

## CONTINUOUS EVALUATION OF CORRUGATING MEDIUM (Data for May and dume, 1972)

Project 2694-2
Repori Thirły-Two
A Progress Report
to
FOURDRINIER KRAFT BOARD INSTITUTE, INC.
This material is intended only for the internal use of authorized persons within Fourdrinier Kraft Board Instifure member companies

July 21, 1972

THE INSTITUTE OF PAPER CHEMISTRY
Appleton, Wisconsin

```
CONTINUOUS EVALUATION OF CORRUGATING MEDIUM
(Data for May and June, 1972)
Project 2694-2
```

Report Thirty-Two
A Progress Report
to
FOURDRINIER KRAFT BOARD INSTITUTE, INC.

# This material is intended only for the internal use of authorized persons within Fourdrinier Kraft Board Institute member companies 

July 21, 1972
SUMMARY ..... 1
INTRODUCTION ..... 4
SUMMARY OF CURRENT MACHINE AVERAGES ..... 6
SUMMARY OF TEST RESULTS FOR INDIVIDUAL MACHINES ..... 8
DISCUSSION OF RESULTS ..... 23

## SUMMARY

PART I. GENERAL
A. Participation Data:

Current Period
Period
Number of machines Number of rolls

May-June, 1972 29
92

Previous Period
March-April, 1972
31
103
B. Distribution of Mediums by Type:

Semi chemical
Bogus
C. New Participants:
D. Nonparticipants:

5. Westvaco (Covington No. 7)

Page 2
Report Thirty-Two

Fourdrinier Kraft Board Institute, Inc.
Project 2694-2

PART II. QUALITY DATA
A. Summary of Physical Test Data

| Test | Report | Machine Averages |  | F.K.I. Averages |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Max. | Min. | Current | Cumulative |
| Basis weight | Cur. | 27.3 | 25.2 | 26.2 | 26.5 |
| lb./1000 ft. ${ }^{2}$ | Prev. | 28.4 | 24.8 | 26.4 | 26.6 |
| Caliper, pt. | Cur. | 10.9 | 9.0 | 10.1 | 10.1 |
|  | Prev. | 10.7 | 9.0 | 10:1 | 10.1 |
| Concora flat | Cur. | 47.0 | 32.8 | 40.7 | 41.2 |
| crush, p.s.i. | Prev. | 46.7 | 34.3 | 40.6 | 41.7 |
| Single-face flat | Cur. | 35.2 | 25.0 | 30.4 | 30.8 |
| crush, p.s.i. | Prev. | 33.2 | 25.9 | 29.5 | 31.2 |

B. Summary of Runnability Data

| Runnability |  | Current Period |  |  | Previous Period |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed, | Tension, | No. | \% of | Cum., | No. | \% of | Cum., |
| f.p.m. | lb./in. | of Rolls | Total | \% | of Rolls | Total | \% |
| $<600$ | Min. | 2 | 2.2 | 100.0 | 6 | 5.8 | 100.0 |
| 600 | Min. | 18 | 19.6 | 97.8 | 13 | 12.6 | 94.2 |
| 600 | 1/2 | 24 | 26.1 | 78.2 | 19 | 18.4 | 81.6 |
| 600 | 1 | 17 | 18.5 | 52.1 | 20 | 19.4 | 63.2 |
| 600 | 1-1/2 | 31 | 33.7 | 33.7 | 45 | 43.7 | 43.7 |

## C. Trends in Quality Data in Current Report with Reference to Data from Previous Report

Physical Tests:

Basis weight:
Caliper:
Concora flat crush:
Single-face flat crush:

Decreased from 26.4 to $26.2 \mathrm{lb} . / \mathrm{M} \mathrm{ft}.{ }^{2}$
Same as previous report
Increased from 40.6 to 40.7 p.s.i.
Increased from 29.5 to 30.4 p.s.i.

Runnability:

```
<600 f.p.m. at minimum tension:
    Decreased from 5.8 to 2.2%
    6 0 0 ~ f . p . m . ~ a t ~ m i n i m u m ~ t e n s i o n : ~
    Increased from 12.6 to 19.6%
    600 f.p.m. at l/2 lb./in. tension: Increased from l8.4 to 26.1%
    6 0 0 ~ f . p . m . ~ a t ~ l ~ l b . / i n . ~ t e n s i o n : ~ D e c r e a s e d ~ f r o m ~ 1 9 . 4 ~ t o ~ 1 8 . 5 \%
    6 0 0 ~ f . p . m . ~ a t ~ l - l / 2 ~ l b . / i n . ~ t e n s i o n : ~ D e c r e a s e d ~ f r o m ~ 4 3 . 7 ~ t o ~ 3 3 . 7 \%
```

Comments: The current runnability is slightly lower than that of the previous period.

## PART III. CONCORA CALIBRATION DATA

A. Summary of Data (Number and Percentage of Machines Included Within the Indicated Ranges)

| Range <br> $\%$ | Current Period |  |  | Previous Period |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. of <br> Machines | $\%$ of <br> Total |  | No. of <br> Machines | $\%$ of <br> Total |  |
| $\pm 1.0$ | 5 | 18.5 |  | 8 | 30.8 |
| $\pm 2.5$ | 12 | 44.4 | 15 | 57.7 |  |
| $\pm 5.0$ | 20 | 74.1 | 20 | 76.9 |  |
| $\pm 10.0$ | 26 | 96.3 | 26 | $100.0^{\mathrm{b}}$ |  |
| $\pm 20.0$ | 27 | $100.0^{\mathrm{a}}$ |  |  |  |

B. Significance of Calibration Data

The current level of agreement between Institute and mill Concora flat crush data is slightly lower than that of the previous period.

[^0]
## INTRODUCTION

As requested by the Technical Division of the Fourdrinier Kraft Board Institute, Inc., the reports pertinent to the continuous evaluation of corrugating medium have been prepared by The Institute of Paper Chemistry on a bimonthly instead of monthly basis since August, 1961. The current report summarizes the data obtained during May and June, 1972 , on 92 rolls of corrugating medium submitted for evaluation from twenty-nine machines.

Each roll was evaluated at the Institute for basis weight, caliper, Concora flat crush (tested immediately after fluting), H. and D. flat crush on single-faced board, and runnability. Runnability was evaluated by corrugating each roll under standardized conditions on the Institute's single-facer into A-flute board at 600 feet per minute with minimum tension and recording the draw factor at this speed and tension if the roll ran satisfactorily. If unsatisfactory runnability occurred at this speed and tension, the single-facer was slowed down in increments of 25 f.p.m. using minimum tension until satisfactory runnability was obtained, i.e., until there was no visual evidence of fractured flutes. In this latter case the draw factor was recorded for the highest speed below 600 f.p.m. (with minimum tension) at which the roll ran satisfactorily. On the other hand, if initial fabrication of the roll was satisfactory at 600 f.p.m. With minimum tension, further runs were made at 600 f.p.m. using higher tension to determine the maximum tension at 600 f.p.m. which the medium could sustain without visual evidence of fracturing. The higher tensions used at 600 f.p.m. were $0.5,1.0$, and $1.5 \mathrm{lb} . / \mathrm{inch}$. For each roll, flat crush was determined on the single-faced board obtained at a speed of 600 f.p.m. with minimum tension, or if the roll could not be corrugated satisfactorily at 600 f.p.m. with minimum tension, flat crush was determined on the single-faced board obtained at the highest speed below 600 f.p.m. at which the medium could be corrugated with
minimum tension. The flat crush results on the single-faced board, in addition to supplying information about quality, also provide data which may be useful to each participant as a means of evaluating the nature of the quantitative relationship between Concora flat crush and combined board flat crush for his medium.

For each participating machine, test data for the current period are shown in Table $I$. A tabulation of the number of rolls and type of medium evaluated is also given in Table $I$ for each machine. The current machine test averages given in Table $I$ are the means for each test property of the averages obtained on all rolls of corrugating medium evaluated from a given machine during the current period. In addition to the current machine test averages, Table $I$ also presents current F.K.I. averages, cumulative F.K.I. averages, and F.K.I. indexes. The current F.K.I. average for each test property is the mean of the current machine averages for the same property for all machines participating in the study during a given period. The cumulative F.K.I. average for a given test property is the mean of the current F.K.I. averages for the same property for the previous twelve-month period excluding the average for the current period. The F.K.I. index for each test property is obtained as follows:

$$
\frac{\text { current F.K.I. average }}{\text { cumulative F.K.I. average }} \times 100=\text { F.K.I. index }(\%)
$$

The F.K.I. index for each test property provides a convenient means of comparing current average quality with corresponding average quality for the previous six periods. An index greater than $100 \%$ indicates, of course, that current average quality is higher than the corresponding average quality for the previous six . periods; similarly an index below $100 \%$ indicates that current average quality is lower than the corresponding average quality for the previous six periods.




The test results obtained on the rolls submitted from the production of individual machines during the current period are shown in Tables II through XXX for Machines $A$ through $Z$ and Machines $A A, B B$, and $C C$, respectively. For each machine, the maximum, minimum, and average results obtained on each roll are shown for all test properties except basis weight for which only the average is shown; in addition, the overall average result for all rolls submitted from a given machine is shown for each test property. The latter overall averages are reported as "current machine averages." A cumulative machine average for each test property is also shown and represents the mean of the current machine averages for the same property for the previous six periods (excluding the current period). Also shown for each machine and for each test property in Tables II to XXX are a machine factor and machine index which are defined as follows:


The machine factor and machine index provide a convenient means for comparing the current machine average for each test property with either the previous results obtained on the same machine for the same test property or with the cumulative result for all machines - i.e., the cumulative F.K.I. average for the same test property.

Page 8
Report Thirty-Two
JABLE II

| SINGLE FACE FLAT CRUSH, PES.I. |  |  | RUNNABILITY |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | DRAW |
| CRI | MIN. | AV. | LB./IN.*A | FACTOR*B |
| $\begin{aligned} & 34.2 \\ & 31.0 \\ & 32.6 \end{aligned}$ | 32.6 | 33.1 | 1. 5 | 1. 574 |
|  | 30.0 | 30.5 | 0.5 | 1.558 |
|  | 31.0 | 32.1 | 0.5 | 1. 553 |
| . | . | 31.9 | . | 1. 562 |
|  |  | 32.6 |  |  |
|  |  | 97.8 |  | . |
|  |  | 103.6 |  |  |

[^1]TABLE IV
SUMMARY DF TEST RESULTS FOR MACHINE $C$
MAY AND JUNE, 1972



SUMMARY OF TEST RESULTS FOR MACHINE D

## MAY AND JUNE, 1972

TYPE OF MEDIUM- SEMICHEMICAL.
CONCORA FLAT CRUSH,
AV.

39.2
38.9

39.0
37.4
104.3
94.7

$\begin{array}{ll}\infty 0 & 0000 \\ 00 & 000 \\ -000 & 00\end{array}$
$\begin{array}{ll}11.0 & 10.1 \\ 10.9 & 10.0\end{array}$

26.3
26.3
26.3
26.2
100.4
99.2

CURRENT MACHINE AVERAGE
CUMULATIVE MACHINE AVERAGE
MACHINE FACTOR, PERCENT
MACHINE INDEX; PERCENT
*See Table II for Notes $A$ and $B$.

Page 10
Report Thirty－Two

Fourdrinier．Kraft Board．Institute，Inc．
Prọject 2694－2


NNN゚ $\begin{array}{cc}10.3 & 38.2 \\ 99.0 & 97.4 \\ 101.0 & 90.3 \\ \\ \text { TABLE VII } & \\ \\ \text { SUMMARY OF TEST RESULTS FOR MACHINE F } \\ \text { MAY AND JUNE，} 1972\end{array}$ $\begin{array}{ll}10.3 & 38.2 \\ 99.0 & 97.4 \\ 101.0 & 90.3 \\ \\ & \\ \text { TABLE VII } \\ \\ \text { MAY AND JUNE，I972 }\end{array}$

trpe of mediun semichemical

| CALIPER，PT． |  |  | CONCORA | FLAT CRUSH P．S．I． |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| max． | MIN． | AV． | max． | MIN． | AV． |
| 10.0 | 9.0 | 9.4 | 42.6 | 36.6 | 39.2 |
| 9.5 | 8.8 | 9.1 | 40.2 | 36.0 | 38.5 |
| 9.3 | 8.5 | 8.9 | 46.2 | 39.0 | 43.3 |
| 9.0 | 8.8 | 9.0 | 45.0 | 42.0 | 43.7 |
|  |  | 9.1 |  |  | 41.2 |
|  |  | 9.2 |  |  | 44.4 |
|  |  | 98.9 |  |  | 92.8 |
|  |  | 90.1 |  |  | 100.0 |



See Table II for Notes $A$ and $B$ ．
type of medium－semichemical $\begin{array}{ll}10.3 & 38.2 \\ 99.0 & 97.4 \\ 101.0 & 90.3 \\ & \\ \text { TABLE VII } \\ \\ \text { MAY AND JUNE，I972 }\end{array}$

## TABLE VI

SUMMARY OF TEST RESULTS FOR MACHINE E
MAY AND JUNE， 1972
BASIS WT．
$n$
0
ベウジウ




SUMMARY DF－TEST RESULTS FOR MACHINE H MAY AND JUNE， 1972

TYPE OF MEDIUM－SEMICHEMICAL


|  | $N \sin +$ ペ！4 NNNN |  |
| :---: | :---: | :---: |
| $\bar{x} \bar{z}$ |  | 嵌 |
|  |  | 足出乐に |
|  | ¢080 | 迷 |
|  | がond | 》 山岕 |
|  |  | $4 \geq 04$ |
| $\begin{aligned} & w \\ & \frac{w}{0} \frac{w}{2} \end{aligned}$ |  | 山士 |
|  | NNN | 20\％ |
|  | 111 | エエ¢山 |
|  |  | ¢山发号 |
|  |  | $\boldsymbol{x} \geq$ い |
|  |  | －w |
| 宮 |  |  |
|  | mNm＋ | 灾ら「 |
|  |  | 뜨늬 |
|  |  |  |
|  |  | U【I |


table $X$
SUMMARY OF TEST RESULTS FOR MACHINE I

TABLE XI

SUMMARY DF TEST RESULTS FOR MACHINE !

## MAY AND JUNE, 1972

TYPE OF MEDIUM- SEMICHEMICAL
RUNNABILITY

LB./IN. FA F'ACTOR\#B ..... | $n$ | $N$ |
| :--- | :--- |
| 0 | 0 |
| $\sim$ | 0 |
|  | 0 |

| I-1 | $4-29-72$ | 404 |
| :--- | :--- | :--- |
| $1-2$ | $5-9-72$ | 405 |
| $I-3$ | $5-23-72$ | 406 |
| $I-4$ | $6-4-72$ | 407 |
|  |  |  |
| CURRENT MACHINE AVERAGE |  |  |
| CUMULATIVE MACHINE AVERAGE |  |  |
| MACHINE FACTOR, PERCENT |  |  |
| MACHINE INDEX, PERCENT |  |  |

$$
\begin{aligned}
& 1.568 \\
& \begin{array}{l}
N O+N \\
N O M \\
N \\
N \\
N
\end{array} \\
& \begin{array}{lll}
0 & 0 & 0 \\
0 \\
0 & 0 \\
N & 0 & 0 \\
N
\end{array} \\
& \text { TYPE OF MEDIUM- SEMICHEMICAL } \\
& \begin{array}{lll}
37.2 & 32.4 & 34.7 \\
42.0 & 37.8 & 39.5 \\
35.4 & 30.6 & 33.8 \\
37.8 & 33.6 & 35.8
\end{array} \\
& \begin{array}{l}
36.0 \\
38.1 \\
94.5 \\
87.4
\end{array} \\
& \begin{array}{rrr}
10.3 & 10.0 & 10.1 \\
10.0 & 9.6 & 9.9 \\
10.2 & 10.0 & 10.0 \\
10.0 & 9.4 & 9.8
\end{array} \\
& \begin{array}{r}
10.0 \\
10.0 \\
100.0 \\
99.0
\end{array} \\
& \text { MAY AND JUNE, } 1972
\end{aligned}
$$

TABLE XII


| SINGLE-FACE FLAT CRUSH, P.S.I. |  |  | RUNNABILITY |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | DRAH |
|  | MIN. | AV. | LB.JIN.*A | FACTOR*B |
| 32.4 | 29.6 | 31.4 | 1.0 | 1. 564 |
| 30.8 | 27.6 | 29.2 | 1.0 | 1. 569 |
| 33.2 | 31.4 | 32.2 | 0.5 | 1.557 |
| 32.2 | 31.0 | 31.6 | 0.5 | 1.563 |
|  |  | 31.1 |  | 1. 563 |
|  |  | 28.5 |  |  |
|  |  | 109.1 |  |  |
|  |  | 101.0 |  |  |

> TABLE XIII
> SUMMARY OF TEST RESULTS FOR MACHINE L MAY AND JUNE, 1972


[^2]
## TABLE XIV

SUMMARY OF TEST RESULTS FOR MACHINE M
may and june, 1972

| $\begin{aligned} & \text { SINGLE-FACE FLAT } \\ & \text { CRUSH, P.S.I. } \\ & \text { MAX. MIN. AV. } \end{aligned}$ |  |  | RUNNABILITY |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | DRAW |
|  |  |  | L8./IN.*A | FACTOR*B |
| $\begin{aligned} & 32.4 \\ & 32.8 \\ & 27.2 \\ & 26.4 \end{aligned}$ | 31.2 | 31.6 | 1.5 | 1. 570 |
|  | 30.4 | 31.6 | 1. 5 | 1. 572 |
|  | 25.8 | 26.3 | 1.0 | 1. 567 |
|  | 25.6 | 26.2 | 1.0 | 1. 564 |
| 28.9 |  |  |  | 1. 568 |
| 30.6 |  |  |  |  |
| 94.4 |  |  |  |  |
| 93.8 |  |  |  |  |


MAY AND JUNE, 1972

RUNNABILITY
LB./IN.*A FACTOR*B




TYPE OF MEOIUM- SEMICHEMICAL

| CALIPER. PT. |  |  |
| :---: | :---: | :---: |
| MAX. | MIN. | AV. |
|  |  |  |
| 9.1 | 8.9 | 9.0 |
| 9.5 | 8.9 | 9.1 |
| 9.5 | 8.9 | 9.1 |
| 9.1 | 8.8 | 9.0 |
|  |  |  |
|  |  | 9.0 |
|  |  | 9.0 |
|  |  | 100.0 |
|  |  | 89.1 |

SIS WT.
LB./M.
FT.
27.0
27.1
27.1
26.8

27.0
27.2
99.3
101.9 7708


See Table II for Notes $A$ and $B$.
TABLE $X$ YI


SUMmARY OF TEST RESULTS FOR MACHINE P

$$
\text { MAY AND JUNE. } 1972
$$

trpe of medium- semichemical

Page 16
Report Thirty-Two
TABLE XVIII


TABLE XX
SUMMARY OF TEST RESULTS FOR MACHINE S


|  |  |  |  | SUMMARY |  | OF TES | RESULTS | MACHINE |  | S |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MAY AND JUNE: 1972 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | TYPE |  | OF MEDIUM- SEM |  | ICHEMI | ICAL |  |  |  |  |  |
| CODE | DATE <br> MADE | $\begin{aligned} & \text { MILL } \\ & \text { ROLL } \\ & \text { NO. } \end{aligned}$ | $\begin{gathered} \text { BASIS WT॰ } \\ \text { LB./M. } \\ \text { SQ•FT. } \end{gathered}$ |  |  |  |  |  | CRUSH. | SINGLE-FACE FLAT |  |  | RUNNABILITY |  |
|  |  |  |  | CALIPER, PT. |  |  | CONCORA | Flat | I. | CRUSH, P.S.I. |  |  | LB./IN.*A | $\begin{aligned} & \text { DRAN } \\ & \text { FACTOR*B } \end{aligned}$ |
|  |  |  |  | MAX. | MIN. | AV. | MAX. | MIN. |  |  |  |  |  |  |
| S-1 3 | 3-7-72 | 9459 | 26.0 | 11.0 | 10.2 | 10.6 | 51.0 | 40.8 | 45.4 | 33.8 | 32.6 | 33.0 | 0.5 | 1.574 |
| $S-2 \quad 3$ | 3-20-72 | 9846 | 26.0 | 11.1 | 10.7 | 11.0 | 48.6 | 43.2 | 46.3 | 32.8 | 31.4 | 32.2 | MIN. | 1.562 |
| S-3 3 | 3-26-72 | 80 | 26.6 | 11.0 | 10.3 | 10.8 | 46.8 | 36.6 | 42.0 | 31.6 | 30.0 | 30.6 | MIN. | 1.559 |
| S-4 4 | 4-6-72 | 417 | 25.7 | 11.1 | 10.5 | 10.8 | 47.4 | 42.6 | 44.9 | 32.4 | 31.0 | 31.7 | MIN. | 1.558 |
| CURRENT | MACHINE | AVERAGE | 26.1 |  |  | 10.8 |  |  | 44.6 |  |  | 31.9 | . | 1.563 |
| CUMULAT I | IVE MACH | INE AVERAGE | 26.2 |  |  | 10.2 |  |  | 45.0 |  |  | 34.1 |  |  |
| MACHINE | FACTOR. | PERCENT | 99.6 |  |  | 105.9 |  |  | 99.1 |  |  | 93.5 |  |  |
| MACHINE | INDEX, P | PERCENT | 98.5 |  |  | 106.9 |  |  | 108.2 |  |  | 103.6 |  |  |



TABLE XXI
SUMMARY OF TEST RESULTS FOR MACHINE

## MAY AND JUNE 1972

TYPE DF NEDIUM- SEMICHEMICAL

CONCORA FLAT CRUSH,
$\begin{array}{lll} & \text { P.S.I. } \\ \text { MAX. MIN. AY. } \\ & & \\ 51.0 & 43.2 & 46.7 \\ 52.2 & 43.2 & 47.4\end{array}$
47.0
47.8
98.3
114.1

CALIPER: PT.
MAX. MIN. AV.

9.1
9.2
8.9

26.5
26.6
26.9
98.9
100.4

CURRENT MACHINE AVERAGE
CUMULAT IVE MACHINE AVERAGE
MACHINE FACTOR, PERCENT
MACHINE INDEX, PERCENT
*See Table II for Notes $A$ and $B$.


Page 18
Report Thirty－Two
$\begin{array}{lr}.0 & 41.5 \\ 2 & 101.8 \\ 0 & 100.7 \\ & \\ & \\ & \\ & \\ & \end{array}$

SUMMARY OF TEST RESULTS FOR MACHINE $V$
MAY AND JUNE． 1972


TYPE OF MEDIUA SEMICHEMICAL
CONCORA FLAT CRUSH．


MAX．MIN．AV．
$\begin{array}{lll}40.2 & 34.8 & 38.4 \\ 39.6 & 34.8 & 37.7\end{array}$
－W／゚日7
－1MSISV日
SQ．FT．
26.6
27.6
27.1

N
in
Nön
No
$\begin{array}{ll}0 & 0 \\ 0 & N \\ 0 & \infty \\ m & \sim \\ m & 0\end{array}$

$\begin{array}{ll}00 & 0000 \\ 00 & 0000 \\ 0 & 00\end{array}$
CALIPER．PT．
MAX．MIN．AY．

10.0
10.1

| SINGLE－FACE FLAT CRUSH．P．S．I． MAX．MIN．AV． |  |  | $\begin{array}{r} \text { RUNNABI } \\ \text { LB./IN.*A } \end{array}$ | $\begin{aligned} & \text { LITY } \\ & \text { DRAW } \\ & \text { FACTOR*B } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| 35.4 | 33.6 | 34.5 | 0.5 | 1.575 |
| 32.6 | 29.0 | 30.9 | 1.5 | 1.571 |
| 32．2 | 31.0 | 31.6 | 1.5 | 1.563 |
| 29．8 | 28.4 | 29．0 | 1.5 | 1． 567 |
|  |  | 31.5 |  | 1． 569 |
|  |  | 31.3 |  |  |
|  |  | 100.6 |  |  |
|  |  | 102.3 |  |  | TABLE XXII

SUMMARY OF TEST RESULTS FOR MACHINE $U$
MAY AND JUNE， 1972
TYPE OF MEDIUM－SEMICHEMICAL
$\bullet_{\bullet}^{\circ} \mathrm{W} / \mathrm{IM}^{\circ} \mathrm{SISVA}$


＊See Table II for Notes $A$ and $B$.

$$
\text { SUMMARY OF TEST RESULTS FOR MACHINE } W
$$

SUMMARY OF TEST RESULTS FOR MACHINE $X$
MAY AND JUNE, 1972
hary of test results for machine $x$
may and june, 1972

## TYPE OF MEDIUM- SEMICHEAICAL



TABLE XXV concora flat crush, $\begin{array}{ccc} & \text { PAS.S.I. } \\ & \text { MIN. } & \text { AV. } \\ & & \\ 45.0 & 37.8 & 41.1 \\ 39.6 & 37.2 & 38.3\end{array}$


| CALIPER, PT. |  |  |
| :---: | :---: | :---: |
| Max. |  | AV. |
| 11.0 | 10.0 | 10. |
| 11.3 | 10.9 | 11. |

10.8
10.4
103.8
106.9

27.6
27.0

27.3
27.1
100.7
103.0

르뭉웅
$\begin{array}{ll}1-12-72 & 320-1 \\ 321-2\end{array}$
CURRENT MACHINE AVERAGE CUMULATIVE MACHINE AVERAGE MACHINE FACTOR, PERCENT
MACHINE INDEX; PERCENT

Page 20
Report Thirty-Two
TABLE XXVI
SUMMARY OF TEST RESULTS FOR MACHINE $Y$

## may and JUNE. 1972

| SINGLE-fACE FLAT CRUSH, P.S.I. |  |  | RUNNABILITY |  |
| :---: | :---: | :---: | :---: | :---: |
| MAX. | MIN. | AV. | LB./IN.*A | FACTOR*B |
| 31.2 | 28.6 | 29.8 | 1.0 | 1.568 |
| 30.2 | 28.6 | 29.3 | 0.5 | 1.560 |
| 29.0 | 28.0. | 28.6 | 1.0 | 1.565 |
| 30.2 | 28.6 | 29.4 | 1.5 | 1.565 |
|  |  | 29.3 |  | 1.565 |
|  |  | 29.4 |  |  |
|  |  | 99.6 |  |  |
|  |  | 95.1 |  |  |

18./IN.*A FACTORFB0
$n$
$n$
$n$

$n$| 4 |
| :--- |
| 4 |
|  |
|  |

22

RY OF TEST RESULTS FOR MACHINE 2
MAY AND JUNE. 1972
TYPE OF MEDIUM SEMICHEMICAL
CONGORA FLAT CRUSH,


NNNN
OON
mon
TYPE OF MEDIUM- SEMICHEMICAL CONCORA FLAT CRUSH.




BASIS HTO
LB. SQ.FT.
26.1
26.0

0
0
0
N
0
0

$$
\begin{array}{lcc} 
& & \text { MILL } \\
\text { DATE } & \text { ROLL } \\
\text { CODE } & \text { MADE } & \text { NO. } \\
& & \\
Y-1 & 5-8-72 & 4302 \\
Y-2 & 5-8-72 & 4312 \\
Y-3 & 6-7-72 & 3932 \\
Y-4 & 6-7-72 & 3942 \\
\\
\text { CURRENT MACHINE AVERAGE } \\
\text { CUMULATIVE MACHINE AVERAGE } \\
\text { MACHINE FACTOR, PERCENT } \\
\text { MACHINE INDEX, PERCENT }
\end{array}
$$

$$
\begin{aligned}
& \text { BASIS HT.O } \\
& \text { LB./M. }
\end{aligned}
$$

TABLE XXVIII
SUmmary of test results for machine an
MAY AND JUNE, 1972


> TABLE XXIX
> SUMMARY OF TEST RESULTS FOR MACHINE BB

$$
\text { MAY AND JUNE, } 1972
$$

TYPE OF MEDIUA- SEMICHEMICAL

$$
\begin{array}{ccccc}
\begin{array}{c}
\text { SINGLE-FACE FLAT } \\
\text { CRUSH, P.S.I. }
\end{array} & \text { RUNNABILITY } \\
\text { MAX. MIN. AV. } & \text { LB./IN.FA } & \text { ORAW } \\
& & & & \\
\text { FACTORFB }
\end{array}
$$

Page 22
Report Thirty-Two

Fourdrinier Kraft Board Institute, Inc. Project 2694-2
TABLE $X X X$
SUmmary of test results for maghime cc


## DISCUSSION OF RESULTS

Shown on page 2, Part II, Section "A" of the Summary are the maximum and minimum current machine averages obtained for each test property during the current period and the previous period. Also shown for each test property is the current F.K.I. average which represents the mean of the current machine averages and hence is indicative of the test level being maintained by the industry as a whole for each test property to the extent that the industry is represented by the participating machines. Also given for each test property is the cumulative F.K.I. average which represents the mean of the current $F$.K.I. averages for the previous six periods.

The runnability data for the 92 rolls evaluated during the current period and the 103 rolls evaluated during the previous period are summarized on page 2 , Part II, Section "B" of the Summary.

Supplementary to the runnability data, draw factors were determined for each roll of medium at 600 f.p.m. with minimum tension (or, for rolls with poor runnability, at the maximum speed runnable with minimum tension) and are given in Tables II through $X X X$ for Machines $A$ through $Z$ and Machines $A A, B B$, and $C C$, respectively.

In Table XXXI, an effort has been made to compare Institute and mill Concora flat crush test results for each machine for the current period. The following information is presented in this table: (I) Current machine average based on Institute data, (2) current machine average based on mill data, (3) the average difference - that is, the difference between the current machine average based on Institute data and the current machine average based on mill data, and (4) the average differences expressed as percentage differences, along with the percentage differences of the previous two-month period. In those cases where mill Concora flat crush data

A COMPARATIVE SUMMARY FOR EACH MACHINE OF THE CONCORA FLAT CRUSH AVERAGES BASED ON INSTITUTE DATA AND MILL DATA


[^3]are still obtained on specimens conditioned after fluting, no average differences between current machine averages based on Institute and mill data are shown. The inclusion of these comparisons is made possible by the fact that interested participants submit their Concord flat crush results to The Institute of Paper Chemistry (on data sheets obtainable from the Institute). This affords each participant an opportunity to review the level of agreement noted for his data with the levels noted for the other participants. Comparisons of this kind are a helpful adjunct to other calibration procedures.

R. C. McKee, Chairman

Container Section



[^0]:    ${ }^{\mathrm{a}}$ Maximum percentage difference was -18.7.
    ${ }^{\mathrm{b}}$ Maximum percentage difference was -9.2 .

[^1]:    SUMMARY OF TEST RESULTS FOR MACHINE B
    TABLE III

    $$
    \text { MAY AND JUNE, } 1972
    $$

    > TYPE OF MEDIUM- SEMICHEMICAL

    | RUNNABILITY |  |
    | :---: | :---: |
    | DRAN |  |
    | LB./IN.*A FACTOR*8 |  |
    |  |  |
    | 1.0 | 1.566 |
    | 0.5 | 1.562 |
    | 1.5 | 1.569 |
    | 1.5 | 1.565 |
    |  |  |
    |  | 1.566 |

    $$
    \begin{gathered}
    \bullet 0 N \\
    7708 \\
    7714
    \end{gathered}
    $$

    

    $$
    \begin{aligned}
    & \text { cein SISVB }
    \end{aligned}
    $$

    $$
    \begin{aligned}
    & \text { GONGORA FLAT CRUSH. }
    \end{aligned}
    $$

[^2]:    *See Table II for Notes $A$ and $B$.

[^3]:     data were submitted.
    ${ }^{b}$ Average difference is the difference between the current machine average based on Institute test results and that based on mill test results with the Institute test results used as the reference.
    ${ }^{c}$ Average difference (percent) is computed by dividing the average difference in p.s.i. by the Institute current machine average and multiplying by 100.
    No identification on rolls.

