense with relatively small manpower investigations. This means a particular component of the response can be treated without aggravating other

responses such as those associated with handling qualities and vibration. One of the disadvantages of optimal control methods is that it is difficult, in a stable numerical sense, to enforce state, control, and measurement constraints except by a trial and error method involving state and control weighting matrices Q and R. Also, it is not generally possible to enforce relative stability, in terms of frequency domain stability margins, even though the system is guaranteed stable in an absolute sense. An additional disadvantage for rotorcraft applications is that all the states need in the control law development are not measureable, resulting in added complexity in the control system. Though the optimal output feedback with compensator design technique reduces this added complexity somewhat, the design procedure involves the solution of a set of nonlinear equations for control law development, resulting in nonuniqueness of the solution. Thus it can be seen that there a advantages an disadvantages with both classical and modern control design methods and that a hybrid method if probably the acceptable alternative. In order to gain insight into how the two types of methods might be combined in flight control system design, this paper deals with the design of a flight control system for the UH-60 Black Hawk helicopter using both classical and modern control theory techniques. These designs are aimed at satisfying certain criteria taken from the revised handling quality specifications. The resulting designs are compared in terms of hardware realization and complexity in the design process and recommendations are made for a unified design approach.