



# Institute of Paper Science and Technology

## PROGRESS REPORT ON FURNISH EVALUATIONS FOR IMPULSE DRYING COMMERCIALIZATION DEMONSTRATION

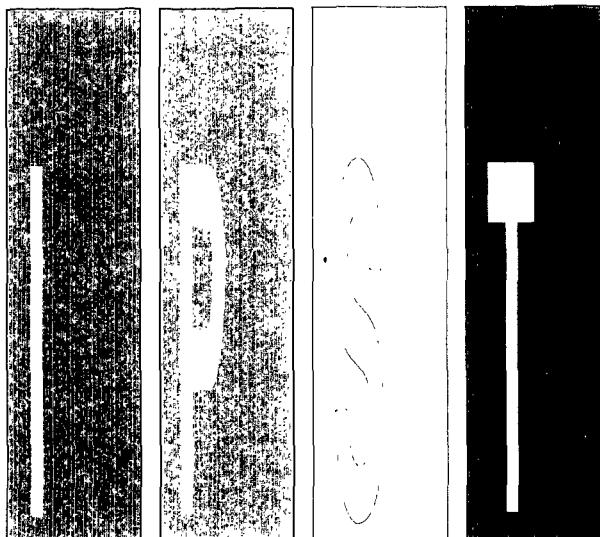
Project 3595

Report 11

to the

MEMBER COMPANIES OF THE INSTITUTE OF PAPER SCIENCE AND TECHNOLOGY

February 1995



Atlanta, Georgia

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INSTITUTE OF PAPER SCIENCE AND TECHNOLOGY

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PROGRESS REPORT ON FURNISH EVALUATIONS FOR IMPULSE DRYING  
COMMERCIALIZATION DEMONSTRATION

Project 3595

Report 11

A Progress Report

to the

MEMBER COMPANIES OF THE INSTITUTE OF PAPER SCIENCE AND TECHNOLOGY

By

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## SUMMARY

Laboratory- and pilot-scale experiments were performed in cooperation with Beloit Corporation and Union Camp Corporation to identify potential furnishes and operating parameters for upcoming high-speed pilot-scale trials and commercial demonstration of impulse drying. These initial experiments focused on determining the relationship between water permeability, refining, and prepressing for specific pulps. Also, mill refined pulp and machine paper were compared to laboratory samples in regards to water permeability and impulse drying performance.

Results indicate that hydrodynamic specific surface is highly dependent on sheet formation and prehandling. Without extreme care in sheet preparation, the permeability test results are highly variable. However, the trends indicate that minimum refining and prepressing as much as possible are necessary to lower the specific surface to the range ( $1-2 \text{ m}^2/\text{g}$ ) necessary for maximum impulse drying efficiency.

Mill refined pulp and machine paper were comparable to laboratory prepared samples in regards to permeability and impulse drying. Impulse drying results in an outgoing solids improvement of up to eight percentage points compared to double-felted pressing. STFI index values showed an increase of up to 3.5% over double-felted pressing. These results were achieved with ingoing solids of 40-42%. At ingoing solids of 35%, impulse drying showed less improvement compared to double-felted pressing, indicating that an impulse dryer should be in the third or fourth press position for maximum efficiency. Ring crush improved 15% over double-felted pressing for the more open furnish, but double-felted pressing produced higher ring crush results for the closed furnish. For all cases impulse drying significantly decreased (up to 56%) Bendtsen roughness compared to double-felted pressing. Comparisons between Beloit and IPST results indicate consistent trends with IPST results being the most conservative.

Other process variables such as platen surface coating, felt type, felt moisture, and prestreaming temperature profiles were investigated. In the laboratory simulations, high felt moisture (>32%) with the R felt resulted in excessive rewet and significant reduction in water removal. The laboratory equipment was not able to obtain prestreaming temperature profiles comparable to machine conditions. Observations indicate that platen surface and felt type have an effect on water removal, sheet physical properties, rewet, and sheet sticking. Because of tradeoffs between these properties and others, the data obtained in these experiments were not sufficient to specify optimum process parameters.

These experiments used furnishes that simulated present commercial furnishes and a conservative nip load. Therefore, the water removal and strength improvements are less than what can potentially be achieved, yet substantial improvement in sheet smoothness was achieved. Maximum commercial nip loads are limited by present engineering constraints, but the top ply hydrodynamic specific surface could be substantially lowered to further improve impulse drying performance.

## INTRODUCTION

Ongoing laboratory- and pilot-scale research at the Institute of Paper Science and Technology (IPST) has demonstrated that heavy weight grades of paper, such as linerboard, can be successfully impulse dried [1-21]. That research has shown that deleterious sheet delamination can be avoided by a combination of processing strategies. These strategies include steps to make the prepressed sheets highly permeable to water flow and steps to reduce excess heat transfer to the sheet that results in excessive internal flash evaporation at the exit of the impulse dryer.

Research at IPST suggests that high sheet Darcian permeability (low hydrodynamic specific surface) can be obtained by limiting refining to the minimum required for product aesthetics and by prepressing the sheet to as high a solids as possible. In addition, IPST research suggests that excessive pressure-dependent heat transfer can be eliminated by using press roll surfaces composed of materials having low thermal conductivity, low heat capacity, and low density.

Laboratory-scale experiments have been conducted with virgin Southern Pine, Douglas Fir, and OCC [1,2,4,6]. Two-ply sheets made from combinations of the above furnishes, at different levels of specific surface, have also been used. Both virgin furnishes have been successfully impulse dried in the laboratory. OCC performed best in regards to moisture removal and strength development when blended with a virgin kraft at concentrations of 50% or less by weight.

Pilot-scale experiments using a sheet-fed shoe press confirmed the laboratory-scale results [3,7]. The impulse drying critical temperature depends on the thermal properties of the roll coating and the specific surface of the heated ply of the sheet. Impulse drying was shown to be superior to single- and double-felted pressing in water removal and important physical properties. Both single-ply and two-ply sheets were successfully impulse dried.

## **RESEARCH OBJECTIVES**

The overall objective of the work reported was to identify potential furnish types and operating windows to be used during the upcoming pilot-scale trials and commercial demonstration of impulse drying. To meet this objective, initial work was performed to meet the following specific objectives.

- Compare mill-refined pulp and machine paper to laboratory-refined pulp and handsheets in regards to water permeability and impulse drying performance.
- Determine the relationship between permeability, prepressing, and refining for specific pulps.
- Refine laboratory-scale operating parameters to better simulate commercial machine conditions.

## EXPERIMENTAL PLANS AND PROCEDURES

This experimental program was a cooperative effort between Union Camp Corporation, Beloit Corporation, and IPST. Union Camp provided the pulp and prepared the handsheets for testing. Beloit prepressed the handsheets and performed some of the physical testing. IPST performed the permeability tests, impulse dried selected furnishes on the MTS laboratory press, and performed the ultrasonic testing. Beloit also performed MTS and pilot-scale impulse drying tests.

For machine linerboard samples, couch trim was grabbed from commercial Union Camp linerboard machines and sealed in plastic bags for transport. The couch trim samples were prepressed to 35% solids prior to testing.

The first set of furnishes evaluated was chosen to simulate present mill furnishes and is described in Table 1. All of these furnishes were made into handsheets for testing. Furnishes W1 and W5 were impulse dried. The remaining furnishes were used for permeability testing.

Table 1. Handsheet furnishes received for impulse drying evaluation.

IPST ID No.	U. C. ID No.	Top Sheet	Bottom Sheet	Nominal Basis Weight <sup>a</sup> (g/m <sup>2</sup> )	Nominal Sheet Solids (%)	No. of Sheets Recv'd
W1	2P1	15% mill refined 4705-35-D, 260 ml CSF	85% mill refined 4705-35-E, 660 ml CSF	190	35 42	25 28
W2	1P1	none	100% mill refined 4705-35-E, 660 ml CSF	190	35 42	4 4
W3	1P2	100% mill refined 4705-35-D, 260 ml CSF	none	190	35 40	4 4
W4	2P2	15% valley beaten 4705-35-B, 650 ml CSF	85% mill refined 4705-35-E, 660 ml CSF	190		none
W5	2P3	15% valley beaten 4705-35-B, 650 ml CSF	85% valley beaten 4705-35-C, 640 ml CSF	190	35 42	25 25
W6	1P3	none	100% valley beaten 4705-35-C, 640 ml CSF	190	35 42	4 4
W7	1P4	100% valley beaten 4705-35-B, 650 ml CSF	none	190	35 42	4 4
W8	1P5	100% valley beaten Hard Wood, 650 ml CSF	none	190	35 42	8 8

a) Basis Weight is nominal oven-dried value based on 42# sheets at 7.5% moisture.

b) Cases W1 through W7 are a mixture of hardwood and pine.

For each furnish to be impulse dried, the following matrix of conditions was used.

Table 2. Impulse drying experimental matrix.

Case	D1	D2	D3	D4	A1	A2	C1	C2	A3	A4	C3	C4
Config.	DF	DF	DF	DF	ID							
Felt Type	B	B	R	R	B	B	B	B	R	R	R	R
Pivot Position	0	0	0	0	0	0	0	0	0	0	0	0
Platen Surface	n/a	n/a	n/a	n/a	A	A	C	C	A	A	C	C
Press Impulse (MPa·s)	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14
no. of temps	n/a	n/a	n/a	n/a	a.n.							
Sin, %	35	42	35	42	35	42	35	42	35	42	35	42
repeats	10	10	10	10	a.n.							

a) Ingoing Sheet Temperature

Impulse Drying = ~65°C (150°F)

Double-felted Pressing = Ambient

b) Ingoing Felt Moisture = 16% (0.2 mr)

c) a.n. = as needed.

A second set of experiments was performed to characterize the relationship of hydrodynamic specific surface to refining level and prepressing. The furnishes used are listed in Table 3.

Table 3. Furnishes used for permeability study.

IPST ID No.	U. C. ID No.	Pulp Type	Freeness (ml)
W9	1P10	100% Hardwood	691
W10	1P11	100% Pine, 93.0 Kappa	754
W11	1P12	50% Hardwood 50% Pine	707 761
W12	1P13	100% Pine	665
W15	1P14	100% Hardwood	670
W16	1P15	100% Hardwood	650
W17	1P16	100% Hardwood	630
W18	1P17	100% Pine	700
W19	1P18	100% Pine	620
W20	1P19	50% Hardwood 50% Pine	670 700
W21	1P20	50% Hardwood 50% Pine	650 660
W22	1P21	50% Hardwood 50% Pine	630 620

Each furnish was prepressed by Beloit as shown in Table 4, except as noted below. For case P1, furnishes W15-W17 and W22 were crushed resulting in questionable or lost samples. For case P2, furnishes W16, W17, and W22 were again crushed; furnish W15 was pressed at 300 and 800 pli. For cases P3-P5 and furnishes W15-W17 and W22, the first pressing was reduced to 300 pli. A few sheets were still crushed, and the data obtained from them were scrutinized.

Table 4. Pressing conditions.

Pressing Case	Roll Nip Pressures (pli)	DF ENP Pressures (pli)	Total Impulse (psi-s)
P1	800	n/a	2.42
P2	500+800	n/a	3.94
P3	500+800+1200	n/a	7.58
P4	500+800	6000	22.12
P5	800	6000+6000	38.78

a) Machine speed = 1650 fpm.

The water permeability tests were performed using procedures previously documented [24]. Compressive loads used were in the range of 200 to 650 lb.-force. Water pressure in the range of 2 to 15 psi was used to ensure flow rates in the range of 0.5 to 30 g/min.

The question was raised about whether the sheet temperature profile was constant in the z-direction during steaming. We embedded thermocouples in a sheet by pressing multiple thin layers ( $65 \text{ g/m}^2$ ) together with thermocouples between the layers. Top and bottom thermocouples were added to give a total of four measurements through the sheet. Table 5 lists the furnishes prepared with thermocouples.

Table 5. Multilayer sheets with thermocouples between the layers.

IPST ID No.	Ply	U. C. ID No.	Pulp Type	Freeness (ml)
W13	Top	1P6	100% Hardwood	691
	Middle & Bottom	1P7 & 1P9	100% Pine, 93.0 Kappa	659
W14	Top	1P8	100% Hardwood	297
	Middle & Bottom	1P7 & 1P9	100% Pine	659

## RESULTS

### FIBER ANALYSIS

For each furnish used for the refining study, samples from the prepared sheets were sent to John D. Hankey & Associates for fiber analysis. The results of the fiber identification are shown in Table 6. Table 7 summarizes the average fiber dimensions.

**Table 6. Fiber identification for various pulp samples.**

Furnish ID IPST		USWK U. C.	UHWK (%)	Softwood Species			Hardwood Species	
W9	1P10	2	98	Mixed species of southern yellow pine (Hard Cook)			Oak, Gum, Yellow Poplar, Maple, and trace amounts of other mixed species	
W10	1P11	97	3	Mixed species of southern yellow pine (Hard Cook)			Mixed, incl. Oak, Gum, Yellow Poplar, and Maple	

**Table 7. Fiber dimensions.**

Case	Pulp	Kappa No.	Freeness (ml CSF)	Length (mm)			Width (µm)	Perimeter (µm)	Cell Wall Thickness (µm)	Coarseness (mg/100 m)
				Arith	LW	WW				
W10	Pine	93.0	754	2.36	3.28	3.86	34.3	82.6	3.5	41.0
W18	Pine	93.0	700	2.44	3.21	3.78	34.6	85.2	4.0	35.8
W12	Pine	93.0	665	2.55	3.29	3.87	35.9	85.0	3.3	35.4
W19	Pine	93.0	620	2.19	2.92	3.46	36.2	85.2	3.2	35.2
W9	Hard	-	691	1.20	1.41	1.57	16.8	45.6	3.0	17.4
W15	Hard	-	670	1.47	1.33	1.47	16.9	46.2	3.1	15.8
W16	Hard	-	650	1.22	1.41	1.58	16.4	45.2	3.1	16.4
W17	Hard	-	630	1.17	1.32	1.43	16.0	44.4	3.1	16.2
W11	Mix	-	734	1.52	2.13	2.97	21.1	58.6	3.6	25.2
W20	Mix	-	685	1.55	2.19	3.01	23.8	60.0	3.1	21.6
W21	Mix	-	655	1.36	1.81	2.37	21.9	57.0	3.3	21.0
W22	Mix	-	625	1.44	2.15	3.11	22.8	58.0	3.1	21.2

### PERMEABILITY

All of the raw permeability data are summarized in Appendix D as permeability versus porosity plots.

#### Couch Trim Sample Set

The permeability data collected for the couch trim samples are summarized in Table 8. Some of the sheets were manually separated at the ply bond and each ply tested.

Table 8. Permeability results for the couch trim samples.

Furnish	Sheet Solids (%)	95% Conf. Interval	OD Basis Weight (g/m <sup>2</sup> )	95% Conf. Interval	Specific Surface (m <sup>2</sup> /g)	95% Conf. Interval	Specific Volume (cm <sup>3</sup> /g)	95% Conf. Interval
Mill #1	36.7	1.6	180	3	5.0	1.2	1.7	0.3
Mill #1 Top Ply	-	-	-	-	15.8	6.0	3.1	0.4
Mill #1 Bottom Ply	-	-	-	-	16.3	8.2	2.95	0.2
Mill #2	25.0	0.3	141	4	5.3	1.6	2.0	0.5
Mill #2 Top Ply	-	-	-	-	4.8	4.2	7.2	3.2
Mill #2 Bottom Ply	-	-	-	-	2.5	1.6	4.3	0.4

It was determined that the permeability test equipment was not working properly (note the large values for specific volume). Therefore, all of the above results are probably in error to some extent. Before continuing with additional tests, the equipment was repaired and checked. All of the data reported in subsequent sections of this report were collected after the repairs.

### Impulse Drying Sample Set

Handsheets made from mill-refined and laboratory-refined pulps were evaluated for impulse drying. In addition to the two-ply sheets, one-ply sheets of each component pulp were tested for permeability. The results are shown in Table 9.

Table 9. Permeability results for the impulse drying samples.

IPST ID No.	U. C. ID No.	Sheet Solids (%)	95% Conf. Interval	OD Basis Weight (g/m <sup>2</sup> )	95% Conf. Interval	Specific Surface (m <sup>2</sup> /g)	95% Conf. Interval	Specific Volume (cm <sup>3</sup> /g)	95% Conf. Interval
W1	2P1	36.8	1.1	174	5	7.3	1.0	2.0	0.1
W1	2P1	47.0	2.3	184	8	5.2	0.6	1.8	0.1
W2	1P1	35.7	1.2	171	9	4.9	1.6	2.0	0.1
W2	1P1	43.5	1.6	169	6	4.9	2.0	1.8	0.1
W3	1P2	32.3	1.8	178	7	60.9	4.9	1.2	0.1
W3	1P2	39.6	1.8	175	6	45.7	6.9	1.6	0.2
W5	2P3	37.1	1.3	183	6	6.0	1.9	1.9	0.1
W5	2P3	42.4	1.3	176	7	5.2	0.8	1.8	0.1
W6	1P3	30.7	2.4	182	4	6.4	2.2	2.0	0.04
W6	1P3	36.6	0.9	181	3	4.0	0.8	2.0	0.02
W7	1P4	31.1	0.2	174	2	11.8	1.2	1.8	0.04
W7	1P4	43.5	1.7	176	5	4.7	0.5	1.7	0.05
W8	1P5	35 <sup>a</sup>	-	170	4	6.9	0.3	2.5	0.1
W8	1P5	42 <sup>a</sup>	-	174	3	6.7	2.1	2.5	0.1

a) Nominal sheet solids.

## **Refining Study Set**

All the sheets fabricated from furnishes W9 to W12 and W15 to W22 were prepressed to five pressing conditions as described above. Figures 1 to 6 show sheet solids after each prepressing as a function of press condition and total impulse for pine, hardwood, and 50/50 blends. For the pine cases, solids ranged from 30 to 48%, while for the hardwood cases, solids ranged from 36 to 51%. For all cases, solids were directly proportional to total press impulse. The same press impulse results in higher solids for samples of higher freeness. The freeness values used for the mixed cases were averages of the component freenesses.

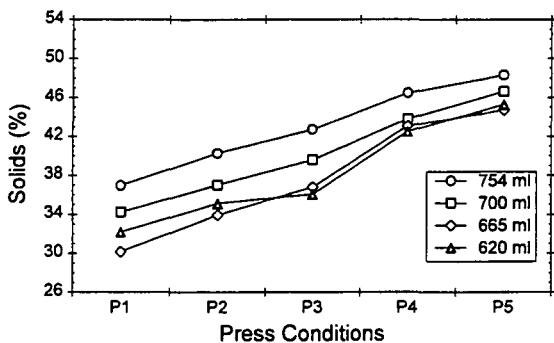


Figure 1. Average sheet solids for pine furnish.

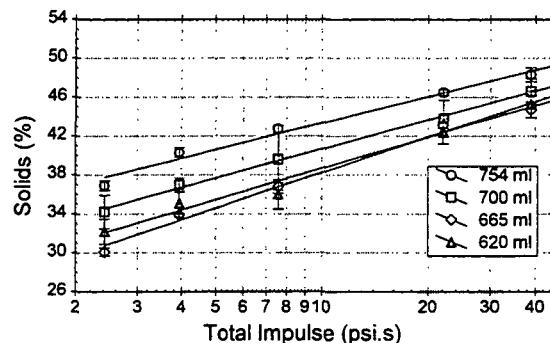


Figure 2. Average sheet solids for pine furnish.

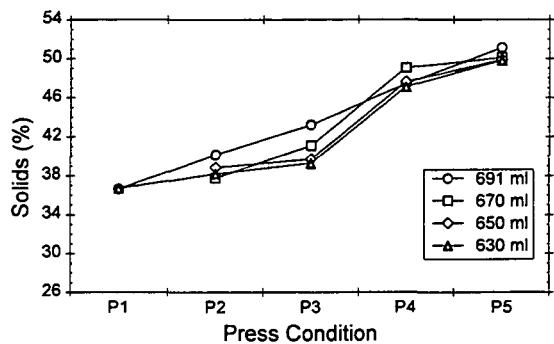


Figure 3. Average sheet solids for hardwood furnish.

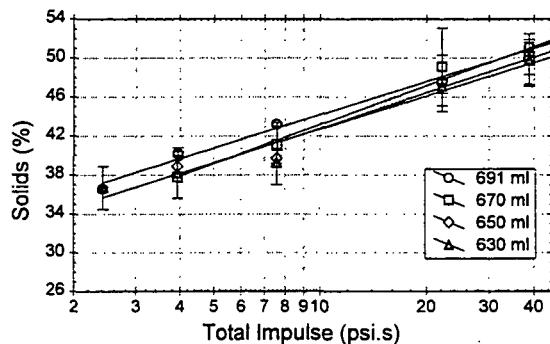


Figure 4. Average sheet solids for hardwood furnish.

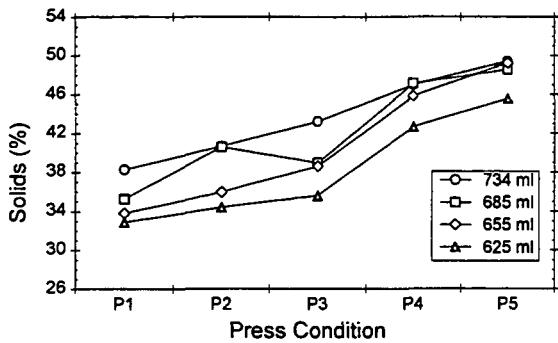


Figure 5. Average sheet solids for mixed furnish.

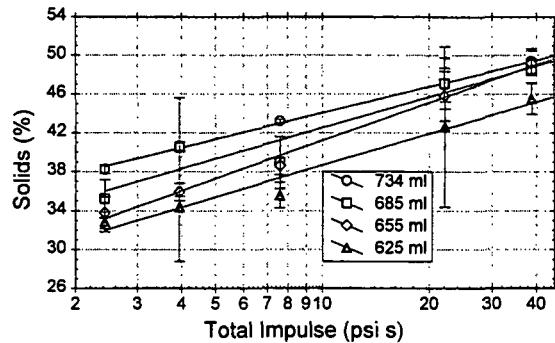


Figure 6. Average sheet solids for mixed furnish.

The sheets were formed and pressed in two batches. The first batch (W9-W12) was received and tested in early September. The second batch (W15-W22) was received about 1.5 months later. Between four and six samples were tested for each case (furnish and prepressing condition). All of the samples were stored in the refrigerator until tested. Since previous work [24] observed that fiber aging affects permeability results, the tests were performed in random order.

Figures 7 through 18 show the dependence of specific surface on storage time measured from pressing date. In general, for the least pressed cases (P1), specific surface increased with storage time. For the pine furnish, there is a general decrease in specific surface with time except for the highest freeness case (W10). For the case W10 (754 ml CSF), there was no aging effect observed.

For the hardwood sheets, the aging effect was more significant and resulted in increased specific surface with time except for the least refined case, W9 (691 ml CSF). For case W9, specific surface increases with time except for the least pressed sheets (P1). There was no observed time correlation for the mixed cases.

In general, the variability of the permeability test results was too great to accurately compensate for aging effects; therefore, for further analysis, all results were time averaged. For some of the cases plotted below, there were data points that were outside of the range plotted. These data points are shown in a box in the plot.

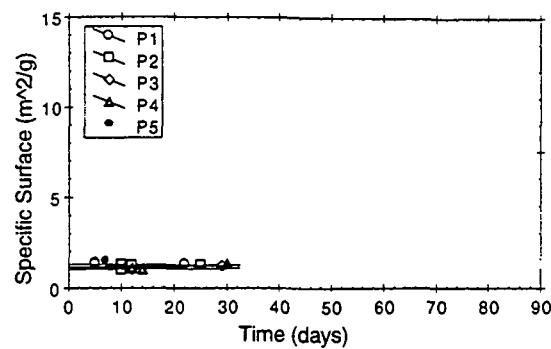


Figure 7. Case W10, pine, 754 ml CSF.

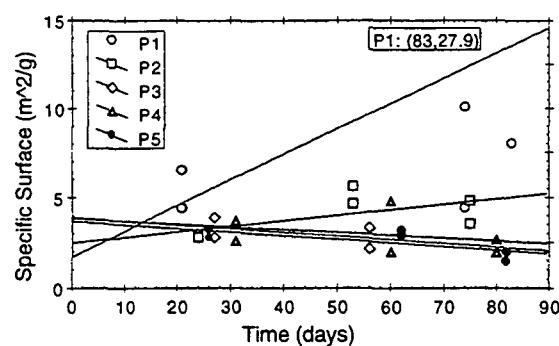


Figure 8. Case W18, pine, 700 ml CSF.

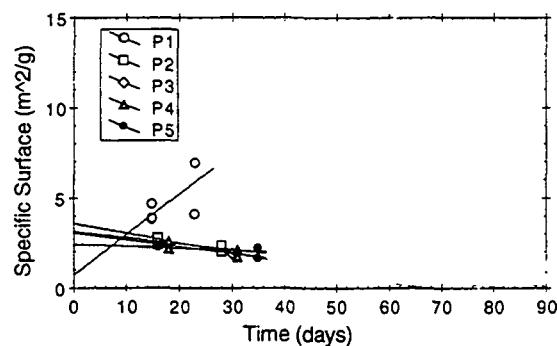


Figure 9. Case W12, pine, 665 ml CSF.

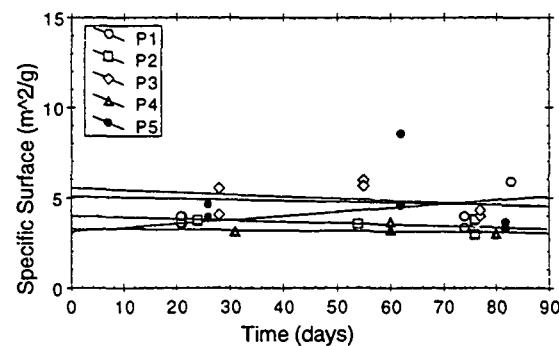


Figure 10. Case W19, pine, 620 ml CSF.

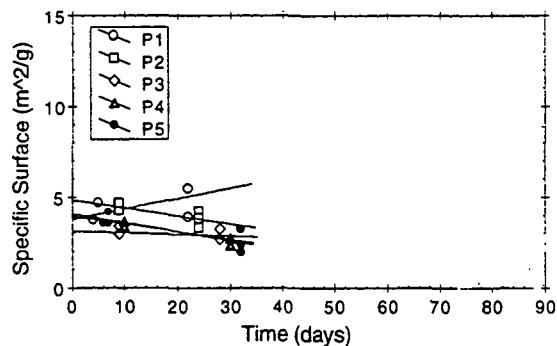


Figure 11. Case W9, hardwood, 691 ml CSF.

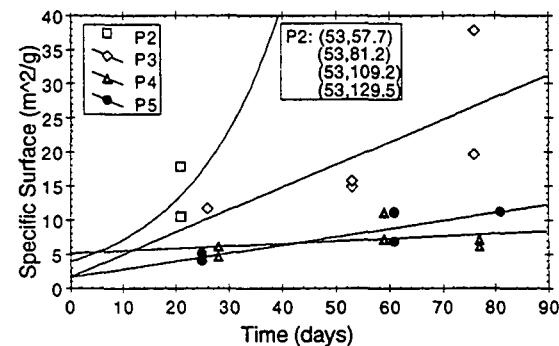


Figure 12. Case W15, hardwood, 670 ml CSF.

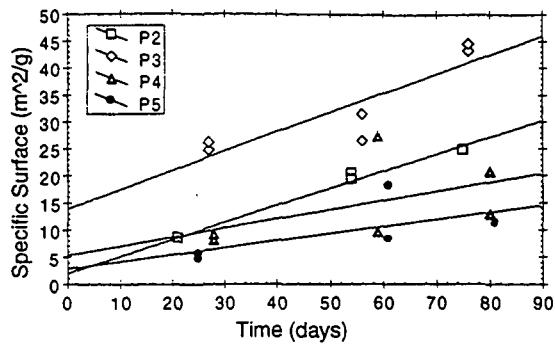


Figure 13. Case W16, hardwood, 650 ml CSF.

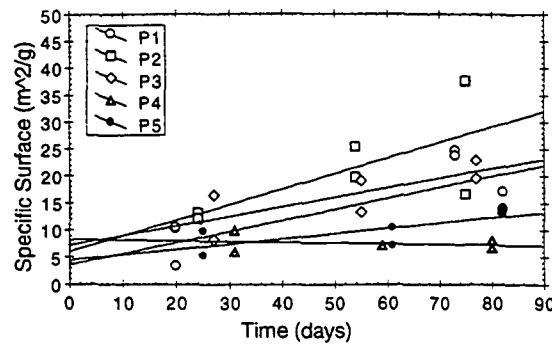


Figure 14. Case W17, hardwood, 630 ml CSF.

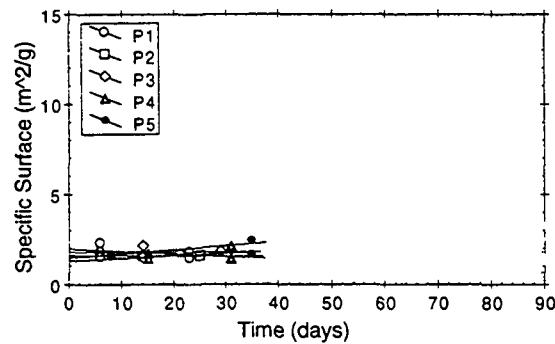


Figure 15. Case W11, mixture, 734 ml CSF.

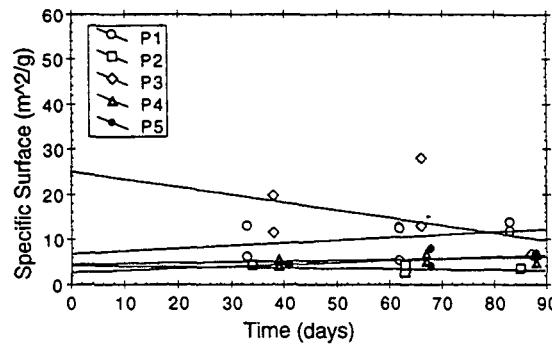


Figure 16. Case W20, mixture, 685 ml CSF.

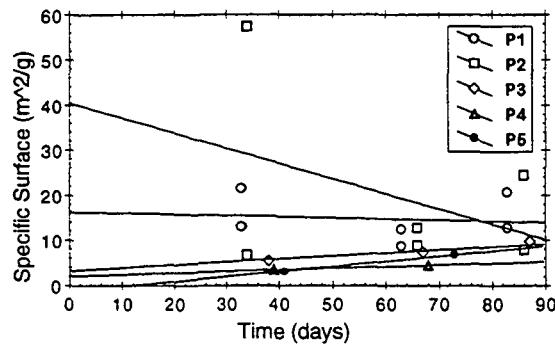


Figure 17. Case W21, mixture, 658 ml CSF.

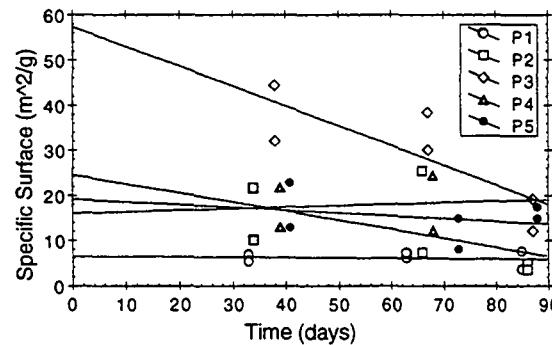


Figure 18. Case W22, mixture, 625 ml CSF.

It was observed that the variability of water permeability measurements for the first batch (furnishes W9-W12) was less than that for the second batch (W15-W22). During prepressing of the sheets from the second batch, sheet crushing was observed for some cases as noted in the procedures section. In general, for the crushed sheets, the specific surface was lower than what was expected.

The dependencies of specific surface and specific volume of swollen fibers on freeness are plotted in Figures 19 through 24. In general, specific surface (Figures 19, 21, and 23) tended to decrease with increased ingoing solids and freeness for both pine and hardwood furnishes. For a given freeness, the specific surface for pine was lower than that for hardwood. These results correspond with previously observed trends [3,6,7].

Figures 20, 22, and 24 show the dependence of specific volume on freeness for different prepressing conditions. Specific volume typically varies in the interval of 1.0 to 1.5 cc/g. Higher values were observed for pine compared to hardwood. Lower solids cases had higher values of specific volume. For pine, there was no observed correlation with freeness (Figure 20), while for hardwood, the specific volume tends to increase with increased freeness.

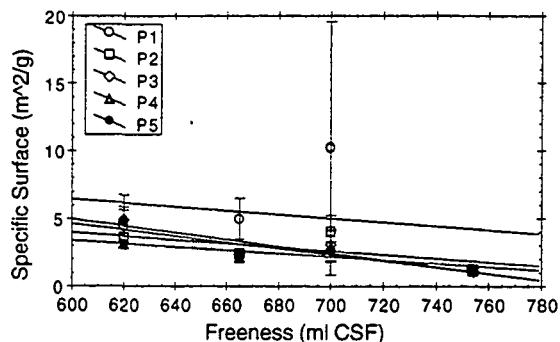


Figure 19. Average specific surface for pine furnish.

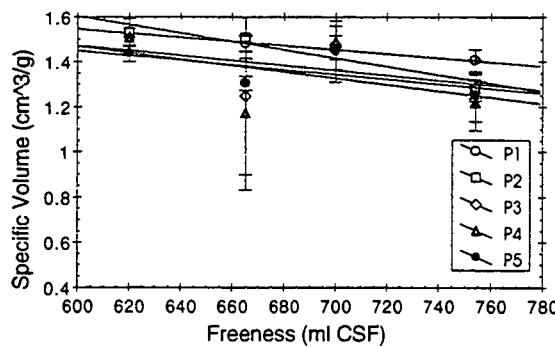


Figure 20. Average specific volume for pine furnish.

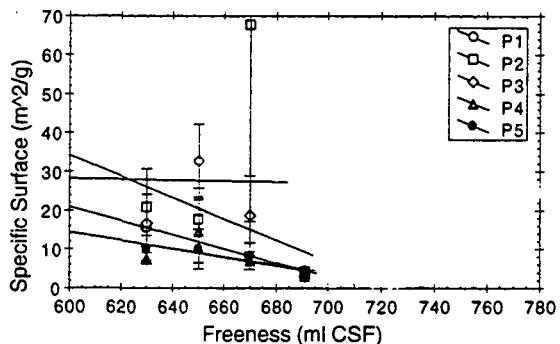


Figure 21. Average specific surface for hardwood furnish.

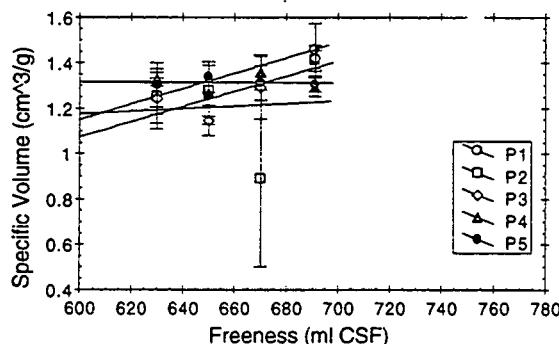


Figure 22. Average specific volume for hardwood furnish.

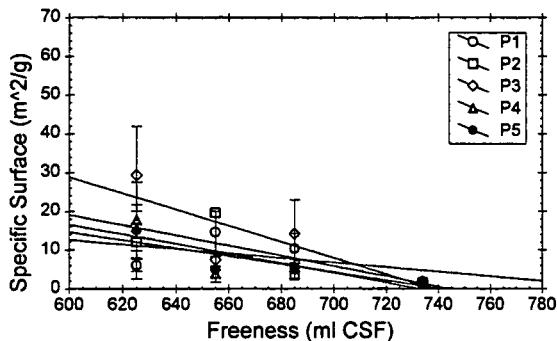


Figure 23. Average specific surface for mixed furnish.

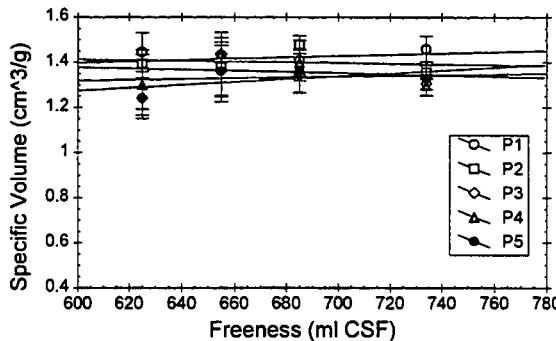


Figure 24. Average specific volume for mixed furnish.

The effect of pine fiber content, in a hardwood mixture, on specific surface for different pressing conditions is shown in Figures 25 through 29. In general, the addition of 50% pine fibers to the hardwood results in virtually the same specific surface as for 100% pine. Some deviations are primarily caused by high variability of specific surface for low freeness furnishes.

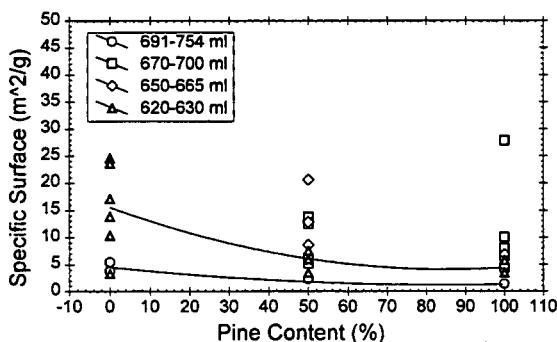


Figure 25. Pressing condition P1.

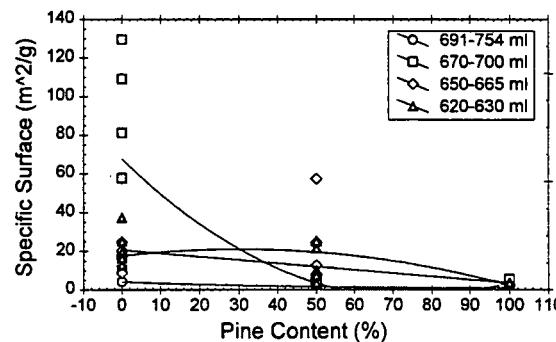


Figure 26. Pressing condition P2.

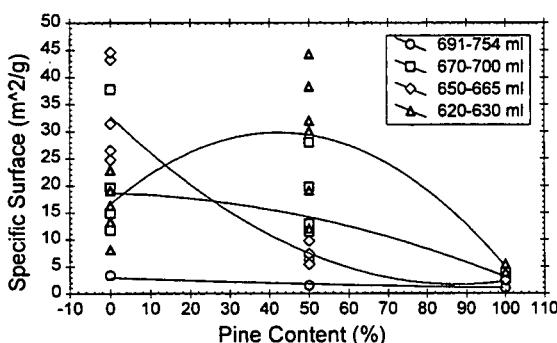


Figure 27. Pressing condition P3.

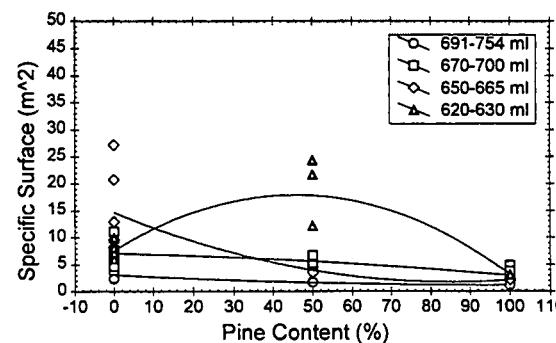


Figure 28. Pressing condition P4.

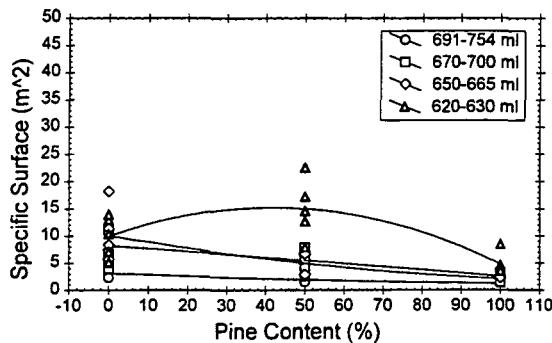


Figure 29. Pressing condition P5.

## IMPULSE DRYING

All impulse drying was done with a presteaming temperature of 65°C. To determine the steaming time, two wire thermocouples were placed between the sheet and the felt, and the temperature was recorded while steaming with the platen surface temperature set at 200°C and the heat shield in place. The steaming time was set to the time at which the slowest temperature profile crosses 55°C. At this time, the sheet temperature should be between 55 and 75°C. The results of these calibrations are shown in Table 10, and the temperature profiles are in Appendix E.

Table 10. Presteam times and temperature ranges obtained.

Furnish	Case	Time (s)	Temp Range (°C)
W1	A1	21	55-75
	A2	18	55-70
	A3	15	55-69
	A4	15	55-66
	C1	11	56-71
	C2	14	55-74
	D1	30	55-76
	D2	34	55-83
W5	A1	19	55-72
	A2	15	55-73
	A3	14	55-64
	A4	16	55-69
	C1	14	55-68
	C2	14	55-71
	D1	32	55-82
	D2	31	55-82

A second calibration procedure measures moisture change during steaming. A sheet and felt were weighed and then steamed as if for impulse drying. However, the sheet and felt were removed from the MTS and weighed again right after steaming. Five repeats were done at five platen surface temperatures, and a best fit to the data was used to determine the moisture change during steaming. Before impulse drying, the sheet moisture level was adjusted such that the sheet solids were at the target level after the steaming step, i.e., just before pressing.

### **Couch Trim Samples**

The effect of ingoing felt moisture was tested using the Mill #1 couch trim. The A platen, R felt, and 35% ingoing solids were used (case A3). The steaming time used was 15s at a temperature of 61-71°C. Results are listed in Table 11, and the raw data are in Appendix A. Felt moisture was observed to make a difference, and it was decided to use 16% for the remainder of the experiments.

Table 11. Results of felt moisture variation impulse drying trials.

Case	Platen Temperature (°C)	Ingoing Felt Moisture (%)	95% Conf. Interval	Ingoing Sheet Solids (%)	95% Conf. Interval	Outgoing Sheet Solids (%)	95% Conf. Interval
A3-PR1	200	16.1	0.2	37.5	3.3	42.9	3.6
A3-PR1	200	34.3	15.9 <sup>a</sup>	37.2	2.8	36.1	9.4
A3-PR1	250	16.6	3.4	36.3	2.4	44.9	1.0
A3-PR1	250	32.7	2.5	33.9	2.1	38.6	3.6

a) The high variation for this case was the result of moisture migration within a stack of wet felts while waiting to perform the experiment.

Critical temperatures were determined from the specific elastic modulus, %CV of SEM, and from visual observations. All of this data are shown in Appendix C. An explanation of the delamination codes is at the beginning of Appendix A. The following procedure was used to determine the critical temperatures.

- 1) Determine the temperature at which the %CV of SEM exceeds a value of 15-20%. In most cases, there was a sharp increase in %CV when delamination first occurred.
- 2) Determine the temperature at which the SEM values peak.
- 3) Determine the highest temperature at which there were no visible delaminations observed.
- 4) If two or more of the above determined temperatures agree, then that was the critical temperature.
- 5) If none of the above temperatures agree, then determine if the density data peak at one of the possible temperatures. For these cases, the critical temperature was the temperature that agrees with the majority of data.
- 6) If all else fails, the critical temperature was determined from the visual observations.

- 7) Round off the temperature to the nearest 5°C.
- 8) Identify any anomalies.

Previous experiments have shown that above the critical temperature, the SEM (and other strength properties) drops. Conversely, the %CV of the SEM rises just above the critical temperature. Therefore, the above procedure will determine a lower limit for the critical temperature for most cases. To determine the upper and lower uncertainties for the critical temperature, the following procedure was used.

- 1) The upper limit was the next higher temperature for which there were data if there was no visible delamination. If there were any visible delaminations, then the upper limit was zero.
- 2) If there was a large jump in the %CV of SEM value at the upper limit (~10 to 40+), then the lower limit was 10°C less than the critical temperature; otherwise, the lower limit was next lower temperature for which there were data.
- 3) If the SEM data do not show a peak at the critical temperature, then the lower limit was the next lower temperature for which there were data.
- 4) The lower limit cannot be less than 100°C (otherwise, it would not be impulse drying).
- 5) Uncertainties are the difference between the critical temperatures and the limits rounded to the nearest 5°C.

Additional Mill #1 couch trim sheets were impulse dried to determine the critical temperature and water removal. Figures 30 through 33 show the data used to determine the critical temperature. For temperatures of 150°C and below, severe sticking affected the results, and these data were ignored when determining the critical temperature. The critical temperature was 255°C, plus zero, minus 55°C. In Figure 32, the observed delamination value of six at 200°C may have been an anomaly.

Figures 34 and 35 show the outgoing solids and felt water gain results. The higher sheet outgoing solids and lower felt water gain at temperatures of 150° and below are a result of sheet sticking. Because sticking was also a problem at high temperatures, the felt water gain was lower than the typical values of 70-90%.

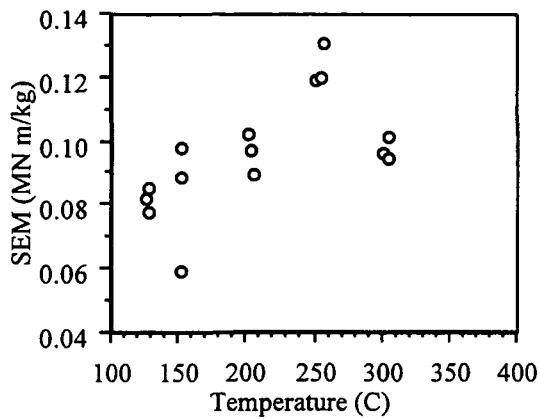


Figure 30. Specific elastic modulus.

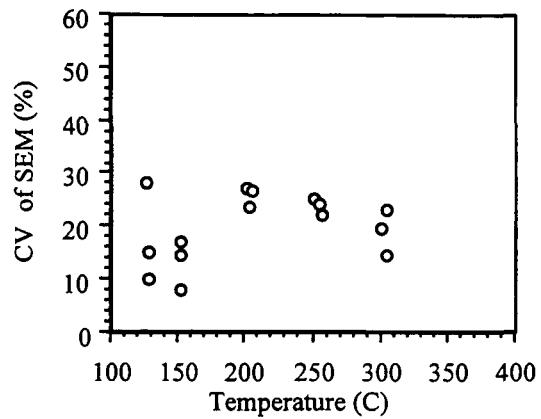


Figure 31. Coefficient of variation of SEM.

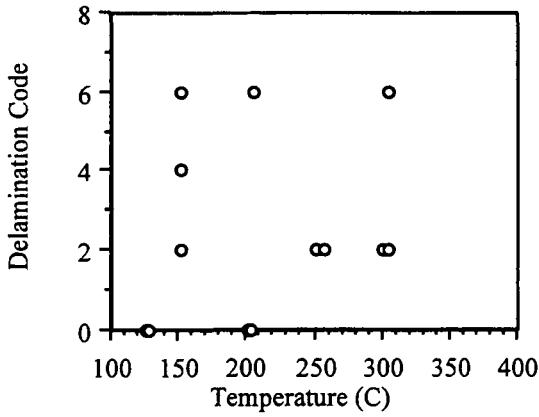


Figure 32. Visual delamination observations. See Appendix A for codes.

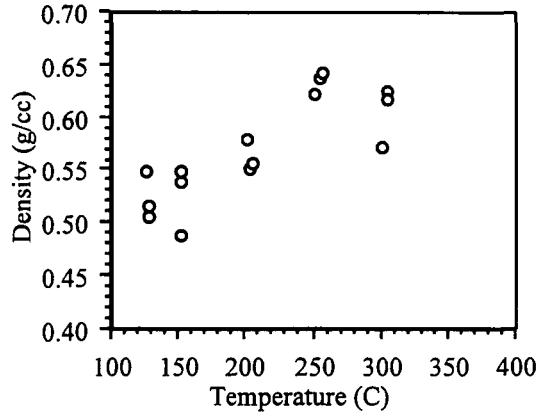


Figure 33. Ultrasonic sheet density.

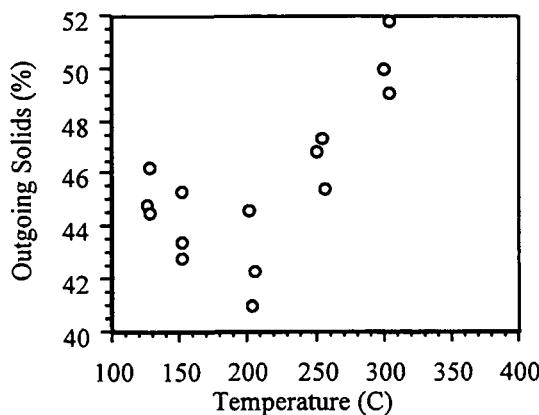


Figure 34. Outgoing sheet solids.

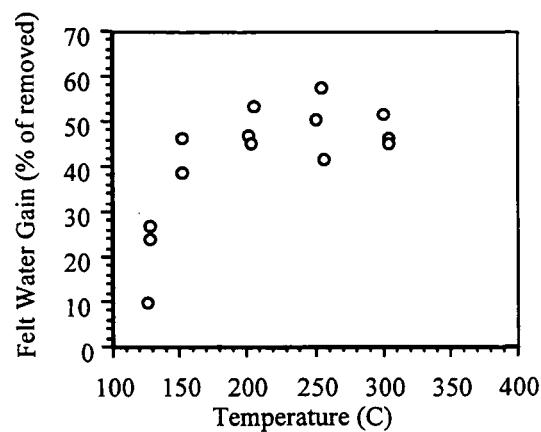


Figure 35. Felt gain of water removed.

Beloit also performed some tests using the Mill #1 and Mill #2 couch trim sheets. Ingoing solids were 36%; the "A" roll coating, "R" felt, and presteaming were used. The results at the critical temperature are tabulated in Table 12 for comparison.

Table 12. Results of Beloit impulse drying tests of couch trim.

Test	Simulator	Mill #1	Mill #2
Critical Temperature (°C)	MTS <sup>a</sup>	177	149
	HRP <sup>b</sup>	204	177
Outgoing Solids (%)	MTS	46.5	50.5
	HRP	51.9	52.9
	DF ENP <sup>c</sup>	47.7	47.8
TAPPI Density (g/cm <sup>3</sup> )	MTS	-	-
	HRP	0.620	0.626
	DF ENP	0.605	0.574
GM STFI Index (Nm/g)	MTS	-	-
	HRP	27.2	27.5
	DF ENP	25.3	25.8
Top Side Bendtsen Rough. (ml/min)	MTS	-	-
	HRP	1650	790
	DF ENP	2330	1840

a) MTS = Beloit MTS.

b) HRP = Beloit impulse drying pilot roll press.

c) DF ENP = Beloit double-felted pilot extended-nip press.

### Prepared Handsheets

Extensive IPST impulse drying trials were conducted for furnishes W1 and W5. A presteam temperature of ~65°C, and an ingoing felt moisture of 16% were used. Before analysis, the impulse drying data were filtered for a basis weight of  $177 \pm 10 \text{ g/m}^2$  (OD), an ingoing solids of 32,35,40 or  $42 \pm 1.0\%$ , and an impulse of  $0.1379 \pm 0.0034 \text{ MPa}\cdot\text{s}$ . Data used for further analysis are listed in Appendix A. Rejected data are listed in Appendix B.

Table 13 lists the experimental conditions used for impulse drying and the critical temperatures obtained. SEM, %CV of SEM, visible delamination codes, and some of the density data that were used to determine the critical temperatures are listed in Appendix C.

Table 13. Impulse drying critical temperatures.

Furnish ID IPST	U. C.	Case	Felt	Specific Sur. (m <sup>2</sup> /g)	95% C.I.	Critical Temp. (°C)	Uncertainty
W1	2P1	A1	B	7.35	0.98	170	+15 -10
W1	2P1	A2	B	5.24	0.58	160	+10 -10
W1	2P1	A3	R	7.35	0.98	155	+10 -10
W1	2P1	A4	R	5.24	0.58	160	+10 -15
W1	2P1	C1	B	7.35	0.98	205	+∞ -10
W1	2P1	C2	B	5.24	0.58	190	+∞ -10
W5	2P3	A1	B	6.00	1.94	175	+10 -10
W5	2P3	A2	B	5.24	0.77	205	+10 -10
W5	2P3	A3	R	6.00	1.94	160	+10 -15
W5	2P3	A4	R	5.24	0.77	170	+15 -25
W5	2P3	C1	B	6.00	1.94	230	+10 -20
W5	2P3	C2	B	5.24	0.77	230	+20 -20

Other physical properties at the critical temperature are listed in Tables 14 and 15, and are shown in Figures 36 through 39.

Table 14. Impulse drying water removal data at the critical temperature.

Furnish	Case	Ingoing Solids (%)	Outgoing Solids (%)	95% Conf. Interval	Moisture Ratio Change	95% Conf. Interval
W1	A1	32	46.6	1.4	0.97	0.25
W1	A2	40	50.0	1.0	0.54	0.09
W1	A3	32	43.4	1.5	0.85	0.03
W1	A4	40	47.6	2.2	0.44	0.05
W1	C1	35	46.5	1.4	0.70	1.02
W1	C2	42	50.3	0.2	0.37	0.37
W1	D1	35	41.6	0.5	0.48	0.06
W1	D2/40	40	44.7	1.4	0.22	0.10
W1	D2/42	42	44.9	3.6	0.17	0.12
W5	A1	32	46.6	0.7	0.96	0.05
W5	A2	40	51.6	0.5	0.58	0.07
W5	A3	32	45.6	1.3	0.92	0.16
W5	A4	40	47.6	11.3	0.42	0.07
W5	C1	35	46.7	1.7	0.69	0.09
W5	C2	42	51.5	1.4	0.45	0.09
W5	D1	35	41.3	0.14	0.43	0.04
W5	D2/40	40	43.6	∞	0.19	∞
W5	D2/42	42	44.3	∞	0.13	∞

Table 15. Impulse drying physical property data at the critical temperature.

Furnish	Case	Density (g/cm <sup>3</sup> )	95% Conf. Interval	STFI Index (N·m/g)	95% Conf. Interval	SEM (MN·m/kg)	95% Conf. Interval
W1	A1	0.683	0.029	30.19	0.06	0.186	0.005
W1	A2	0.722	0.072	-	-	0.172	0.020
W1	A3	0.665	0.076	30.06	2.80	0.154	0.028
W1	A4	0.678	0.066	29.47	$\infty$	0.148	0.044
W1	C1	0.670	0.070	29.21	13.59	0.165	0.038
W1	C2	0.699	0.006	29.12	1.67	0.166	0.013
W1	D1	0.614	0.020	29.15	0.80	0.133	0.015
W1	D2/40	0.660	0.047	29.19	3.16	0.143	0.013
W1	D2/42	0.653	0.241	29.74	6.68	0.144	0.019
W5	A1	0.710	0.016	31.03	1.46	0.168	0.009
W5	A2	0.734	0.008	29.44	$\infty$	0.176	0.012
W5	A3	0.699	0.029	31.61	3.46	0.158	0.018
W5	A4	0.722	0.051	31.96	$\infty$	0.151	0.057
W5	C1	0.711	0.007	30.70	1.41	0.165	0.017
W5	C2	0.728	0.014	29.77	2.03	0.160	0.013
W5	D1	0.640	0.028	30.95	0.62	0.142	0.010
W5	D2/40	0.670	$\infty$	32.98	$\infty$	0.140	$\infty$
W5	D2/42	0.643	$\infty$	32.50	$\infty$	0.149	$\infty$

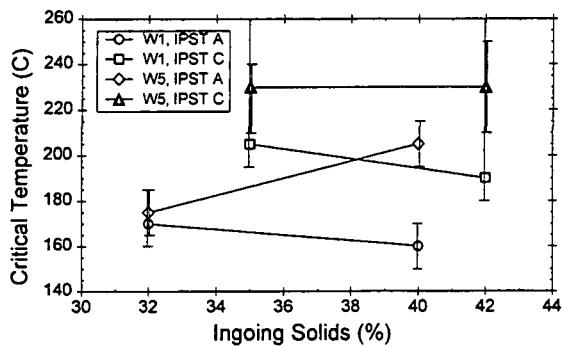


Figure 36. Critical temperatures for B felt.

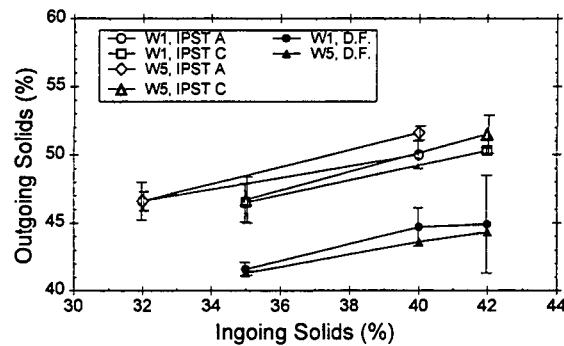


Figure 37. Outgoing solids for B felt.

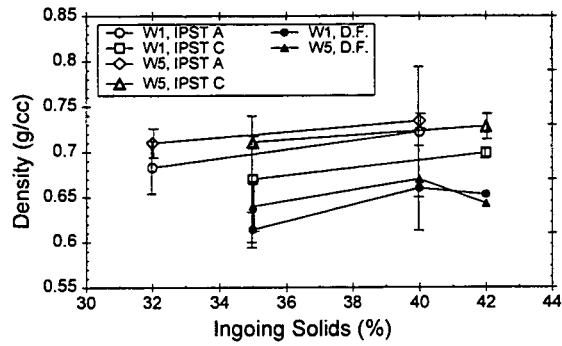


Figure 38. Density for B felt.

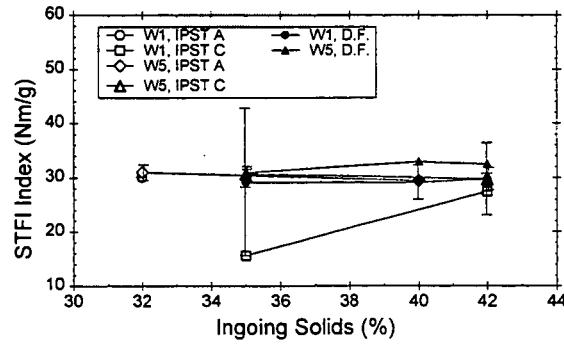


Figure 39. STFI index for B felt.

The following data, obtained by Beloit, are shown in Table 16 for comparison. The roll surface was "A" and the R felt used. The Beloit MTS impulse was 0.16 MPa·s; presteaming was used; and the felts were air dried. Presteaming was also used for the HRP and HTP impulse drying cases. The control case was prepressed and finish dried. The commercial case was prepressed and then run through a three-nip single-felted roll press at 500, 800, and 1200 pli. All physical property data reported were at the critical temperatures.

Table 16. Comparison of IPST and Beloit impulse drying results at the critical temperature.

Test	Furnish	Nominal Ingoing Solids (%)	Cont <sup>d</sup>	Com <sup>e</sup>	IPST MTS	Beloit MTS	Beloit HRP	Beloit ENP HTP	Beloit ENP DF
Critical Temp. (°C)	W1 (2P1)	36	-	-	155	177	<177	177	-
	W1 (2P1)	42	-	-	160	177	<177	177	-
	W5 (2P3)	36	-	-	160	204	177	204	-
	W5 (2P3)	42	-	-	170	204	177	204	-
Outgoing Solids (%)	W1 (2P1)	36	-	38.0	43.4	48.8	49.7	48.0	46.3
	W1 (2P1)	42	-	-	47.6	51.7	51.3	49.2	48.3
	W5 (2P3)	36	-	37.4	45.6	49.4	48.8	46.9	45.6
	W5 (2P3)	42	-	-	47.6	50.8	51.2	50.6	48.2
IPC Density <sup>b</sup> (g/cc)	W1 (2P1)	36	0.615	0.686	0.665	0.775	0.825	0.815	0.800
	W1 (2P1)	42	0.705	-	0.678	0.805	0.845	0.825	0.815
	W5 (2P3)	36	0.617	0.708	0.699	0.825	0.820	0.870	0.860
	W5 (2P3)	42	0.785	-	0.722	0.840	0.835	0.835	0.815
GM STFI Index <sup>a</sup> (Nm/g)	W1 (2P1)	36	26.1	26.4	30.1	27.8	28.0	25.4	29.3
	W1 (2P1)	42	-	-	29.5	27.2	30.0	26.9	29.3
	W5 (2P3)	36	25.7	28.7	31.6	30.9	29.8	30.0	32.5
	W5 (2P3)	42	28.6	-	32.0	30.2	30.3	30.8	31.0
MD Ring Crush Index (Nm/g)	W1 (2P1)	36	13.7	14.3	-	-	13.4	13.4	15.6
	W1 (2P1)	42	-	-	-	-	15.0	12.9	16.4
	W5 (2P3)	36	12.1	14.4	-	-	14.0	13.8	-
	W5 (2P3)	42	13.6	-	-	-	11.8	15.2	12.9
CD Ring Crush Index (Nm/g)	W1 (2P1)	36	7.4	8.4	-	-	10.7	9.6	11.2
	W1 (2P1)	42	-	-	-	-	10.6	8.6	11.2
	W5 (2P3)	36	7.2	9.2	-	-	11.5	11.0	-
	W5 (2P3)	42	8.3	-	-	-	9.9	11.5	9.8
Top Side Bendtsen Rough. (ml/min)	W1 (2P1)	36	1120	1580	-	1780	960	1080	1680
	W1 (2P1)	42	2460	-	-	1570	920	1180	1750
	W5 (2P3)	36	1450	1550	-	1460	880	1000	2020
	W5 (2P3)	42	1730	-	-	1410	910	1120	1830

a) The IPST STFI results are not a geometric mean (the sheets were hand-formed).

b) The IPST densities are from the ultrasonic tests.

c) Beloit pilot ENP press operated as an impulse dryer.

d) Cont = Control case, ingoing conditions.

e) Com = Commercial case, three-nip roll press.

## STEAMING TEMPERATURE PROFILES

The objective of this part of the experiments was to try to induce a temperature gradient within the sheet during presteaming. This would enable the MTS to better simulate actual commercial machine conditions.

After preparing the sheets with thermocouples, the sheets were steamed in the MTS nip. The B felt and heat shield were used, and the platen temperature was set at 200°C. Data collection was started, and then the steam was turned on. The first set of results is shown in Figures 40 through 44. One of the thermocouples failed during the embedding process; therefore, some of the temperatures show a flat line.

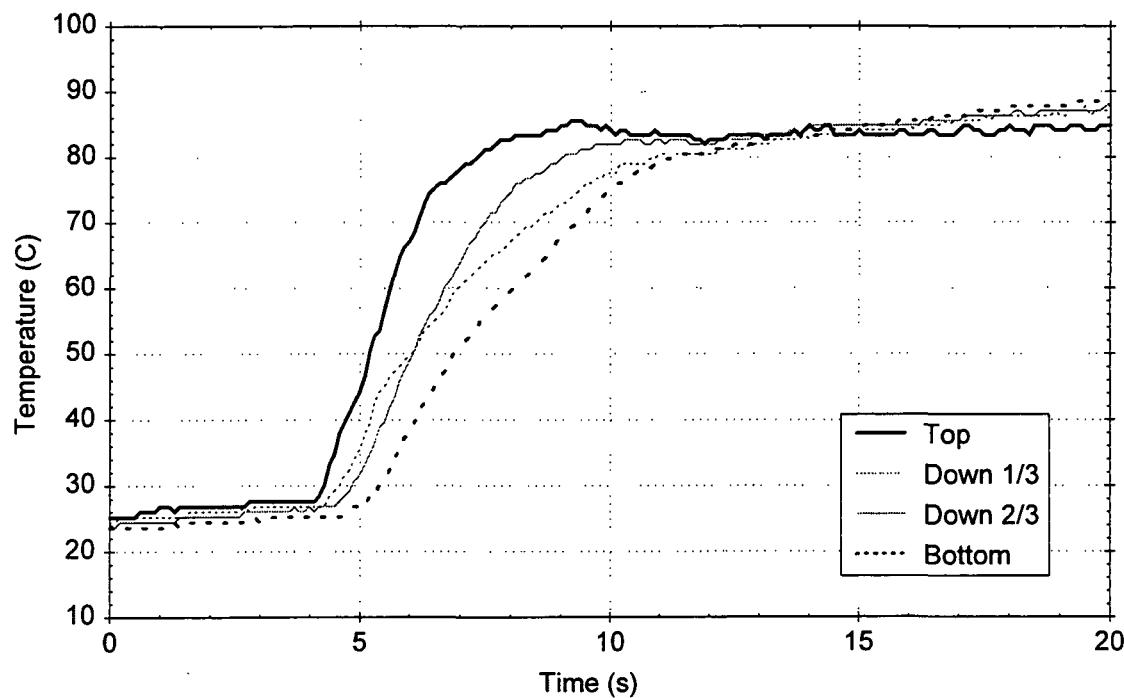


Figure 40. Furnish W13, 35% solids, repeat 1.

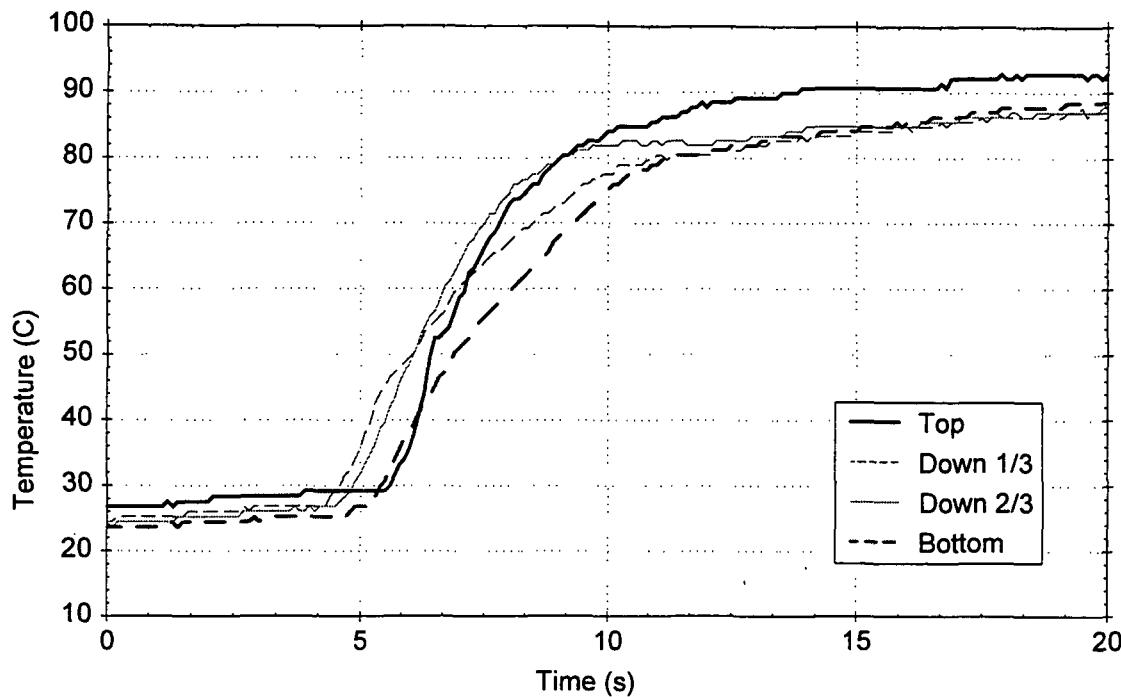


Figure 41. Furnish W13, 35% solids, repeat 2.

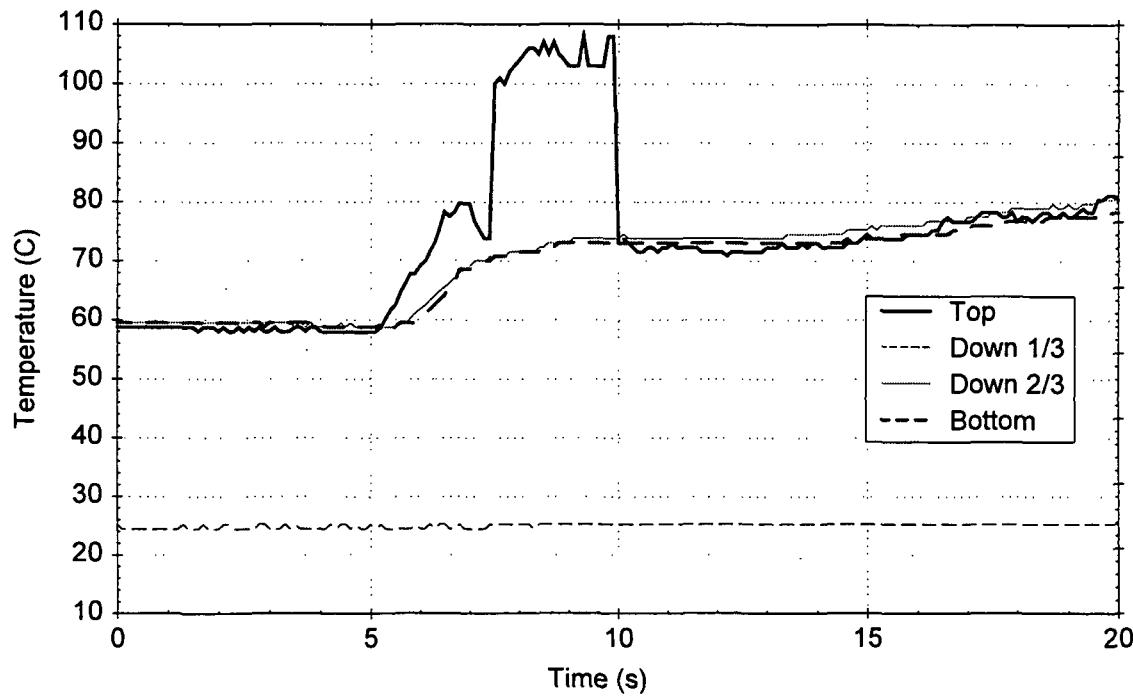


Figure 42. Furnish W14, 35% solids, repeat 1.

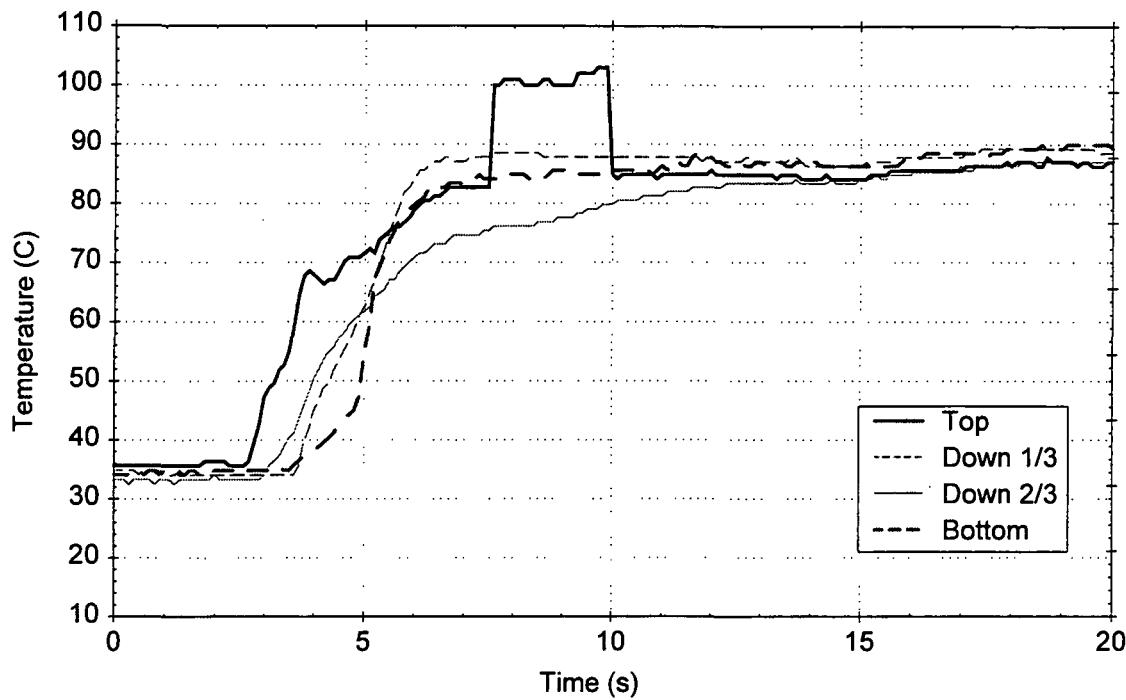


Figure 43. Furnish W14, 35% solids, repeat 2.

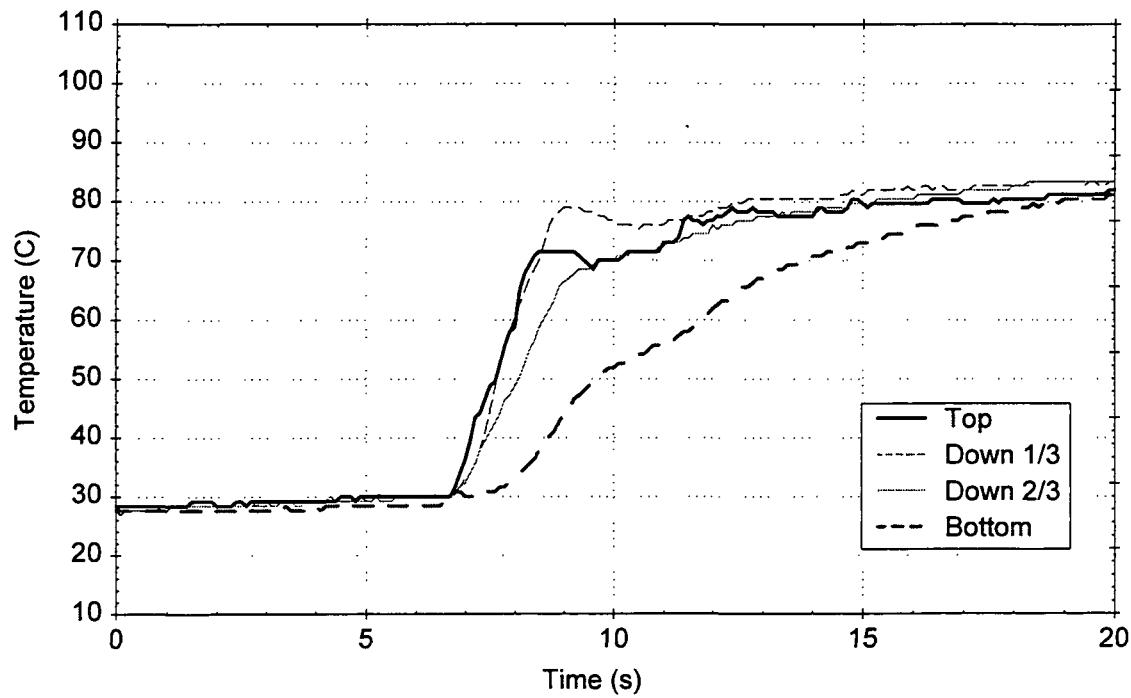


Figure 44. Furnish W14, 35% solids, repeat 3.

From the above results, it was observed that the top thermocouple was lifting from the sheet resulting in inaccurate temperature measurements. Because the felts have a curl, it is possible that enough steam was hitting the bottom of the sheet, reducing the

possible temperature gradient. For the next set of tests, the sheet was taped to the felt to prevent steaming from the bottom. Also, the top thermocouple was taped to the sheet with porous tape.

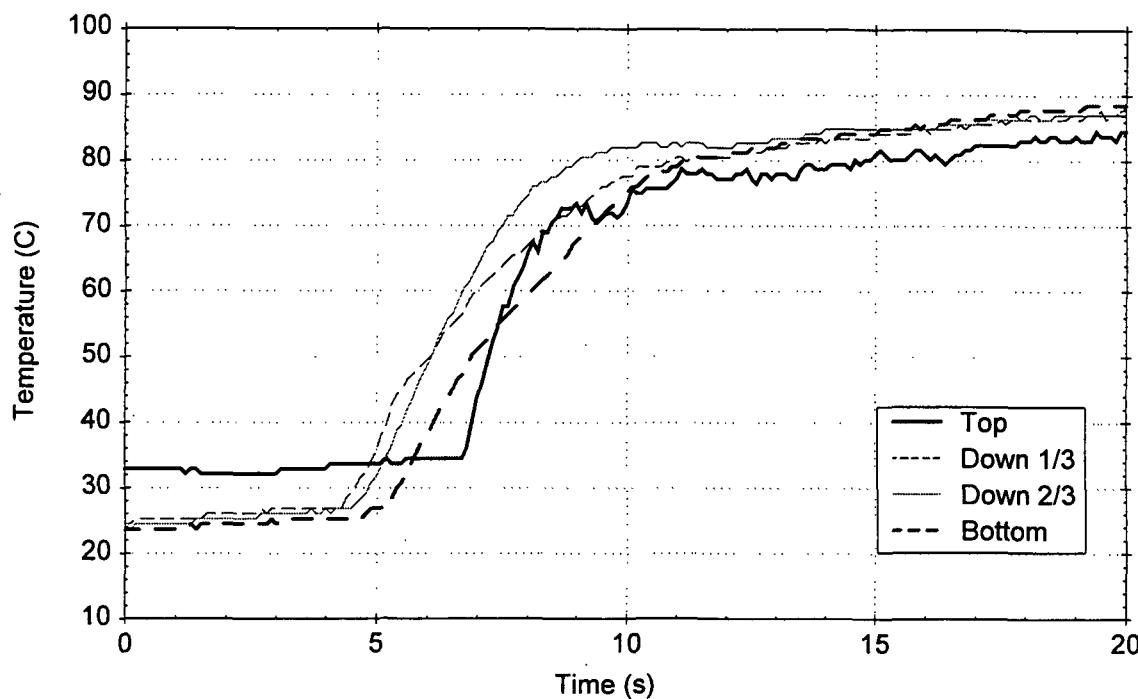


Figure 45. Furnish W13, 35% solids, sheet taped to felt, repeat 1.

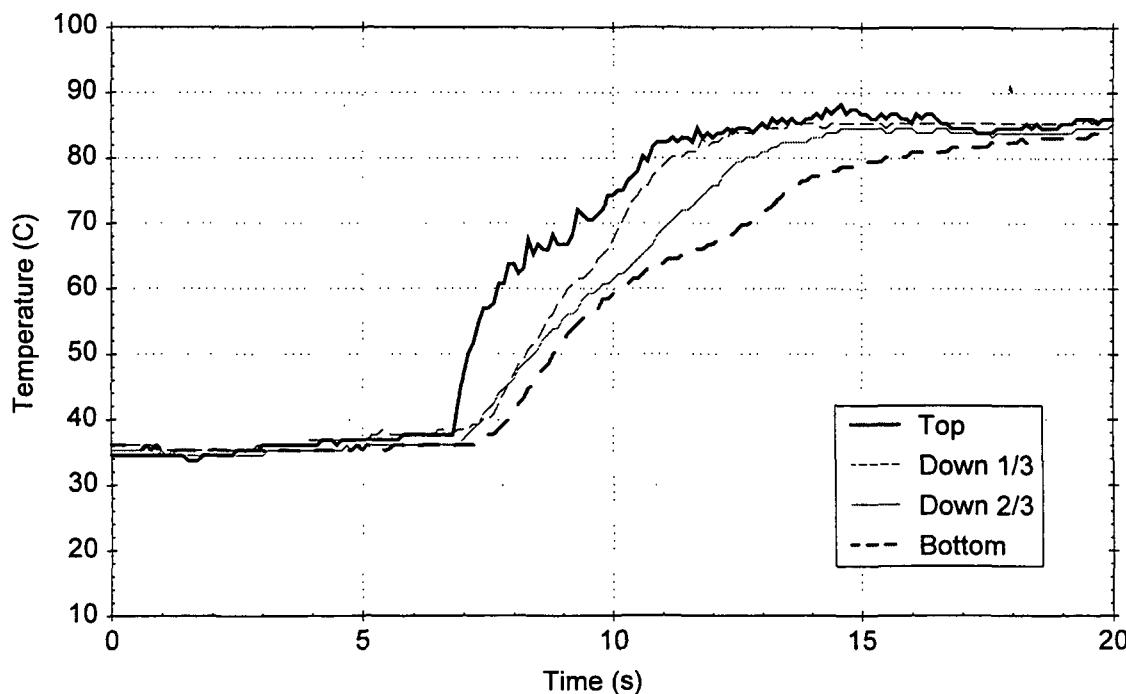


Figure 46. Furnish W13, 35% solids, sheet taped to felt, repeat 2.

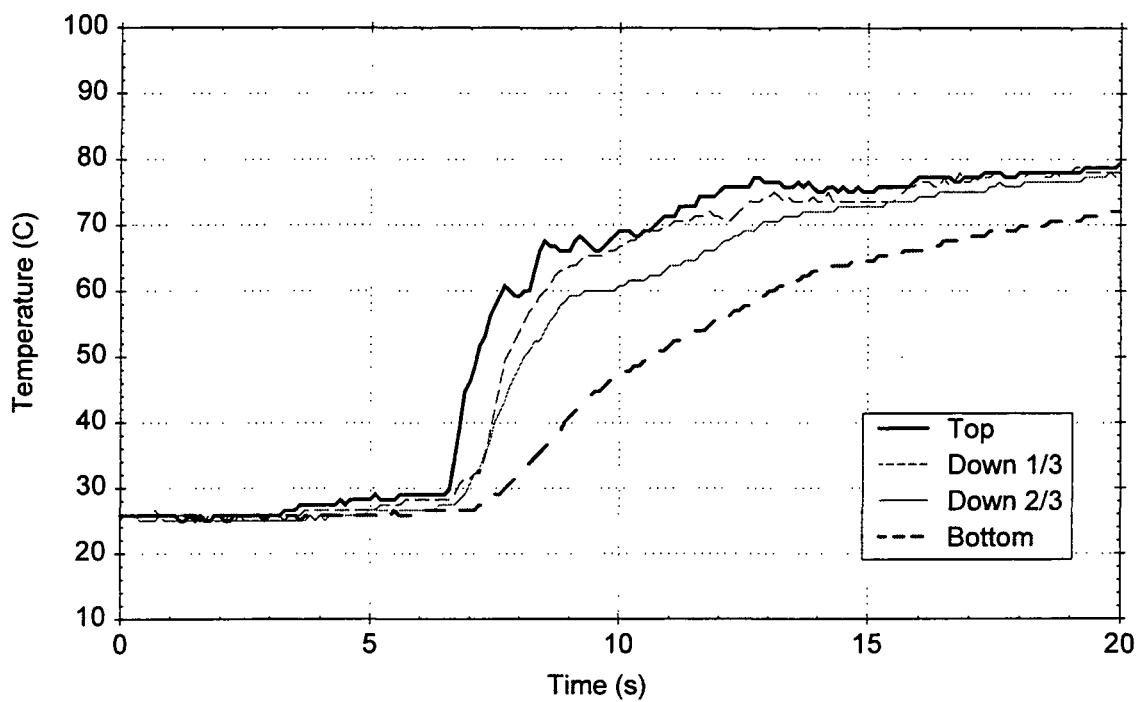


Figure 47. Furnish W14, 35% solids, sheet taped to felt, repeat 1.

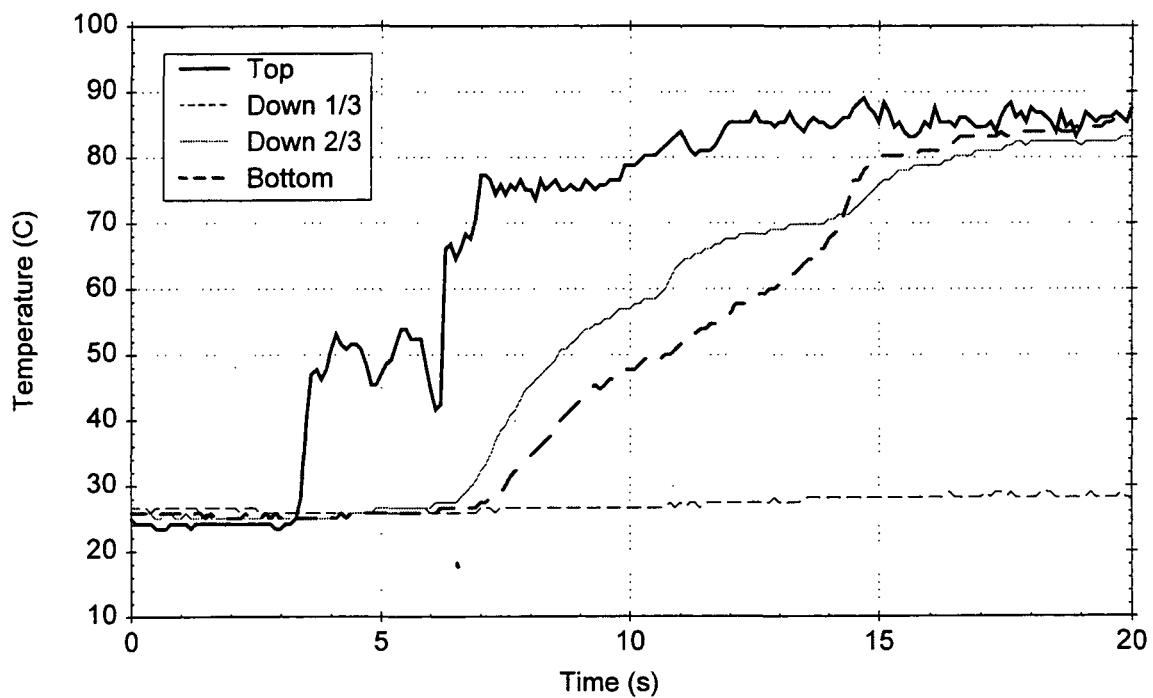


Figure 48. Furnish W14, 35% solids, sheet taped to felt, repeat 2.

For the last trial, a maximum gradient was formed by steaming only until the top surface reached 75°C. The result is shown in Figure 49.

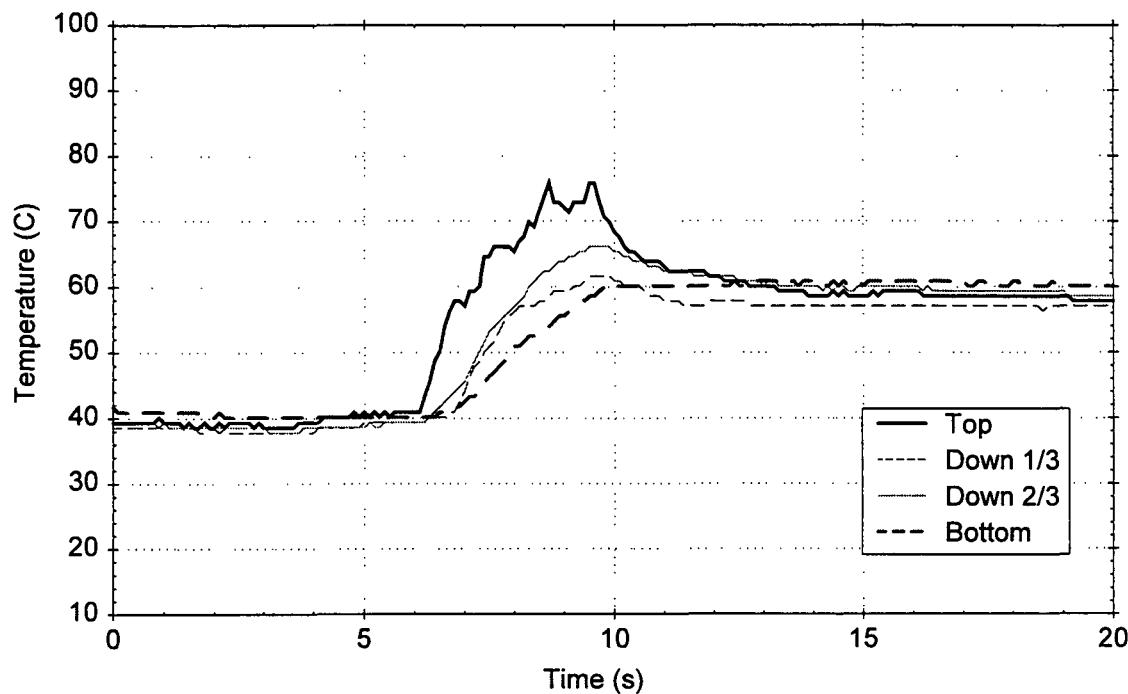


Figure 49. Furnish W14, 35% solids, sheet taped to felt, repeat 3.

Although a temperature gradient does exist during MTS steaming, the sheets reach equilibrium within two to three seconds after turning off the steam. Since it takes nine seconds for the MTS head to close during a hit, any temperature gradient will disappear before a hit can be made. It may be possible to reduce the closure time to about two seconds, but this is still too slow to test a significant temperature gradient.

## CONCLUSIONS

The following conclusions can be drawn from this work.

- 1) There is no observable difference between mill-refined pulp and machine-formed paper, and laboratory-prepared pulp and laboratory-formed handsheets in regards to water permeability and impulse drying. Observed differences can be attributed to process variables such as refining level and prepressing.
- 2) As reported in previous experiments, specific surface can be minimized by minimally refining the pulp and prepressing the sheet as much as possible. Under the same processing conditions, pine has a lower specific surface than hardwood.
- 3) Permeability results are highly dependent on sheet preparation and preprocessing. For consistent results, it is important that preparation techniques be standardized and followed rigorously. An aging effect was observed that increases as the furnish becomes more closed.
- 4) IPST impulse drying results were consistent with previous experiments showing an increase in outgoing solids of 2-8 percentage points for the A platen and 5-7 percentage points for the C platen compared to double-felted pressing for 40-42% ingoing solids. STFI index values showed an increase of up to 3.5%. However, for 35% ingoing solids, impulse drying was no better than double-felted pressing.
- 5) Beloit impulse drying results had a less dramatic improvement in water removal (up to 3.8 percentage points) compared to double-felted pressing. They also had up to 15% improvement in ring crush and up to 56% decrease in Bendtsen roughness compared to double-felted pressing.
- 6) Although there was a bias in the results between IPST and Beloit, the trends were consistent, with the IPST results being the most conservative. Some of the differences may be a result of different testing conditions between laboratories.
- 7) Felt type and moisture levels have an observable effect on water removal, rewet, and sheet sticking. The best combination was the B felt at 16% moisture or less.
- 8) Present laboratory equipment cannot recreate expected machine presteaming temperature profiles in the sheet. Additional experiments are needed to determine the effect of different presteaming temperatures on impulse drying efficiency.

## **RECOMMENDATIONS FOR FUTURE WORK**

This work was based on furnishes that simulated presently utilized commercial furnishes and a conservative nip loading. Therefore, the results indicate what could be achieved in a worst case scenario. The next phase of impulse drying work should use a less refined top ply to improve the sheet permeability. Also, recycled fiber should be evaluated.

It is not possible to directly test the effect of sheet temperature gradients on impulse drying with the MTS. The next set of experiments should look at the effect of different levels of presteam sheet temperature on impulse drying.

## **ACKNOWLEDGMENTS**

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## REFERENCES

1. Orloff, D.I., "Impulse Drying of Recycled Multi-ply Linerboard: Laboratory-scale Studies," TAPPI Journal, 77(2):169 (1994).
2. Kerschner, Craig M., "The Effects of Platen Material and Pressure on Impulse Drying," IPST A190 Project, (May 1994).
3. Orloff, D.I., and Phelan, P.M., "Impulse Drying of Multi-Ply Linerboard - Pilot Scale Shoe Press Experiments," U.S. Department of Energy Report No. DOE/CE/40738-T8, (January 1994).
4. Orloff, D.I., "Impulse Drying of Recycled Multi-ply Linerboard: Laboratory-scale Studies," Proceedings of the 1993 TAPPI Engineering Conference, pp.1021-1030, TAPPI Press, (September 1993).
5. Orloff, D.I., and Phelan, P.M., "Heat Transfer During Impulse Drying: The Influence of Press Impulse and Pressure Profile," HTD-Vol. 238, Heat and Mass Transfer in Pulp and Paper Processing, pp.17-23, ASME, (August 1993).
6. Orloff, D.I., "Impulse Drying Performance Database for Heavy Weight Grades of Paper," Technical Division of the CKPG of the American Paper Institute Report No. 1, (December 1992).
7. Orloff, D.I., "A Comparison of Impulse Drying to Double Felted Pressing on Pilot-Scale Shoe Presses and Roll Presses," U.S. Department of Energy Report No. DOE/CE/40738-T7, (August 1992).
8. Orloff, D.I., Jones, G.L., and Phelan, P.M., "Effects of Heating Mode on Roll Durability and Efficiency of Impulse Drying," HTD-Vol. 193, Fundamentals of Heat Transfer in Porous Media, pp.141-150, ASME, (August 1992).
9. Lenling, W.J., Smith, M.F., and Orloff, D.I., "Thermal Coating Development for Impulse Drying," International Thermal Spray Conference, Orlando, FL, (June 1992). (Given Best Paper of Conference Award).
10. Orloff, D.I., and Sobczynski, S.F., "Impulse Drying Pilot Press Demonstration: Ceramic Surfaces Inhibit Delamination," Proceedings of the Fourth International Conference on New Available Techniques and Current Trends, pp.180-198, SPCI'92 ATICELCA, Bologna, Italy, (May 1992).
11. Orloff, D.I., and Lindsay, J.D., "Advances in Wet Pressing," IPST Executives' Conference, Atlanta, GA, (May 1992).

12. Orloff, D.I., and Lindsay, J.D, "The Influence of Yield, Refining and Ingoing Solids on the Impulse Drying Performance of a Ceramic Coated Press Roll," Proceedings of the 1992 TAPPI Papermakers Conference, pp.85-94, Nashville, TN, (April 1992).
13. Orloff, D.I., "Impulse Drying of Paper: A Review of Recent Research," Proceedings of the 14th National Industrial Energy Technology Conference, pp.110-116, Houston, TX, (April 1992).
14. Orloff, D.I., et al., "Method and Apparatus for Drying Web," U.S. Patent Number 5101574, Issued April 7, 1992.
15. Orloff, D.I., "High-Intensity Drying Processes - Impulse Drying Report Six," U.S. Department of Energy Report No. DOE/CE/40738-T6, (July 1991).
16. Orloff, D.I., "Impulse Drying: Controlling Delamination in Heavy Weight Grades," IPST Executives' Conference, Atlanta, GA, (May 1991).
17. Orloff, D.I., "Impulse Drying: Heterogeneous Press Surfaces Offer New Product Opportunities," TAPPI Journal, 75(5): pp.172-176 (May 1992). Also presented at the TAPPI Non-Wovens Conference (May 1991).
18. Orloff, D.I., "Impulse Drying of Linerboard: Control of Delamination," Journal of Pulp and Paper Science, 18(1), J23-J32 (January 1992). Also presented at the 77th Annual Meeting of the Technical Section of the Canadian Pulp and Paper Association, (January 1991).
19. Orloff, D.I., "High-Intensity Drying Processes - Impulse Drying Report Five," U.S. Department of Energy Report No. DOE/CE/40738-T5, (September 1990).
20. Orloff, D.I., "Impulse Drying of Paper - Fundamentals of Delamination and Its Control," Presented at the Annual Meeting of the American Society of Chemical Engineers, (November 1989).
21. Orloff, D.I., "High-Intensity Drying Processes - Impulse Drying Report Four," U.S. Department of Energy Report No. DOE/CE/40738-T4, (May 1989).
22. Walpole, R.E., and Myers, R.H., "Probability and Statistics for Engineers and Scientists," Fourth Edition, Macmillan Publishing Company, New York, N.Y., ISBN 0-02424210-1, (1989).
23. Carslaw, H.S., and Jaeger, J.C., "Conduction of Heat in Solids," Clarendon Press, Oxford, England, (1947).

24. Lindsay, J.D., and Wallin, J.R., "Characterization of In-Plane Fluid Flow in Paper," Proceedings of the AIChE Forest Products Symposium, pp.121-129, (1989 and 1990).



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## APPENDIX A

The following tables contain the data that were used for analysis. The coded comments are explained below.

### Delamination Codes

- 0: None
- 1: Small Blisters ( $\leq 1\text{mm}$ )              < half the sheet
- 2: Medium Blisters (1mm to 1cm) < half the sheet
- 3: Small Blisters               $\geq$  half the sheet
- 4: Large Blisters ( $> 1\text{cm}$ )              < half the sheet
- 5: Medium Blisters               $\geq$  half the sheet
- 6: Large Blisters               $\geq$  half the sheet
- 7: Split Sheet
- 9: Other (explain in Comments)

### Rewet Codes

- 10: None
- 11: Slight Edge Rewet,              < half the edge
- 12: Moderate Edge Rewet,               $\geq$  half the edge
- 13: Slight Rewet,              < 1/3 of sheet
- 14: Moderate Rewet,              1/3 to 2/3 of sheet
- 15: Severe Rewet,              > 2/3 of sheet
- 19: Other (explain in Comments)

### Stick Codes

- 20: None
- 21: Slight Picking (surface disturbed)
- 22: Moderate Picking (a few fibers stuck to platen)
- 23: Severe Picking (many fibers stuck to platen)
- 25: Slight Sticking (sheet lifted, but released immediately, no picking)
- 26: Moderate Sticking (sheet stuck, but released on its own, may have picking)
- 27: Severe Sticking (sheet stuck, but could be easily peeled off, may have picking)
- 28: Extreme Sticking (sheet stuck, difficult to peel off)
- 29: Other (explain in Comments)

Table A1. Data with the IPST A platen and the Mill #1 couch trim.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM (MN/m <sup>2</sup> )	SEM (%CV)	IMPULSE (MPa.s)	OD BASIS WEIGHT (g/m <sup>2</sup> )	SHEET SOLIDS (%)	SHEET SOLIDS (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT MOISTURE (%)	FELT GAIN/LOSS (%)	WATER REMOVED (kg/m <sup>2</sup> )	US DENSITY (g/cm <sup>3</sup> )	AVERAGE STF INDEX (Nm/g)	95% C.I.	DELAM CODE	REWET CODE	STICK PICK CODE	COMMENTS
A3PR111	127	0.078	10.26	0.145	179.8	34.9	46.3	0.702	16.9	19.1	27.0	0.126	0.507	0	10	28			
A3PR112	127	0.085	15.29	0.142	186.4	36.5	44.5	0.488	16.4	17.8	24.2	0.091	0.517	0	10	27			
A3PR113	126	0.082	28.05	0.141	174.0	36.7	44.8	0.490	17.5	18.0	10.2	0.085	0.548	0	10	28			
A3PR114	152	0.059	16.95	0.136	175.5	34.3	45.3	0.708	11.0	15.1	46.3	0.124	0.489	6	10	28			
A3PR115	152	0.098	8.16	0.140	177.7	34.8	42.8	0.537	16.0	18.4	38.6	0.096	0.539	2	10	27			
A3PR116	151	0.089	14.61	0.144	177.9	35.2	43.4	0.539	17.2	20.0	46.4	0.096	0.549	4	10	27			
A3PR117	206	0.090	26.67	0.137	183.5	34.6	42.3	0.524	16.6	19.9	53.3	0.096	0.556	6	13	20			
A3PR118	202	0.102	27.45	0.136	184.6	36.2	44.6	0.520	16.9	19.8	46.9	0.096	0.578	0	13	20			
A3PR119	203	0.097	23.71	0.138	173.0	34.1	41.0	0.496	19.7	22.1	45.4	0.086	0.550	0	14	20			
A3PR110	301	0.096	19.79	0.134	180.6	35.5	50.0	0.813	17.1	21.7	51.5	0.147	0.572	2	10	26			
A3PR111	304	0.101	14.85	0.131	183.7	36.3	49.1	0.724	16.6	20.6	46.5	0.133	0.625	2	13	26			
A3PR112	304	0.095	23.16	0.131	183.1	37.1	51.8	0.767	17.2	21.2	45.1	0.140	0.616	6	12	20			
A3PR113	256	0.131	22.14	0.133	188.7	35.8	45.4	0.590	17.3	20.2	41.6	0.111	0.643	2	13	27			
A3PR114	254	0.120	24.17	0.142	185.8	36.5	47.4	0.629	17.7	21.9	57.5	0.117	0.636	9	13	20	LARGE BLISTERS ON TH		
A3PR115	251	0.119	25.21	0.138	183.5	36.0	46.9	0.644	13.2	17.3	50.4	0.118	0.622	2	13	20			

Table A2. Data with the IPST A platen.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM (MN/m <sup>2</sup> )	SEM %CV	IMPULSE (MPa.s)	OD BASIS WEIGHT (g/m <sup>2</sup> )	OD SOLIDS IN (%)	OD SHEET SOLIDS OUT (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	AVERAGE STFI INDEX (Nm/g)	95% C.I. (g/cm <sup>3</sup> )	DELM. CODE	PICK CODE	STICK COMMENTS				
<b>At Critical Temperature</b>																		
W1A1T16	170.5	0.186	11.29	0.1357	179.6	33.0	46.0	0.855	17.7	21.8	67.2	0.154	0.684	0	10	20		
W1A1T17	169.7	0.184	11.41	0.1367	174.0	31.6	46.8	1.024	17.5	22.8	72.9	0.178	0.671	0	10	20		
W1A1T19	185.8	0.188	10.64	0.1394	173.8	31.7	47.0	1.029	17.5	23.0	72.1	0.179	0.694	30.194	1.411	0	10	20
<b>Not At Critical Temperature</b>															NO TRANSERA DATA			
W1A1T20	188.3	0.184	9.78	0.1367	176.9	32.3	47.9	1.011	16.8	21.8	65.4	0.179	0.686	0	10	20		
W1A1T21	212.1	0.207	11.11	0.1384	173.4	31.8	49.4	1.120	16.8	22.7	71.6	0.194	0.723	0	10	20		
W1A1T24	212.1	0.184	4.89	0.1395	175.3	32.0	49.2	1.095	17.3	22.6	64.8	0.192	0.699	0	10	20		
W1A1T38	359.8	0.195	4.10	0.1353	176.9	32.3	52.9	1.203	17.1	20.5	36.5	0.213	0.691	0	10	20		
W1A1T39	358.9	0.199	3.02	0.1394	176.1	31.9	54.6	1.299	16.7	20.8	43.3	0.229	0.692	0	10	20		
W1A1T40	357.2	0.208	3.85	0.1406	180.8	32.8	53.5	1.181	16.6	20.7	45.4	0.214	0.699	0	10	20		
W1A1T44	207.0	0.186	4.84	0.1350	170.3	31.1	47.4	1.108	17.2	22.7	68.9	0.189	0.686	0	10	20		
W1A1T50	186.6	0.182	6.59	0.1385	173.0	31.5	47.7	1.080	16.8	22.7	74.8	0.187	0.703	0	10	20		
<b>Delaminated</b>															STUCK ON EDGE			
W1A1T06	189.2	0.109	22.94	0.1411	170.3	31.1	47.5	1.108	16.7	22.6	72.3	0.189	0.645	6	10	20		
W1A1T08	188.3	0.162	9.88	0.1351	172.8	31.5	47.5	1.071	17.3	23.1	76.6	0.185	0.623	4	10	20		
W1A1T15	162.0	0.170	10.00	0.1405	172.8	31.6	46.0	0.988	16.5	21.4	68.7	0.171	0.688	1	10	20		
W1A1T25	212.9	0.194	9.28	0.1380	175.7	31.9	49.3	1.108	16.6	22.5	72.5	0.195	0.683	2	10	20		
W1A1T28	230.8	0.181	2.76	0.1383	171.9	31.1	50.2	1.219	16.8	23.1	70.9	0.210	0.712	1	10	20		
W1A1T29	232.5	0.183	15.86	0.1397	177.7	32.2	50.4	1.124	16.7	22.7	72.8	0.200	0.701	2	10	20		
W1A1T33	249.4	0.176	3.98	0.1381	171.7	31.2	50.5	1.222	16.2	22.3	69.0	0.210	0.686	1	10	20		
W1A1T42	212.1	0.129	27.91	0.1410	179.6	32.7	49.0	1.020	17.2	22.8	74.1	0.183	0.648	6	10	20		
W1A1T47	189.2	0.180	11.67	0.1374	173.4	31.8	48.3	1.080	17.3	23.0	75.7	0.187	0.703	2	10	20		
W1A1T48	188.3	0.172	8.72	0.1381	171.3	31.2	48.2	1.131	17.0	22.9	74.3	0.194	0.693	2	10	20		
W1A1T56	145.0	0.134	11.94	0.1379	177.5	32.3	46.7	0.950	17.0	22.7	74.5	0.169	0.678	21.256	0.844	2	10	20
W1A1T65	169.7	0.118	31.36	0.1355	179.4	32.6	47.1	0.946	16.9	22.3	74.3	0.170	0.656	27.308	3.498	7	10	20
W1A1T66	171.4	0.131	24.43	0.1386	171.9	31.3	46.7	1.051	17.2	23.1	76.0	0.181	0.662	25.182	0.978	6	10	20
W1A1T67	170.5	0.112	32.14	0.1388	176.1	32.2	47.6	1.006	17.1	22.9	76.4	0.177	0.670	28.203	1.765	7	10	20
<b>At Critical Temperature</b>															STEAMED 21 SEC			
W1A2T14	162.0	0.170	7.06	0.1380	177.1	39.0	50.4	0.576	16.7	19.3	59.2	0.102	0.690	0	10	20		
W1A2T16	170.5	0.161	10.50	0.1374	181.0	39.6	49.6	0.598	17.4	19.7	58.6	0.092	0.729	0	10	20		
W1A2T20	170.5	0.165	4.85	0.1374	181.5	39.7	50.2	0.525	17.3	19.5	53.1	0.095	0.747	0	10	20		
<b>Not At Critical Temperature</b>															RETEST			
W1A2T25	212.9	0.178	8.43	0.1376	186.0	40.9	52.3	0.530	17.2	19.4	52.8	0.099	0.731	0	10	20		
W1A2T26	228.2	0.184	8.15	0.1380	185.0	40.4	53.1	0.593	17.4	20.3	59.9	0.110	0.751	0	10	20		
W1A2T28	230.8	0.181	4.97	0.1368	184.1	40.1	53.0	0.606	17.1	19.9	59.7	0.112	0.717	0	10	20		
W1A2T33	254.5	0.190	3.68	0.1381	183.3	39.5	54.0	0.676	17.2	20.0	52.3	0.124	0.739	0	10	20		
W1A2T43	357.2	0.180	4.44	0.1372	180.0	39.2	57.4	0.807	16.9	20.1	51.4	0.145	0.745	0	10	20		
W1A2T48	144.2	0.156	7.10	0.1383	184.1	40.3	48.8	0.433	16.8	18.6	50.6	0.080	0.693	31.042	1.490	0	10	20
W1A2T50	144.2	0.150	14.67	0.1375	181.5	39.8	48.6	0.456	17.5	19.5	56.1	0.083	0.699	30.054	1.347	0	10	20
W1A2T56	173.1	0.167	8.38	0.1367	179.6	39.8	50.0	0.514	16.9	19.2	58.0	0.092	0.707	0	10	20		
<b>Delaminated</b>															STUCK ON EDGE			
W1A2T07	188.3	0.135	28.89	0.1383	183.3	40.1	50.6	0.521	17.0	19.6	61.8	0.095	0.667	4	10	20		
W1A2T08	188.3	0.102	50.00	0.1398	180.8	39.6	50.3	0.538	17.1	19.7	61.9	0.097	0.648	6	10	20		
W1A2T10	187.5	0.117	33.33	0.1369	183.5	40.3	52.3	0.571	17.5	20.1	57.6	0.105	0.669	6	10	20		
W1A2T23	214.6	0.187	13.37	0.1402	180.2	39.3	52.6	0.641	17.3	20.4	63.0	0.116	0.744	2	10	20		
W1A2T29	230.8	0.174	13.22	0.1375	182.7	40.0	52.4	0.591	16.7	19.5	59.5	0.108	0.726	4	10	20		
W1A2T32	257.9	0.180	14.44	0.1382	184.1	40.1	53.7	0.634	17.1	19.9	54.9	0.117	0.724	2	10	20		
W1A2T38	292.7	0.204	2.94	0.1384	180.6	39.1	54.8	0.733	16.7	20.1	59.8	0.132	0.751	1	10	20		
W1A2T39	291.9	0.189	11.11	0.1390	183.9	39.8	55.1	0.694	16.8	19.9	54.0	0.128	0.749	1	10	20		
W1A2T44	355.5	0.186	5.91	0.1389	179.6	39.0	56.6	0.802	16.6	19.9	53.0	0.144	0.741	1	10	20		
W1A2T47	358.1	0.177	7.91	0.1389	179.0	39.5	58.5	0.823	16.8	19.9	48.6	0.147	0.727	1	10	20		
W1A2T52	187.5	0.162	12.35	0.1391	180.4	40.1	52.1	0.576	17.0	20.0	64.0	0.104	0.730	4	10	20		
W1A2T53	186.6	0.145	18.62	0.1394	180.2	39.8	51.1	0.556	16.7	19.3	59.2	0.100	0.716	4	10	20		
W1A2T54	179.8	0.163	11.04	0.1360	177.3	39.0	50.5	0.515	16.5	19.3	59.6	0.104	0.730	4	10	20		
W1A2T55	175.6	0.157	21.02	0.1377	181.7	40.4	51.0	0.515	16.9	19.3	59.4	0.094	0.706	6	10	20		
W1A2T57	173.1	0.171	7.02	0.1383	184.3	40.6	50.1	0.466	17.4	19.7	63.5	0.108	0.710	1	10	20		
W1A2T58	171.4	0.175	6.29	0.1372	179.4	39.5	50.0	0.532	17.1	19.7	61.5	0.095	0.703	1	10	20		
W1A2T59	169.7	0.174	9.20	0.1381	185.2	40.8	50.3	0.463	17.0	19.3	61.1	0.086	0.719	2	10	20		
W1A2T60	168.8	0.168	11.90	0.1374	182.7	40.2	50.0	0.490	17.4	19.6	56.7	0.089	0.698	2	10	20		

Table A2 Continued. Data with the IPST A platen.

PLATEN SURFACE	TEMP (C)	SEM (MN/m²q)	SEM %CV	OD BASIS	SHEET WEIGHT (g/m²)	SHEET SOLIDS IN (%)	SHEET SOLIDS OUT (%)	FELT MOISTURE CHANGE (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT MOISTURE SHEET LOSS (%)	WATER REMOVED (kg/m²)	US DENSITY (g/cm³)	AVERAGE STIFF INDEX (Nm@1.95% C.I.)	REWET CODE	STICK/PICK CODE	COMMENTS	STICK/STUCK ON CORNER
W1A2T61	200.2	0.147	10.88	0.1319	160.0	39.8	52.0	0.567	17.2	20.0	60.9	0.106	0.724	6	10	5	10	20
W1A2T62	200.2	0.179	8.38	0.1387	180.4	39.3	51.7	0.590	17.0	19.7	57.9	0.111	0.719	2	10	6	10	20
W1A2T63	199.4	0.182	6.59	0.1394	180.4	39.6	51.7	0.590	17.4	20.2	59.8	0.107	0.707					
W1A2T64	201.1	0.130	24.62	0.1392	182.7	40.0	52.0	0.576	16.8	19.5	60.0	0.105	0.686					
W1A2T65	200.2	0.154	27.27	0.1381	179.8	39.6	52.0	0.601	16.7	19.5	60.2	0.108	0.702					
W1A2T66	162.9	0.142	14.79	0.1401	179.4	39.0	50.8	0.597	17.1	19.9	61.6	0.107	0.702	27.549	4	10	10	20
W1A2T68	162.0	0.137	27.74	0.1391	179.4	39.4	49.7	0.528	16.9	20.1	79.0	0.095	0.695	26.055	1.116	7	10	20
W1A2T69	162.0	0.131	21.37	0.1365	179.2	39.3	51.2	0.589	17.0	16.6	68.4	0.106	0.666	25.810	2.249	4	10	20
W1A2T72	152.7	0.162	10.49	0.1359	182.7	40.6	49.5	0.442	16.6	19.1	70.3	0.081	0.664	29.842	2.018	2	10	20
<b>At Critical Temperature</b>																		
A3W1T05	144.2	0.136	8.82	0.1354	171.9	31.2	42.2	0.835	17.1	21.7	79.8	0.144	0.599	0	13	0	13	20
W1A3T38	145.9	0.177	11.30	0.1418	173.6	31.5	43.2	0.857	17.5	21.8	72.4	0.149	0.711	31.175	1.944	0	13	20
W1A3T39	144.2	0.155	18.06	0.1382	176.9	31.9	44.3	0.878	16.7	22.4	90.6	0.155	0.686	30.076	1.588	0	13	20
W1A3T40	144.2	0.146	11.64	0.1364	173.8	32.2	43.9	0.830	17.2	21.7	76.2	0.144	0.662	28.921	1.576	0	10	20
<b>Delaminated</b>																		
A3W1T06	186.6	0.131	23.66	0.1350	171.9	31.2	45.7	1.015	15.2	20.8	77.8	0.175	0.659	4	13	20		
A3W1T08	188.3	0.117	38.46	0.1360	177.1	32.0	44.9	0.886	17.7	22.2	73.3	0.159	0.575	6	13	20		
A3W1T11	205.3	0.111	38.74	0.1393	173.4	31.4	45.7	0.998	17.1	22.8	83.5	0.173	0.627	6	14	20		
A3W1T12	203.6	0.127	26.77	0.1373	176.3	31.8	44.9	0.918	17.4	22.0	71.3	0.162	0.611	6	13	20		
A3W1T14	203.6	0.086	50.90	0.1387	176.9	31.9	46.1	0.963	15.4	20.7	76.0	0.170	0.571	6	13	20		
A3W1T15	202.8	0.093	47.31	0.1392	177.9	32.5	46.4	0.923	16.6	21.4	72.2	0.164	0.572	6	13	20		
A3W1T16	169.7	0.144	21.53	0.1358	175.1	31.0	42.6	0.882	17.3	22.0	79.0	0.151	0.629	4	13	20		
A3W1T17	169.7	0.140	8.57	0.1357	175.3	31.8	44.8	0.920	16.6	21.6	75.7	0.161	0.640	4	13	20		
A3W1T18	171.4	0.129	27.13	0.1371	181.0	32.7	43.0	0.732	17.3	21.4	75.6	0.133	0.606	4	13	20		
A3W1T20	173.1	0.116	30.17	0.1378	179.0	32.3	43.7	0.811	17.1	21.5	75.1	0.145	0.599	4	13	20		
A3W1T21	162.0	0.174	13.22	0.1357	171.7	31.0	43.8	0.943	16.9	22.1	81.3	0.162	0.691	4	13	20		
A3W1T23	162.0	0.146	19.86	0.1396	172.8	31.2	42.4	0.852	17.5	21.8	74.2	0.147	0.643	4	13	20		
A3W1T24	162.9	0.141	16.31	0.1354	179.8	32.4	43.8	0.802	16.0	20.6	75.9	0.144	0.629	4	13	20		
A3W1T25	164.6	0.150	19.33	0.1391	173.4	31.3	42.3	0.828	17.5	21.9	78.0	0.144	0.661	4	14	20		
A3W1T27	156.1	0.153	16.34	0.1386	172.2	31.2	42.4	0.841	16.6	21.1	77.4	0.145	0.629	1	13	20		
A3W1T29	154.4	0.163	9.20	0.1370	177.1	32.0	43.3	0.817	16.8	21.1	74.6	0.145	0.644	1	13	20		
A3W1T30	155.2	0.145	15.17	0.1375	181.2	32.8	41.5	0.643	17.1	20.5	69.8	0.117	0.619	2	13	20		
<b>At Critical Temperature</b>																		
A4W1T02	145.0	0.128	8.59	0.1372	178.6	39.0	46.6	0.417	17.5	20.0	62.8	0.074	0.647	0	10	20		
A4W1T21	160.3	0.162	9.26	0.1406	178.8	39.5	47.7	0.439	17.5	19.8	73.0	0.078	0.694	0	13	20		
W1A4T34	145.0	0.154	7.14	0.1416	182.1	39.7	48.4	0.456	17.5	20.0	76.8	0.083	0.692	29.468	1.389	0	10	20
<b>Not At Critical Temperature</b>																		
A4W1T15	170.5	0.157	10.83	0.1389	182.3	39.6	47.7	0.429	17.1	19.3	68.6	0.078	0.662	0	10	20		
A4W1T16	173.1	0.145	8.28	0.1392	178.6	39.0	48.0	0.484	17.1	19.6	72.2	0.086	0.647	0	13	20		
W1A4T27	128.9	0.142	7.75	0.1374	180.8	39.4	47.6	0.436	17.2	20.7	111.0	0.079	0.658	28.955	1.213	0	10	20
<b>Delaminated</b>																		
A4W1T05	186.6	0.129	40.31	0.1381	182.5	39.7	49.1	0.481	17.3	19.1	48.4	0.088	0.643	4	13	20		
A4W1T06	186.6	0.094	58.51	0.1387	180.6	39.4	49.6	0.524	18.1	20.7	67.6	0.095	0.598	6	13	20		
A4W1T07	186.6	0.101	55.46	0.1366	182.5	39.5	49.5	0.512	17.0	19.4	63.0	0.093	0.607	6	13	20		
A4W1T13	206.2	0.080	55.00	0.1391	180.0	39.0	50.2	0.574	16.6	19.4	64.1	0.103	0.598	6	13	20		
A4W1T17	173.1	0.161	15.53	0.1385	184.1	40.0	48.2	0.428	17.2	19.5	70.6	0.079	0.658	2	13	20		
A4W1T24	162.0	0.144	7.64	0.1369	181.0	40.0	49.4	0.472	17.2	19.5	66.4	0.085	0.681	1	13	20		
W1A4T37	161.2	0.104	15.38	0.1353	186.6	40.8	50.4	0.467	17.6	20.3	76.0	0.087	0.694	27.378	1.397	7	10	20
W1A4T40	161.2	0.129	17.05	0.1369	180.6	39.5	49.0	0.489	17.3	18.5	33.3	0.088	0.683	30.907	1.253	4	10	20
W1A4T41	161.2	0.098	31.25	0.1372	182.3	39.8	49.1	0.475	16.7	19.3	71.0	0.087	0.653	25.638	0.985	7	10	20
W1A4T42	175.6	0.110	26.36	0.1401	183.9	40.1	50.5	0.513	16.4	19.7	83.3	0.094	0.696	27.126	1.923	7	10	20
W1A4T43	176.5	0.101	34.65	0.1403	179.4	39.0	49.3	0.534	17.2	18.7	36.8	0.096	0.658	24.123	1.981	7	10	20
W1A4T44	175.6	0.090	28.89	0.1344	181.2	39.5	49.3	0.500	17.0	18.8	50.7	0.091	0.657	25.580	1.401	7	10	20
W1A4T45	174.8	0.090	38.89	0.1384	181.7	39.9	49.6	0.489	17.1	19.6	68.5	0.089	0.660	25.351	1.770	7	10	20
<b>At Critical Temperature</b>																		
W5A1T33	174.8	0.162	8.64	0.1360	174.2	31.8	47.9	1.060	17.8	23.2	73.0	0.185	0.732	0	10	20		
W5A1T34	173.9	0.180	7.78	0.1383	176.9	32.4	46.8	0.951	22.1	70.6	0.168	0.742	0	10	20			
W5A1T36	174.8	0.179	7.82	0.1372	177.7	32.2	45.9				70.8	0.164	0.734	0	10	20		

Table A2 Continued. Data with the IPST A platen.

PLATEN SURFACE SAMPLE ID	TEMP (C)	SEM (MN/m <sup>2</sup> /g)	SEM %CV	IMPULSE (MPa·s)	OD BASIS WEIGHT (g/m <sup>2</sup> )	SHEET SOLIDS IN (%)	SHEET SOLIDS OUT (%)	SHEET MOISTURE CHANGE (%)	FELT GAIN (%)	FELT LOSS (%)	WATER REMOVED (g/cm <sup>3</sup> )	US DENSITY INDEX (Nm/g <sup>3</sup> )	AVERAGE STF 95% C.I. CODE	REWEET CODE	STICKY CODE	COMMENTS	
W5A1T44	167.1	0.139	12.23	0.1367	174.2	31.6	47.5	1.060	23.4	79.9	0.185	0.687	29.521	2.603	0	10	
W5A1T45	166.3	0.171	12.26	0.1365	179.4	32.7	45.7	0.867	17.6	22.7	0.156	0.693	30.775	2.404	0	10	
W5A1T46	165.4	0.169	14.79	0.1370	180.0	32.8	46.1	0.881	17.4	22.3	0.159	0.691	32.728	3.052	0	10	
W5A1T47	174.8	0.172	8.72	0.1404	180.2	32.8	47.5	0.947	17.0	22.6	0.06	0.171	0.712	30.987	1.289	0	10
W5A1T49	174.8	0.168	7.14	0.1380	174.4	31.8	45.9	0.967	16.8	21.9	73.0	0.169	0.694	32.564	1.481	0	10
W5A1T50	174.8	0.168	7.14	0.1396	174.8	31.9	45.9	0.961	17.0	22.3	74.0	0.168	0.702	29.497	0.923	0	10
<b>Not At Critical Temperature</b>																	
A1W5T04	229.9	0.178	8.43	0.1388B	180.6	32.9	49.4	1.016	16.9	22.1	67.5	0.184	0.705	0	10	20	
W5A1T11	188.3	0.175	7.87	0.1345	170.9	31.2	47.9	1.121	17.3	23.1	73.7	0.192	0.725	0	0	10	
W5A1T14	188.3	0.163	7.98	0.1371	171.7	31.3	47.3	1.081	16.2	21.8	72.5	0.186	0.691	0	10	20	
W5A1T15	187.5	0.164	4.88	0.1370	174.0	31.6	47.1	1.039	17.1	22.4	68.8	0.181	0.686	0	10	20	
W5A1T16	211.3	0.185	8.65	0.1389	175.0	31.8	48.2	1.076	16.1	21.8	72.3	0.188	0.720	0	10	20	
W5A1T17	211.3	0.178	3.93	0.1383	172.8	31.4	48.0	1.018	17.1	22.6	69.3	0.190	0.700	0	10	20	
W5A1T19	211.3	0.182	7.14	0.1384	178.1	32.4	48.2	1.018	17.2	22.3	69.0	0.181	0.711	0	10	20	
W5A1T26	358.1	0.183	2.73	0.1361	177.9	32.5	53.0	1.193	17.3	21.0	40.3	0.212	0.735	0	10	20	
W5A1T30	145.0	0.149	8.05	0.1380	181.7	33.0	46.0	0.853	17.0	21.4	69.4	0.155	0.686	32.097	1.678	0	10
W5A1T56	188.3	0.174	11.49	0.1377	177.1	32.2	46.8	0.975	17.3	22.8	75.4	0.173	0.708	29.841	0.683	0	10
<b>Delaminated</b>																	
A1W5T03	229.9	0.162	6.17	0.1391	179.4	32.7	49.0	1.017	17.1	22.4	67.3	0.183	0.710	1	10	20	
W5A1T24	229.1	0.157	3.49	0.1381	180.6	32.9	49.0	1.005	16.8	21.9	64.9	0.182	0.694	2	10	20	
W5A1T25	260.5	0.172	3.14	0.1362	172.8	31.6	49.7	1.152	17.1	22.8	68.1	0.199	0.701	2	10	20	
W5A1T25	257.9	0.191	3.14	0.1362	178.1	32.7	50.5	1.081	16.9	22.4	66.5	0.193	0.707	2	10	20	
W5A1T32	174.8	0.166	12.05	0.1369	170.5	31.2	47.0	1.075	17.5	23.0	72.5	0.183	0.734	2	10	20	
W5A1T38	201.9	0.171	19.30	0.1376	177.5	32.2	49.0	1.063	17.6	23.0	71.2	0.188	0.726	4	10	20	
W5A1T39	201.1	0.161	13.04	0.1390	170.5	31.2	47.9	1.114	17.6	23.1	69.9	0.190	0.708	2	10	20	
W5A1T52	187.5	0.168	8.33	0.1382	177.5	32.3	47.2	0.974	16.6	22.4	79.0	0.173	0.721	4	10	20	
W5A1T54	187.5	0.161	8.70	0.1393	177.1	32.2	46.5	0.958	17.4	22.9	76.3	0.170	0.706	31.976	0.947	2	10
W5A1T55	186.6	0.148	27.03	0.1383	179.2	32.7	47.8	0.966	17.6	23.2	78.7	0.173	0.694	28.255	4.518	4	10
<b>At Critical Temperature</b>																	
W5a2T54	212.1	0.192	5.21	0.1396	185.8	40.7	51.2	0.505	17.4	19.7	57.3	0.094	0.738	0	10	20	
W5a2T55	213.8	0.177	9.04	0.1378	180.8	39.4	51.7	0.606	17.0	20.2	65.7	0.110	0.729	0	10	20	
W5a2T61	209.6	0.173	8.09	0.1369	185.2	40.1	51.7	0.558	17.3	20.0	60.6	0.103	0.729	0	10	20	
W5a2T62	204.5	0.172	6.98	0.1384	184.3	40.0	51.4	0.557	16.4	19.4	63.5	0.103	0.730	0	10	20	
W5a2T78	196.0	0.166	6.63	0.1391	178.4	39.0	52.2	0.651	16.7	19.9	64.3	0.116	0.743	29.436	2.692	0	10
<b>Not At Critical Temperature</b>																	
A2W5T01	231.6	0.175	10.86	0.1365	186.0	40.8	52.2	0.535	17.3	19.9	60.4	0.100	0.750	0	10	20	
A2W5T04	229.1	0.168	4.76	0.1370	182.7	40.1	52.0	0.571	16.4	19.1	57.8	0.104	0.748	0	10	20	
A2W5T05	230.8	0.157	5.73	0.1375	179.0	39.2	51.5	0.611	16.6	19.2	54.4	0.109	0.720	0	10	20	
W5a2T09	162.9	0.138	8.70	0.1378	183.7	40.2	48.7	0.433	17.2	18.7	58.9	0.080	0.693	0	10	20	
W5a2T10	162.0	0.162	5.56	0.1365	186.0	40.6	48.6	0.406	16.9	18.7	53.8	0.075	0.693	0	10	20	
W5a2T12	188.3	0.155	7.74	0.1386	181.9	39.8	50.2	0.519	17.1	19.7	60.6	0.094	0.693	0	10	20	
W5a2T19	254.5	0.201	5.97	0.1372	185.2	40.3	52.9	0.593	16.9	19.9	64.9	0.110	0.739	0	10	20	
W5a2T22	272.4	0.185	3.24	0.1383	177.7	39.0	53.9	0.705	16.9	19.0	56.0	0.125	0.718	0	10	20	
W5a2T25	212.4	0.198	3.03	0.1380	180.0	39.4	53.0	0.654	17.2	20.1	56.5	0.118	0.727	0	10	20	
W5a2T29	299.5	0.184	7.07	0.1406	185.4	40.5	54.1	0.623	16.9	19.2	47.6	0.115	0.755	0	10	20	
W5a2T30	297.0	0.177	3.95	0.1373	180.8	39.5	54.8	0.453	17.5	19.6	55.1	0.128	0.735	0	10	20	
W5a2T32	322.4	0.166	16.27	0.1403	184.8	40.4	54.7	0.645	16.9	19.3	47.9	0.119	0.706	0	10	20	
W5a2T37	355.5	0.185	4.32	0.1389	182.7	39.9	56.3	0.732	16.3	18.9	44.1	0.134	0.737	0	10	20	
W5a2T38	356.4	0.192	5.21	0.1382	179.8	39.8	56.7	0.749	17.0	19.4	42.4	0.135	0.732	0	10	20	
W5a2T39	356.9	0.195	2.56	0.1392	178.6	39.3	55.5	0.743	16.6	19.3	46.2	0.133	0.747	0	10	20	
W5a2T41	145.9	0.174	13.79	0.1392	182.9	39.9	48.5	0.445	17.3	19.3	54.4	0.081	0.744	33.056	2.048	0	10
W5a2T43	144.2	0.169	4.73	0.1359	180.4	39.7	48.4	0.453	17.5	19.6	60.1	0.082	0.720	34.815	2.376	0	10
W5a2T47	175.6	0.170	8.82	0.1378	179.0	39.3	49.6	0.527	17.4	20.1	63.9	0.094	0.718	31.554	1.531	0	10
W5a2T68	145.0	0.142	10.56	0.1378	180.0	39.5	48.2	0.454	16.9	19.4	71.1	0.082	0.692	31.591	1.589	0	10
W5a2T70	145.9	0.160	11.25	0.1385	183.7	40.4	48.5	0.411	17.3	19.2	59.5	0.075	0.685	33.524	0.743	0	10
W5a2T71	171.4	0.197	4.57	0.1366	183.9	40.5	49.0	0.431	17.1	18.9	50.7	0.079	0.732	34.650	1.947	0	10
W5a2T72	169.7	0.186	7.53	0.1370	179.6	39.6	48.7	0.470	17.1	19.2	57.1	0.084	0.721	32.611	0	10	20
W5a2T73	170.5	0.176	6.82	0.1376	177.5	39.1	49.1	0.522	17.1	19.8	68.4	0.093	0.706	33.572	2.038	0	10
W5a2T74	171.4	0.163	9.82	0.1402	180.2	39.6	51.1	0.570	16.3	19.5	69.2	0.103	0.701	29.731	2.042	0	10
W5a2T77	188.3	0.152	11.84	0.1385	185.4	40.5	50.9	0.503	17.0	19.6	65.3	0.093	0.705	30.965	1.375	0	10

Table A2 Continued. Data with the IPST A platen.

PLATEN SURFACE SAMPLE ID	TEMP (C)	SEM (MN/m²g)	SEM (%CV)	IMPULSE (MPa)	OD BASIS WEIGHT (g/m²)	SHEET SOLIDS IN (%)	SHEET MOISTURE OUT (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT GAIN/LOSS (%)	WATER REMOVED (%)	US DENSITY (kg/m³)	AVERAGE STIFFNESS INDEX (N/mm)	95% C.I. DELAM. CODE	REWET CODE	STICKY PICK CODE	COMMENTS	
W5A2T88	187.5	0.186	12.37	0.1407	186.4	40.7	49.7	16.9	19.1	61.9	0.083	0.739	32.365	2.552	0	10	20	
Delaminated																		
W5A2T53	212.9	0.170	11.76	0.1404	179.0	39.1	51.1	60.2	17.1	20.1	67.1	0.108	0.735	2	10	20		
W5A2T53	207.9	0.163	14.11	0.1383	183.5	40.0	50.9	55.6	16.9	19.4	58.3	0.098	0.731	4	10	20		
W5A2T60	219.7	0.172	15.12	0.1396	176.9	39.3	52.0	61.7	17.3	19.7	52.3	0.109	0.738	4	10	20		
W5A2T63	205.3	0.174	9.77	0.1361	178.8	39.1	49.9	55.6	17.2	19.7	59.4	0.099	0.744	31.020	2.371	4	10	20
W5A2T81	205.3	0.175	8.57	0.1378	181.0	39.7	50.7	55.0	16.9	19.7	65.3	0.100	0.719	31.540	1.199	2	10	20
W5A2T82																		
At Critical Temperature																		
W5A3T31	145.0	0.150	8.67	0.1354	179.0	32.4	45.2	87.1	16.9	23.0	99.8	0.156	0.686	30.571	0.650	0	10	20
W5A3T52	161.2	0.162	14.81	0.1358	177.9	32.3	45.4	89.0	17.0	22.6	89.4	0.158	0.705	33.191	0.896	0	10	20
W5A3T54	162.9	0.163	11.04	0.1395	174.8	31.7	46.2	99.3	17.1	22.9	83.4	0.174	0.707	31.065	1.742	0	10	20
Not At Critical Temperature																		
A3W5T09	171.4	0.154	11.69	0.1366	180.6	32.6	42.6	71.8	17.2	21.3	79.6	0.130	0.665	0	13	20		
A3W5T12	189.2	0.158	11.39	0.1359	177.3	32.2	43.3	79.4	16.7	21.1	78.7	0.141	0.676	0	13	20		
A3W5T15	188.3	0.167	13.77	0.1375	175.0	31.8	44.3	89.3	16.1	21.1	77.5	0.156	0.668	0	13	20		
A3W5T16	205.3	0.173	10.98	0.1390	175.7	32.2	43.4	80.4	17.0	21.9	87.7	0.141	0.686	0	14	20		
A3W5T17	206.2	0.161	9.94	0.1382	177.9	32.4	43.8	80.7	17.0	21.6	78.3	0.144	0.682	0	13	20		
A3W5T19	206.2	0.167	15.57	0.1377	180.4	32.7	44.3	79.8	16.8	21.3	78.7	0.144	0.687	0	13	20		
A3W5T20	207.0	0.156	16.03	0.1378	176.1	31.9	43.5	83.9	16.9	20.8	64.5	0.148	0.672	0	13	20		
A3W5T22	229.9	0.182	11.54	0.1394	177.5	32.4	45.9	9.10	17.6	22.3	72.5	0.161	0.677	0	13	20		
Delaminated																		
A3W5T18	205.3	0.166	13.25	0.1369	178.8	32.6	45.1	85.6	17.1	22.0	81.6	0.153	0.684	2	13	20		
A3W5T22	227.4	0.181	6.08	0.1378	179.8	33.0	47.1	90.9	15.6	20.5	72.6	0.163	0.687	1	13	20		
A3W5T23	229.1	0.163	7.36	0.1359	180.8	32.9	46.4	88.7	14.6	19.7	73.7	0.160	0.671	1	10	29		
A3W5T36	188.3	0.106	31.13	0.1364	173.4	31.5	47.8	1.069	16.7	22.7	80.4	0.189	0.659	26.391	1.485	7	10	20
W5A3T36	187.5	0.093	23.66	0.1411	181.2	32.8	48.4	98.4	17.2	22.7	79.8	0.178	26.847	7	10	20		
W5A3T38	186.6	0.081	24.69	0.1372	174.8	31.6	48.5	1.102	17.1	23.3	82.8	0.193	0.671	26.268	1.305	7	10	20
W5A3T39	186.6	0.082	31.71	0.1378	173.4	31.4	48.8	1.138	16.8	23.1	81.1	0.197	0.653	26.033	1.919	7	10	20
A4W5T40	186.6	0.116	23.28	0.1408	177.7	32.1	45.9	93.9	17.4	23.4	91.5	0.167	0.684	6	10	20		
W5A3T46	162.0	0.145	17.93	0.1392	172.2	31.2	45.6	1.014	17.2	23.9	97.8	0.175	0.688	31.662	2.633	4	10	20
W5A3T53	162.0	0.114	42.11	0.1378	176.9	31.9	45.4	9.29	16.8	22.7	92.7	0.164	0.685	27.487	1.010	7	10	20
W5A3T58	169.7	0.142	17.61	0.1400	173.8	31.3	46.3	1.038	16.8	23.5	93.5	0.180	0.662	32.158	1.232	4	10	20
W5A3T59	170.5	0.142	17.61	0.1400	173.8	31.3	46.3	1.038	16.8	23.5	93.5	0.180	0.662	32.158	1.232	4	10	20
At Critical Temperature																		
A4W5T01	145.0	0.146	12.33	0.1395	178.1	39.0	46.7	424	17.8	19.8	65.5	0.076	0.718	0	13	20		
W5A4T32	145.9	0.155	18.71	0.1402	187.0	40.4	48.5	414	16.8	19.7	88.4	0.077	0.726	31.955	0.906	0	10	20
Not At Critical Temperature																		
A4W5T18	205.3	0.165	7.88	0.1369	181.2	39.4	48.6	479	16.8	19.3	67.5	0.087	0.691	0	13	20		
A4W5T19	205.3	0.167	8.98	0.1366	180.0	39.2	48.0	471	17.1	19.4	65.3	0.085	0.689	0	19	20		
A4W5T24	226.5	0.170	7.06	0.1361	185.6	40.5	50.6	493	17.2	19.6	64.6	0.091	0.709	0	10	20		
Delaminated																		
A4W5T15	188.3	0.145	12.41	0.1375	182.3	39.7	47.8	425	17.2	19.5	73.7	0.078	0.684	1	13	20		
A4W5T16	204.5	0.165	12.12	0.1361	179.0	39.1	48.8	508	17.2	20.1	79.9	0.091	0.707	1	13	20		
W5A4T37	175.6	0.135	23.70	0.1365	185.4	40.3	50.5	500	16.9	20.1	85.3	0.093	0.715	2.303	4	10	20	
W5A4T40	174.8	0.131	22.90	0.1365	186.8	40.6	49.7	452	17.4	20.1	79.9	0.085	0.707	29.789	1.664	6	10	20

Table A3. Data with the IPST C platen.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM (MN/m²g)	SEM %CV	IMPULSE (MPa·s)	OD BASIS WEIGHT (g/mm²)	Sheet SOLIDS IN (%)	Sheet SOLIDS OUT (%)	FELT MOISTURE RATIO (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT GAIN/LOSS (%)	WATER REMOVED (Kg/m²)	US DENSITY (g/cm³)	AVERAGE STIFF INDEX (Nm/g)	95% C.I. DELAM. CODE	REWET CODE	STICKY PICK CODE	COMMENTS
<b>At Critical Temperature</b>																		
W1C1T08	194.4	0.168	8.33	0.1397	172.2	34.2	46.6	0.781	16.6	20.4	65.3	0.134	0.675	30.279	1.666	0	10	20
W1C1T12	206.7	0.162	10.49	0.1363	181.7	36.0	46.4	0.620	17.2	20.1	59.3	0.113	0.664	28.140	1.519	0	10	20
<b>Not At Critical Temperature</b>																		
W1C1T10	192.5	0.175	8.00	0.1360	173.8	34.7	46.3	0.723	16.9	20.1	59.6	0.126	0.677	30.014	0.854	0	10	20
W1C1T18	183.1	0.155	4.52	0.1360	177.9	35.4	45.5	0.627	17.3	20.3	62.3	0.111	0.665	31.898	1.470	0	10	20
W1C1T19	184.0	0.170	9.41	0.1393	178.4	35.3	45.4	0.632	17.1	19.7	54.6	0.113	0.659	30.830	1.110	0	10	20
W1C1T20	184.9	0.162	8.64	0.1385	174.4	34.6	45.1	0.678	16.7	19.8	58.2	0.118	0.652	30.798	1.032	0	10	20
W1C1T23	169.8	0.155	12.90	0.1362	181.0	35.8	44.8	0.560	16.9	19.5	56.2	0.101	0.629	28.542	0.881	0	10	20
W1C1T25	168.9	0.160	11.25	0.1393	177.3	35.2	45.7	0.648	17.1	20.3	66.7	0.115	0.653	28.357	0.453	0	10	20
<b>Delaminated</b>																		
W1C1T15	207.6	0.145	15.86	0.1373	179.8	35.5	47.1	0.694	16.4	19.8	63.6	0.125	0.675	28.153	3.015	6	10	20
<b>At Critical Temperature</b>																		
W1C2T16	183.1	0.165	8.48	0.1356	176.5	41.9	50.4	0.399	17.2	18.9	57.5	0.070	0.699	29.255	0.694	0	10	20
W1C2T18	183.1	0.167	10.18	0.1385	180.2	42.9	50.3	0.341	17.5	18.9	51.7	0.061	0.698	28.992	1.355	0	10	20
W1C2T02	147.2	0.174	8.05	0.1405	179.2	42.7	48.8	0.295	17.1	18.5	56.8	0.053	0.700	31.425	1.620	0	10	20
W1C2T07	192.5	0.162	18.52	0.1394	177.9	42.6	50.3	0.359	17.2	18.7	50.2	0.064	0.700	30.055	1.543	1	10	20
W1C2T08	192.5	0.147	16.33	0.1412	174.4	41.4	50.9	0.453	17.6	19.3	52.9	0.079	0.692	28.799	3.260	4	10	20
<b>At Critical Temperature</b>																		
W5C1T11	212.3	0.175	13.71	0.1372	177.7	36.3	46.3	0.671	16.4	19.6	61.0	0.119	0.716	29.475	1.752	0	10	20
W5C1T12	213.3	0.168	11.31	0.1382	180.8	36.0	46.2	0.619	16.9	19.9	63.5	0.112	0.706	31.259	0.604	0	10	20
W5C1T13	211.4	0.165	10.30	0.1378	175.0	34.7	46.1	0.711	17.1	20.4	61.8	0.125	0.710	31.432	0.564	0	10	20
<b>Not At Critical Temperature</b>																		
W5C1T02	147.2	0.174	8.05	0.1405	179.2	42.7	48.8	0.295	17.1	18.5	56.8	0.053	0.700	31.425	1.620	0	10	20
W5C1T07	192.5	0.162	18.52	0.1394	177.9	42.6	50.3	0.359	17.2	18.7	50.2	0.064	0.700	30.055	1.543	1	10	20
W5C1T08	192.5	0.147	16.33	0.1412	174.4	41.4	50.9	0.453	17.6	19.3	52.9	0.079	0.692	28.799	3.260	4	10	20
<b>At Critical Temperature</b>																		
W5C1T11	212.3	0.175	12.32	0.1372	177.7	36.3	44.2	0.517	17.0	19.4	58.2	0.093	0.664	29.305	1.237	0	10	20
W5C1T12	213.3	0.168	9.35	0.1371	172.4	35.4	43.8	0.619	16.9	19.8	66.3	0.107	0.671	32.916	1.355	0	10	20
W5C1T13	211.4	0.165	9.62	0.1401	177.9	35.3	46.3	0.672	17.4	20.6	62.9	0.120	0.663	31.201	0.767	0	10	20
W5C1T14	193.4	0.160	10.63	0.1379	178.8	35.9	46.5	0.637	17.4	20.3	58.3	0.114	0.692	31.113	0.960	0	10	20
W5C1T10	193.4	0.156	12.18	0.1374	180.0	35.6	47.2	0.693	17.3	20.9	66.5	0.125	0.687	30.514	1.109	0	10	20
<b>Delaminated</b>																		
W5C1T17	230.3	0.139	16.55	0.1373	177.7	35.2	46.9	0.707	17.2	20.6	63.9	0.126	0.706	30.157	2.141	2	10	20
W5C1T21	239.7	0.134	19.40	0.1408	171.3	34.0	48.1	0.866	18.0	22.5	73.9	0.148	0.726	30.954	0.702	4	10	20
<b>At Critical Temperature</b>																		
W5C2T11	212.3	0.161	4.97	0.1390	180.4	43.0	51.3	0.376	16.8	18.5	58.0	0.068	0.739	30.558	2.936	0	10	20
W5C2T12	213.3	0.149	8.72	0.1387	173.2	41.1	50.3	0.447	17.4	19.2	55.3	0.077	0.718	28.563	0.837	0	10	20
W5C2T18	231.2	0.161	5.69	0.1374	177.3	41.9	52.4	0.476	17.2	19.1	50.8	0.084	0.725	32.803	1.367	0	10	20
W5C2T21	249.2	0.169	8.88	0.1376	173.6	41.3	52.0	0.499	17.0	19.4	63.7	0.087	0.725	31.144	1.969	0	10	20
<b>Not At Critical Temperature</b>																		
W5C2T05	147.2	0.140	7.86	0.1379	174.4	41.5	47.9	0.321	17.7	18.8	45.2	0.056	0.698	30.955	1.846	0	10	20
W5C2T06	194.4	0.157	8.28	0.1357	179.6	42.6	50.1	0.353	17.1	18.4	46.4	0.063	0.728	29.693	1.506	0	10	20
W5C2T07	194.4	0.176	6.82	0.1372	180.2	42.7	49.5	0.324	17.7	18.8	43.6	0.058	0.737	32.613	1.339	0	10	20
W5C2T10	192.5	0.150	5.33	0.1405	172.2	41.0	49.3	0.414	17.5	18.9	45.2	0.071	0.725	27.874	3.208	0	10	20
W5C2T25	250.1	0.145	10.34	0.1379	180.4	43.0	53.5	0.458	17.6	19.6	58.3	0.083	0.703	27.310	1.351	0	10	20
W5C2T26	269.0	0.202	6.44	0.1389	176.7	42.2	52.1	0.450	16.8	18.8	57.2	0.080	0.767	32.869	0.790	0	10	20
W5C2T27	269.9	0.218	5.05	0.1400	179.4	42.8	51.7	0.399	16.9	18.5	50.8	0.072	0.774	33.904	0.897	0	10	20
W5C2T28	268.1	0.172	8.72	0.1380	178.1	42.3	50.0	0.441	17.5	19.3	51.8	0.079	0.729	28.595	0.929	0	10	20
W5C2T32	286.9	0.165	9.09	0.1402	176.7	41.8	53.6	0.528	17.1	18.7	39.1	0.093	0.728	30.515	1.788	0	10	20
<b>Delaminated</b>																		
W5C2T16	232.2	0.185	7.03	0.1396	176.1	42.0	50.8	0.411	17.1	19.0	58.1	0.072	0.760	31.686	3.344	1	10	20

Table A4. Data for the double-felted pressing control cases.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM (MN/m²kg)	SEM %CV	OD BASIS IMPULSE (MPa.s)	OD BASIS WEIGHT (g/m²)	OD SHEET SOLIDS (%)	OD SHEET SOLIDS (%)	OD MOISTURE IN (%)	OD MOISTURE OUT (%)	AVERAGE STI INDEX (Nm/g)	US REMOVED DENSITY (kg/cm³)	95% C.I. DELAM CODE	REWET CODE	STICKY PICK CODE	COMMENTS
W1D1T04	99.0	0.141	23.40	0.1349	174.6	34.6	41.2	0.469	19.7	56.3	0.082	0.611	29.616	1.219	0
W1D1T04	99.0	0.119	19.33	0.1415	180.4	35.9	41.9	0.404	16.8	48.4	0.073	0.604	28.234	0.845	0
W1D1T05	98.1	0.149	15.44	0.1370	171.7	34.2	41.1	0.492	16.7	56.4	0.073	0.604	28.234	0.845	0
W1D1T06	99.0	0.132	17.42	0.1396	173.0	34.4	42.1	0.532	16.3	43.3	0.085	0.636	29.909	0.364	0
W1D1T07	99.0	0.123	14.63	0.1382	173.0	34.4	41.7	0.510	16.7	17.5	0.092	0.625	28.986	0.621	0
W1D1T08	99.0	0.123	14.63	0.1382	173.0	34.4	41.7	0.510	17.1	39.8	0.088	0.596	29.009	0.902	0
W1D1T09	99.0	0.147	17.69	0.1426	168.6	40.4	45.2	0.265	17.6	48.6	0.045	0.677	29.210	1.537	0
At 40% Solids															
W1D2T01	99.0	0.145	11.72	0.1378	173.4	40.8	44.7	0.216	16.3	47.0	0.037	0.664	30.455	0.988	0
W1D2T04	99.0	0.137	18.98	0.1356	170.5	40.7	44.1	0.188	18.1	36.5	0.032	0.640	27.910	2.274	0
W1D2T09	98.1	0.145	24.14	0.1354	177.1	41.6	44.6	0.161	18.3	18.7	0.029	0.672	29.217	0.773	0
At 42% Solids															
W1D2T05	99.0	0.142	11.97	0.1395	176.5	41.7	45.1	0.180	17.5	17.0	0.032	0.634	30.267	1.087	0
W1D2T10	98.1	0.158	12.66	0.1382	177.5	35.0	41.3	0.495	16.3	19.1	0.077	0.670	30.910	1.237	0
W5D1T01	99.0	0.141	21.99	0.1339	172.2	34.2	41.2	0.495	18.0	24.3	0.085	0.649	30.926	2.926	0
W5D1T01	99.0	0.141	17.73	0.1315	178.8	35.4	41.2	0.401	16.8	17.9	0.072	0.648	32.004	1.173	0
W5D1T03	99.0	0.139	15.11	0.1393	176.5	35.1	41.3	0.429	16.6	20.0	0.076	0.651	31.030	1.867	0
W5D1T04	99.0	0.127	23.62	0.1399	175.3	35.0	41.5	0.443	17.1	34.4	0.078	0.629	30.565	3.078	0
W5D1T05	99.0	0.144	22.92	0.1401	180.2	35.6	41.5	0.398	17.7	18.7	0.072	0.591	30.275	0.712	0
W5D1T09	99.0	0.149	13.42	0.1383	174.2	41.9	44.3	0.133	18.3	19.5	0.023	0.643	32.503	0.457	0
W5D1T10	99.0	0.158	12.66	0.1382	177.5	35.0	41.3	0.434	18.1	20.2	0.077	0.670	30.910	1.237	0
W5D1T10	99.0	0.140	10.71	0.1377	168.8	40.3	43.6	0.191	18.4	16.8	0.032	0.670	32.984	2.178	0
At 40% Solids															
W5D2T09	99.0	0.149	13.42	0.1383	174.2	41.9	44.3	0.133	18.3	18.9	0.023	0.643	32.503	0.457	0
W5D2T09	99.0	0.149	13.42	0.1383	174.2	41.9	44.3	0.133	18.3	17.0	0.023	0.643	31.7	20	TOP BOTTOM
At 42% Solids															
W5D2T05	99.0	0.149	13.42	0.1383	174.2	41.9	44.3	0.133	18.3	18.9	0.023	0.643	32.503	0.457	0
W5D2T05	99.0	0.149	13.42	0.1383	174.2	41.9	44.3	0.133	18.3	17.0	0.023	0.643	31.7	20	TOP BOTTOM

## **APPENDIX B**

The following tables contain the data that were not used for analysis. Data were not used if the ingoing solids or basis weight were out of the established range. Also rejected were data where the sheet stuck to the platen (except at the corner) or showed any other anomalous behavior.

Table B1. Data with the IPST A platen.

PLATEN SURFACE	SAMPLE ID	TEMP (C)	SEM (MN/m²kg)	SEM %CV	IMPULSE WEIGHT (MPa.s)	OD BASIS WEIGHT (g/m²)	SHEET SOLIDS (%)	SHEET MOISTURE IN (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT GAIN/LOSS (%)	WATER REMOVED (%)	US DENSITY (Kg/m³)	AVERAGE STFI INDEX (Nm/g)	95% C.I. DELAM CODE	REWET CODE	STICK PICK CODE	COMMENTS
W1AIT01	145.9	0.149	10.74	0.1260	179.0	32.6	46.1	0.895	17.2	21.8	70.6	0.160	0.649	0.000	0	10	27	
W1AIT02	145.0	0.140	6.43	0.1300	178.8	32.6	45.5	0.868	17.3	21.9	70.0	0.155	0.623	0.000	0	10	27	
W1AIT03	144.2	0.152	7.89	0.1225	177.3	32.4	45.1	0.870	17.4	22.2	75.9	0.154	0.628	29.532	1.516	0	10	26
W1AIT04	144.2	0.164	8.54	0.1299	171.9	31.3	45.0	0.866	17.2	22.5	75.2	0.166	0.635	0.000	0	10	29	
W1AIT05	145.0	0.138	7.97	0.1352	170.5	31.0	57.6	1.486	17.2	22.0	45.6	0.253	0.633	0.000	0	10	28	
W1AIT07	189.2	0.093	37.63	0.1367	167.4	30.5	47.1	1.151	16.1	22.3	74.2	0.193	0.612	0.000	6	10	20	
W1AIT09	187.5	0.088	27.27	0.1388	184.1	33.7	47.4	0.856	16.7	21.5	72.8	0.158	0.595	0.000	6	10	20	
W1AIT10	187.5	0.098	31.63	0.1382	189.7	34.6	47.7	0.796	16.9	21.4	73.6	0.151	0.599	0.000	6	10	20	
W1AIT11	162.0	0.168	12.50	0.1120	186.8	34.2	45.3	0.716	17.3	21.1	64.4	0.134	0.659	0.000	0	10	20	
W1AIT12	162.0	0.160	9.38	0.1256	180.2	33.0	46.2	0.865	17.2	21.5	65.7	0.156	0.652	29.728	1.274	0	10	20
W1AIT13	162.9	0.179	7.26	0.1357	166.8	30.5	46.5	1.127	17.3	23.1	75.6	0.188	0.676	28.792	2.032	1	10	25
W1AIT14	163.7	0.177	6.21	0.1415	173.4	31.6	47.0	1.035	17.8	23.1	71.6	0.180	0.675	0.000	0	10	29	
W1AIT16	179.0	0.190	4.47	0.1372	181.9	33.1	47.0	0.900	17.4	22.3	69.4	0.164	0.583	30.293	0.957	0	10	20
W1AIT22	212.9	0.179	10.61	0.1120	175.9	32.3	50.4	1.112	16.9	22.4	67.7	0.196	0.701	0.000	0	10	20	
W1AIT23	212.9	0.149	20.81	0.1380	181.9	33.2	49.7	1.003	17.3	22.5	69.6	0.182	0.685	0.000	2	10	20	
W1AIT26	437.9	0.160	9.38	0.1448	169.1	31.1	55.4	1.416	16.3	19.7	31.7	0.239	0.682	0.000	0	10	20	
W1AIT27	232.5	0.166	4.62	0.1391	169.7	30.8	53.8	1.382	17.2	23.0	59.9	0.234	0.678	0.000	1	10	28	
W1AIT30	231.6	0.182	5.34	0.1390	169.9	30.8	50.1	1.255	16.8	22.9	68.3	0.213	0.694	0.000	2	10	20	
W1AIT31	229.9	0.190	4.21	0.1383	169.7	30.8	50.5	1.269	16.9	23.5	71.3	0.215	0.698	0.000	1	10	20	
W1AIT32	252.0	0.179	7.03	0.1393	175.0	31.9	55.5	1.334	16.2	21.8	57.5	0.233	0.692	0.000	1	10	27	
W1AIT34	252.0	0.193	4.66	0.1377	174.6	31.9	51.5	1.189	17.0	22.7	66.6	0.208	0.688	0.000	1	10	25	
W1AIT35	249.4	0.191	6.28	0.1382	170.3	31.1	50.6	1.237	16.8	22.8	66.3	0.211	0.679	0.000	1	10	25	
W1AIT36	252.0	0.175	13.71	0.1372	181.0	33.2	52.4	1.104	17.2	22.5	63.8	0.200	0.665	0.000	1	10	20	
W1AIT37	358.1	0.201	4.48	0.1355	166.8	30.4	53.8	1.432	16.9	21.0	39.6	0.239	0.720	0.000	0	10	20	
W1AIT41	212.1	0.181	12.71	0.1294	184.3	33.6	48.8	0.929	16.9	22.5	76.0	0.171	0.692	0.000	0	10	20	
W1AIT43	214.6	0.142	33.10	0.1377	183.3	33.4	49.0	0.951	17.1	22.5	73.2	0.174	0.647	0.000	5	10	20	
W1AIT46	204.5	0.180	7.78	0.1352	167.8	30.6	53.0	1.383	17.0	23.5	68.7	0.232	0.651	0.000	2	10	27	
W1AIT48	189.2	0.183	10.38	0.1380	169.1	30.9	47.0	1.110	17.1	22.7	72.2	0.188	0.676	0.000	0	10	20	
W1AIT49	186.6	0.163	5.52	0.1372	185.4	33.5	48.7	0.934	17.2	22.4	74.0	0.173	0.684	0.000	0	10	20	
W1AIT51	179.0	0.178	7.87	0.1379	166.2	30.4	47.3	1.180	17.1	22.6	67.5	0.196	0.677	0.000	0	10	27	
W1AIT52	145.0	0.154	10.39	0.1379	182.9	33.7	45.5	0.768	17.2	21.7	76.4	0.141	0.673	32.156	1.287	0	10	20
W1AIT53	145.9	0.145	13.10	0.1315	176.3	32.5	45.4	0.873	17.1	22.0	73.8	0.154	0.647	32.455	1.118	0	10	20
W1AIT54	145.0	0.148	6.76	0.1363	182.9	33.6	46.2	0.810	17.5	22.2	74.0	0.148	0.663	28.908	0.813	0	10	20
W1AIT55	145.0	0.144	9.03	0.1367	164.9	30.4	48.4	1.227	17.3	22.9	68.0	0.202	0.661	0.000	1	10	27	
W1AIT56	178.1	0.173	6.94	0.1398	169.3	31.2	50.3	1.215	16.9	22.3	63.6	0.206	0.659	0.000	0	10	27	
W1AIT57	178.1	0.167	12.57	0.1422	160.0	29.5	48.0	1.299	16.7	22.7	70.6	0.208	0.674	0.000	0	10	27	
W1AIT59	145.0	0.151	7.95	0.1377	174.4	31.8	49.6	1.128	17.1	22.3	63.9	0.197	0.663	30.332	1.532	0	10	20
W1AIT60	145.0	0.150	13.33	0.1396	173.2	31.5	47.0	1.047	17.4	23.3	80.1	0.181	0.676	30.102	2.137	2	10	25
W1AIT61	144.2	0.153	6.54	0.1395	177.3	32.3	46.5	0.942	16.9	22.2	77.5	0.167	0.658	29.946	2.399	0	10	25
W1AIT62	144.2	0.154	8.44	0.1374	175.3	32.0	46.5	0.977	17.4	22.8	77.7	0.171	0.675	28.374	1.716	0	10	25
W1AIT63	170.5	0.127	33.07	0.1376	183.1	33.4	50.3	1.215	16.7	21.9	77.8	0.159	0.671	27.124	2.202	7	10	20
W1AIT64	169.7	0.114	28.95	0.1394	170.3	31.1	47.7	1.122	17.0	23.0	75.6	0.191	0.660	26.155	1.477	7	10	25
W1AIT66	162.0	0.127	22.83	0.1405	171.5	30.9	47.4	1.123	16.7	23.5	86.6	0.193	0.695	0.000	0	10	20	
W1AIT69	153.5	0.150	14.00	0.1365	172.4	31.2	46.7	1.064	17.2	23.2	81.1	0.183	0.663	29.431	1.774	2	10	26
W1AIT70	152.7	0.156	12.18	0.1345	183.9	33.4	46.9	0.866	16.9	21.7	73.3	0.159	0.655	28.815	2.100	0	10	20
W1AIT71	152.7	0.153	23.53	0.1382	173.2	31.4	45.2	0.970	17.5	23.0	76.6	0.168	0.644	30.414	4.247	4	10	25
W1AIT72	153.5	0.160	12.50	0.1384	174.8	31.8	46.4	0.984	16.8	22.4	77.4	0.172	0.686	29.848	1.627	2	10	25
W1AIT73	154.4	0.141	15.60	0.1373	183.1	33.4	47.5	0.892	17.9	22.9	74.3	0.163	0.647	29.392	1.336	2	10	26
W1A2T01	145.9	0.157	10.19	0.1442	190.3	41.7	49.3	0.374	17.0	18.7	54.8	0.071	0.686	0	0	10	20	
W1A2T02	145.0	0.172	3.49	0.1459	192.4	42.0	49.4	0.358	17.0	18.4	51.5	0.069	0.681	0	0	10	20	
W1A2T03	145.0	0.149	7.38	0.1462	173.4	37.8	51.9	0.716	17.1	19.3	41.2	0.124	0.663	0	0	10	28	
W1A2T04	145.9	0.153	11.11	0.1394	179.0	39.1	49.4	0.535	16.5	18.3	44.8	0.096	0.661	0	0	10	28	
W1A2T05	145.0	0.164	7.93	0.1542	180.0	39.3	49.5	0.526	17.2	19.6	57.1	0.095	0.664	0	0	10	26	
W1A2T06	189.2	0.138	32.61	0.1429	182.9	40.0	50.1	0.504	17.3	19.9	64.2	0.092	0.688	0	0	10	20	
W1A2T08	187.5	0.108	34.26	0.1392	175.5	38.5	50.5	0.620	17.1	20.0	60.3	0.109	0.659	0	0	10	20	
W1A2T11	162.0	0.183	6.56	0.1412	186.6	41.2	49.5	0.406	16.9	18.4	42.9	0.076	0.701	0	0	10	20	
W1A2T12	162.9	0.179	7.26	0.1386	175.0	38.2	49.6	0.600	16.9	19.7	60.8	0.105	0.699	0	0	10	20	
W1A2T13	162.9	0.186	8.06	0.1391	175.0	38.3	49.0	0.569	16.9	19.5	58.6	0.100	0.704	0	0	10	20	
W1A2T15	162.0	0.171	8.19	0.1377	174.4	38.2	48.9	0.571	16.6	19.0	56.9	0.100	0.703	0	0	10	20	
W1A2T17	1																	

Table B1 Continued. Data with the IPST A platen.

PLATEN SURFACE ID	SAMPLE ID	TEMP (C)	SEM (MN/mkg)	SEM %CV	OD BASIS WEIGHT (g/m <sup>2</sup> )	IMPULSE (Mpa.s)	SHEET SOLIDS IN (%)	SHEET SOLIDS OUT (%)	SHEET MOISTURE CHANGE (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	WATER REMOVED (%)	US DENSITY (kg/m <sup>3</sup> )	AVERAGE STFI INDEX (Nm/g)	STICKY PICK CODE	REWET CODE	COMMENT
W1A2116	169.7	0.169	11.24	0.1376	188.3	41.1	49.1	39.7	16.8	18.4	50.7	0.075	0.697	0	10	20	
W1A2119	171.4	0.174	11.49	0.1380	193.0	42.3	50.8	39.8	16.8	18.5	48.9	0.077	0.707	0	10	20	
W1A2122	212.1	0.176	6.82	0.1414	178.8	38.8	52.0	65.9	17.1	20.0	58.4	0.118	0.720	0	10	20	
W1A2122	213.8	0.190	7.37	0.1382	178.1	38.7	52.8	68.7	16.6	19.9	61.1	0.122	0.735	0	10	20	
W1A2124	213.8	0.176	11.36	0.1387	188.5	41.1	52.7	53.5	16.8	19.2	54.0	0.101	0.728	1	10	20	
W1A2127	229.1	0.184	4.89	0.1398	171.5	37.7	52.8	75.4	17.2	20.9	65.2	0.129	0.727	0	10	20	
W1A2130	229.9	0.186	4.30	0.1357	174.6	38.1	52.0	70.5	16.6	20.2	66.4	0.123	0.740	0	10	20	
W1A2131	256.2	0.173	15.61	0.1390	198.2	43.3	54.8	487	16.4	18.3	44.6	0.097	0.740	0	10	20	
W1A2134	255.4	0.193	3.11	0.1388	179.6	38.9	54.7	745	16.8	20.1	57.6	0.134	0.735	0	10	20	
W1A2135	257.1	0.186	2.69	0.1388	174.8	38.1	54.2	782	16.8	20.4	60.6	0.137	0.739	0	10	20	
W1A2136	293.6	0.204	2.94	0.1403	174.6	37.8	55.1	830	17.0	20.7	60.3	0.145	0.753	1	10	20	
W1A2137	294.4	0.200	5.00	0.1381	175.9	38.1	54.8	799	16.9	20.4	56.8	0.141	0.742	0	10	20	
W1A2140	295.3	0.206	5.34	0.1402	171.7	37.5	54.9	846	16.7	20.4	60.2	0.145	0.758	0	10	20	
W1A2141	356.4	0.176	4.55	0.1440	180.0	39.9	59.0	814	16.3	19.6	51.4	0.147	0.737	1	10	20	
W1A2142	358.9	0.179	6.15	0.1414	185.0	40.4	57.1	723	16.6	19.4	47.5	0.134	0.741	0	10	20	
W1A2146	145.0	0.159	11.95	0.1350	178.6	39.7	50.6	544	16.5	18.0	35.4	0.097	0.692	0	10	27	
W1A2147	144.2	0.160	15.63	0.1377	197.2	43.6	49.7	283	17.0	18.2	47.9	0.056	0.701	28.5	18	29	
W1A2149	145.9	0.152	11.18	0.1371	186.0	41.2	49.2	398	17.3	19.2	61.1	0.074	0.693	30.190	2.194	0	
W1A2151	188.3	0.143	15.38	0.1391	186.8	41.3	51.7	487	17.3	20.0	70.5	0.091	0.737	6	10	20	
W1A2167	162.9	0.147	21.77	0.1399	188.7	40.9	50.5	465	16.9	18.7	44.8	0.088	0.681	27.863	1.498	4	
W1A2170	162.0	0.164	12.80	0.1386	176.5	38.5	49.5	578	16.2	19.4	71.6	0.102	0.677	28.500	3.684	4	
W1A2171	152.7	0.175	7.43	0.1362	177.5	38.9	49.5	553	16.8	20.1	79.5	0.098	0.699	30.851	0.753	0	
W1A2173	152.7	0.146	9.59	0.1423	174.4	38.3	53.5	743	17.0	20.5	64.5	0.130	0.656	28.608	1.538	10	
W1A2174	154.4	0.150	8.67	0.1386	170.7	37.3	49.4	657	16.5	20.2	74.2	0.112	0.650	28.884	2.761	0	
W1A2175	152.7	0.173	7.51	0.1386	196.1	42.8	50.6	360	17.3	18.8	50.5	0.071	0.657	27.941	1.795	0	
A3W1T01	145.0	0.121	22.31	0.1240	167.8	30.4	42.7	951	16.6	22.2	84.5	0.160	0.581	0	13	20	
A3W1T02	145.9	0.120	17.50	0.1174	171.3	31.2	42.5	849	17.3	21.7	75.9	0.146	0.581	6	14	20	
A3W1T03	145.0	0.116	12.93	0.1304	180.4	32.6	42.7	889	17.0	20.9	76.7	0.124	0.591	0	13	20	
A3W1T04	144.2	0.126	8.73	0.1329	180.6	32.7	42.4	700	18.2	22.0	77.0	0.126	0.593	0	13	21	
A3W1T07	187.5	0.104	36.54	0.1352	187.7	34.1	45.4	732	15.9	19.9	71.7	0.137	0.594	4	13	20	
A3W1T09	188.3	0.117	41.88	0.1377	171.5	31.1	43.9	936	16.3	21.3	76.7	0.161	0.565	6	13	20	
A3W1T10	189.2	0.102	44.12	0.1342	174.0	31.4	43.4	878	17.8	22.2	72.7	0.153	0.578	6	14	20	
A3W1T13	205.3	0.103	33.98	0.1394	170.1	30.6	43.7	975	19.0	23.8	73.8	0.166	0.581	6	14	20	
A3W1T13	171.4	0.148	10.14	0.1343	182.1	32.9	43.7	924	17.3	21.1	68.3	0.137	0.646	0	13	20	
A3W1T19	164.6	0.147	17.01	0.1366	167.6	30.2	42.1	929	17.0	22.1	80.7	0.156	0.636	4	13	20	
A3W1T22	154.4	0.163	13.50	0.1376	160.8	29.3	42.5	1086	15.9	21.4	79.5	0.171	0.662	2	13	20	
A3W1T26	155.2	0.155	9.68	0.1379	183.7	33.2	42.6	6686	17.4	20.9	71.9	0.122	0.630	0	13	20	
W1A3T31	128.1	0.162	11.14	0.1323	173.0	31.3	44.1	926	15.8	20.7	73.2	0.160	0.634	29.880	0.976	13	
W1A3T32	128.1	0.140	27.17	0.1307	188.7	34.2	44.5	649	16.9	19.9	60.9	0.123	0.645	28.347	2.634	10	
W1A3T33	128.1	0.135	20.74	0.1351	178.6	32.4	43.9	811	18.0	23.0	90.9	0.145	0.653	29.241	0.642	10	
W1A3T34	128.1	0.155	10.97	0.1382	174.6	31.7	50.1	1162	17.2	22.6	66.9	0.203	0.678	29.716	2.864	0	
W1A3T35	128.1	0.146	11.64	0.1408	175.9	31.8	44.0	8689	17.2	22.0	79.7	0.153	0.654	30.518	1.208	0	
W1A3T36	145.9	0.162	13.58	0.1406	170.1	30.8	44.4	992	17.9	23.4	82.8	0.169	0.706	30.020	0.990	13	
W1A3T37	145.0	0.166	7.23	0.1386	184.1	33.9	45.4	746	15.6	20.7	90.8	0.137	0.698	30.325	1.633	13	
W1A3T41	153.5	0.168	12.03	0.0985	176.7	32.1	44.0	841	16.9	22.5	93.6	0.149	0.683	30.134	0.668	13	
W1A3T42	154.4	0.146	20.55	0.1109	177.1	32.1	44.5	864	17.4	23.0	92.0	0.153	0.650	28.125	1.081	10	
W1A3T43	152.7	0.134	15.67	0.1188	162.0	29.4	45.5	1201	16.6	23.2	84.5	0.195	0.653	26.275	2.712	4	
W1A3T44	153.5	0.111	33.33	0.1242	163.1	29.6	44.8	1142	17.9	23.4	76.7	0.185	0.631	25.504	4.028	7	
W1A3T45	153.5	0.131	20.61	0.1286	179.4	32.7	45.7	8655	16.7	21.7	78.8	0.155	0.658	26.762	1.242	6	
A4W1T01	144.2	0.134	6.72	0.1374	176.1	38.2	46.3	456	16.5	18.8	68.2	0.080	0.671	0	13	20	
A4W1T03	144.2	0.137	11.68	0.1368	176.3	38.4	46.9	469	16.8	19.1	68.2	0.083	0.653	0	10	20	
A4W1T04	148.4	0.131	6.87	0.1353	176.5	38.5	46.3	439	17.0	19.4	73.8	0.078	0.642	0	13	20	
A4W1T08	187.5	0.135	31.78	0.1367	178.8	38.7	49.2	549	16.5	19.2	67.2	0.098	0.629	4	13	20	
A4W1T09	186.6	0.116	37.07	0.1378	176.1	38.2	48.9	575	18.4	21.3	72.6	0.101	0.607	4	13	20	
A4W1T10	204.5	0.161	8.07	0.1385	180.2	38.9	51.8	638	17.2	20.3	66.4	0.115	0.687	4	13	20	
A4W1T11	205.3	0.156	26.92	0.1402	167.4	36.5	49.5	721	17.4	20.9	73.3	0.121	0.672	2	13	20	
A4W1T12	203.6	0.107	57.94	0.1386	178.4	38.6	50.2	589	17.5	20.4	67.7	0.107	0.629	6	13	20	
A4W1T14	205.3	0.098	47.47	0.1408	175.3	38.0	49.2	604	17.0	20.1	71.7	0.106	0.601	6	13	20	
A4W1T18	170.5	0.158	8.23	0.1375	178.6	38.8	47.9	498	17.3	20.2	78.5	0.087	0.662	0	13	20	

Table B1 Continued. Data with the IPST A platen.

PLATEN SURFACE SAMPLE ID	TEMP (C)	SEM (MN/m²/g)	SEM %CV	OD BASIS IMPULSE WEIGHT (MPa·s)	SHEET SOLIDS IN (%)	SHEET SOLIDS OUT (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT MOISTURE LOSS (%)	FELT GAIN SHEET (%)	FELT REMOVED WATER (%)	AVERAGE STFI INDEX (Nm/g)	US DENSITY (kg/m³)	US DEFLAM CODE	REWET CODE	STICKY PICK CODE	COMMENTS		
A4W1T19	171.4	0.158	11.39	0.1389	172.8	37.4	48.4	60.07	17.2	20.5	77.6	0.105	0.662	0	13	20			
A4W1T20	161.2	0.156	9.62	0.1423	182.3	40.0	47.2	0.385	17.2	19.1	62.8	0.070	0.681	4	13	20			
A4W1T22	161.2	0.164	13.41	0.1356	168.8	36.7	47.6	0.627	17.4	20.3	70.3	0.106	0.692	2	13	20			
A4W1T23	160.3	0.173	8.67	0.1358	162.4	36.5	47.3	0.631	17.1	19.7	63.0	0.102	0.688	0	13	20			
A4W1T25	160.3	0.135	12.59	0.1356	137.8	36.9	48.1	0.628	17.4	19.7	65.5	0.087	0.666	0	13	20	VERY SLIGHT REWET SHEET OFF CENTER, W/ WITH RACQUET		
A4W1T26	161.2	0.146	10.96	0.1405	139.5	37.8	49.1	0.607	17.2	19.4	64.8	0.085	0.693	0	19	20	WITH RACQUET		
WIA4T28	128.9	0.139	11.51	0.1349	177.9	38.7	46.4	0.428	17.3	20.9	113.6	0.076	0.690	28.264	1.790	0	10	25	WITH RACQUET
WIA4T29	128.9	0.139	7.91	0.1384	174.4	37.8	46.9	0.515	17.7	20.9	90.1	0.090	0.690	29.823	1.707	0	10	25	WITH RACQUET
WIA4T30	128.1	0.152	11.18	0.1357	176.9	38.2	48.2	0.544	17.6	20.6	79.2	0.096	0.673	30.393	1.104	0	10	27	WITH RACQUET
WIA4T31	128.1	0.144	9.03	0.1397	174.0	37.9	50.4	0.653	16.9	19.2	49.1	0.114	0.695	29.354	2.583	0	10	28	WITH RACQUET
WIA4T32	145.0	0.155	10.97	0.1393	178.4	38.7	48.0	0.498	16.8	19.6	74.4	0.089	0.701	30.213	2.566	0	13	20	WITH RACQUET
WIA4T33	145.0	0.150	12.67	0.1392	177.7	38.8	48.3	0.507	16.8	19.4	66.5	0.090	0.688	30.724	1.510	0	10	20	WITH RACQUET
WIA4T35	145.0	0.114	9.65	0.1370	194.7	42.6	50.6	0.372	16.9	19.2	74.5	0.072	0.653	26.149	1.164	0	10	20	WITH RACQUET
WIA4T36	144.2	0.138	7.97	0.1389	176.5	38.5	48.2	0.519	17.4	18.8	35.2	0.092	0.672	29.319	1.709	0	10	27	WITH RACQUET
WIA4T38	162.0	0.103	21.18	0.1367	178.8	38.8	48.7	0.522	17.0	19.6	67.9	0.093	0.673	26.515	1.620	6	10	20	WITH RACQUET
WIA4T39	162.0	0.129	22.48	0.1404	175.0	38.9	51.6	0.633	17.0	18.6	32.2	0.113	0.683	27.561	1.742	4	10	20	WITH RACQUET
WIA4T46	174.8	0.102	24.51	0.1388	179.4	38.9	49.1	0.586	17.0	19.6	64.8	0.096	0.655	25.754	0.425	7	10	20	WITH RACQUET
A1W5T01	229.1	0.174	12.07	0.1337	167.2	30.6	48.9	1.226	16.3	22.5	71.8	0.205	0.734	1	10	25			
A1W5T02	229.9	0.155	4.52	0.1384	169.5	30.9	49.6	1.220	17.2	23.1	69.2	0.207	0.710	1	10	20			
A1W5T06	144.2	0.142	18.31	0.1461	176.7	32.1	44.8	0.881	17.1	21.6	66.3	0.156	0.679	1	10	26			
A1W5T07	146.7	0.113	23.89	0.1382	179.0	32.8	48.4	0.978	16.7	20.4	49.0	0.175	0.633	2	10	28			
A1W5T08	145.0	0.111	26.13	0.1373	182.7	33.1	56.7	1.255	17.0	19.7	27.0	0.229	0.609	2	10	28			
A1W5T09	162.9	0.155	14.19	0.1692	180.6	33.1	48.8	0.893	17.3	22.4	76.4	0.161	0.708	1	1	20			
A1W5T10	161.2	0.142	21.13	0.1255	186.4	34.0	45.0	0.720	17.5	21.0	60.8	0.134	0.666	0	10	20			
W5A1T12	188.3	0.170	13.53	0.1373	166.6	30.4	47.5	1.185	17.1	22.9	70.9	0.197	0.698	0	10	20			
W5A1T13	188.3	0.153	8.50	0.1367	169.1	30.8	49.3	1.218	17.3	23.3	72.9	0.206	0.697	0	10	20			
W5A1T13	211.3	0.174	5.17	0.1391	168.9	30.6	48.6	1.213	17.2	23.0	70.0	0.204	0.712	1	10	20			
W5A1T20	211.3	0.179	8.38	0.1372	155.4	28.2	48.4	1.476	17.1	23.7	71.1	0.229	0.708	1	10	20			
W5A1T21	249.4	0.192	2.60	0.1393	186.0	33.9	49.5	0.933	17.0	21.7	61.4	0.174	0.740	0	10	20			
W5A1T22	252.0	0.178	6.18	0.1392	181.7	33.2	49.8	1.001	16.9	22.0	65.6	0.182	0.697	1	1	20			
W5A1T23	252.8	0.185	3.24	0.1401	181.9	33.2	50.6	1.033	17.1	22.3	66.1	0.188	0.708	2	10	20			
W5A1T27	145.9	0.155	13.55	0.1283	173.4	31.5	50.2	1.218	17.3	22.5	62.4	0.204	0.698	30.974	2.384	0	10	27	USED SPATULA
W5A1T18	211.3	0.174	5.17	0.1391	168.9	30.6	48.6	1.213	17.2	23.0	70.0	0.204	0.712	0	10	27	USED SPATULA		
W5A1T29	145.0	0.179	8.38	0.1372	155.4	28.2	48.4	1.476	17.1	23.7	71.1	0.229	0.708	1	10	20	RETEST,STUCK ON EDG		
W5A1T31	144.2	0.149	10.07	0.1369	167.0	30.2	45.5	1.110	17.3	23.0	75.5	0.185	0.691	31.472	3.533	0	10	29	
W5A1T35	175.6	0.165	16.97	0.1374	181.7	33.6	46.9	0.840	17.4	22.1	71.5	0.185	0.720	0	10	20			
W5A1T37	204.5	0.167	12.57	0.1385	170.3	30.9	48.2	1.184	17.2	23.5	75.4	0.198	0.739	4	10	20			
W5A1T40	200.2	0.181	12.15	0.1365	183.5	33.6	50.2	1.179	17.3	22.4	71.9	0.171	0.732	1	10	20			
W5A1T41	199.4	0.171	9.94	0.1352	178.0	32.4	48.8	1.037	17.5	23.3	74.3	0.188	0.666	28.533	3.068	0	10	27	
W5A1T42	167.1	0.146	10.27	0.1370	173.0	31.4	46.0	1.011	17.8	22.9	71.2	0.176	0.687	30.705	1.651	0	10	27	
W5A1T43	166.3	0.163	12.88	0.1365	181.7	33.2	46.2	0.854	17.0	23.0	78.9	0.155	0.726	32.193	2.113	0	10	20	
W5A1T48	175.6	0.165	16.97	0.1374	181.7	33.1	46.8	0.888	17.5	22.7	79.2	0.161	0.698	29.377	3.004	4	10	20	
W5A1T51	188.3	0.161	11.80	0.1390	188.9	34.4	49.9	1.270	17.1	23.6	78.2	0.204	0.741	32.096	1.446	0	10	20	
W5A1T53	188.3	0.166	5.42	0.1379	176.1	38.9	51.8	0.638	16.3	19.1	57.7	0.113	0.724	0	10	20			
A2W5T02	229.1	0.154	4.55	0.1373	183.1	40.3	49.0	0.438	17.2	19.1	54.6	0.105	0.691	0	10	20			
A2W5T03	230.8	0.153	7.19	0.1335	180.9	37.5	48.7	0.613	17.1	20.0	64.3	0.105	0.690	0	10	20			
W5A2T06	162.9	0.141	7.09	0.1349	170.9	43.6	49.5	0.270	18.1	17.0	47.6	0.054	0.707	0	10	20			
W5A2T07	162.9	0.166	6.63	0.1352	198.8	43.6	50.0	0.433	17.0	18.8	52.7	0.081	0.722	0	10	20			
W5A2T08	162.9	0.172	8.14	0.1405	187.4	41.1	49.6	0.811	17.1	20.9	66.3	0.132	0.688	0	10	20			
W5A2T11	188.3	0.163	5.52	0.1396	162.2	35.4	49.6	0.673	17.0	20.2	66.4	0.113	0.698	0	10	20			
W5A2T13	188.3	0.163	5.52	0.1403	167.8	36.8	48.9	0.673	17.0	20.2	66.4	0.113	0.698	0	10	20			
W5A2T14	187.5	0.172	8.14	0.1356	183.4	42.2	49.9	0.363	17.1	18.6	49.3	0.070	0.702	0	10	20			
W5A2T16	254.5	0.193	5.18	0.1502	177.9	39.0	53.5	0.696	16.0	19.8	69.5	0.124	0.751	0	10	20			
W5A2T17	257.1	0.183	7.65	0.1422	185.6	40.5	53.3	0.594	16.9	20.0	63.3	0.110	0.751	0	10	20			
W5A2T18	255.4	0.197	5.08	0.1436	185.2	40.7	53.5	0.591	16.5	19.5	62.8	0.110	0.731	0	10	20			
W5A2T20	257.1	0.205	1.95	0.1370	170.9	37.3	52.7	0.794	16.3	20.1	65.4	0.134	0.737	0	10	20			
W5A2T21	272.4	0.174	7.47	0.1389	188.3	41.4	54.2	0.570	16.7	19.3	54.2	0.107	0.737	0	10	20			
W5A2T23	272.4	0.191	4.71	0.1405	175.3	38.3	53.7	0.750	16.7	19.8	54.7	0.131	0.729	1	1	1			

Table B1 Continued. Data with the IPST A platen.

PLATEN SURFACE	SAMPLE ID	TEMP (C)	SEM (MN/mkg)	SEM %CV	OD BASIS	SOLIDS WEIGHT (g/m <sup>2</sup> )	IMPULSE (MPa.s)	SHEET IN OUT (%)	MOISTURE CHANGE (%)	FELT IN (%)	MOISTURE IN (%)	FELT OUT (%)	MOISTURE OUT (%)	WATER REMOVED (%)	US INDEX (Kg/m <sup>2</sup> )*3)	AVERAGE STF INDEX (Nm/g)	95% C.I.	DELM. CODE	REWET CODE	STICK PICK CODE	COMMENTS
W5A2174	273.2	0.177	6.21	0.1386	187.4	41.0	53.5	0.587	16.3	18.7	52.3	0.106	0.717	0	10	20	0	10	20		
W5A2126	297.0	0.161	6.21	0.1406	190.8	41.7	54.5	0.563	17.6	19.9	49.8	0.107	0.733	1	10	20	0	10	20		
W5A2127	298.7	0.181	6.08	0.1425	184.3	40.2	54.0	0.632	16.7	19.4	52.6	0.117	0.724	0	0	10	20	0	10	20	
W5A2128	296.1	0.178	4.49	0.1383	176.5	38.5	53.7	0.736	17.1	20.0	54.5	0.130	0.720	0	0	10	20	0	10	20	
W5A2131	321.6	0.167	6.59	0.1388	177.5	38.8	57.0	0.822	16.6	19.7	50.9	0.146	0.725	0	0	10	20	0	10	20	
W5A2132	322.4	0.179	7.26	0.1407	187.7	41.2	55.1	0.616	16.8	19.1	43.2	0.116	0.696	0	0	10	20	0	10	20	
W5A2134	322.4	0.194	4.12	0.1421	189.9	41.7	54.7	0.573	16.9	18.9	43.3	0.109	0.718	0	0	10	20	0	10	20	
W5A2145	145.9	0.157	6.81	0.1417	199.4	43.7	55.8	0.498	16.9	18.5	38.3	0.059	0.707	0	0	10	20	0	10	20	
W5A2135	321.6	0.191	2.92	0.1419	181.2	39.7	56.2	0.739	16.3	18.9	42.9	0.134	0.743	0	0	10	20	0	10	20	
W5A2136	357.2	0.171	9.36	0.1378	171.5	37.7	58.5	0.981	16.8	19.4	40.3	0.151	0.737	0	0	10	20	0	10	20	
W5A2140	356.4	0.174	3.45	0.1384	178.6	38.9	47.8	0.478	17.2	19.1	50.6	0.085	0.714	33.692	1.217	0	10	20	0	10	
W5A2142	145.0	0.162	8.64	0.1432	162.6	36.3	49.6	0.734	17.4	20.8	66.7	0.119	0.757	32.861	2.108	0	10	20	0	10	
W5A2144	144.2	0.160	11.88	0.1371	176.3	38.5	48.0	0.519	16.8	19.3	61.4	0.091	0.707	31.974	1.353	0	11	20	0	10	
W5A2146	145.9	0.157	8.92	0.1384	168.9	36.0	47.5	0.672	17.3	20.6	71.2	0.107	0.752	32.321	4.615	0	10	20	0	10	
W5A2148	174.8	0.179	5.59	0.1413	169.1	37.1	49.5	0.677	17.1	20.3	65.8	0.114	0.750	31.525	1.701	0	10	20	0	10	
W5A2148	174.8	0.171	9.36	0.1375	172.2	37.8	49.3	0.613	17.2	20.2	66.9	0.106	0.723	32.874	1.232	0	10	20	0	10	
W5A2149	175.6	0.170	12.94	0.1384	173.4	31.7	51.7	0.679	17.2	20.4	64.1	0.118	0.706	31.608	1.606	0	10	20	0	10	
W5A2150	174.8	0.166	4.22	0.1374	162.6	36.3	49.6	0.503	16.7	19.0	57.3	0.094	0.757	31.282	2.108	0	10	20	0	10	
W5A2151	212.9	0.167	16.77	0.1389	187.2	41.0	51.6	0.630	16.7	19.9	68.5	0.113	0.741	0	0	10	20	0	10	20	
W5A2152	212.9	0.163	9.20	0.1387	179.6	38.9	51.5	0.630	16.9	20.6	72.9	0.120	0.744	34.221	1.689	0	10	20	0	10	
W5A2156	203.6	0.166	3.61	0.1384	176.3	38.4	54.9	0.682	16.9	19.8	48.7	0.120	0.744	32.164	4.519	0	10	20	0	10	
W5A2157	202.8	0.176	7.95	0.1385	170.7	38.6	52.9	0.703	17.3	20.3	56.7	0.134	0.753	30.773	1.422	0	10	20	0	10	
W5A2158	210.4	0.157	4.46	0.1380	169.7	37.4	53.1	0.792	17.1	21.1	70.7	0.117	0.757	31.282	1.456	0	10	20	0	10	
W5A2159	209.6	0.190	4.74	0.1382	168.4	37.9	51.4	0.694	17.5	20.7	63.2	0.117	0.733	31.616	1.238	0	10	20	0	10	
W5A2164	219.7	0.178	10.11	0.1378	170.7	38.1	51.6	0.686	17.3	20.7	68.2	0.117	0.755	31.755	1.238	0	10	20	0	10	
W5A2165	220.6	0.170	9.41	0.1383	177.7	38.7	52.2	0.686	17.2	20.3	63.1	0.118	0.719	0	0	10	20	0	10	20	
W5A2166	145.0	0.142	9.15	0.1346	177.7	39.1	51.9	0.635	17.4	20.3	56.7	0.120	0.744	30.443	1.387	0	10	20	0	10	
W5A2167	145.0	0.176	15.91	0.1375	189.7	41.2	48.2	0.356	17.6	19.2	58.7	0.068	0.740	31.271	1.349	0	10	20	0	10	
W5A2169	145.0	0.159	9.43	0.1355	187.2	40.8	48.1	0.372	16.4	18.4	62.6	0.070	0.704	31.652	0.995	0	10	20	0	10	
W5A2175	170.5	0.190	8.95	0.1392	189.1	41.5	49.7	0.358	16.8	18.7	58.6	0.075	0.755	31.616	1.238	0	10	20	0	10	
W5A2176	196.0	0.166	16.27	0.1388	163.1	35.9	50.8	0.817	17.0	21.2	76.3	0.133	0.767	30.803	4.309	4	10	20	0	10	
W5A2177	196.8	0.184	6.52	0.1384	172.8	38.2	51.4	0.676	16.7	20.3	71.1	0.117	0.756	31.776	1.745	2	10	20	0	10	
W5A2179	195.1	0.174	8.62	0.1381	168.6	37.2	50.1	0.692	16.6	20.3	70.2	0.117	0.741	29.851	1.069	0	10	20	0	10	
W5A2180	196.8	0.159	25.79	0.1404	175.9	38.6	50.8	0.622	16.7	19.9	68.0	0.109	0.724	28.369	1.918	4	10	20	0	10	
W5A2183	204.5	0.156	5.13	0.1376	159.3	35.0	52.8	0.969	16.8	21.6	73.7	0.154	0.726	31.856	1.529	0	10	20	0	10	
W5A2184	203.6	0.160	16.25	0.1383	169.3	37.2	53.4	0.813	16.7	20.8	69.8	0.138	0.693	27.425	2.759	4	10	20	0	10	
W5A2185	188.3	0.160	8.13	0.1366	174.8	37.0	50.4	0.664	16.5	20.0	68.0	0.116	0.724	32.359	1.456	0	10	20	0	10	
W5A2186	188.3	0.147	8.84	0.1355	175.0	38.1	50.6	0.651	17.2	20.8	74.3	0.114	0.719	29.642	0.744	0	10	20	0	10	
W5A2189	187.5	0.180	9.44	0.1410	176.9	38.6	49.4	0.563	16.5	19.1	58.2	0.100	0.734	33.208	1.353	0	10	20	0	10	
A3W5101	145.9	0.130	10.77	0.1421	168.0	30.5	42.0	0.882	16.1	21.7	92.0	0.150	0.628	0.000	0.000	0	13	20	0	13	
A3W5102	145.9	0.112	7.14	0.1417	174.2	31.7	44.0	0.887	16.7	22.0	86.7	0.154	0.611	0.000	0.000	0	13	20	0	13	
A3W5103	145.9	0.131	9.92	0.1377	157.1	28.5	40.3	1.030	16.4	22.0	85.9	0.162	0.602	0.000	0.000	0	13	20	0	13	
A3W5104	145.9	0.140	7.86	0.1382	167.8	30.4	49.8	0.895	17.0	21.9	82.3	0.150	0.616	0.000	0.000	0	13	20	0	13	
A3W5105	145.0	0.142	8.45	0.1395	163.3	29.4	41.3	0.983	16.1	21.6	84.2	0.161	0.657	0.000	0.000	0	13	20	0	13	
A3W5106	171.4	0.178	15.73	0.1573	180.3	32.5	42.2	0.707	17.0	21.1	80.6	0.127	0.696	0.000	0.000	0	13	20	0	13	
A3W5108	172.2	0.159	13.21	0.1327	181.0	32.8	43.2	0.737	16.7	20.9	79.7	0.133	0.672	0.000	0.000	0	13	20	0	13	
A3W5110	171.4	0.148	10.14	0.1367	167.0	30.1	41.6	0.918	17.2	22.1	81.0	0.153	0.665	0.000	0.000	0	14	20	0	14	
A3W5111	187.5	0.155	15.48	0.1312	169.9	30.8	42.8	0.909	16.7	21.0	68.8	0.154	0.677	0.000	0.000	0	13	20	0	13	
A3W5113	179.0	0.153	17.65	0.1342	178.1	32.4	45.7	0.901	17.0	22.2	80.7	0.160	0.664	0.000	0.000	0	13	20	0	13	
A3W5114	186.6	0.166	9.64	0.1363	169.7	30.7	42.6	0.909	16.6	21.5	79.4	0.154	0.664	0.000	0.000	0	13	20	0	13	
A3W5121	229.1	0.172	11.05	0.1346	172.4	31.5	47.7	1.077	15.1	20.6	70.6	0.186	0.697	1	10	26	0	10	26	0	
A3W5124	229.1	0.164	8.54	0.1378	175.9	32.0	47.7	1.035	17.2	22.4	74.3	0.182	0.676	0	0	13	20	0	13	20	

Table B1 Continued. Data with the IPST A platen.

PLATEN SURFACE SAMPLE ID	TEMP (C)	SEM (MN/m²q)	SEM %CV	SEM %	IMPULSE (MPa.s)	IMPULSE %	OD BASIS WEIGHT (g/m²)	SHEET SOLIDS IN (%)	SHEET SOLIDS OUT (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT MOISTURE LOSS (%)	FELT WATER REMOVED (Kg/m²)	US DENSITY (Nm³/g)	AVERAGE STIFF INDEX	95% C.I. CODE	REWET CODE	STICK PICK CODE	COMMENTS
W5A3T37	187.5	0.100	18.00	0.1426	184.6	33.6	48.5	0.912	17.1	22.9	86.5	0.168	0.679	1.603	7	10	20	WITH RACKET	
W5A3T41	178.1	0.115	16.52	0.1276	184.3	33.4	47.6	0.895	17.3	21.9	70.2	0.165	0.698	29.224	1.083	7	10	20	WITH RACKET
W5A3T42	178.1	0.087	28.74	0.1412	185.2	33.3	47.9	0.912	17.8	23.9	94.8	0.169	0.670	1.780	7	10	27	WITH RACKET	
W5A3T43	171.4	0.085	20.00	0.1381	177.3	32.0	50.4	1.135	16.2	22.0	71.4	0.201	0.680	27.484	1.148	7	10	27	WITH RACKET
W5A3T44	171.4	0.102	26.47	0.1413	179.0	32.2	46.2	0.936	16.7	22.9	90.6	0.168	0.675	27.239	1.901	7	10	25	WITH RACKET
W5A3T45	162.0	0.133	21.05	0.1345	185.8	33.4	45.9	0.821	17.0	23.1	101.0	0.152	0.702	31.339	2.636	6	10	20	WITH RACKET
W5A3T47	153.5	0.153	5.88	0.1214	173.8	31.5	46.6	1.023	16.7	23.5	97.3	0.178	0.705	31.809	1.356	0	10	26	WITH RACKET
W5A3T48	154.4	0.146	13.70	0.1277	178.1	32.4	45.7	0.900	16.6	22.8	98.6	0.160	0.679	32.127	1.508	0	10	25	WITH RACKET
W5A3T49	153.5	0.149	18.79	0.1354	185.6	33.4	46.1	0.822	16.5	22.8	104.2	0.152	0.687	31.461	1.047	0	10	20	WITH RACKET
W5A3T50	152.7	0.155	14.19	0.1375	182.7	33.1	45.4	0.822	16.5	22.5	98.8	0.150	0.681	31.222	0.577	0	10	20	WITH RACKET
W5A3T51	154.4	0.155	17.42	0.1340	178.8	32.2	44.9	0.883	16.9	23.0	99.9	0.158	0.667	30.684	2.655	0	10	20	WITH RACKET
W5A3T55	162.9	0.157	20.38	0.1389	184.3	33.3	45.8	0.818	16.9	22.6	96.9	0.151	0.681	31.689	2.577	1	10	20	WITH RACKET
W5A3T56	162.9	0.149	15.44	0.1394	188.7	34.0	46.1	0.769	16.9	22.6	99.5	0.145	0.676	31.414	0.825	0	10	20	WITH RACKET
W5A3T57	169.7	0.148	24.32	0.1387	169.7	30.6	46.3	1.114	16.9	23.9	94.0	0.189	0.697	28.604	1.913	4	10	20	WITH RACKET
W5A3T60	170.5	0.130	27.69	0.1334	178.6	32.3	45.4	0.890	16.9	23.1	98.0	0.159	0.679	28.144	2.796	7	10	20	WITH RACKET
W5A3T61	171.4	0.152	19.74	0.1385	183.3	33.3	47.3	0.893	16.8	23.2	98.6	0.164	0.686	30.418	0.795	4	10	20	WITH RACKET
AAM5T02	147.6	0.139	5.76	0.1411	157.7	34.8	46.2	0.713	17.3	20.7	75.3	0.112	0.733	0	13	20	0	13	20
AAM5T03	144.2	0.143	7.69	0.1375	172.8	37.8	45.0	0.421	17.1	19.2	70.5	0.073	0.714	0	0	13	20	0	13
AAM5T04	144.2	0.149	6.04	0.1388	167.8	36.7	46.2	0.559	17.8	20.6	71.6	0.094	0.725	0	0	13	20	0	13
AAM5T05	145.9	0.165	6.67	0.1388	170.1	37.0	45.6	0.506	17.0	19.3	63.2	0.086	0.701	0	0	13	20	0	13
AAM5T06	169.7	0.151	9.27	0.1394	188.9	41.1	47.4	0.324	17.1	18.7	62.8	0.061	0.732	0	1	13	20	0	13
AAM5T07	169.7	0.166	7.83	0.1390	167.4	36.5	45.9	0.561	16.8	19.3	66.5	0.094	0.713	0	0	13	20	0	13
AAM5T08	171.4	0.172	11.05	0.1386	174.2	37.4	46.8	0.532	17.1	20.0	76.8	0.093	0.704	0	0	19	20	0	19
AAM5T09	171.4	0.153	7.19	0.1394	178.1	38.7	46.7	0.441	17.2	19.6	72.8	0.078	0.696	2	2	13	20	0	13
AAM5T10	171.4	0.149	10.74	0.1400	188.7	41.3	47.6	0.318	16.6	18.2	60.4	0.060	0.691	0	0	19	20	0	19
AAM5T11	188.3	0.177	9.04	0.1391	173.6	38.1	47.7	0.532	16.5	19.1	68.5	0.092	0.714	2	2	10	20	0	10
AAM5T12	189.2	0.145	10.34	0.1373	170.7	37.2	46.9	0.559	17.2	20.0	72.6	0.095	0.673	1	1	13	20	0	13
AAM5T13	188.3	0.173	8.09	0.1377	164.7	35.9	46.5	0.634	17.1	20.3	74.1	0.104	0.680	1	1	13	20	0	13
AAM5T14	188.3	0.171	7.60	0.1385	174.2	35.5	46.9	0.765	16.4	20.1	75.5	0.120	0.705	1	1	13	20	0	13
AAM5T15	207.0	0.167	10.18	0.1402	173.8	37.8	48.1	0.564	16.8	19.4	65.7	0.098	0.698	0	0	19	20	0	19
AAM5T20	205.3	0.189	9.52	0.1386	180.4	38.9	48.8	0.519	16.0	18.8	71.7	0.094	0.692	0	0	19	20	0	19
AAM5T21	229.1	0.164	7.32	0.1305	179.4	39.5	51.4	0.587	16.7	19.8	72.1	0.105	0.709	0	0	13	20	0	13
AAM5T22	228.2	0.170	4.71	0.1310	178.6	39.4	52.1	0.619	15.8	18.7	61.8	0.111	0.720	0	0	10	20	0	10
AAM5T23	229.9	0.191	5.76	0.1343	187.2	41.1	50.6	0.457	16.7	19.1	67.1	0.086	0.733	0	0	13	20	0	13
AAM5T25	225.7	0.163	5.20	0.1377	194.5	42.4	51.8	0.428	17.3	19.5	65.7	0.083	0.718	0	0	13	20	0	13
W5A4T26	128.1	0.146	13.70	0.1393	173.4	37.7	48.1	0.529	16.9	20.9	108.9	0.091	0.713	32.293	4.934	0	10	29	WITH RACKET, STUCK O
W5A4T27	128.1	0.129	16.28	0.1429	179.8	39.0	48.1	0.483	17.4	21.2	111.1	0.087	0.680	28.509	1.958	0	10	20	WITH RACKET
W5A4T28	128.9	0.126	13.49	0.1367	162.9	35.2	47.9	0.754	17.4	21.8	89.0	0.123	0.677	28.349	3.661	0	10	27	WITH RACKET, STUCK O
W5A4T29	128.9	0.153	9.80	0.1390	156.2	34.0	45.9	0.766	18.0	22.8	103.4	0.120	0.693	32.194	3.918	0	10	29	WITH RACKET, STUCK O
W5A4T30	128.1	0.138	15.94	0.1394	183.9	40.0	47.2	0.386	16.8	19.7	96.7	0.071	0.691	31.743	1.422	2	10	26	WITH RACKET
W5A4T31	145.9	0.157	11.46	0.1366	179.0	38.9	47.9	0.486	17.3	20.5	92.5	0.087	0.730	31.707	1.838	0	10	20	WITH RACKET
W5A4T33	145.0	0.146	9.59	0.1367	170.5	37.3	49.2	0.648	17.0	20.0	67.2	0.111	0.718	30.569	1.765	0	10	20	WITH RACKET
W5A4T34	145.0	0.159	10.69	0.1405	187.7	40.6	48.5	0.403	16.7	18.8	66.3	0.076	0.714	31.107	1.035	0	10	20	WITH RACKET
W5A4T35	144.2	0.147	12.24	0.1403	160.4	34.9	47.7	0.765	17.0	21.2	83.9	0.123	0.692	31.688	1.127	0	10	20	WITH RACKET
W5A4T36	175.6	0.160	8.75	0.1368	171.3	37.2	49.0	0.647	16.6	20.6	87.5	0.111	0.743	30.635	1.422	2	10	20	WITH RACKET
W5A4T38	175.6	0.145	8.28	0.1368	173.8	37.9	49.0	0.594	16.6	20.1	81.8	0.103	0.732	29.352	2.285	1	10	20	WITH RACKET
W5A4T39	173.9	0.125	24.80	0.1424	180.6	39.2	49.0	0.513	17.3	20.7	91.4	0.083	0.710	27.807	2.768	7	10	20	WITH RACKET
W5A4T41	187.5	0.120	17.50	0.1362	173.2	37.8	49.7	0.630	16.9	20.4	79.7	0.109	0.720	28.663	1.074	7	10	20	WITH RACKET
W5A4T42	188.3	0.103	28.16	0.1408	172.2	37.6	49.3	0.628	16.8	20.5	85.0	0.108	0.703	27.723	1.485	7	10	20	WITH RACKET
W5A4T43	187.5	0.116	25.00	0.1374	187.7	40.9	50.1	0.448	17.2	20.1	87.7	0.084	0.720	27.434	1.368	7	10	20	WITH RACKET

Table B2. Data with the IPST C platen.

PLATEN SURFACE	SAMPLE ID	TEMP (C)	SEM (MN/mkg)	SEM %CV	IMPULSE (MPas)	BASIS (g/m²)	OD WEIGHT (%)	SHEET SOLIDS IN OUT (%)		SHEET SOLIDS IN OUT (%)		FELT MOISTURE IN OUT (%)		FELT GAIN SHEET LOSS (%)		WATER REMOVED DENSITY (Kg/m²)		AVERAGE STFI INDEX (Nm/kg)		95% C.I. DELAM CODE		REWET CODE		STICKY PICK CODE		COMMENTS			
W1C1T01	147.2	0.159	11.32	0.1404	166.0	33.0	44.8	0.797	17.1	21.0	68.4	0.132	0.691	29.281	2.706	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T02	147.2	0.158	12.66	0.1422	158.7	31.5	45.1	0.651	17.1	20.2	66.1	0.114	0.667	30.074	1.295	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T03	147.2	0.158	12.66	0.1422	163.7	32.6	44.8	0.837	17.4	21.5	70.6	0.149	0.685	26.638	2.853	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T04	148.1	0.155	9.03	0.1418	177.8	31.6	45.4	0.659	17.3	19.7	60.7	0.137	0.668	28.148	1.989	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T05	149.1	0.151	11.88	0.1396	189.7	31.6	46.7	0.834	17.1	21.3	69.5	0.141	0.693	29.566	1.366	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T06	149.4	0.168	11.90	0.1404	168.6	33.6	46.7	0.834	17.1	21.3	69.5	0.141	0.693	29.630	1.064	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T07	149.4	0.157	9.55	0.1386	184.6	37.1	47.4	0.588	17.4	20.3	63.1	0.108	0.674	26.962	1.517	2	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T08	192.5	0.166	11.45	0.1414	173.1	32.4	46.7	0.946	17.5	21.8	68.8	0.154	0.646	31.534	3.036	2	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T09	192.5	0.172	13.37	0.1393	186.2	36.9	47.4	0.589	16.8	19.7	61.5	0.112	0.701	29.684	0.910	1	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T10	208.6	0.172	8.05	0.1395	162.6	32.2	48.5	1.043	17.4	22.5	73.0	0.170	0.684	26.179	1.520	2	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T11	207.6	0.149	23.70	0.1355	182.3	36.2	47.3	0.650	17.3	20.2	58.1	0.118	0.661	27.185	1.990	6	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T12	206.7	0.135	23.70	0.1355	173.1	35.0	45.3	0.652	17.2	20.5	67.0	0.115	0.689	29.630	1.064	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T13	148.1	0.155	11.76	0.1396	189.7	31.6	46.7	0.834	17.1	21.3	69.5	0.141	0.693	29.630	1.064	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T14	149.1	0.168	11.90	0.1404	168.6	33.6	46.7	0.834	17.1	21.3	69.5	0.141	0.693	29.630	1.064	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T15	149.4	0.157	9.78	0.1380	182.5	36.4	45.3	0.540	16.8	19.3	57.9	0.099	0.625	29.953	1.346	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T16	183.1	0.173	9.83	0.1393	176.1	35.0	45.1	0.774	17.3	21.0	67.7	0.131	0.670	30.762	1.286	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T17	183.1	0.165	4.24	0.1382	168.8	33.5	45.1	0.541	17.1	19.5	55.7	0.101	0.660	30.252	1.337	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T18	169.8	0.159	11.32	0.1394	186.4	36.8	45.9	0.388	17.2	18.7	46.8	0.075	0.633	29.506	2.221	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T19	168.9	0.156	19.87	0.1391	194.3	38.6	45.4	0.388	17.2	18.7	46.8	0.075	0.633	29.506	2.221	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T20	169.8	0.151	7.28	0.1380	182.5	36.4	45.3	0.540	16.8	19.3	57.9	0.099	0.625	29.953	1.346	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C1T21	146.2	0.141	13.48	0.1394	186.2	44.3	49.3	0.226	17.3	19.9	34.9	0.042	0.678	28.398	1.076	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T01	147.2	0.173	9.25	0.1390	187.0	44.6	49.2	0.207	17.0	17.7	38.5	0.039	0.716	29.734	2.189	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T02	147.2	0.175	8.00	0.1414	175.3	41.7	48.4	0.331	16.9	18.1	49.6	0.058	0.706	30.249	1.236	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T03	147.2	0.168	7.14	0.1392	180.4	43.6	48.6	0.237	17.3	18.4	54.8	0.043	0.708	30.071	1.162	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T04	206.7	0.135	23.70	0.1355	182.3	36.7	50.9	0.320	17.2	18.5	48.4	0.059	0.715	30.834	4	10	20	20	20	20	20	20	20	20	20	20	20	20	
W1C2T05	192.5	0.160	20.00	0.1380	184.3	44.3	50.9	0.342	17.4	18.8	49.2	0.062	0.690	30.331	1.162	1	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T06	192.5	0.162	12.35	0.1385	181.7	43.2	50.8	0.288	17.6	18.3	51.6	0.054	0.692	29.767	1.081	1	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T10	194.4	0.157	8.28	0.1406	180.6	42.9	50.3	0.311	17.0	18.3	51.6	0.057	0.689	27.407	0.913	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T11	208.6	0.138	13.04	0.1372	186.4	44.3	51.1	0.244	17.1	17.9	33.2	0.046	0.677	28.231	1.438	4	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T12	207.6	0.138	20.29	0.1407	192.2	45.9	52.5	0.253	17.2	18.2	47.5	0.049	0.683	29.851	2.482	4	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T13	207.6	0.167	5.39	0.1391	186.8	44.7	51.1	0.281	17.4	18.3	41.3	0.052	0.726	29.082	1.353	4	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T14	208.6	0.149	19.46	0.1385	189.9	45.7	51.5	0.247	17.5	18.2	35.2	0.047	0.711	29.025	1.533	2	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T15	208.6	0.159	11.84	0.1384	186.4	44.6	51.2	0.288	17.6	18.3	31.0	0.054	0.714	28.403	1.318	4	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T16	183.1	0.152	16.45	0.1368	183.5	43.6	50.5	0.244	17.1	17.8	33.2	0.046	0.677	29.620	1.627	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T17	184.9	0.153	9.15	0.1377	190.5	45.4	50.1	0.244	17.1	17.8	40.9	0.048	0.672	31.106	1.146	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T20	184.0	0.172	6.98	0.1389	188.7	45.1	50.9	0.253	17.5	18.4	31.0	0.052	0.728	30.458	1.228	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T21	169.9	0.171	11.11	0.1391	183.3	43.7	49.9	0.284	17.1	17.8	41.2	0.049	0.695	30.791	1.490	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T22	170.8	0.156	10.26	0.1387	184.6	44.0	49.9	0.287	17.3	18.2	44.7	0.049	0.723	32.131	1.032	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T23	169.8	0.180	12.22	0.1370	189.7	48.0	52.1	0.182	17.3	18.0	40.4	0.043	0.704	28.562	2.354	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T24	169.8	0.180	8.13	0.1387	187.4	45.1	50.2	0.227	17.3	18.0	40.4	0.043	0.736	30.997	1.547	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T25	147.2	0.138	23.02	0.1303	180.2	35.6	45.3	0.600	17.1	18.1	64.8	0.108	0.692	30.057	1.931	0	10	20	20	20	20	20	20	20	20	20	20	20	20
W1C2T26	147.2	0.145	13.79	0.1333	167.6	33.4	43.4	0.688	17.1	20.3	65.4	0.115	0.660	30.562															

Table B2 Continued. Data with the IPST C platen.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM SEM (MN/m²kg)	SEM (%CV)	OD BASIS WEIGHT (g/m²)	SHEET SOLIDS (%)	SHEET CUT (%)	SHEET SOLIDS MOISTURE RATIO (%)	FELT IN (%)	FELT OUT (%)	FELT SHEET LOSS (%)	WATER REMOVED (%)	US DENSITY (kg/m³)	AVERAGE STFI INDEX (Nm/g)	STFI CODE	REWET CODE	DELAM CODE	STICKY PICK CODE	COMMENTS
W5C2T15	213.3	0.146	6.16	0.141	185.6	44.6	51.3	0.294	17.7	18.8	46.0	0.055	0.726	28.712	2.095	0	10	20
W5C2T17	232.2	0.145	6.21	0.137	185.4	44.0	53.0	0.387	17.5	19.1	52.3	0.072	0.724	29.165	2.171	0	10	20
W5C2T19	231.2	0.201	8.46	0.135	166.4	50.0	52.5	0.525	17.5	19.6	53.8	0.087	0.725	32.575	1.984	0	10	20
W5C2T20	232.2	0.169	10.65	0.138	185.2	44.1	51.2	0.316	17.2	18.2	40.5	0.059	0.726	30.008	1.560	0	10	20
W5C2T22	249.2	0.184	4.89	0.139	180.6	43.4	52.3	0.389	17.1	18.6	45.5	0.070	0.724	30.354	1.896	0	10	20
W5C2T23	249.2	0.184	5.43	0.139	171.3	40.7	51.1	0.502	17.8	19.7	52.6	0.086	0.738	32.550	0.567	0	10	20
W5C2T24	251.1	0.183	7.65	0.138	162.2	38.7	51.2	0.630	17.5	20.0	57.8	0.102	0.730	33.076	3.122	0	10	20
W5C2T29	269.9	0.200	5.00	0.136	180.2	43.1	51.9	0.391	16.6	18.1	47.6	0.070	0.740	31.052	2.005	0	10	20
W5C2T30	267.1	0.190	6.32	0.139	189.1	45.2	52.9	0.320	17.0	17.7	24.2	0.060	0.751	31.528	2.049	0	10	20
W5C2T31	288.8	0.166	7.83	0.138	195.3	46.4	55.5	0.355	17.5	18.6	36.5	0.069	0.731	28.554	1.112	0	10	20
W5C2T33	278.4	0.183	4.92	0.139	188.5	44.5	54.5	0.415	17.2	19.0	50.9	0.078	0.787	32.885	1.720	0	10	20
W5C2T34	258.6	0.180	16.67	0.144	171.1	40.2	51.7	0.549	16.7	18.8	51.3	0.094	0.755	30.965	2.461	4	10	20
W5C2T35	259.6	0.166	10.24	0.141	167.8	40.0	53.4	0.628	17.3	20.1	64.6	0.105	0.736	29.882	1	10	20	
W5C2T36	260.5	0.167	16.17	0.139	161.0	38.3	51.6	0.674	17.2	20.1	63.1	0.108	0.759	32.436	1.768	4	10	20
W5C2T37	259.6	0.153	11.11	0.138	184.8	43.9	53.8	0.416	17.5	19.2	46.8	0.077	0.747	29.855	1.182	0	10	20
W5C2T38	258.6	0.165	15.76	0.138	163.9	40.5	52.2	0.552	17.5	19.8	59.2	0.094	0.745	29.1173	1.357	2	10	20

Table B3. Data for the double-felted pressing control cases.

SAMPLE ID	PLATEN SURFACE TEMP (C)	SEM (MN/mkg)	SEM %CV	IMPULSE (MPa.s)	OD BASIS WEIGHT (g/m <sup>2</sup> )	OD SHEET SOLIDS IN (%)	OD SHEET SOLIDS OUT (%)	FELT MOISTURE IN (%)	FELT MOISTURE OUT (%)	FELT GAIN/LOSS (%)	AVERAGE STI INDEX (Nm/g)	95% C.I.	DELAM CODE	PICK CODE	STICK COMMENTS		
WID1T01	99.0	0.136	19.85	0.116	189.7	37.6	41.8	0.268	17.8	18.9	45.2	0.639	28.923	1.127	0	20 TOP BOTTOM	
WID1T02	99.0	0.123	21.14	0.1236	181.5	36.1	41.6	0.366	16.5	17.5	44.8	0.636	0.616	28.577	1.062	0	10 TOP TOP
WID1T03	99.0	0.130	16.15	0.1324	175.7	35.0	41.2	0.434	18.2	20.0	59.7	0.076	0.606	30.247	1.499	0	10 TOP BOTTOM
WID1T04	99.0	0.135	16.30	0.1398	170.7	33.9	41.7	0.551	17.2	18.9	52.6	0.094	0.621	28.927	0.881	0	10 TOP BOTTOM
WID1T05	99.0	0.137	17.52	0.159	166.6	33.1	41.2	0.593	16.5	18.1	36.7	0.099	0.617	29.100	1.787	0	10 TOP BOTTOM
WID1T06	99.0	0.137	17.52	0.159	166.6	33.1	41.2	0.593	17.6	19.5	45.6	0.099	0.617	29.100	1.787	0	10 TOP TOP
WID1T10	99.0	0.150	13.33	0.1520	176.1	41.7	45.3	0.189	18.2	18.3	5.0	0.033	0.678	30.728	1.504	0	10 TOP BOTTOM
WID2T02	98.1	0.150	12.58	0.1439	177.3	42.0	45.7	0.193	16.3	16.4	7.1	0.034	0.659	29.040	1.220	0	10 TOP BOTTOM
WID2T03	99.0	0.138	17.39	0.1439	177.3	42.0	45.7	0.193	17.8	18.5	44.0	0.042	0.679	28.426	2.077	0	10 TOP BOTTOM
WID2T04	98.1	0.151	12.58	0.1290	164.9	39.3	43.8	0.257	17.9	18.6	41.5	0.042	0.679	28.426	2.077	0	10 TOP BOTTOM
WID2T06	98.1	0.158	12.03	0.1318	178.8	42.4	45.2	0.149	16.6	17.7	56.8	0.027	0.662	32.978	0.450	0	10 TOP BOTTOM
WID2T07	98.1	0.133	18.05	0.1338	181.5	43.2	46.1	0.146	17.6	18.0	44.6	0.026	0.634	29.216	0.890	0	10 TOP BOTTOM
WID2T08	98.1	0.127	24.41	0.1381	187.7	37.3	42.2	0.314	18.3	19.7	60.0	0.059	0.642	28.894	1.165	0	10 TOP BOTTOM
WSD1T02	99.0	0.150	20.67	0.1386	157.9	31.5	40.3	0.695	16.8	17.5	26.3	0.110	0.666	30.143	6.476	0	10 TOP BOTTOM
WSD1T06	98.1	0.126	13.49	0.1366	165.1	32.9	40.5	0.576	17.8	20.3	58.2	0.095	0.614	30.130	1.727	0	10 TOP BOTTOM
WSD1T07	99.0	0.142	16.20	0.1364	158.1	31.4	40.4	0.707	16.8	18.3	33.7	0.112	0.630	28.699	2.667	0	10 TOP BOTTOM
WSD1T08	99.0	0.142	8.45	0.1358	181.7	44.0	45.8	0.092	17.8	18.1	62.8	0.112	0.630	36.4	12.1	0	10 TOP BOTTOM
WSD2T01	99.0	0.145	6.90	0.1387	182.1	43.7	45.2	0.078	18.4	18.7	46.6	0.017	0.702	31.994	1.263	0	10 TOP BOTTOM
WSD2T01	99.0	0.140	7.14	0.1389	183.3	43.8	45.5	0.083	18.1	18.3	48.0	0.015	0.684	32.040	1.988	0	10 TOP BOTTOM
WSD2T02	99.0	0.133	17.29	0.1371	183.9	43.8	45.4	0.080	18.0	18.0	65.0	0.015	0.640	30.094	1.539	0	10 TOP BOTTOM
WSD2T03	99.0	0.145	6.90	0.1387	182.1	43.7	45.2	0.078	16.0	15.8	-28.9	0.015	0.617	30.782	1.710	0	10 TOP BOTTOM
WSD2T04	99.0	0.140	11.05	0.1376	183.9	43.8	45.4	0.084	16.6	16.5	-21.0	0.015	0.720	33.824	0.909	0	10 TOP BOTTOM
WSD2T06	98.1	0.152	13.16	0.1385	183.1	43.7	45.6	0.094	18.2	18.3	21.4	0.017	0.689	33.063	1.836	0	10 TOP BOTTOM
WSD2T07	98.1	0.140	10.00	0.1366	183.9	44.0	45.2	0.063	18.4	18.6	40.6	0.012	0.682	31.153	1.164	0	10 TOP BOTTOM
WSD2T08	98.1	0.153	13.73	0.1385	181.7	43.3	44.9	0.080	16.7	16.4	-52.8	0.014	0.693	31.058	2.348	0	10 TOP BOTTOM
WSD2T10	99.0										-2.1						

## APPENDIX C

The following figures show the specific elastic modulus, %CV of SEM, visual delamination code, and selected density plots used to determine the critical temperature.

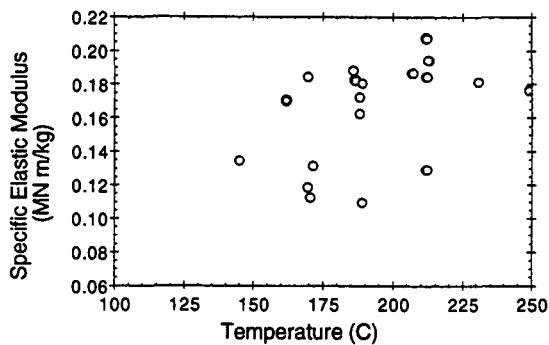


Figure C1. Case W1A1.

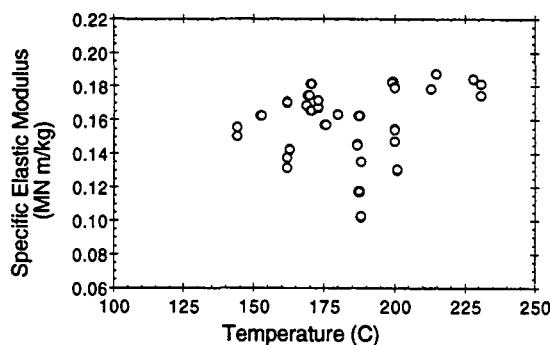


Figure C2. Case W1A2.

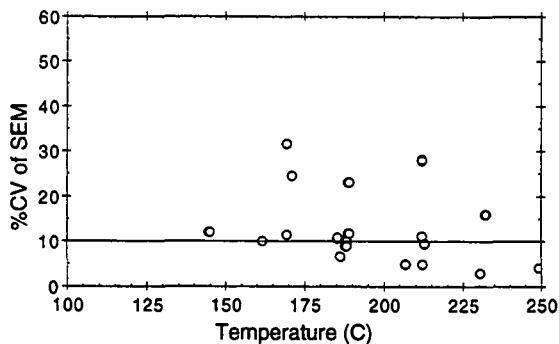


Figure C3. Case W1A1.

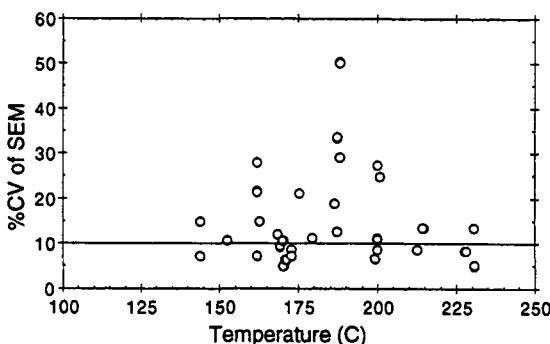


Figure C4. Case W1A2.

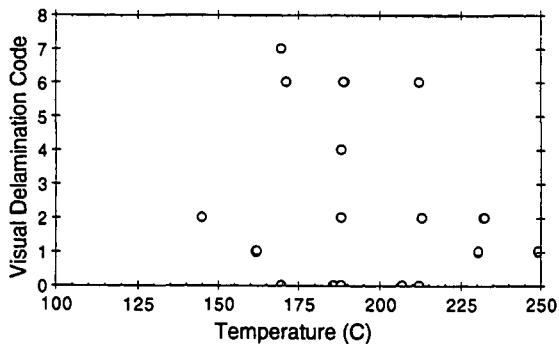


Figure C5. Case W1A1.

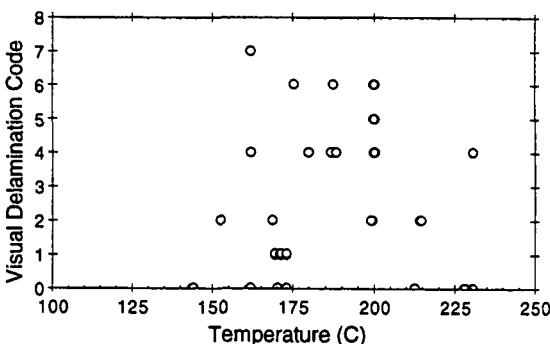


Figure C6. Case W1A2.

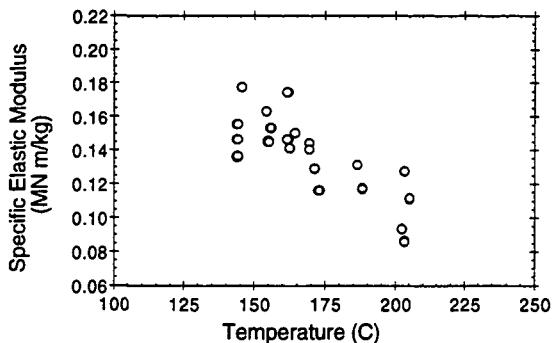


Figure C7. Case W1A3.

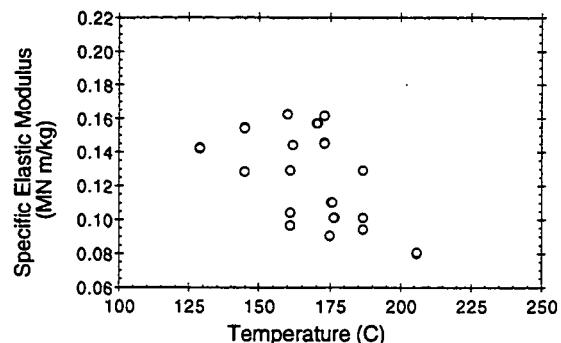


Figure C8. Case W1A4.

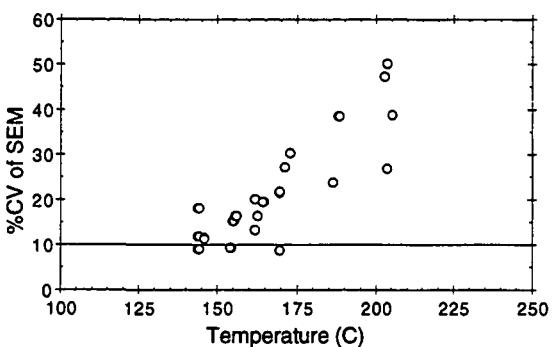


Figure C9. Case W1A3.

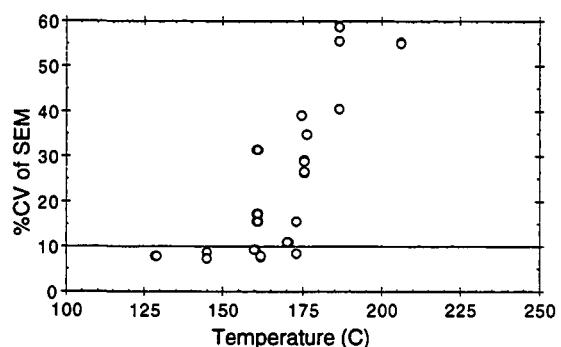


Figure C10. Case W1A4.

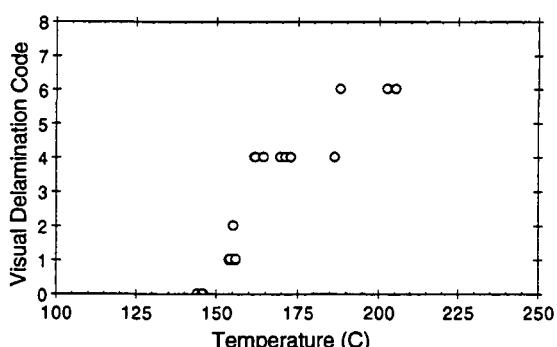


Figure C11. Case W1A3.

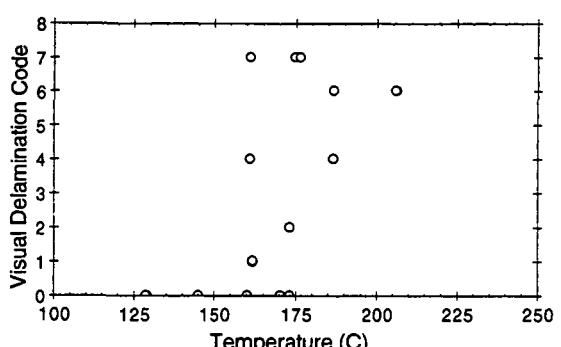


Figure C12. Case W1A4.

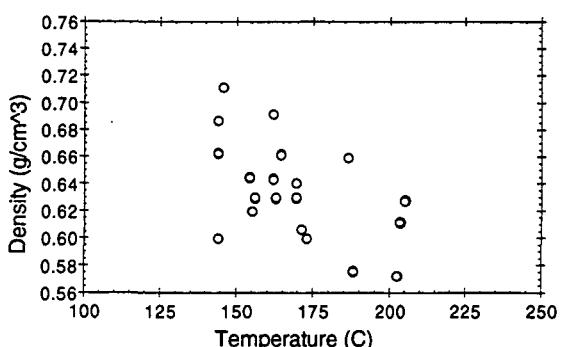


Figure C11A. Case W1A3.

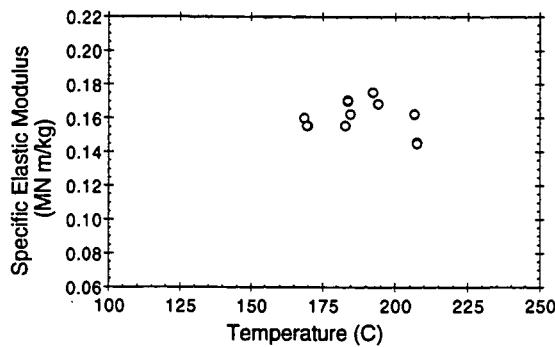


Figure C13. Case W1C1.

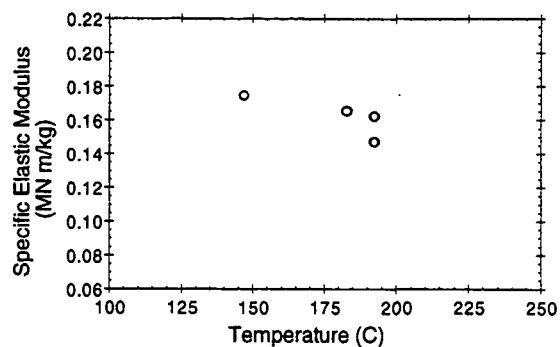


Figure C14. Case W1C2.

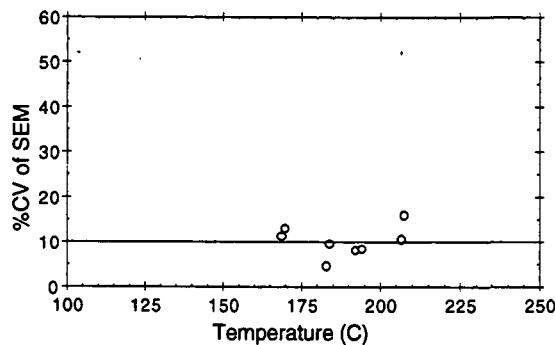


Figure C15. Case W1C1.

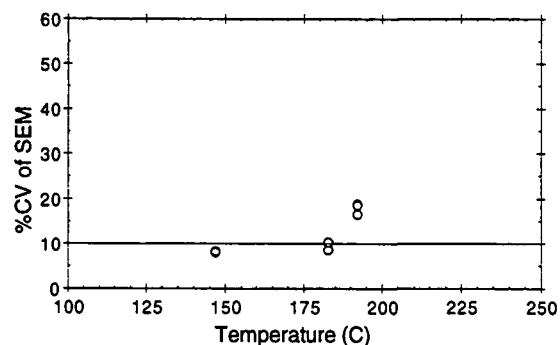


Figure C16. Case W1C2.

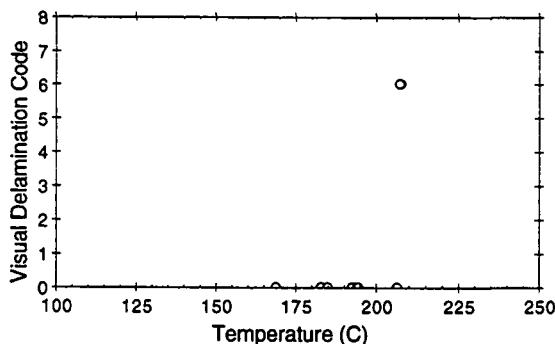


Figure C17. Case W1C1.

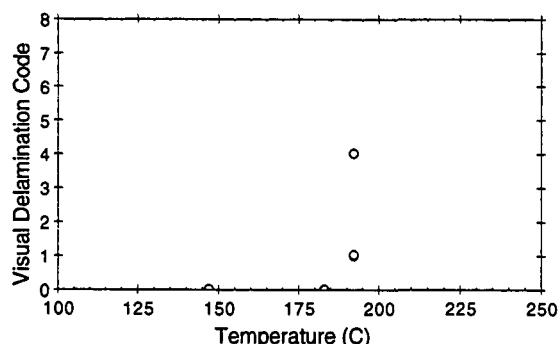


Figure C18. Case W1C2.

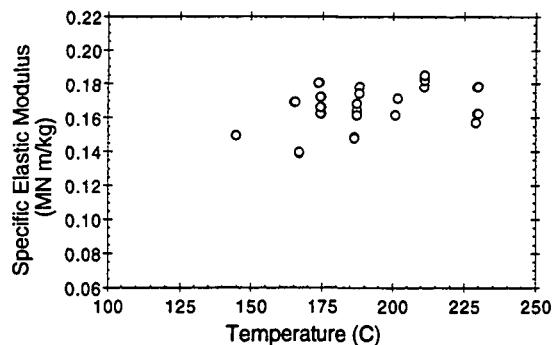


Figure C19. Case W5A1.

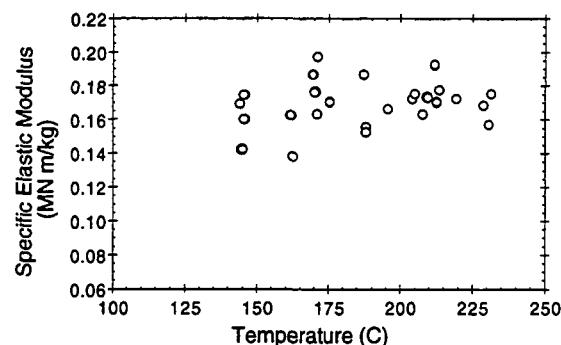


Figure C20. Case W5A2.

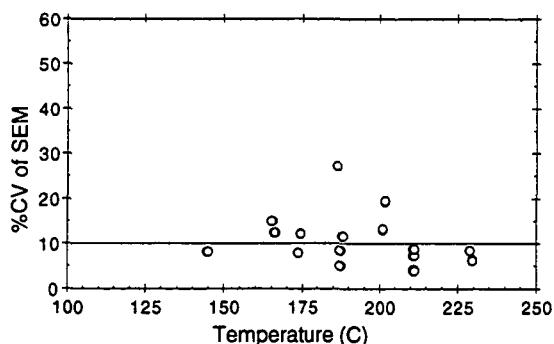


Figure C21. Case W5A1.

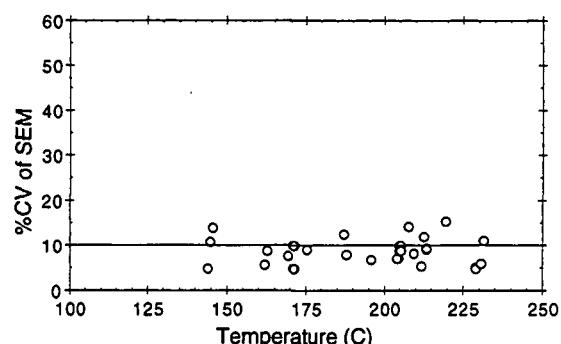


Figure C22. Case W5A2.

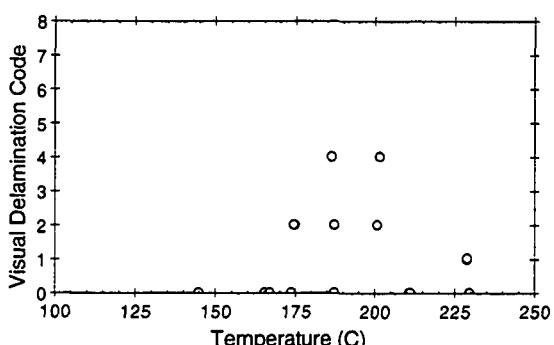


Figure C23. Case W5A1.

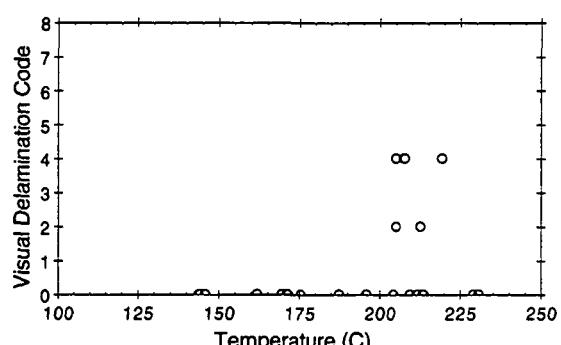


Figure C24. Case W5A2.

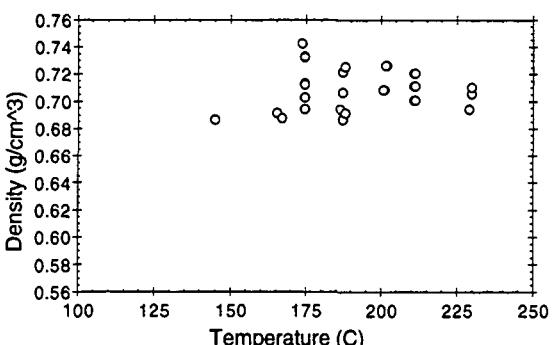


Figure C23A. Case W5A1.

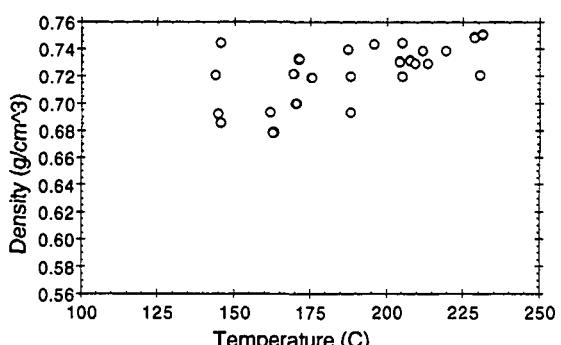


Figure C24A. Case W5A2.

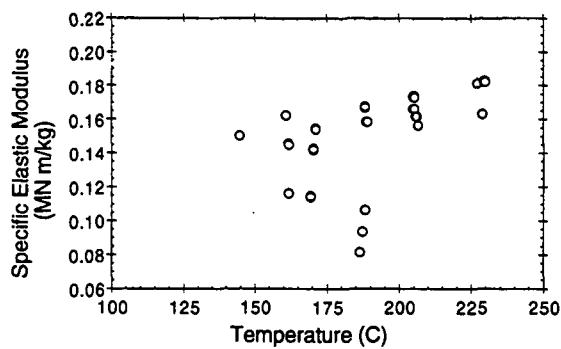


Figure C25. Case W5A3.

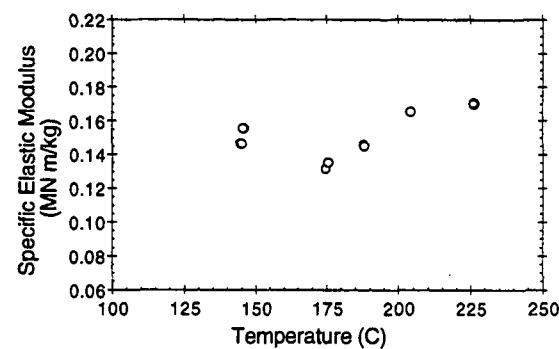


Figure C26. Case W5A4.

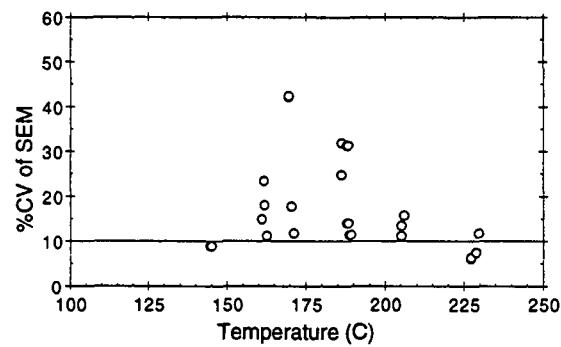


Figure C27. Case W5A3.

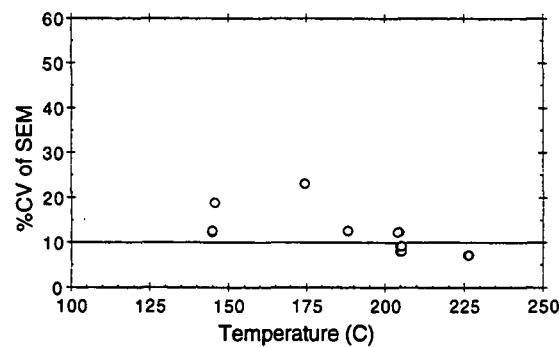


Figure C28. Case W5A4.

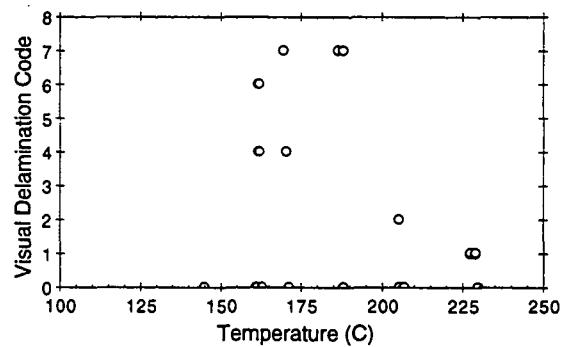


Figure C29. Case W5A3.

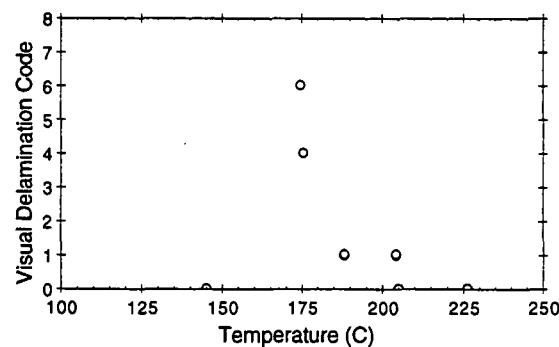


Figure C30. Case W5A4.

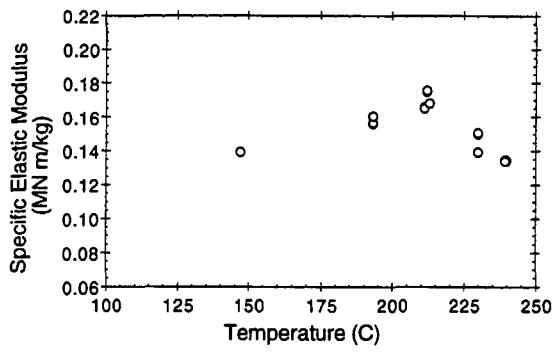


Figure C31. Case W5C1.

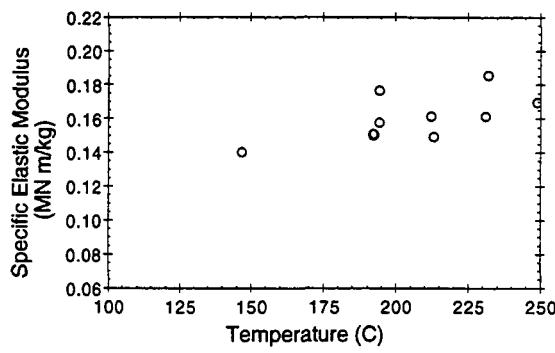


Figure C32. Case W5C2.

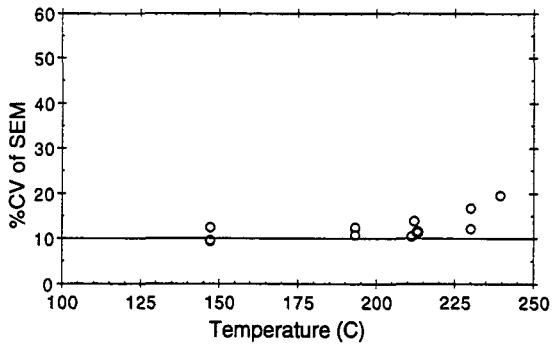


Figure C33. Case W5C1.

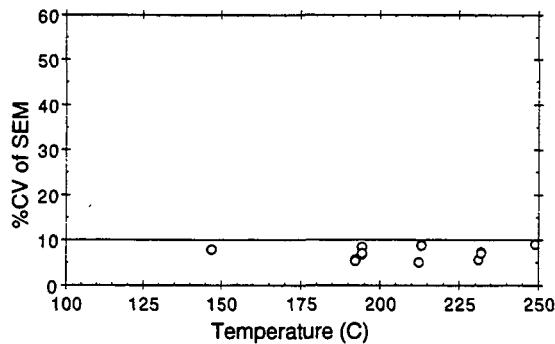


Figure C34. Case W5C2.

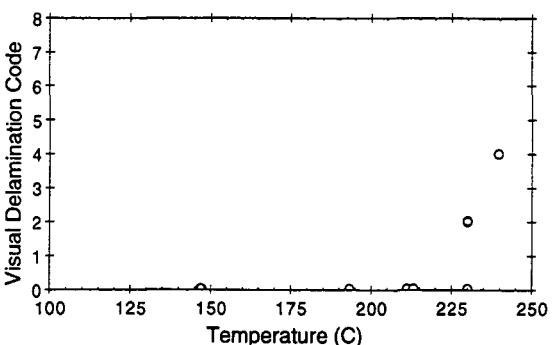


Figure C35. Case W5C1.

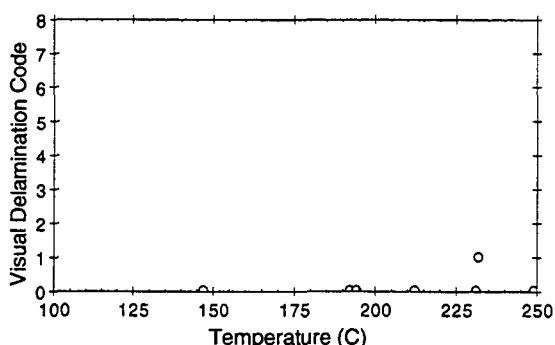


Figure C36. Case W5C2.

## APPENDIX D

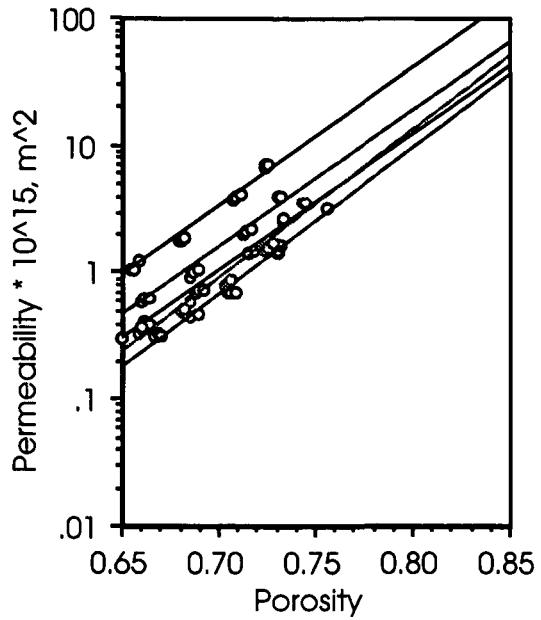


Figure D1. Mill #1 furnish, whole sheet.

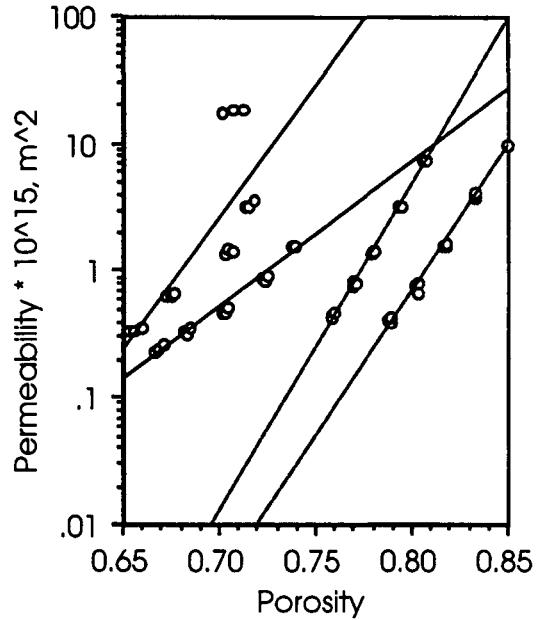


Figure D2. Mill #1 furnish, whole sheet.

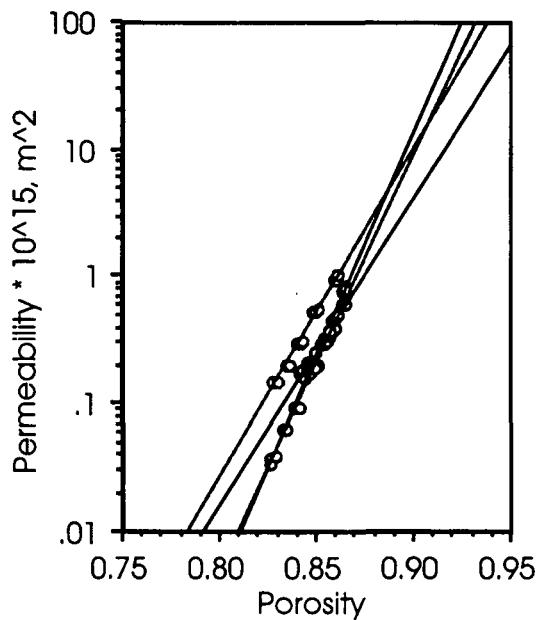


Figure D3. Mill #1 furnish, top ply.

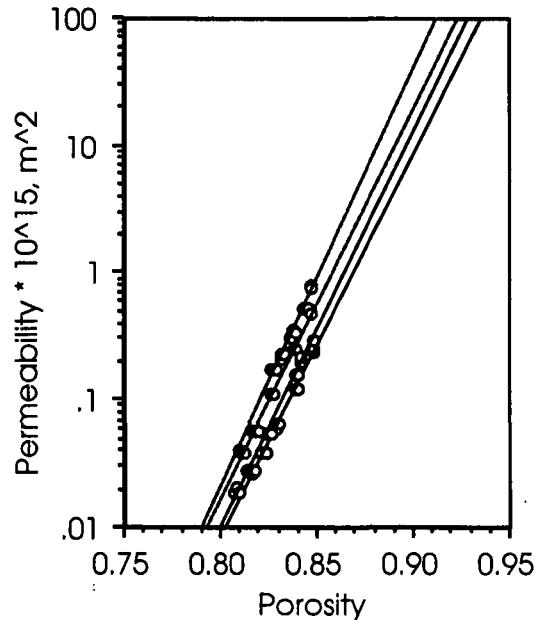


Figure D4. Mill #1 furnish, bottom ply.

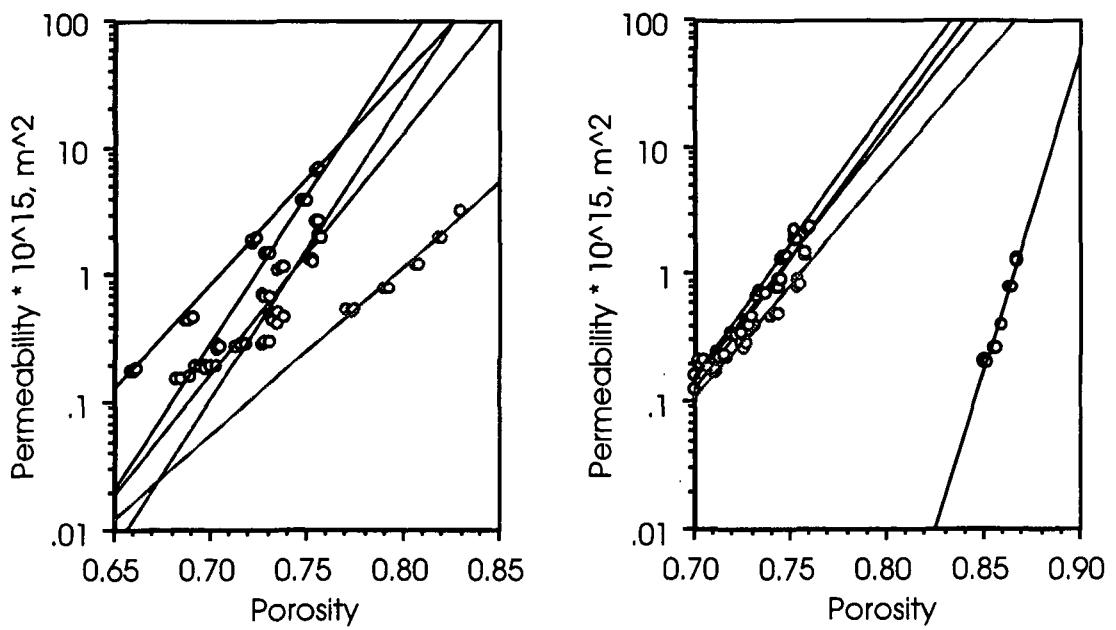


Figure D5. Mill #2 furnish, whole sheet.

Figure D6. Mill #2 furnish, whole sheet.

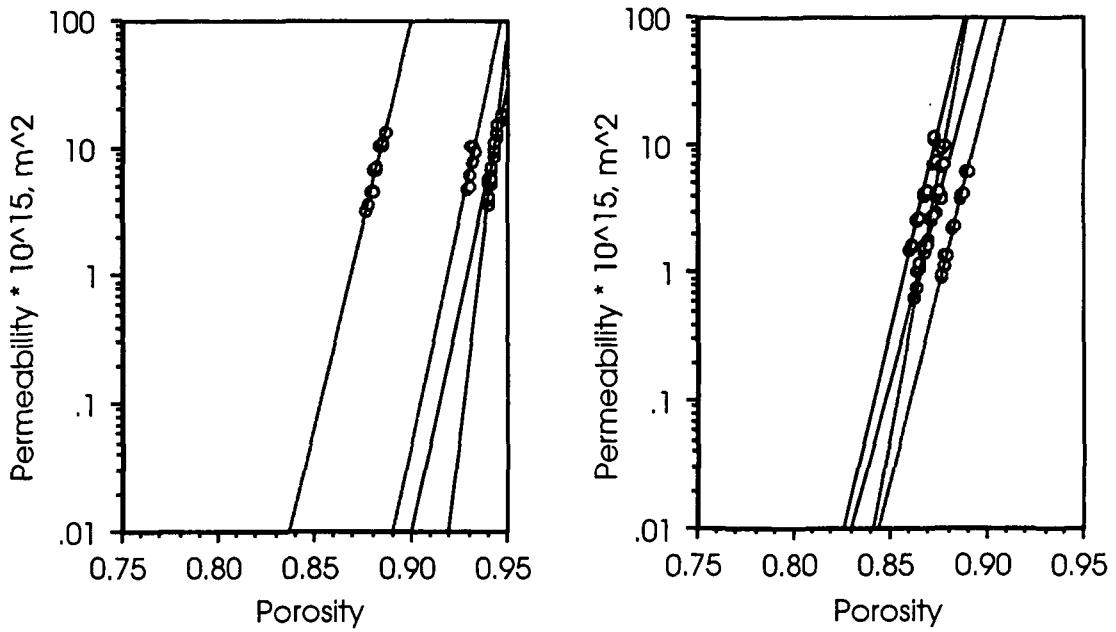


Figure D7. Mill #2 furnish, top ply.

Figure D8. Mill #2 furnish, bottom ply.

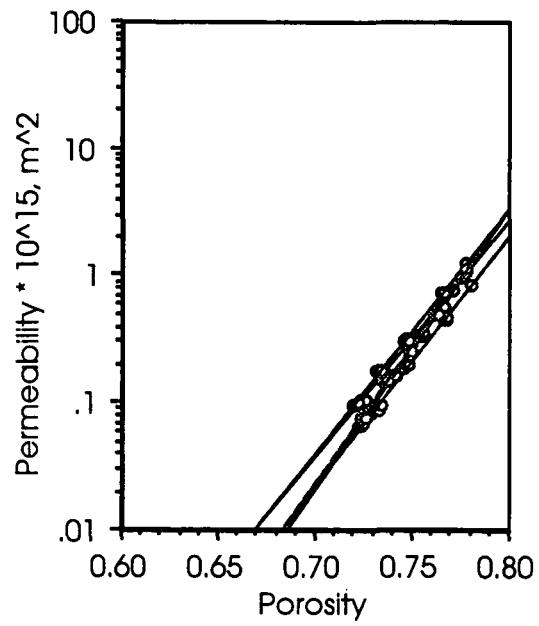


Figure D9. Furnish W1, solids 35%.

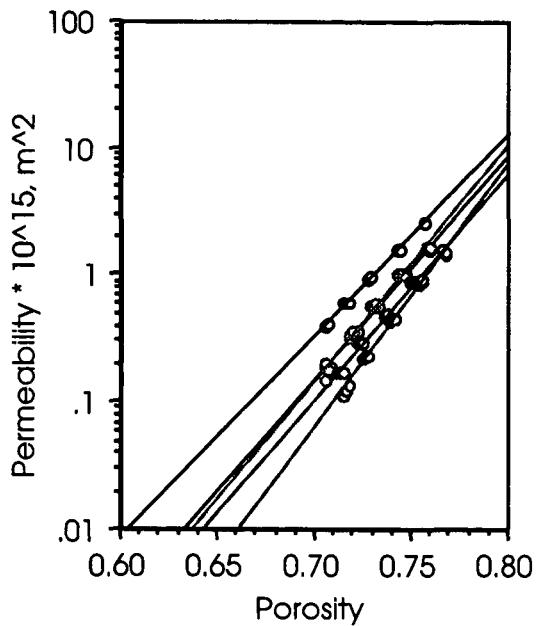


Figure D10. Furnish W1, solids 42%.

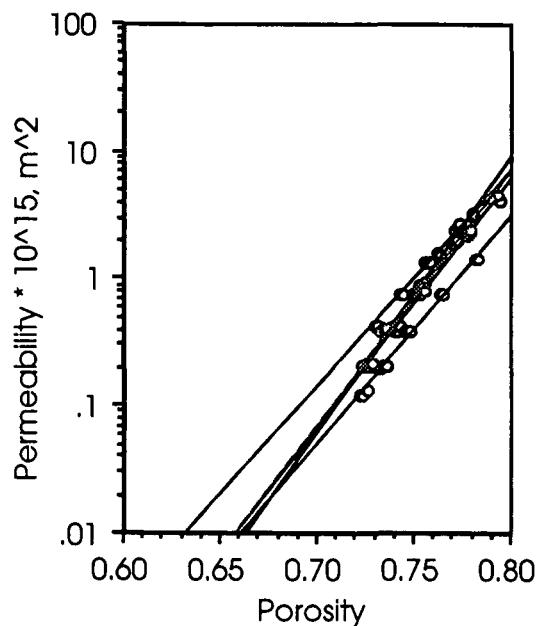


Figure D11. Furnish W2, solids 35%.

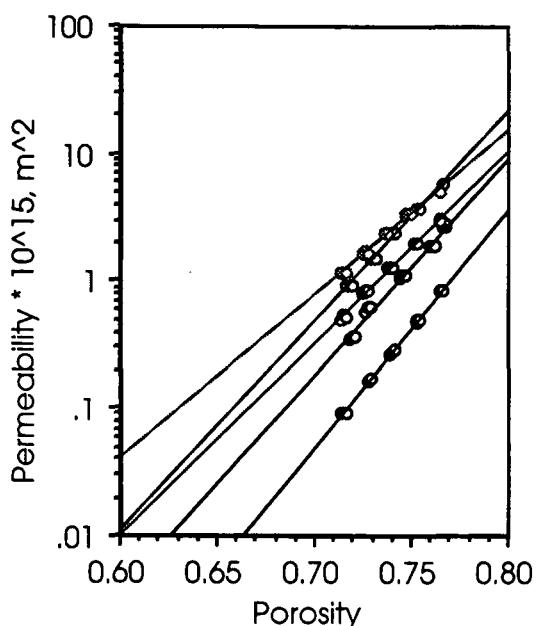


Figure D12. Furnish W2, solids 42%.

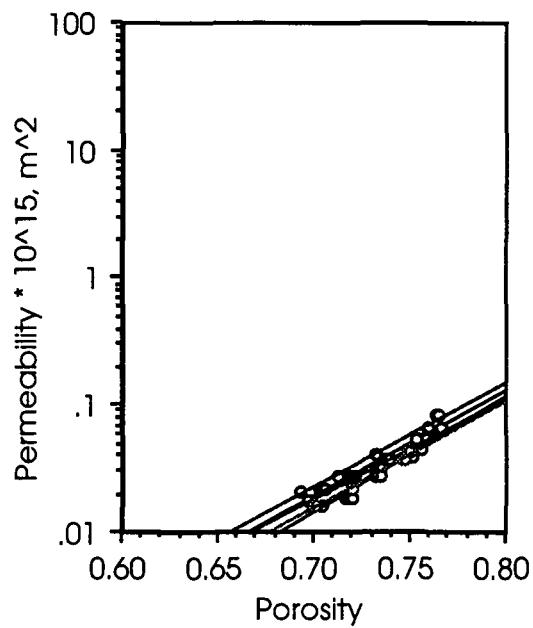


Figure D13. Furnish W3, solids 35%.

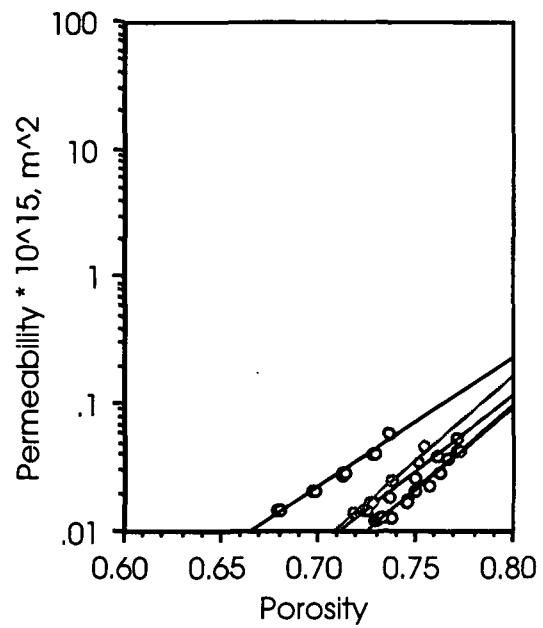


Figure D14. Furnish W3, solids 40%.

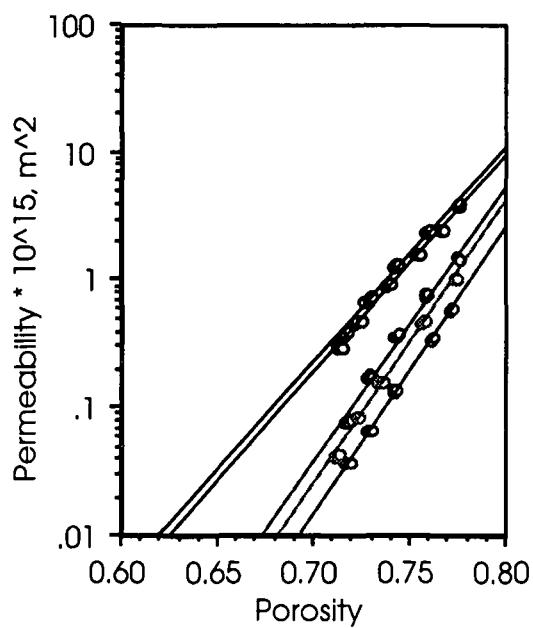


Figure D15. Furnish W5, solids 35%.

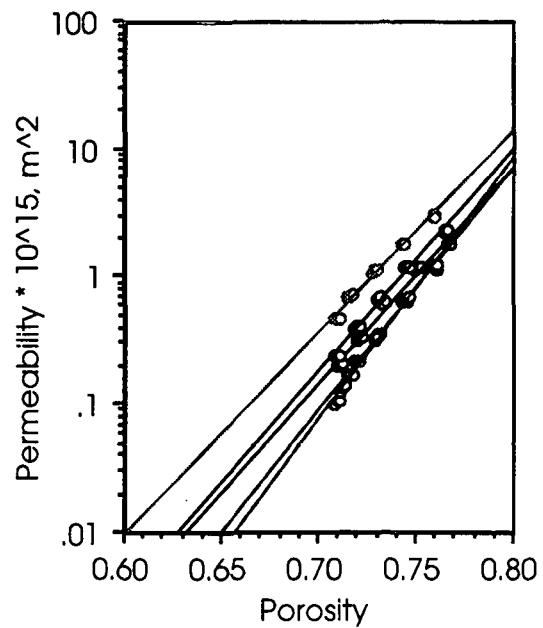


Figure D16. Furnish W5, solids 42%.

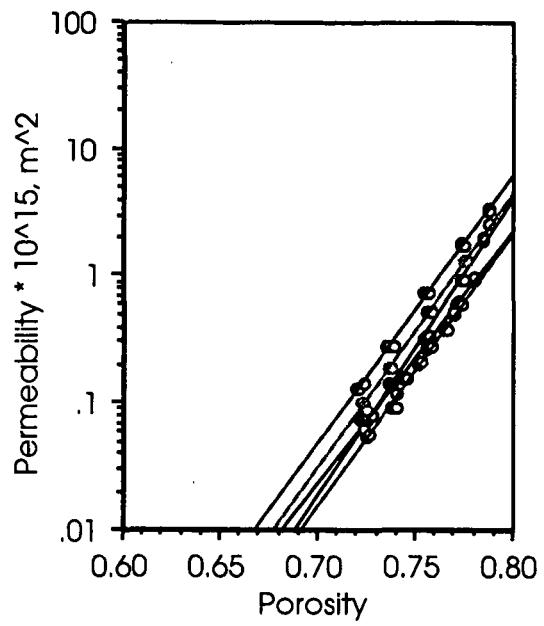


Figure D17. Furnish W6, solids 35%.

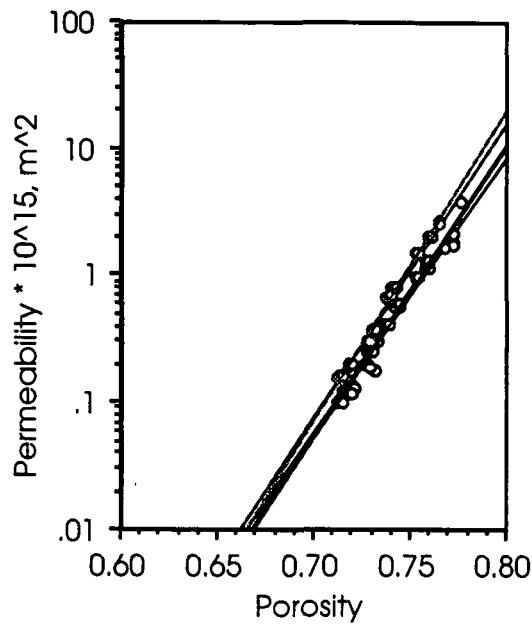


Figure D18. Furnish W6, solids 42%.

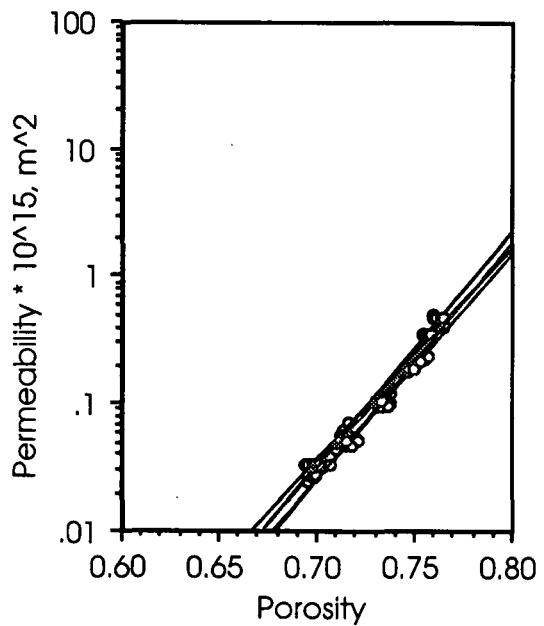


Figure D19. Furnish W7, solids 35%.

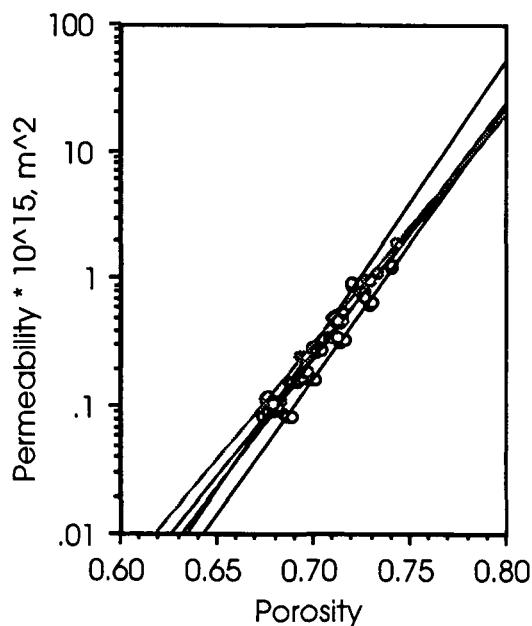


Figure D20. Furnish W7, solids 42%.

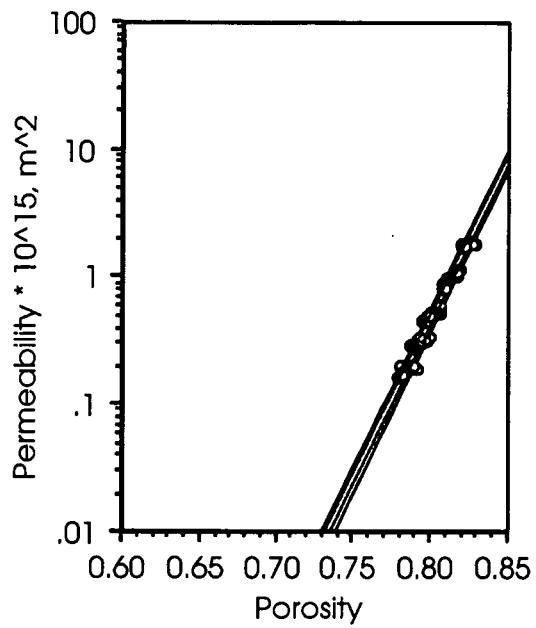


Figure D21. Furnish W8, solids 35%.

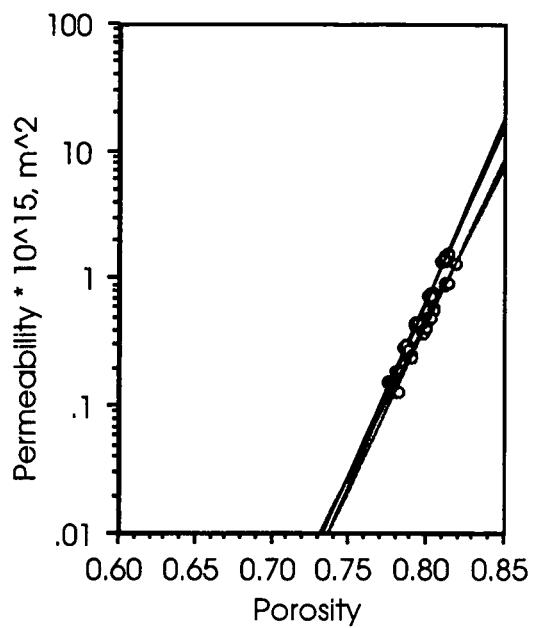


Figure D22. Furnish W8, solids 42%.

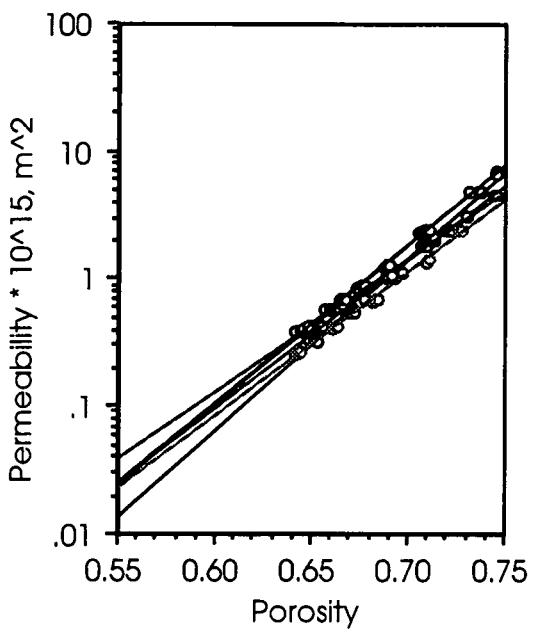


Figure D23. Furnish W9, press condition P1.

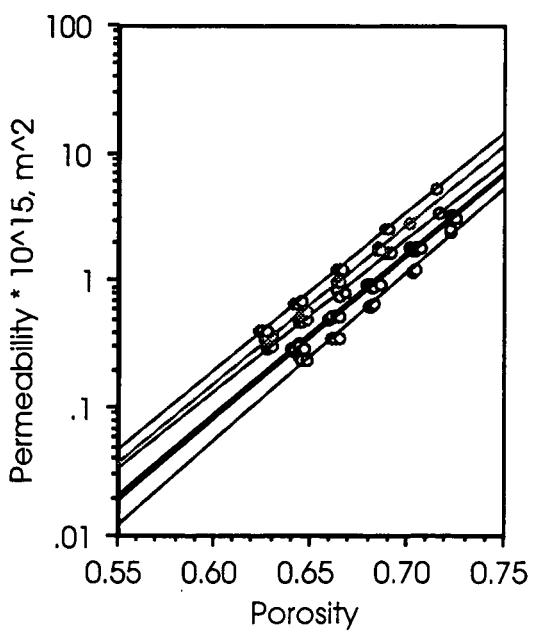


Figure D24. Furnish W9, press condition P2.

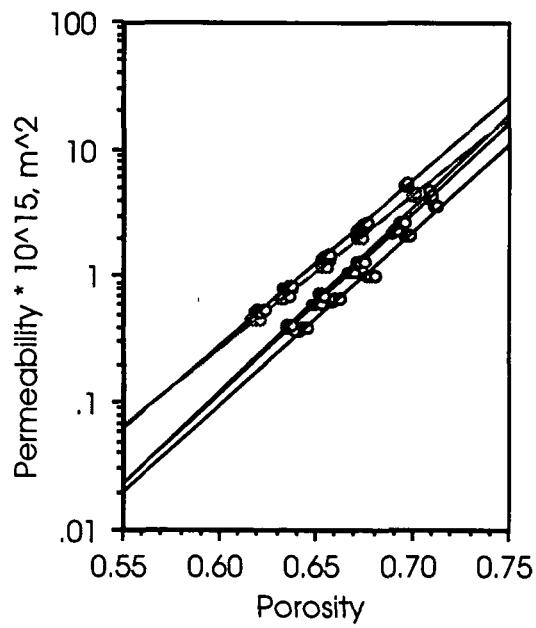


Figure D25. Furnish W9, press condition P3.

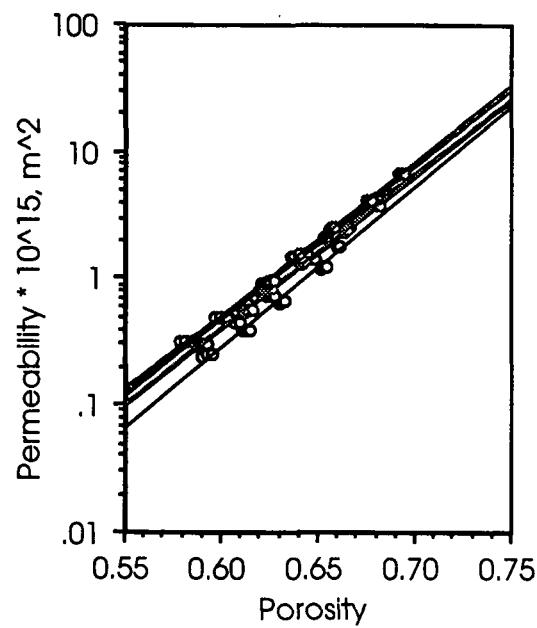


Figure D26. Furnish W9, press condition P4.

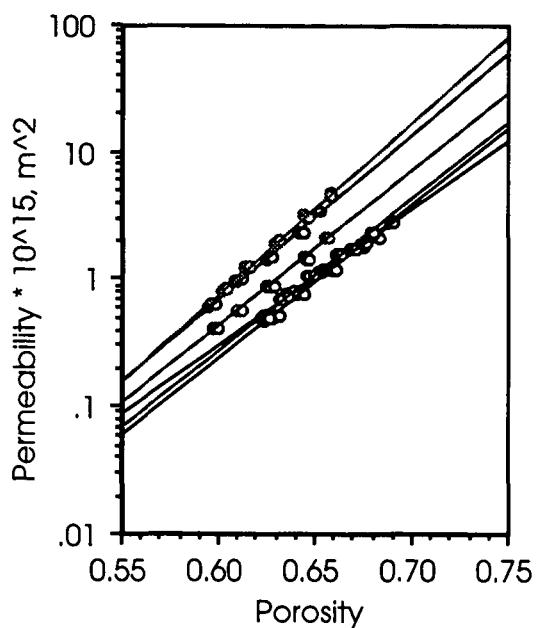


Figure D27. Furnish W9, press condition P5.

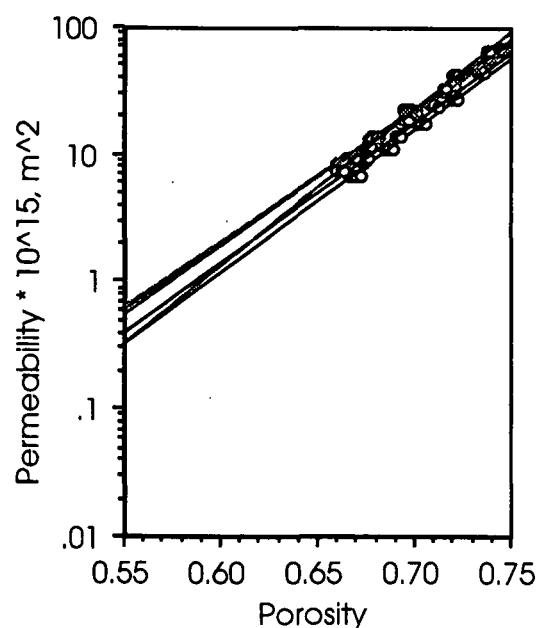


Figure D28. Furnish W10, press condition P1.

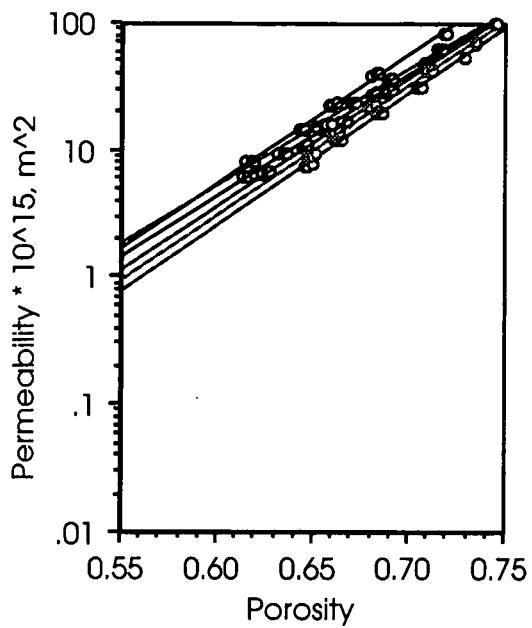


Figure D29. Furnish W10, press condition P2.

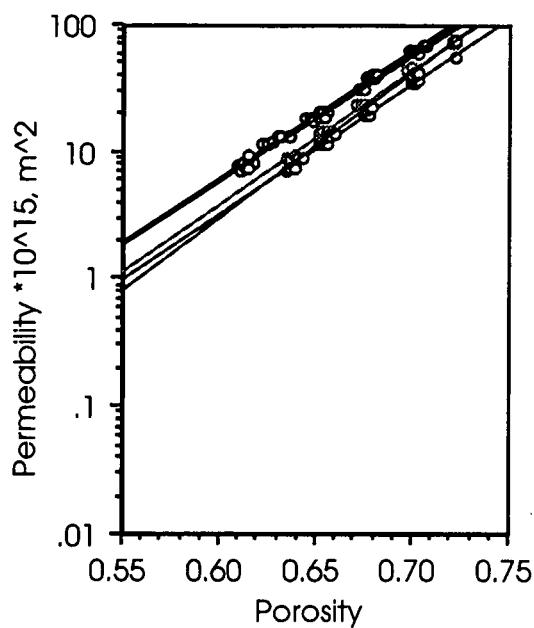


Figure D30. Furnish W10, press condition P3.

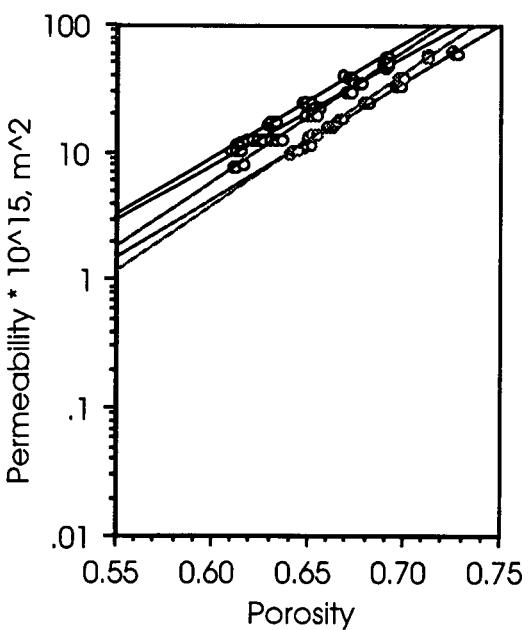


Figure D31. Furnish W10, press condition P4.

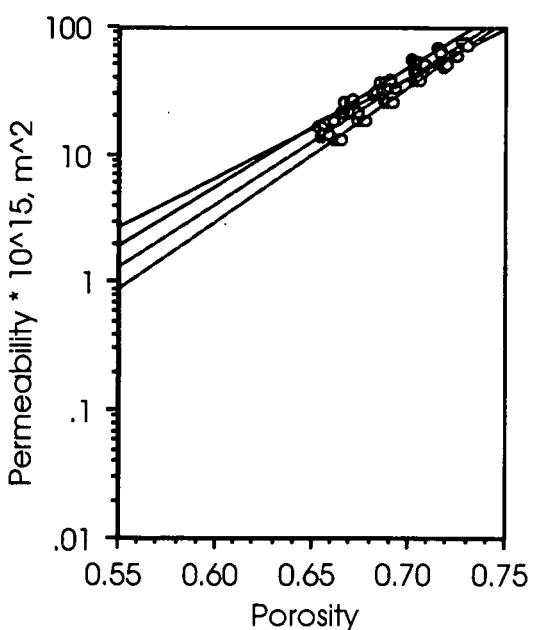


Figure D32. Furnish W10, press condition P5.

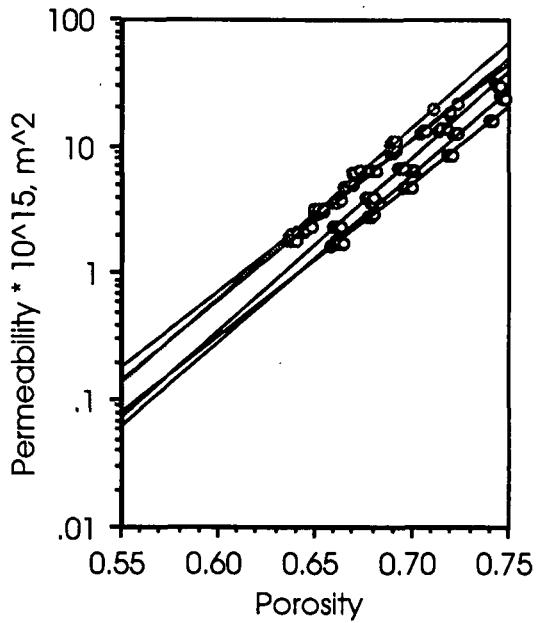


Figure D33. Furnish W11, press condition P1.

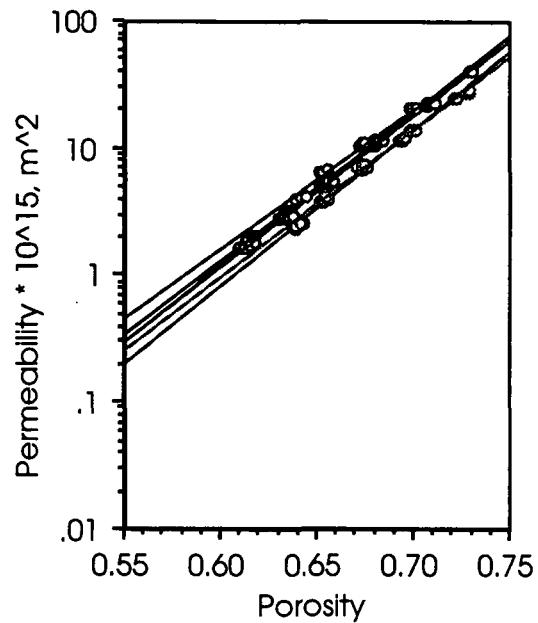


Figure D34. Furnish W11, press condition P2.

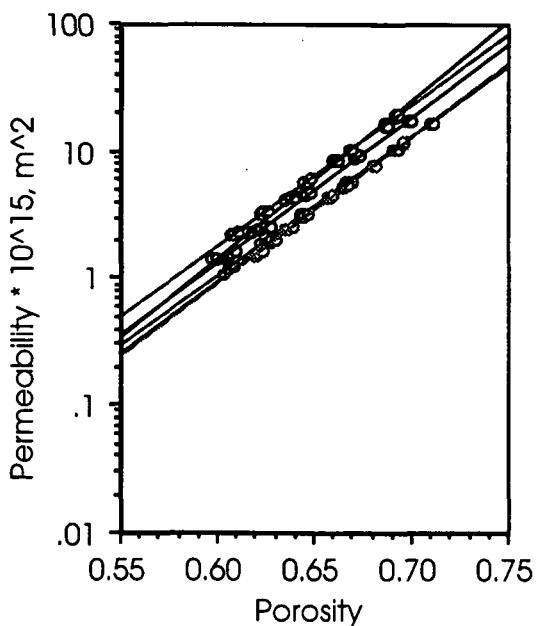


Figure D35. Furnish W11, press condition P3.

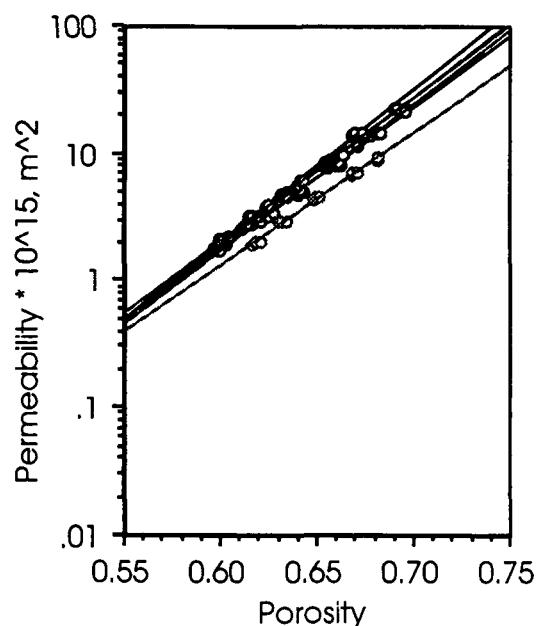


Figure D36. Furnish W11, press condition P4.

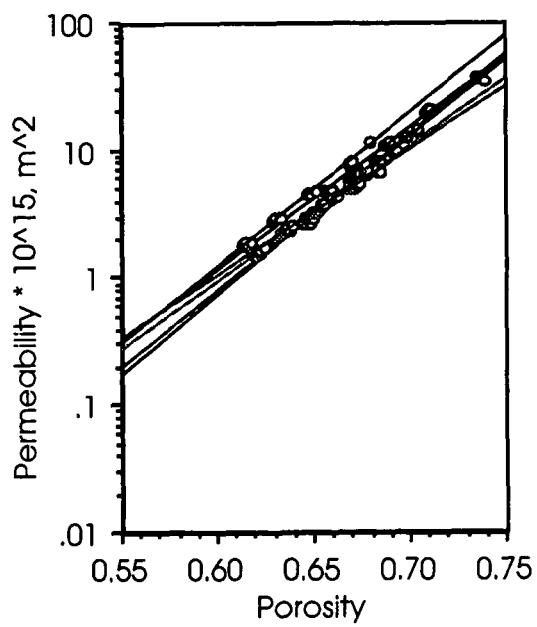


Figure D15. Furnish W37, press condition P5.

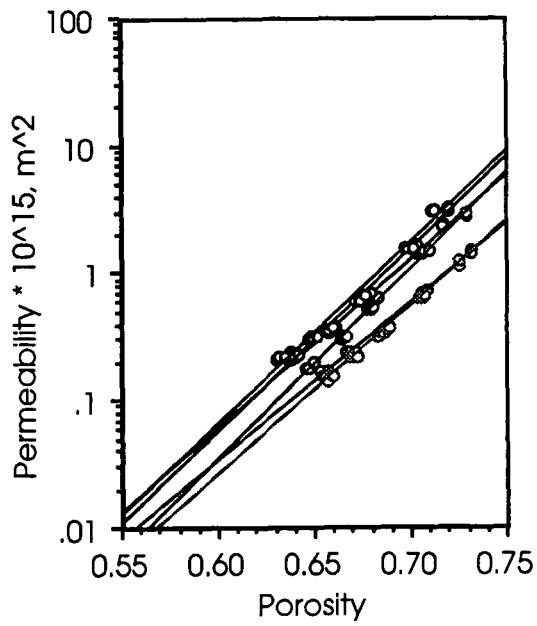


Figure D38. Furnish W12, press condition P1.

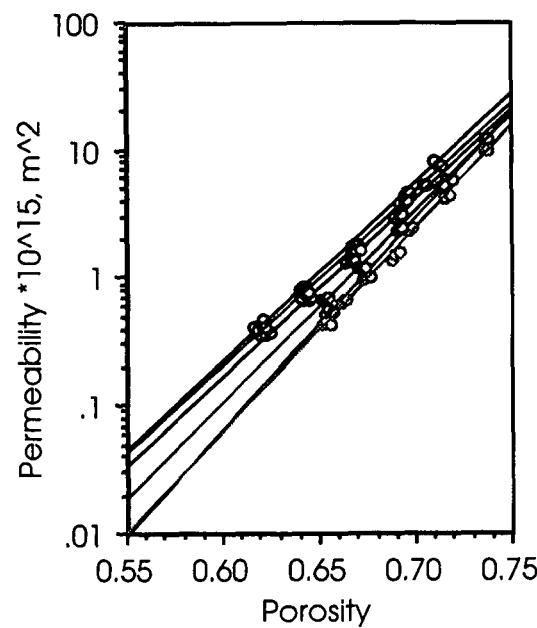


Figure D39. Furnish W12, press condition P2.

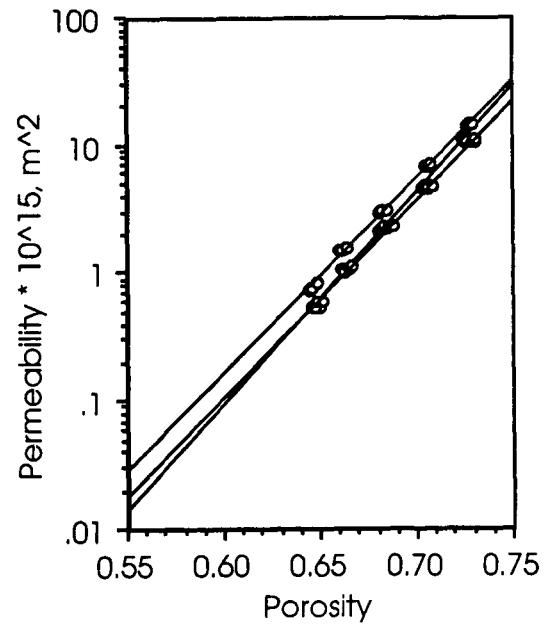


Figure D40. Furnish W12, press condition P3.

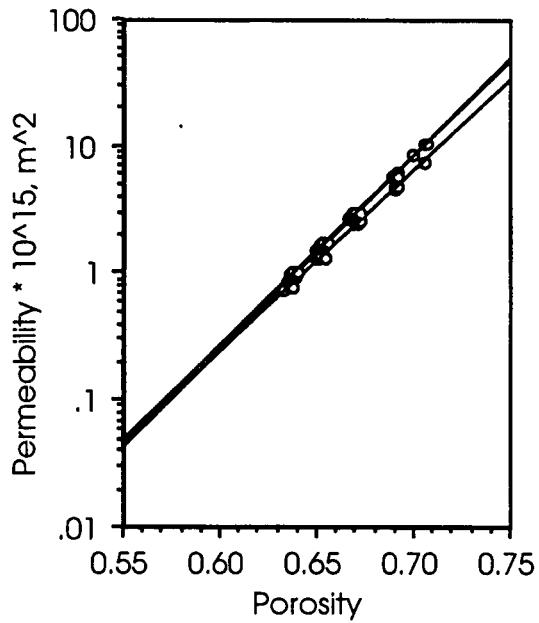


Figure D41. Furnish W12, press condition P4.

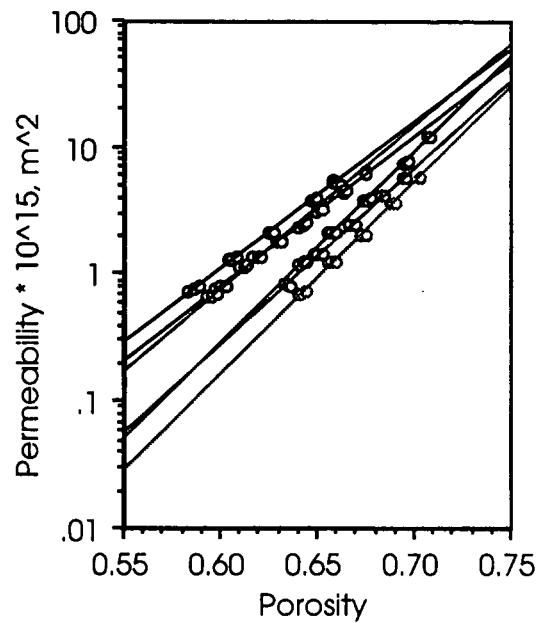


Figure D42. Furnish W12, press condition P5.

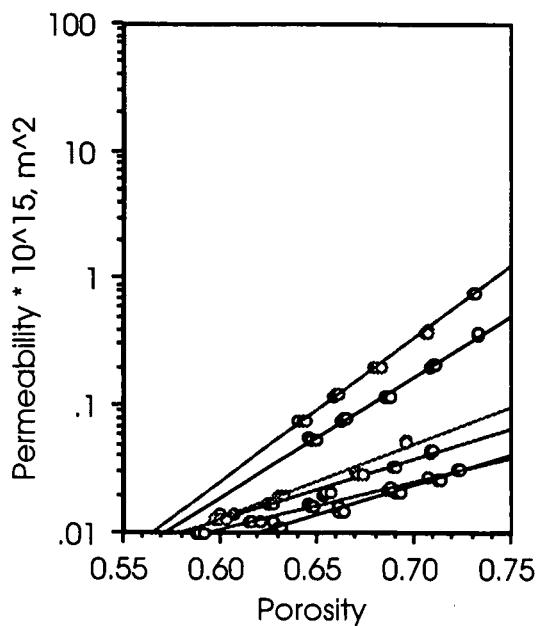


Figure D43. Furnish W15, press condition P2.

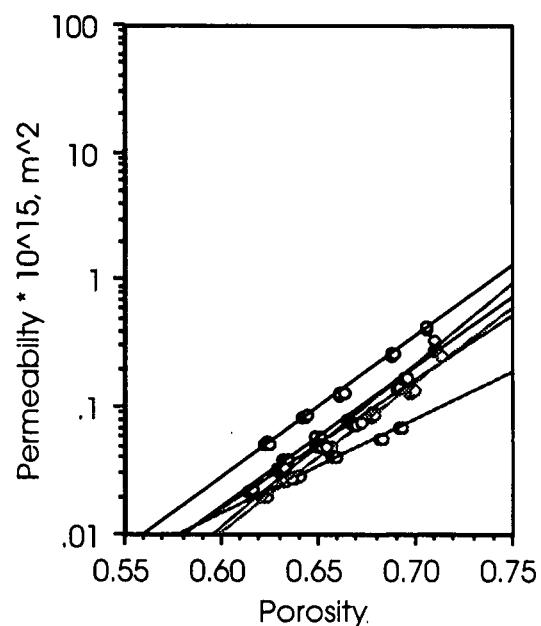


Figure D44. Furnish W15, press condition P3.

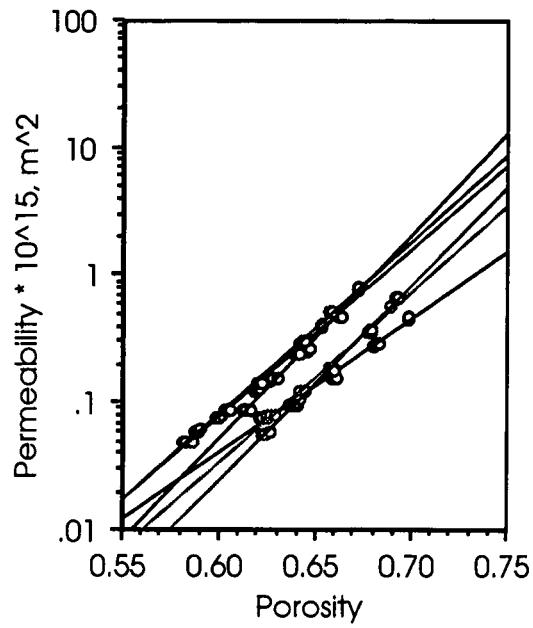


Figure D45. Furnish W15, press condition P4.

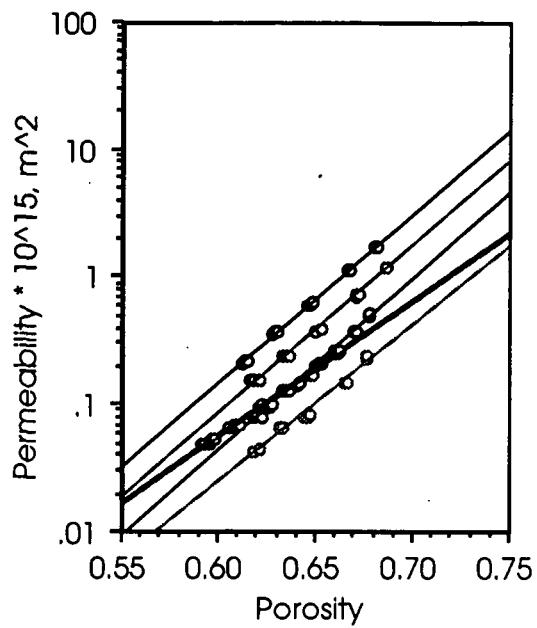


Figure D46. Furnish W15, press condition P5.

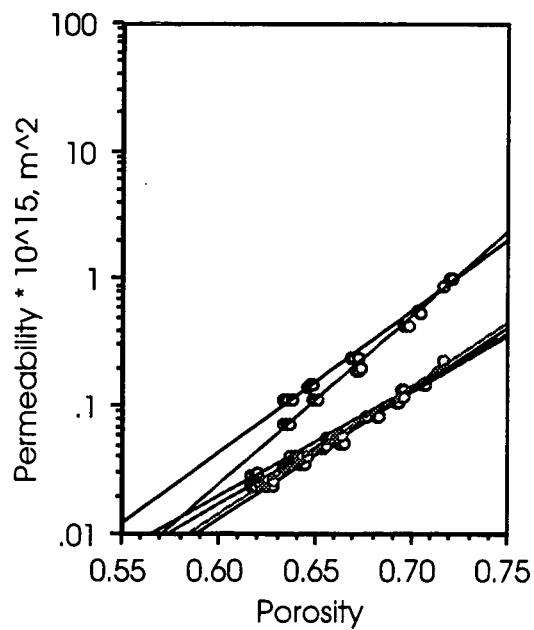


Figure D47. Furnish W16, press condition P2.

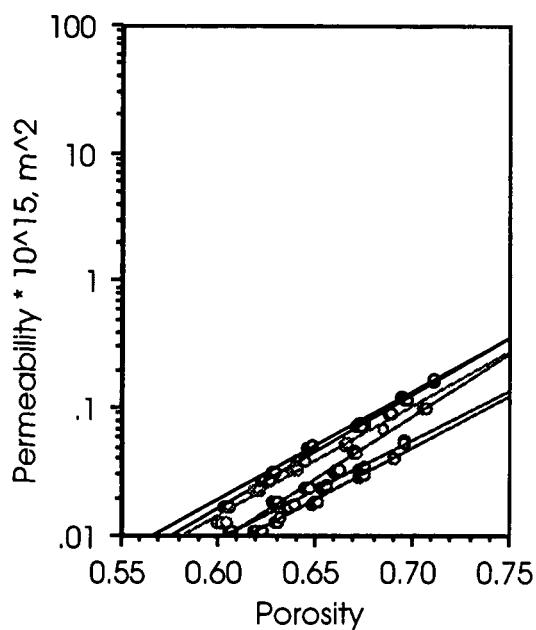


Figure D48. Furnish W16, press condition P3.

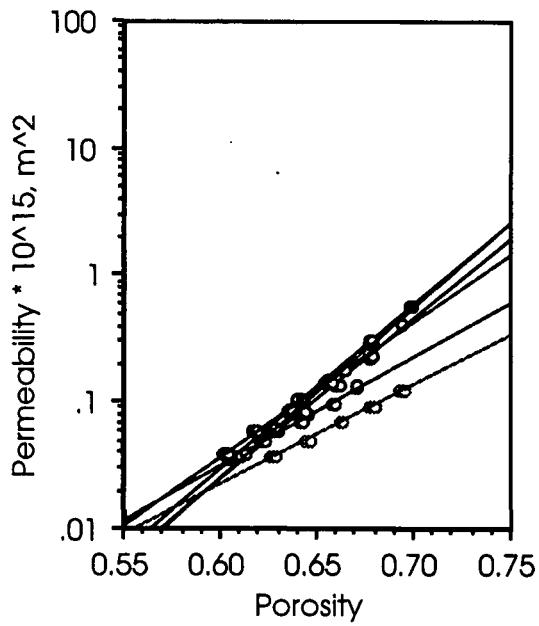


Figure D49. Furnish W16, press condition P4.

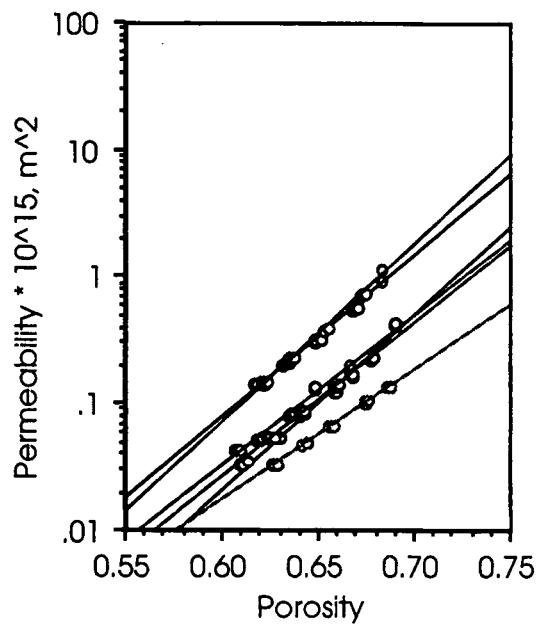


Figure D50. Furnish W16, press condition P5.

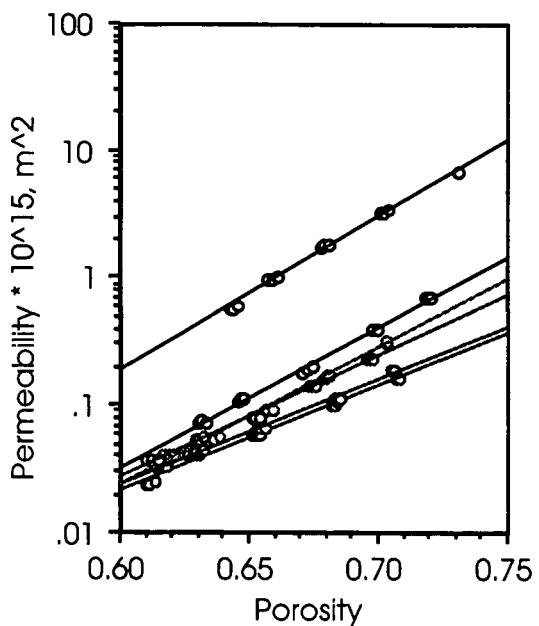


Figure D51. Furnish W17, press condition P1.

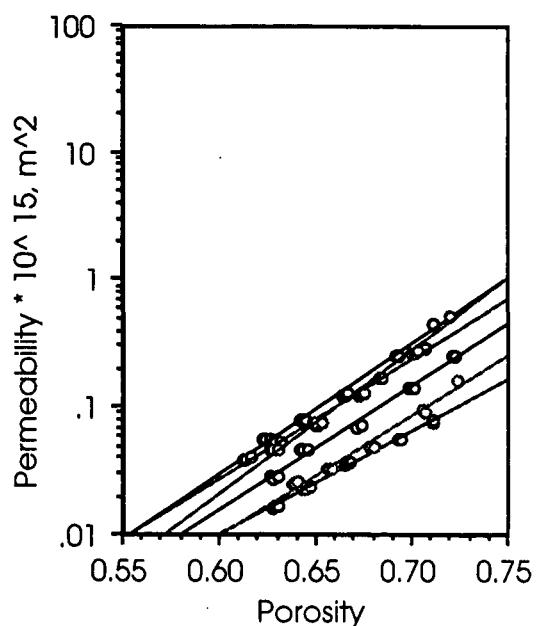


Figure D52. Furnish W17, press condition P2.

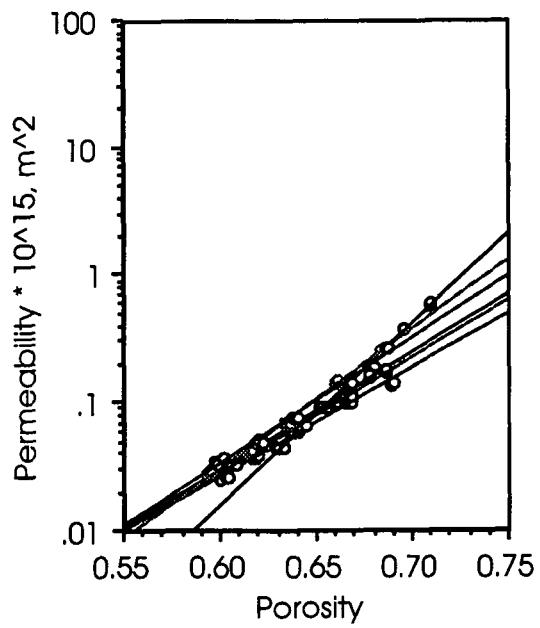


Figure D53. Furnish W17, press condition P3.

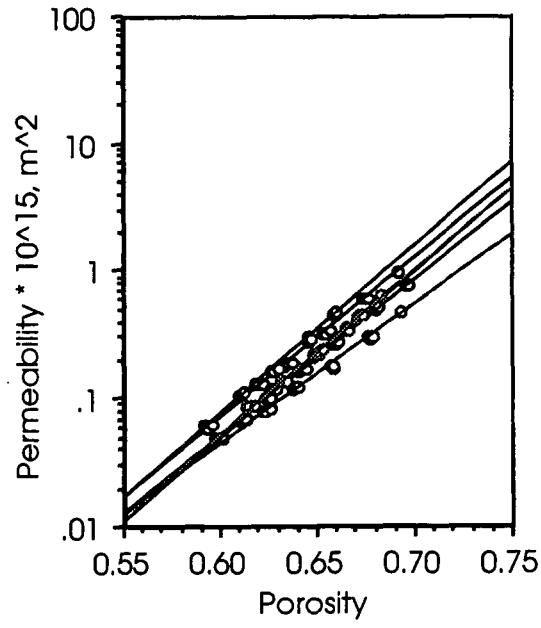


Figure D54. Furnish W17, press condition P4.

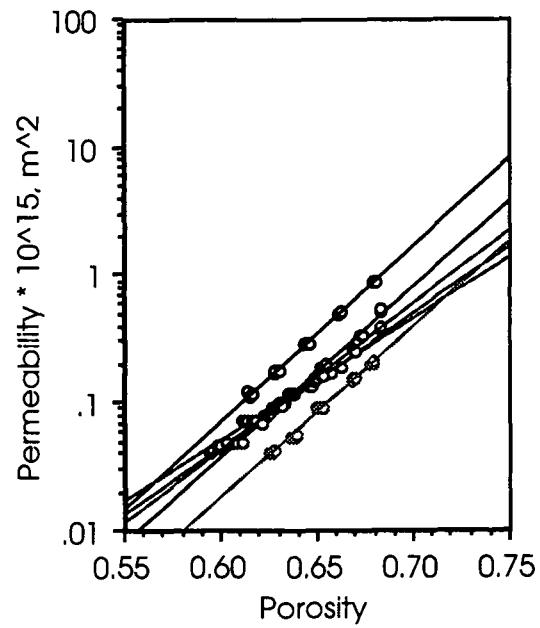


Figure D55. Furnish W17, press condition P5.

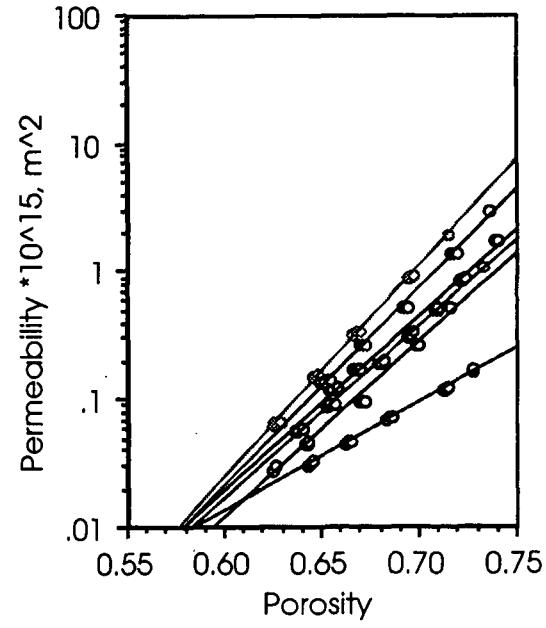


Figure D56. Furnish W18, press condition P1.

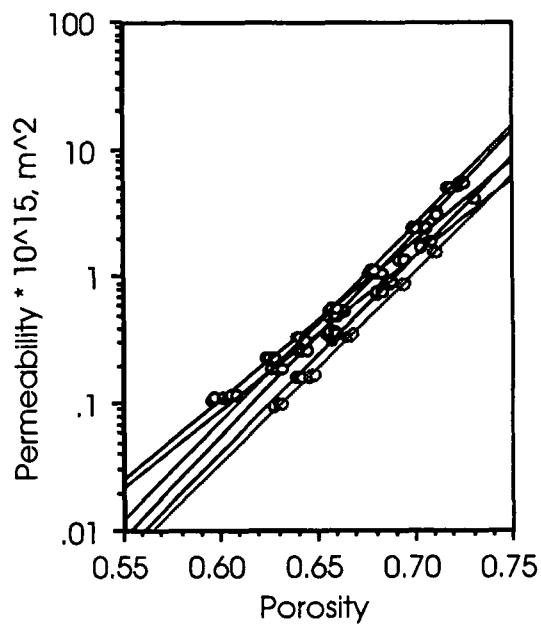


Figure D57. Furnish W18, press condition P2.

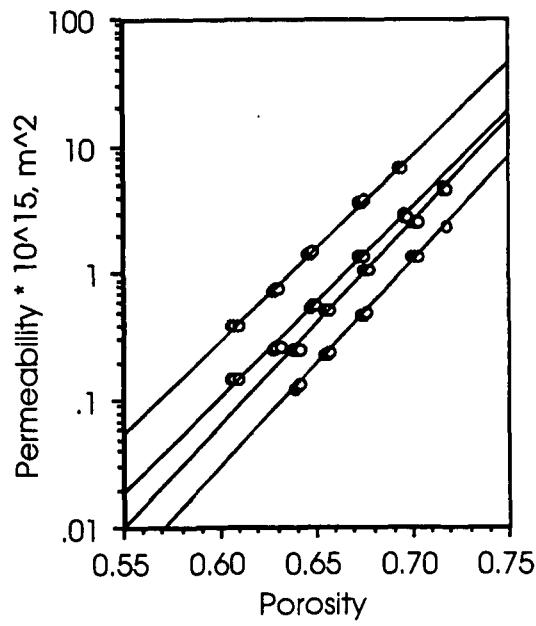


Figure D58. Furnish W18, press condition P3.

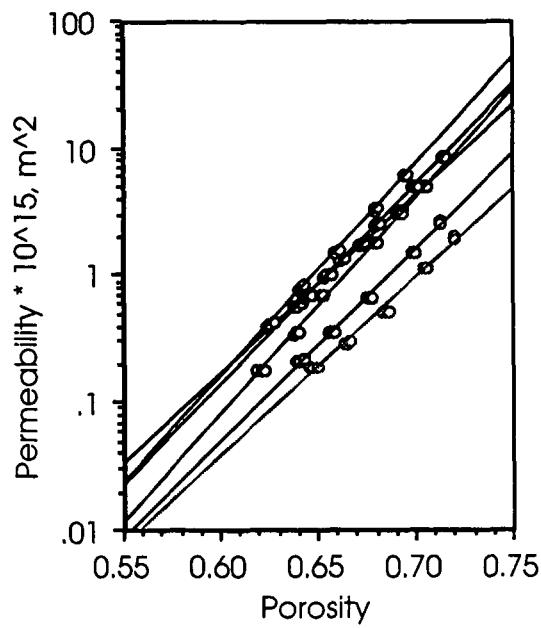


Figure D59. Furnish W18, press condition P4.

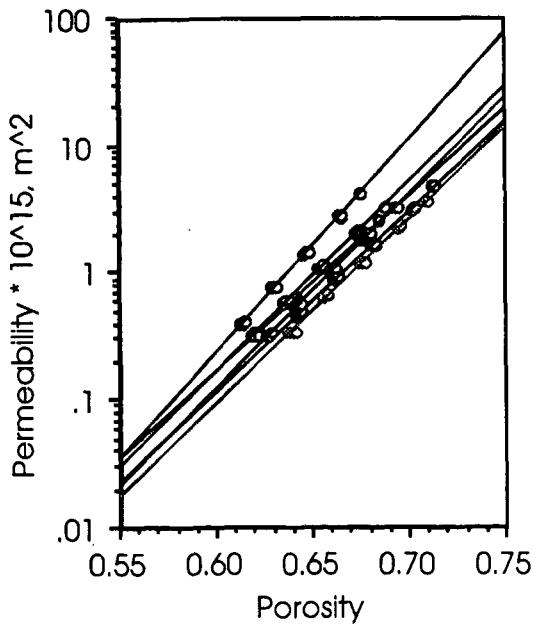


Figure D60. Furnish W18, press condition P5.

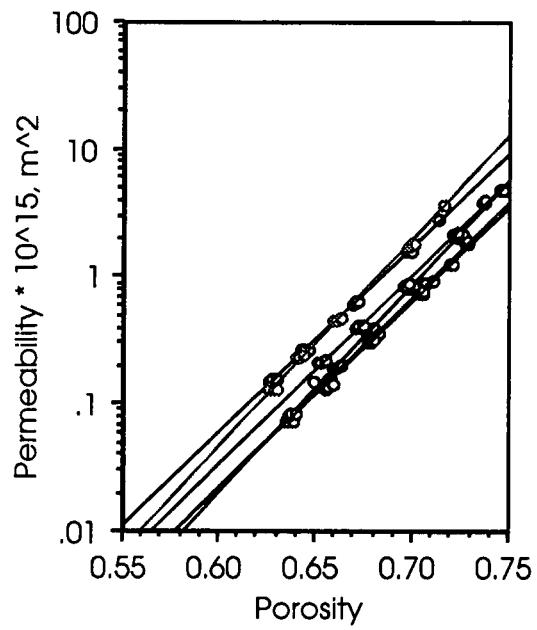


Figure D61. Furnish W19, press condition P1.

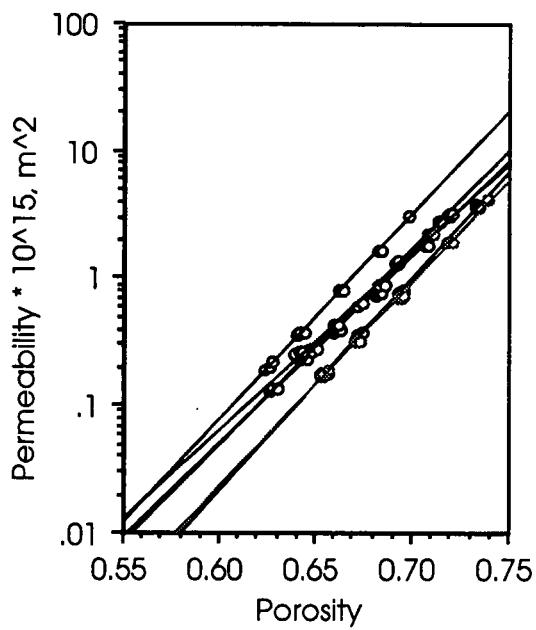


Figure D62. Furnish W19, press condition P2.

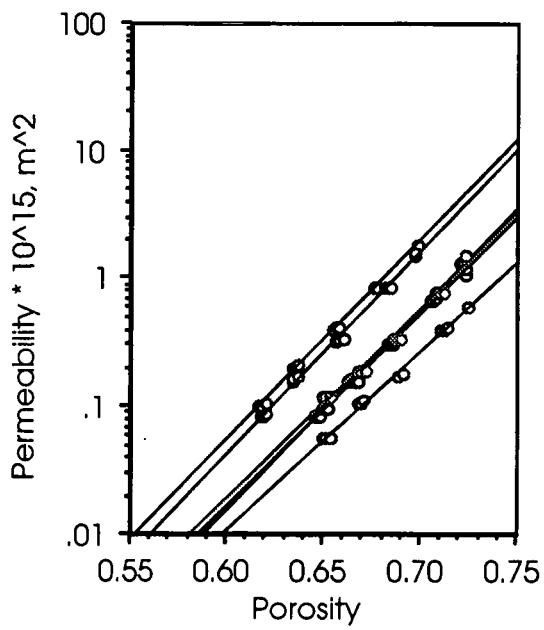


Figure D63. Furnish W19, press condition P3.

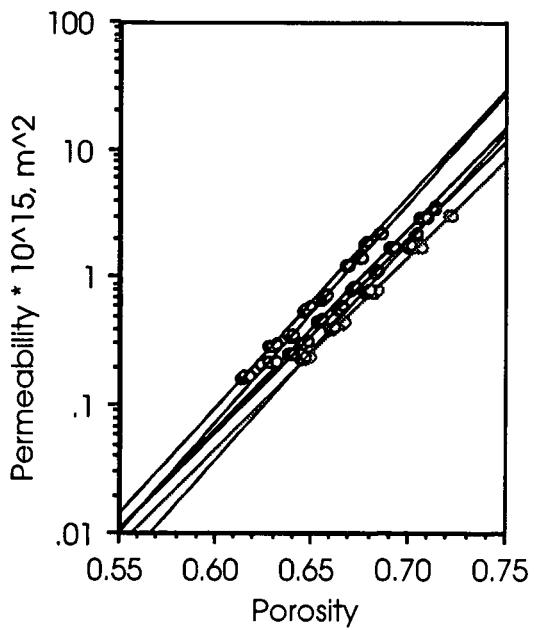


Figure D64. Furnish W19, press condition P4.

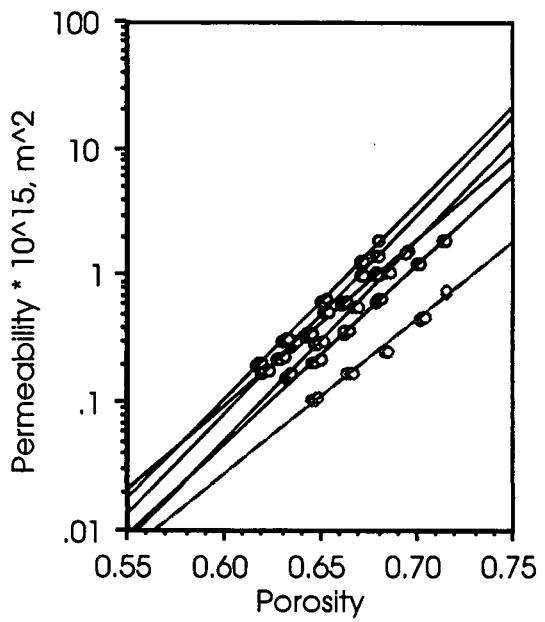


Figure D65. Furnish W19, press condition P5.

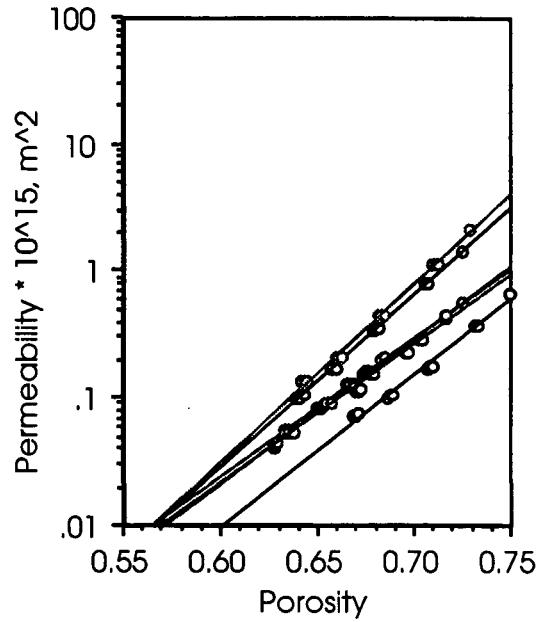


Figure D66. Furnish W20, press condition P1.

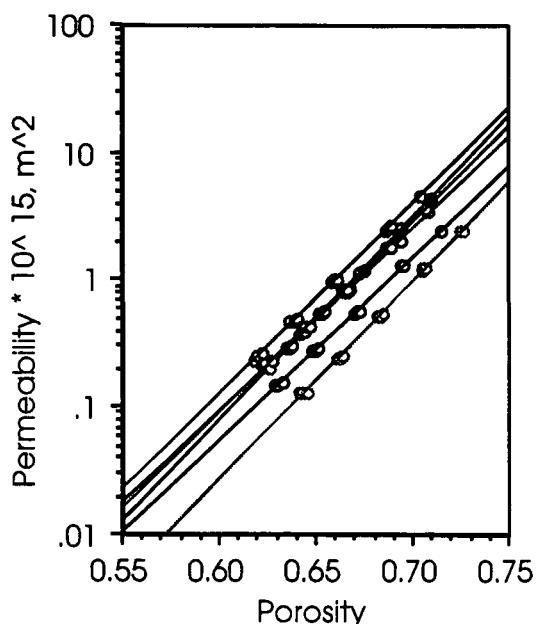


Figure D67. Furnish W20, press condition P2.

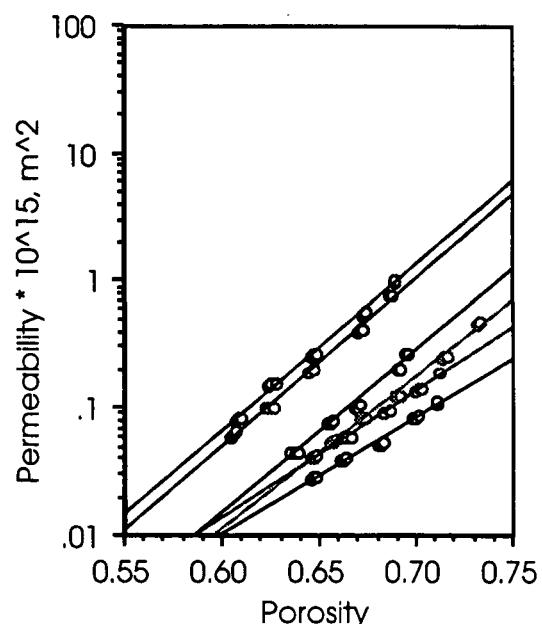


Figure D68. Furnish W20, press condition P3.

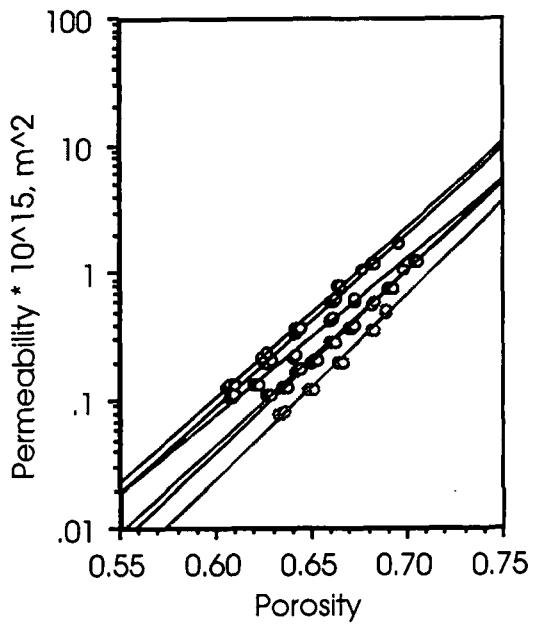


Figure D69. Furnish W20, press condition P4.

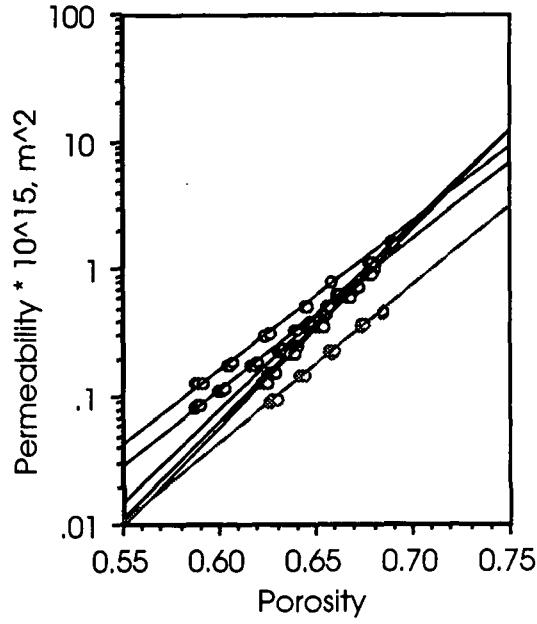


Figure D70. Furnish W20, press condition P5.

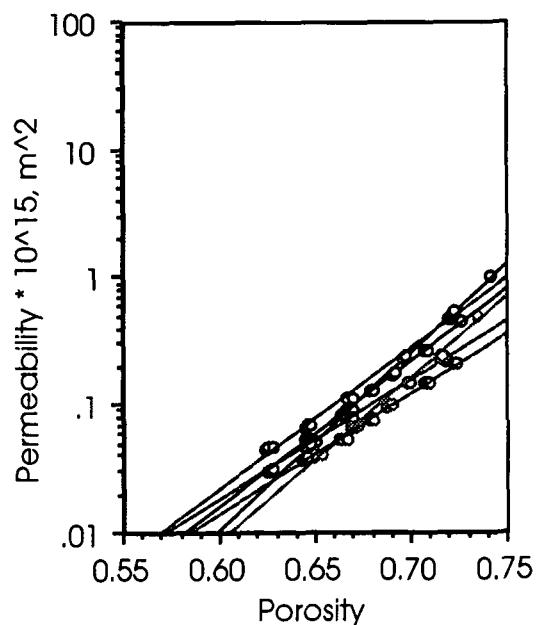


Figure D71. Furnish W21, press condition P1.

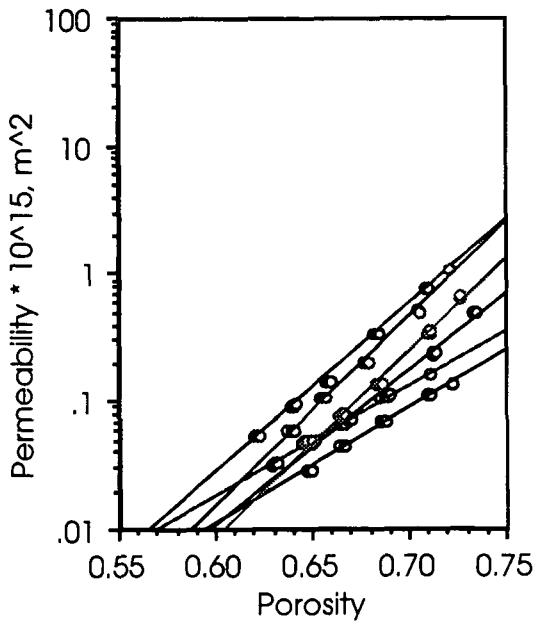


Figure D72. Furnish W21, press condition P2.

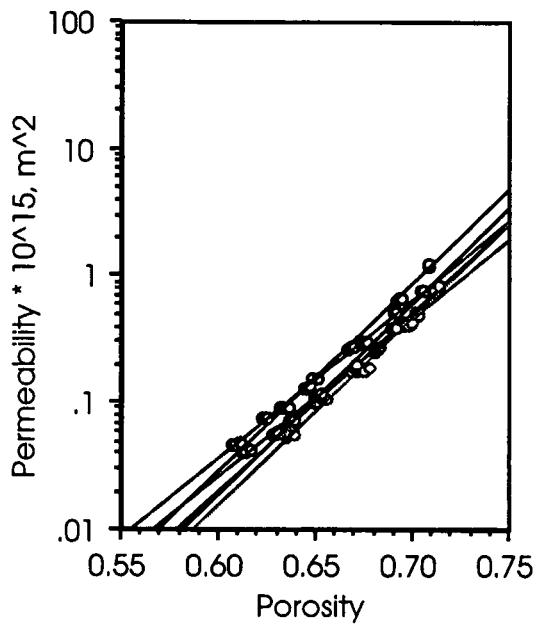


Figure D73. Furnish W21, press condition P3.

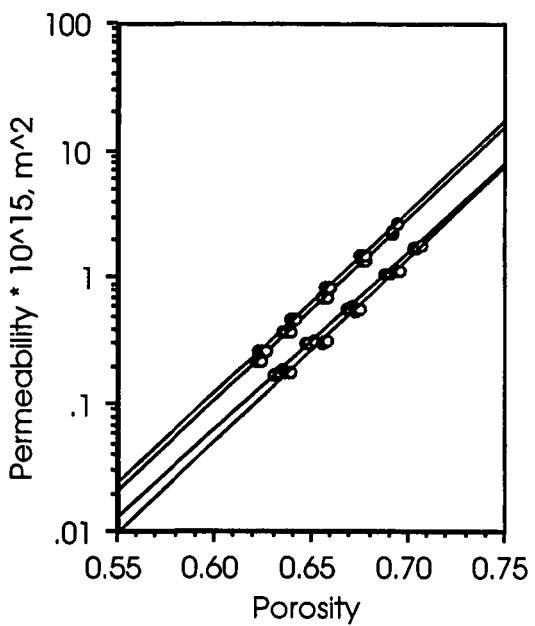


Figure D74. Furnish W21, press condition P4.

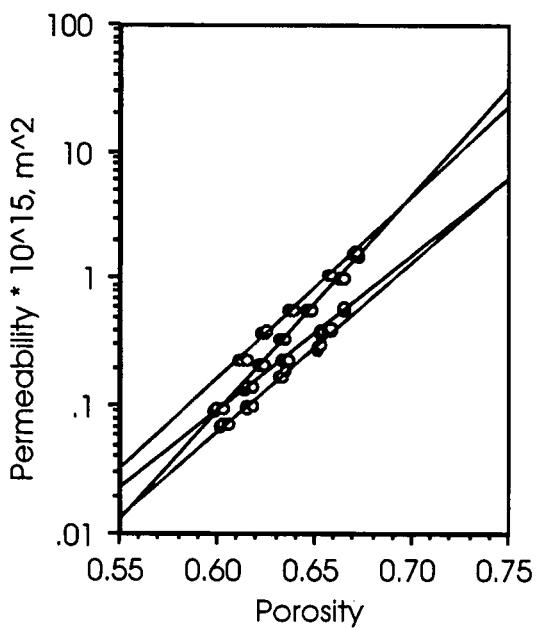


Figure D75. Furnish W21, press condition P5.

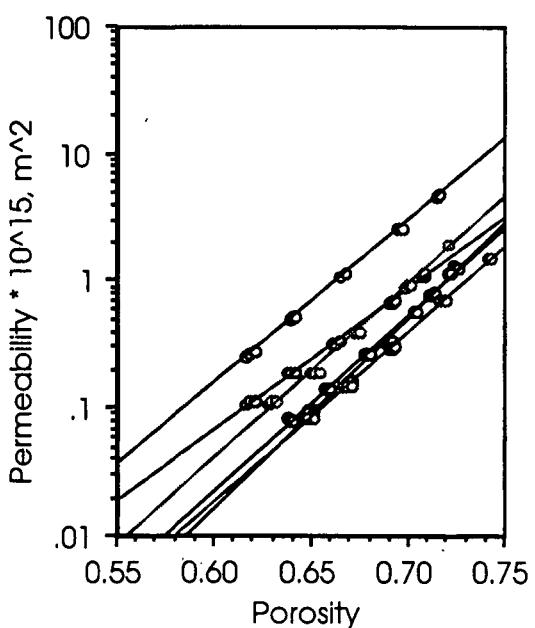


Figure D76. Furnish W22, press condition P1.

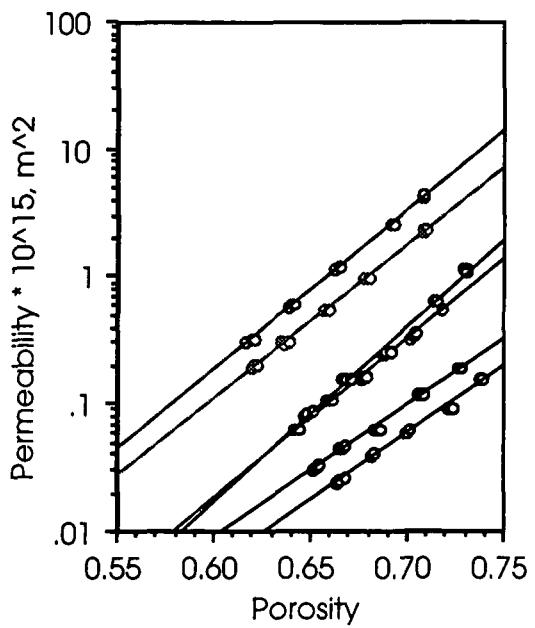


Figure D77. Furnish W22, press condition P2.

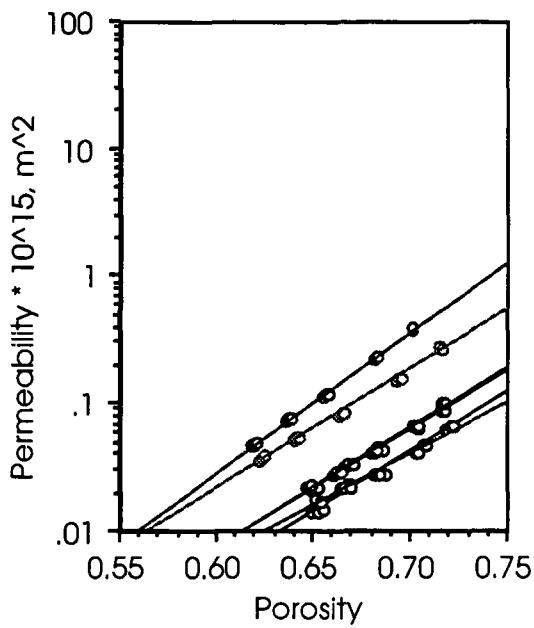


Figure D78. Furnish W22, press condition P3.

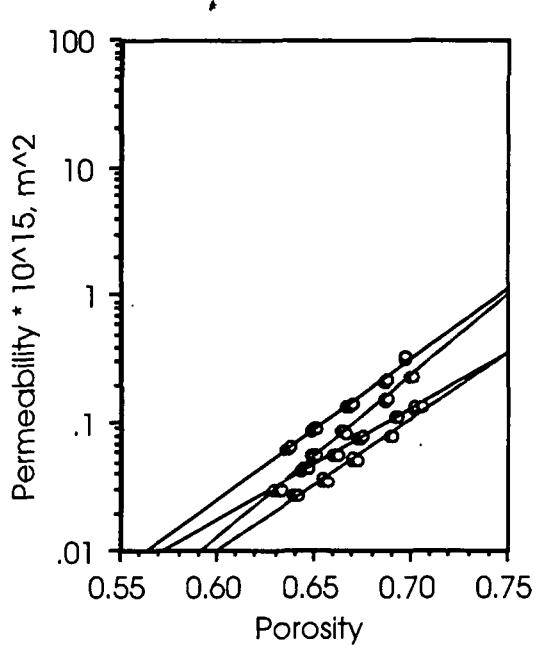


Figure D79. Furnish W22, press condition P4.

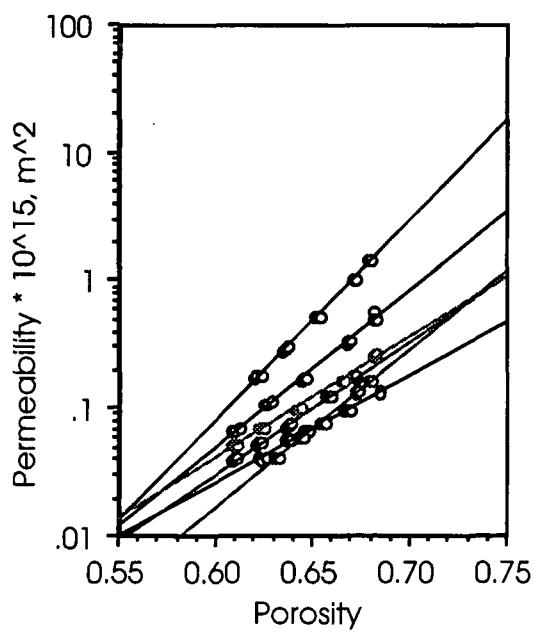


Figure D80. Furnish W22, press condition P5.

## APPENDIX E

The following figures show the temperatures recorded during presteaming. Time zero is when the steam is first turned on. The steaming time was set to the time when the lowest temperature exceeded 55°C.

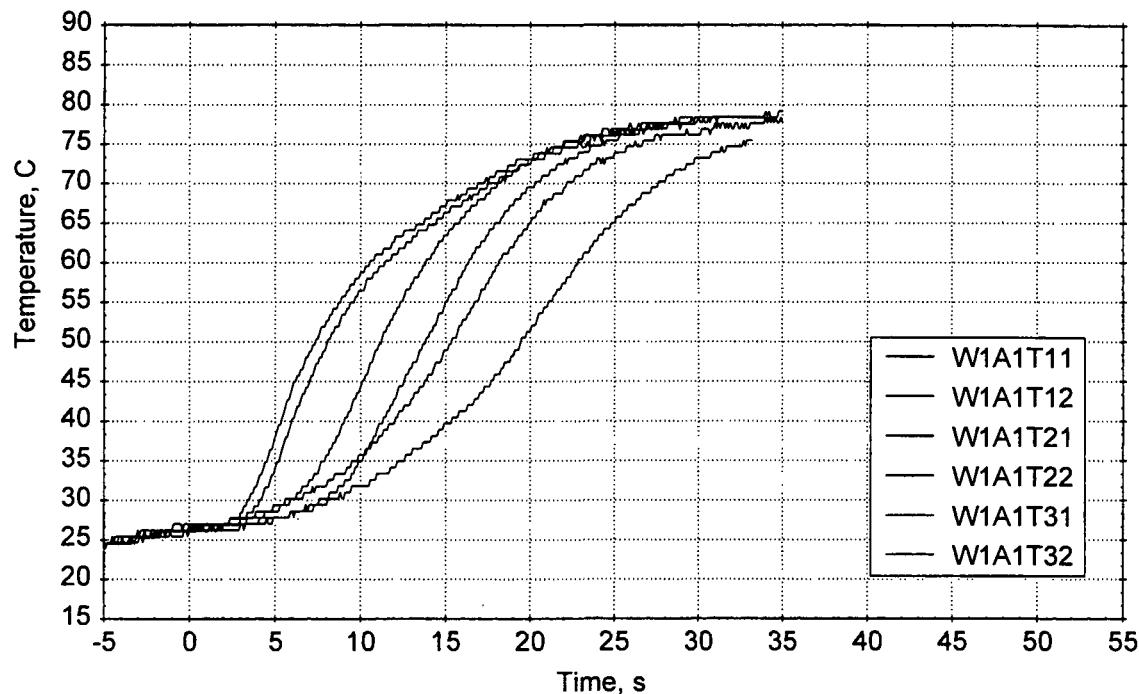


Figure E1. Furnish W1 (2P1), A platen, B felt, 35% sheet solids.

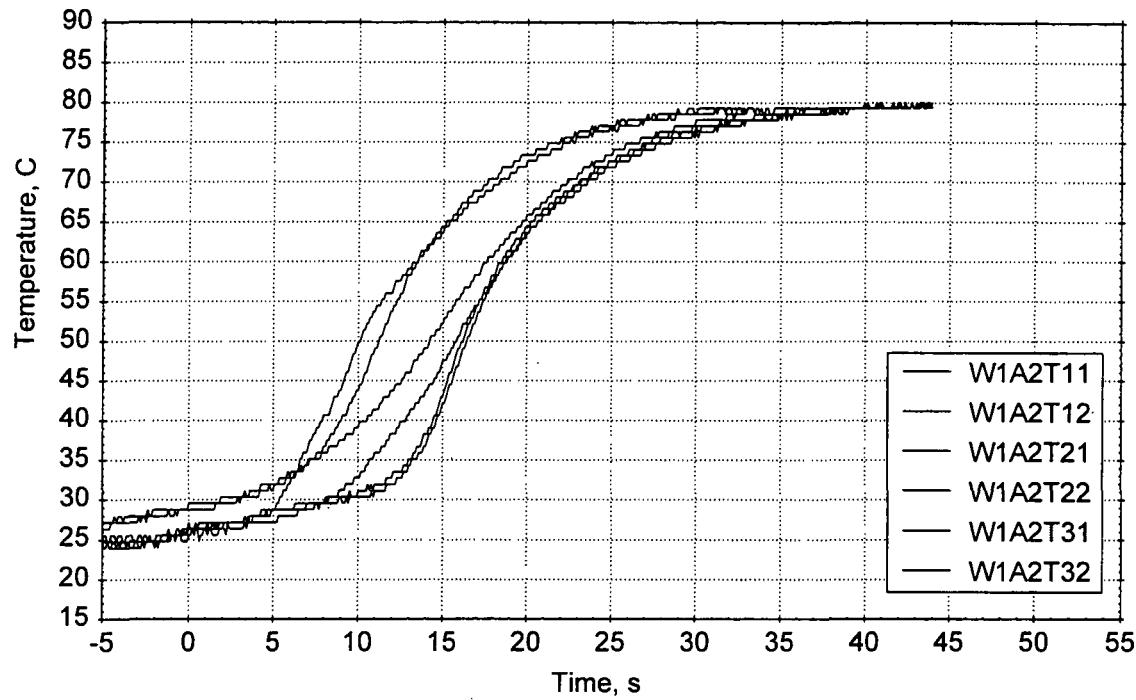


Figure E2. Furnish W1 (2P1), A platen, B felt, 42% sheet solids.

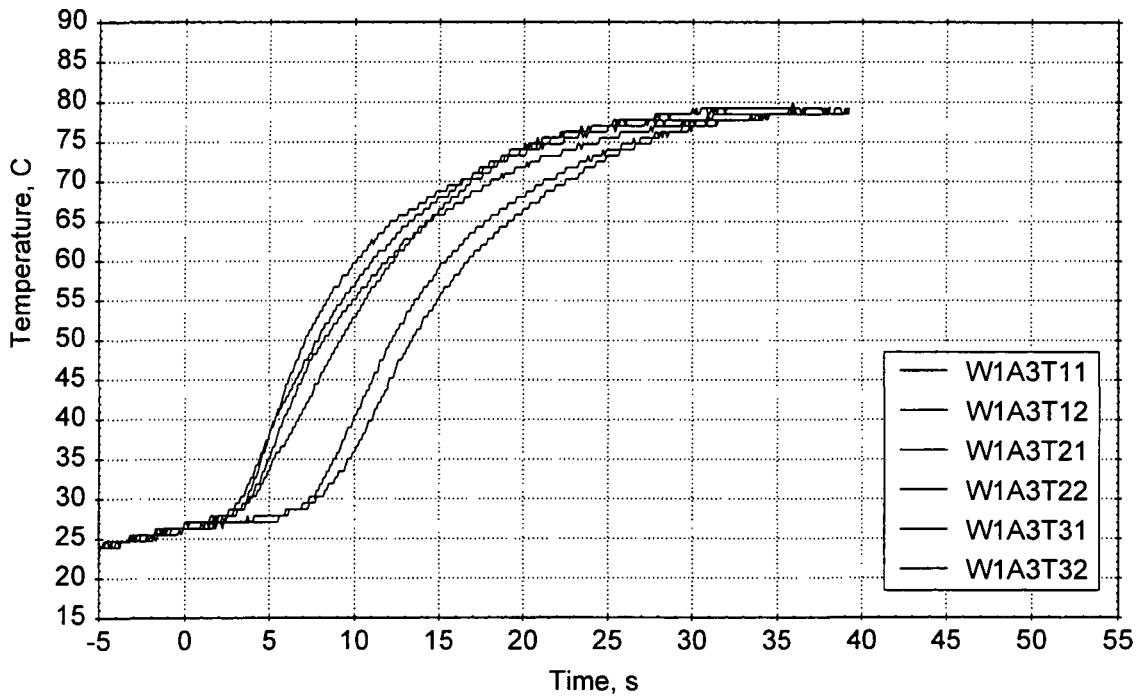


Figure E3. Furnish W1 (2P1), A platen, R felt, 35% sheet solids.

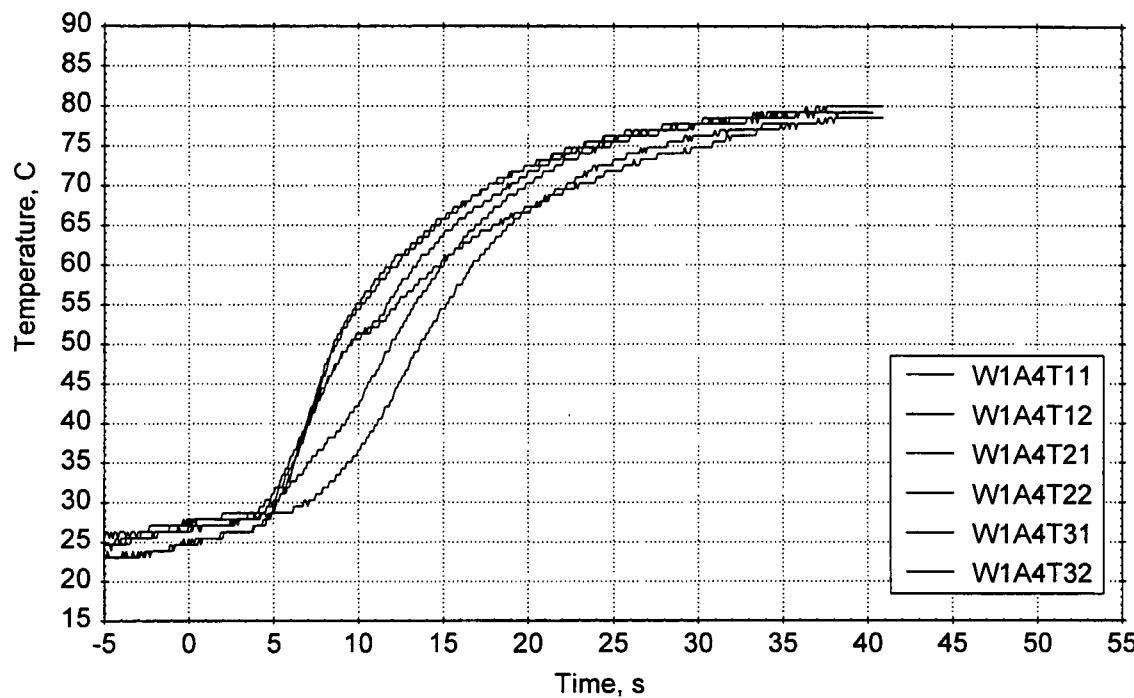


Figure E4. Furnish W1 (2P1), A platen, R felt, 42% sheet solids.

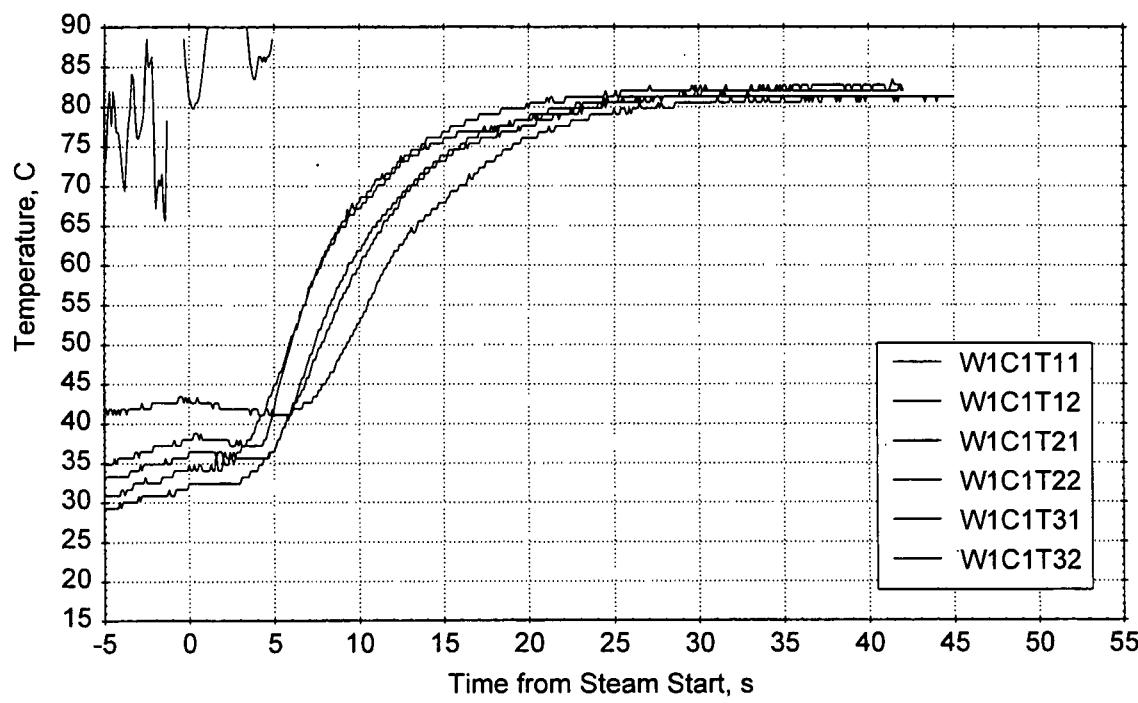


Figure E5. Furnish W1 (2P1), C platen, B felt, 35% sheet solids.

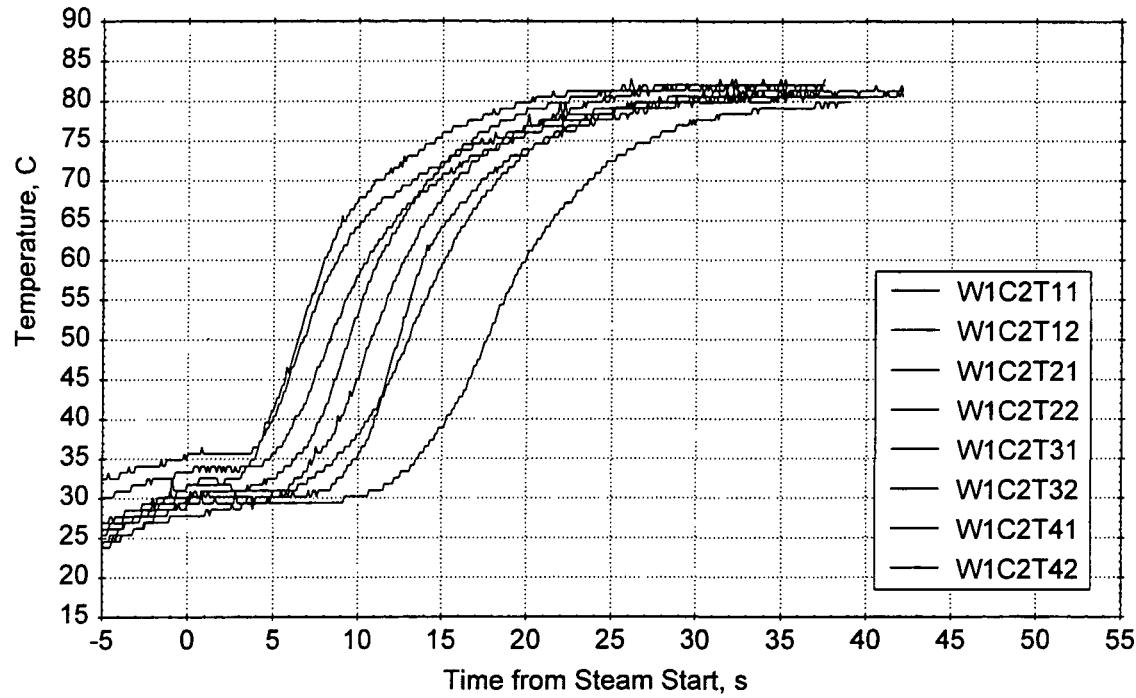


Figure E6. Furnish W1 (2P1), C platen, B felt, 42% sheet solids.

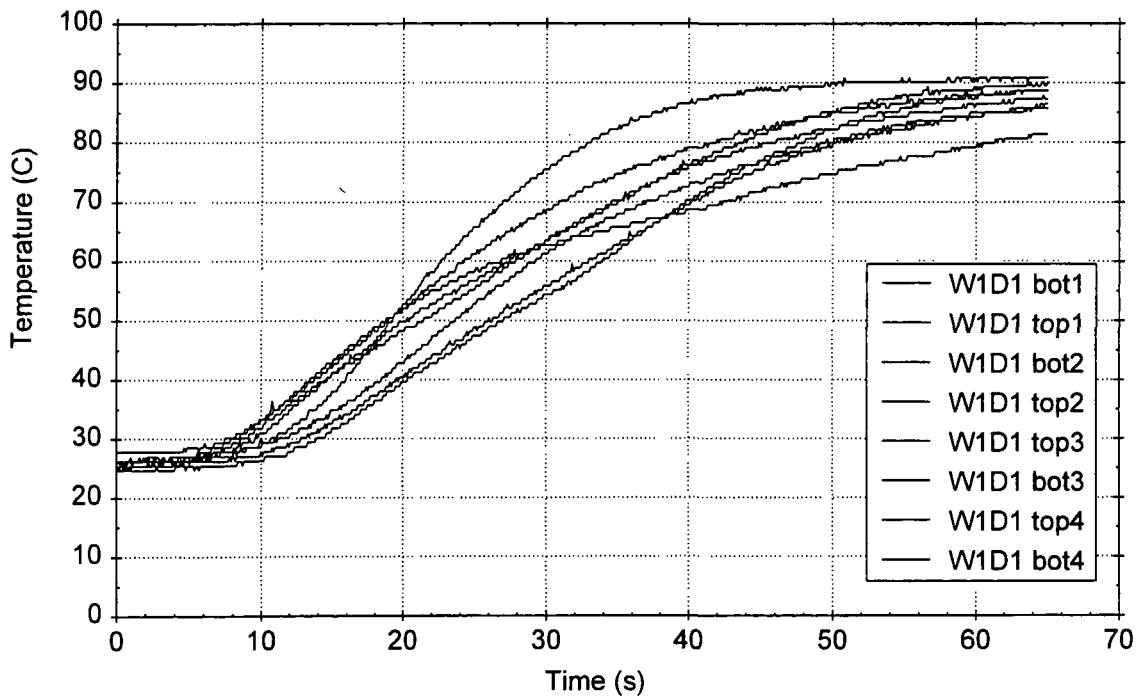


Figure E7. Furnish W1 (2P1), double-felted pressing, B felt, 35% sheet solids.

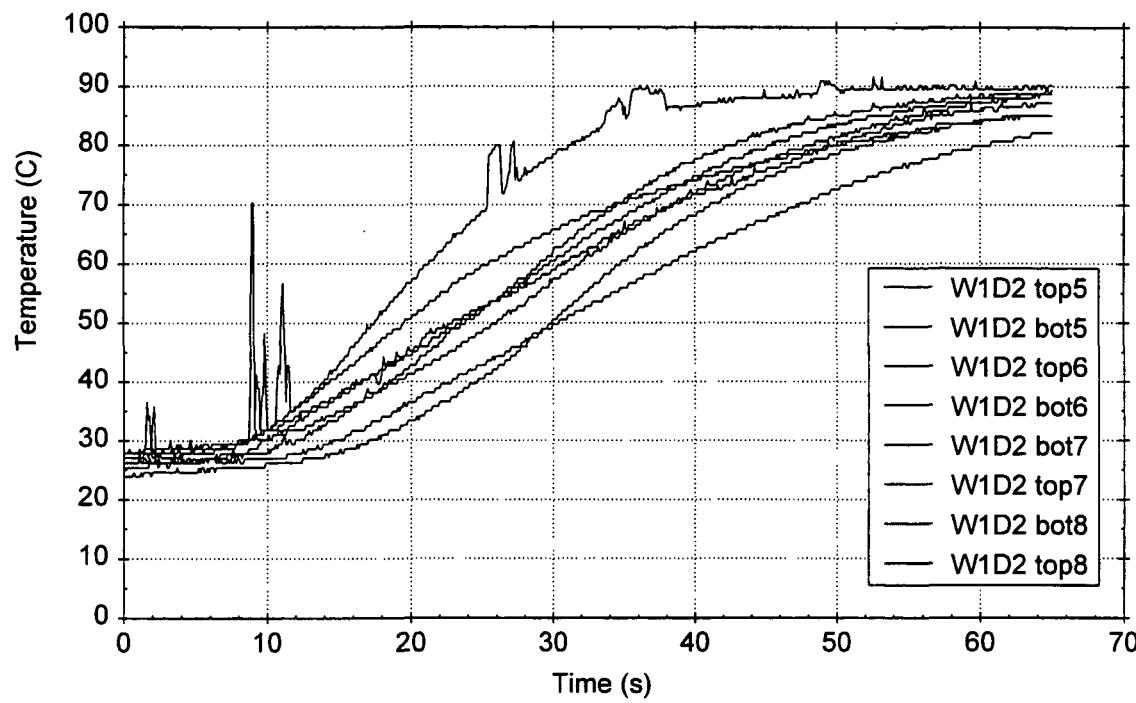


Figure E8. Furnish W1 (2P1), double-felted pressing, B felt, 42% sheet solids.

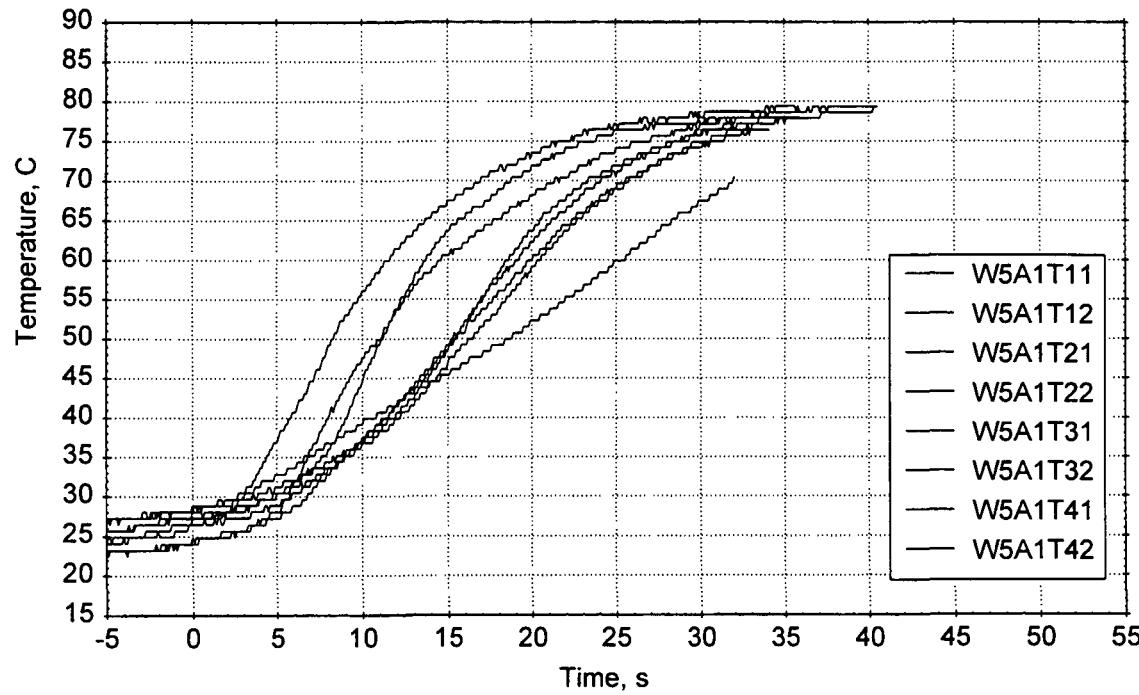


Figure E9. Furnish W5 (2P3), A platen, B felt, 35% sheet solids.

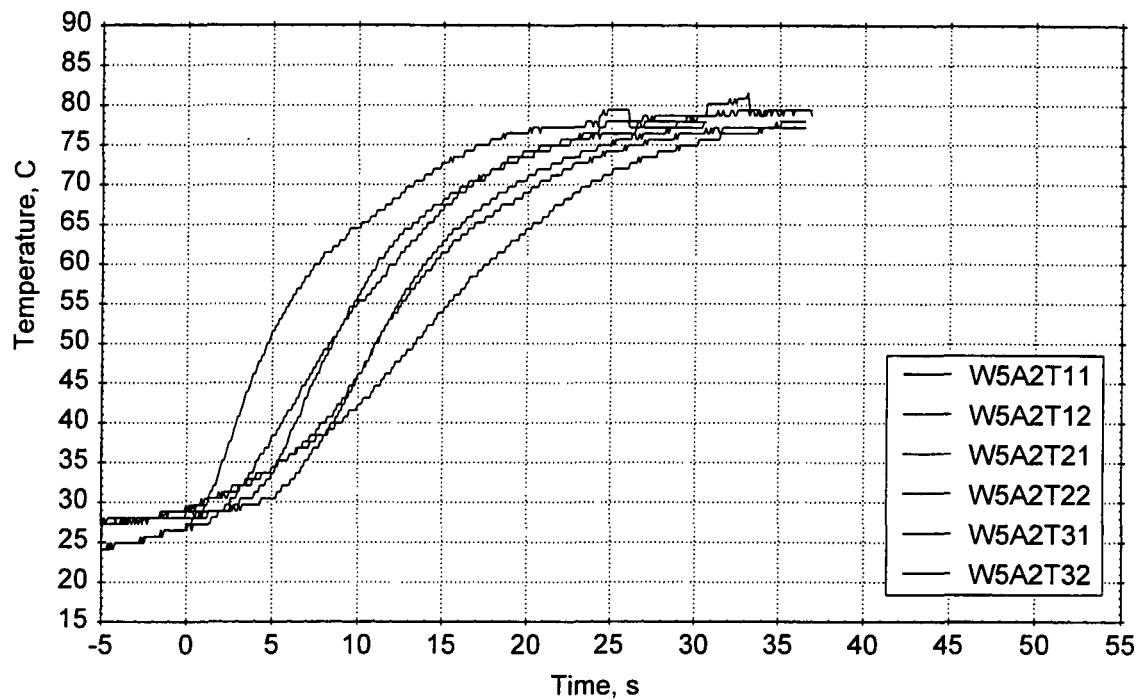


Figure E10. Furnish W5 (2P3), A platen, B felt, 42% sheet solids.

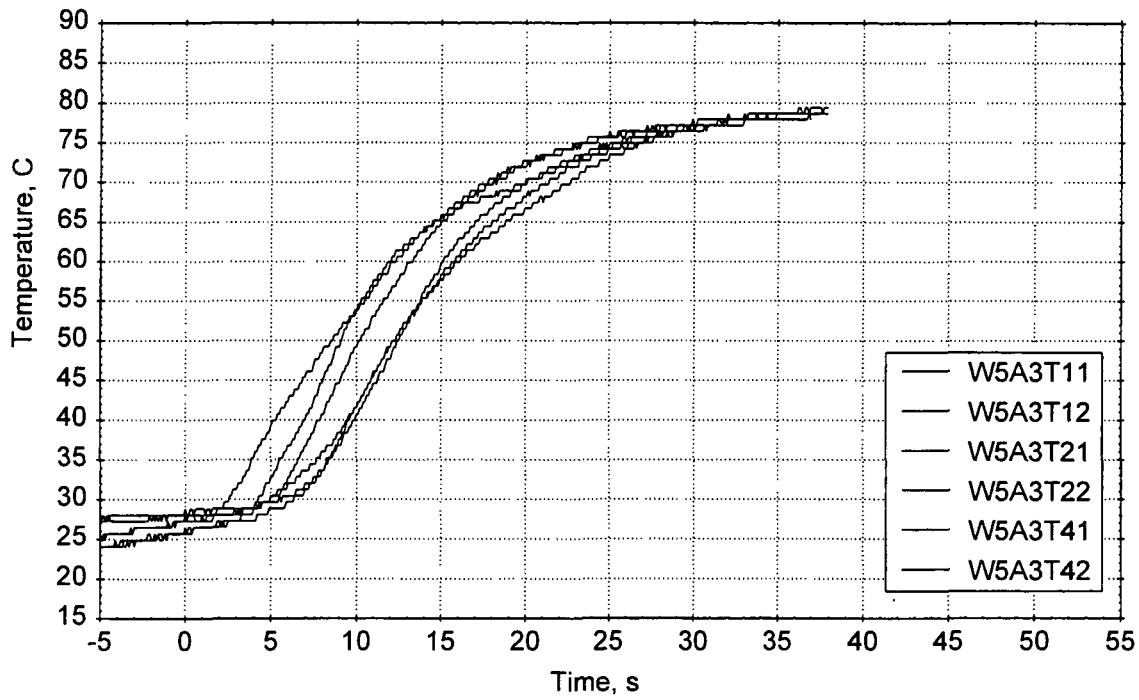


Figure E11. Furnish W5 (2P3), A platen, R felt, 35% sheet solids.

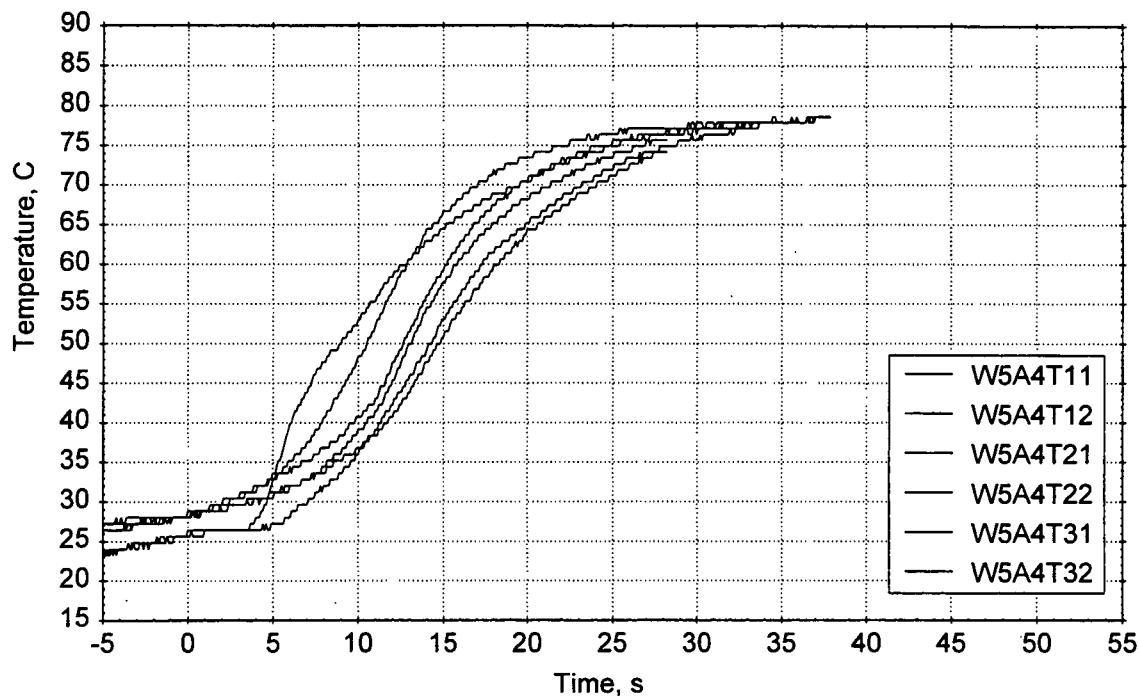


Figure E12. Furnish W5 (2P3), A platen, R felt, 42% sheet solids.

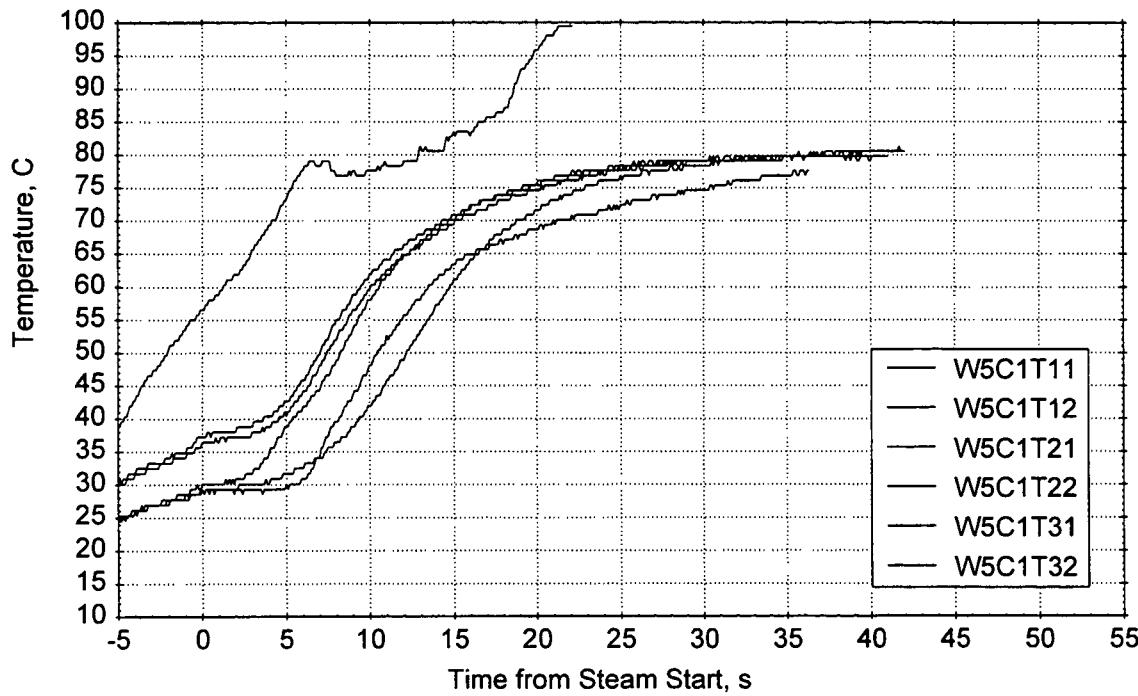


Figure E13. Furnish W5 (2P3), C platen, B felt, 35% sheet solids.

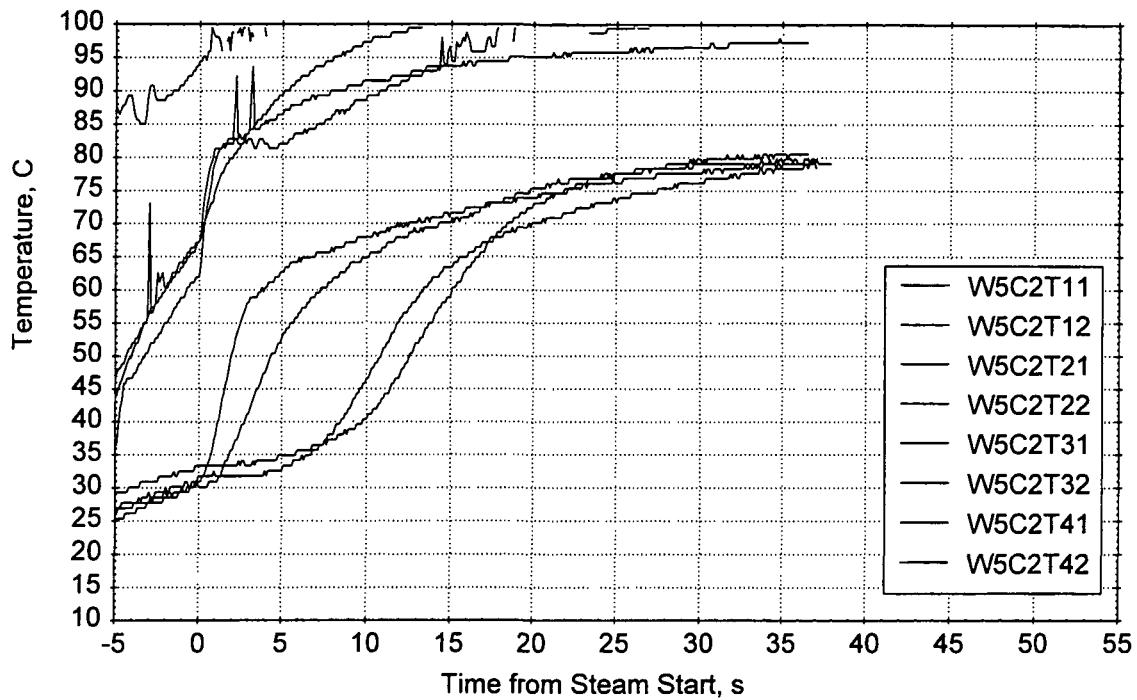


Figure E14. Furnish W5 (2P3), C platen, B felt, 42% sheet solids.

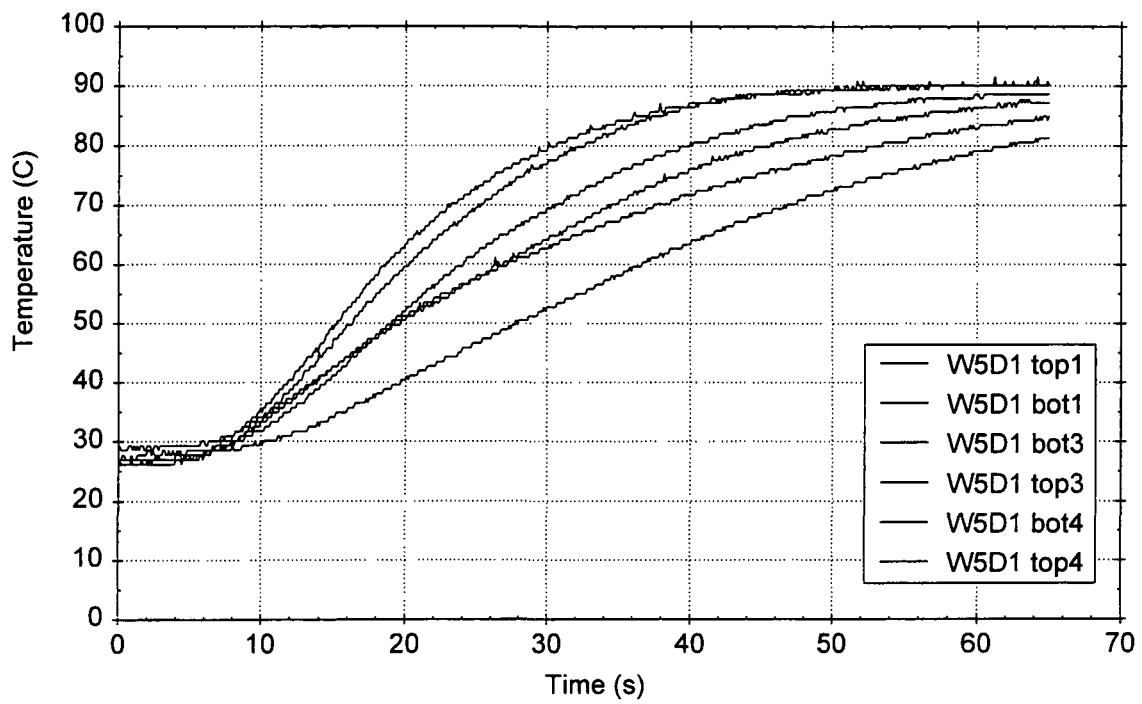


Figure E15. Furnish W5 (2P3), double-felted pressing, B felt, 35% sheet solids.

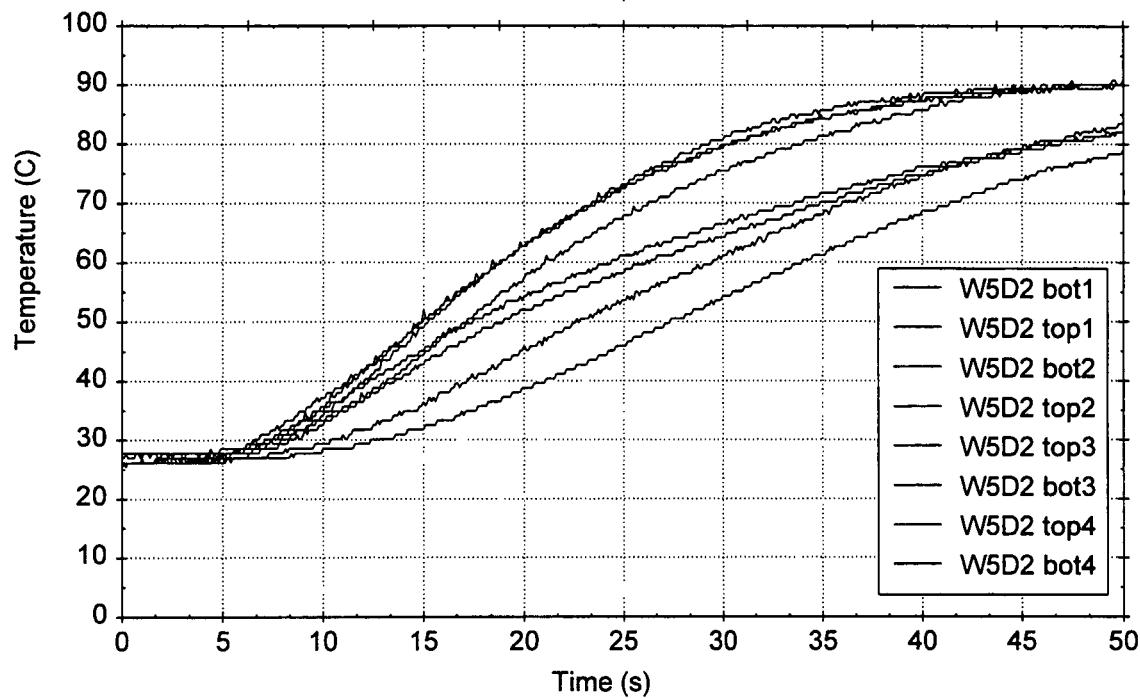


Figure E16. Furnish W5 (2P3), double-felted pressing, B felt, 42% sheet solids.

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