# STUDY OF PAPER BOARD QUALITY 

 AS RELATED TO FIBER BOX PERFORMANCE
## REPORT NUMBER I

Baseline Studies 1. The Evaluation of Current Kraft Liners and Corrugating Mediums*

## REPORT TO

FOURDRINIER, KRAFT BOARD INSTITUTE, INC.

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Baseline Studies 1. The Evaluation of Current Kraft Liners and Corrugating Mediums

## REPORT TO

FOURDRINIER KRAFT BOARD INSTITUTE, INC.
Appleton, Wisconsin

THE INSTITUTE OF PAPER CHEMISTRY
OCTOBER, 1945

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## A STUDY OF PAPERBOARD QUALITY AS RELATED TO BOX PERFORMANCE

Baseline Studies. I. The Evaluation of Current Kraft Liners and Corrugating Mediums

## GENERAL INTRODUCTION

Project 1108 of The Institute of Paper Chemistry is. $a \cdot$ long range program of research and development, - which has as its objective the development of the basic information needed for improving the measurement and control of the quality of box components and box performance. It was apparent that an objective scientific approach to this problem would require the development of more adequate means of evaluating the quality of boxes and box components. In other words, it is necessary to create reliable "yardsticks" for the selection of raw materials, for the control of manufacturing and converting variables, for the facilitation of design, and for the measurement and prediction of performance.

The broad outline of procedure for the development of basic information was as follows:
I. Review of literature and previous experience
II. Review of existing test methods
III. Review of available box performance data
IV. Instrumentation or improvement of present testing methods and the development of new methods
V. Research, testing and development (including field observation of performance and analysis of field hazards) on materials and methods of fabrication related to physical properties and design of
A. Paperboard
B. Combined board
C. Boxes
VI. Interpretation and application of results

This study was undertaken in 1944 in co-operation with the Fourdrinier Kraft Board Institute, whose membership was composed of the following organizations:
The Brown Paper Mill Company, Inc.
The Chesapeake Corporation
Hummel-Ross Fibre Corporation
International Paper Company, Southern Kraft Division
National Container Corporation
St. Joe Paper Company
Union Bag \& Paper Corporation
West Virginia Pulp \& Paper Company
These mills produce a substantial percentage of the kraft liner and corrugating board made in this country.

## INTRODUCTION TO BASELINE STUDY

Essential to any long-range program of this nature is the establishment of a baseline for reference throughout the course of the study. It was decided, therefore, that an index of the quality of the current production of the co-operating mills should be established as a baseline. This baseline was to be determined as accu-
rately as was feasible within the limitations imposed by existing testing techniques and by wartime operating conditions in the paperboard-industry. The baseline study was to be undertaken as early as possible. However, some of the work under Sections I, II, III, and IV outlined above was to be pursued concurrently with the baseline study. The procedure for the establishment of the baseline was divided into two phases.

The first phase of the baseline study was concerned with the problem of sampling, in a truly impartial cross-sectional manner, the current routine production of the co-operating mills and evaluating these samples as completely as possible by means of existing board testing methods. It is with this phase of the baseline study that the present report is primarily concerned.
As it would have been almost impossible to determine the quality index for each grade currently manufactured by the various mills, it was decided to base the index on $42-\mathrm{lb}$. D.F.B.S. (dry finish both sides) kraft liner and $.009 / 26-\mathrm{lb}$. corrugating medium production.

The selection of sample rolls was to be done by representatives of The Institute of Paper Chemistry from converters' warehouse stocks, rather than at the producing mills. The producing mills had no previous knowledge or control of the time or place of sampling or of the identity or quantity of their product sampled. Samples from the selected rolls were evaluated in the laboratories of The Institute of Paper Chemistry. The rolls thus sampled were set aside for subsequent use by The Institute of Paper Chemistry in the second phase of the baseline study.

Phase two of the baseline study involved (1) the selection of the most representative rolls of each mill's sampled production, and (2) the fabrication of these representative rolls into corrugated combined boards and their conversion into boxes. The corrugating operation and the conversion into boxes were to be carried out by an impartial boxmaker under carefully controlled, but normal, conditions of manufacture and according to a predetermined schedule of component combinations. Evaluation of the combined board and boxes produced was then to be carried out at The Institute of Paper Chemistry by means of conventional board and box testing methods.

The purpose of this phase of the baseline study was threefold. First, it would provide information concerning the deviation in test values which may be obtained with a given group of component parts under closely controlled conditions of corrugating and box making. Second, it would provide a further means of comparing
the quality of board from the various mills. Third, it would provide additional data required for the establishment of the current quality index-namely, data on combined board and boxes.

In order to complete the baseline study within a reasonable period of time, it was necessary to limit the variables of combination and box design. Accordingly, it was decided that the corrugated board should be "B" flute with starch adhesive and that the combined board should be converted into R.S.C. 24 No. $2 \frac{1}{2}$ can size domestic can boxes with stitched joints.

## SUMMARY

This report covers the first phase of a baseline study which, in turn, is a part of a long-range investigation of paperboard and fiber-box performance.

The results of this phase of the study indicate that the average quality of the sampled $42-\mathrm{lb}$. D.F.B.S. Fourdrinier kraft liner and of $.009 / 26-\mathrm{lb}$. kraft and bogus corrugating mediums were as follows:

|  | Liner | Corrugating <br> Medium |
| :--- | :---: | :---: |
| Basis weight, lb./1000 sq. ft. | 42.1 | 26.8 |
| Caliper, in. | 0.015 | 0.010 |
| Apparent density, lb./cu. ft. | 33.7 | 32.3 |
| Bursting strength, points | 98 | 62 |
| G. E. puncture, units | 36 | 18 |
| Moisture, $\%$ | 8.1 | 9.4 |
| Riehle compression, lb. |  |  |
| $\quad$ In | 29.0 | 17.6 |
| Across | 22.5 | 13.0 |



Corrugati Medium

| Elmendori tear, g./sheet |  |  |
| :---: | :---: | :---: |
| In | 354 | $223{ }^{\circ}$ |
| Across | $39+$ | 251 |
| Amthor tensile, lib./in. |  |  |
| In | 77.8 | 49.5 |
| Across | 37.8 | 24.8 |
| Amthor stretch, \% |  |  |
| In | 2.1 | 1.9 |
| Across | 3.7 | 4.3 |

It should be remembered that these data are based on the actual rolls sampled and on conventional test methods.

- For those tests in-which-orientation of the specimen is specified, the approximate ratios observed in the in-machine direction and in the across-machine direction were as follows:


The ratio of the bursting strength to the G. E. puncture test on 42-lb. D.F.B.S. Fourdrinier kraft liner was of the order of 2.7:1.

The ratio was not computed for the $.009 / 26-\mathrm{lb}$. corrugating medium since the relatively high capacity of the G. E. puncture tester did not allow sufficient subdivision of the scale to permit distinguishing betweenthe low values obtained with any degree of accuracy.

## SAMPLING PROCEDURE

The materials tested were 42-lb. D.F.B.S. (dry finish both sides) Fourdrinier kraft liners and $.009 / 26-\mathrm{lb}$. kraft and bogus Fourdrinier corrugating mediums. All the component rolls from which the samples were obtained were manufactured by member mills of the Fourdrinier Kraft Board Institute. Inasmuch as some of the members of the Fourdrinier Kraft Board Institute operate more than one mill, it was decided to establish the baseline of current production by giving equal representation to each mill, rather than to each parent company, in the cross-sectional sampling. In this way, the coverage of the field was substantially complete in respect to the quality of board produced by individual mills, as well as within a given company.

The component samples were obtained by three members of the staff of 'The Institute of Paper Chemistry from full rolls selected at random in a large number of converters' warchouses. An attempt was made to secure sample rolls produced during the first quarter of 1945. Wherever possible, the production period covered by this sampling was narrow enough to be considered current, yet broad enough to eliminate the day-to-day variation in each mill's operation.

At the beginning of this program, each Fourdrinier Kraft Board Institute member submitted a complete list of customers to The Institute of Paper Chemistry. The co-operating converters were chosen by The Institute of Paper Chemistry from these customer lists, partly on the basis of geographic location and partly by the necessity of adequately sampling grades of each mill's production.

The collection of random rolls of liner and corrugating medium proved to be a difficult and laborious task. The hand-to-mouth supply of most converters, caused by the shortage of materials, made it necessary to search more widely and more diligently than had been anticipated. The sampling program was started on March 19, 1945 and completed on May 26, 1945, during which time a total of 280 rolls had been sampled and set aside in 41 converters' warehouses.

The original program called for the sampling of five rolls, selected at random, of each grade of each mill's production in each of four converters' warehouses. The samples from each of the 20 rolls per mill per grade would give a cross-sectional view of the current production for each mill for the grades selected. As may be observed from Table I, it was necessary in some cases to modify the number of rolls sampled because of the scarcity of materials. This was especially true with respect to the corrugating mediums, as additional government restrictions regarding the use of $.009 / 26-\mathrm{lb}$. kraft corrugating medium went into effect soon after this program of sampling was initiated.

TARLE 1
NUMBER OF ROLLS SELECTED PER MILL

| 42-lh. D.F.B.S. Ciner |  | .00\% $/ 26-\mathrm{lb}$. Corrugating Medium |  |
| :---: | :---: | :---: | :---: |
| Mill | Roll Samples | Mill | Roll Samples |
| A | 28 | S | 10 |
| H | 21 | T | 10 |
| C | - 15 | - -U | 21 |
| D | 21 | V | 13* |
| $1:$ | 11 | W | 1.3 |
| F | 10 | X | 14 |
| C | 15 | $Y$ | 10 |
| H | 14 | 7 | 11 |
| I | 22 |  |  |
| J | 21 |  |  |
|  | 178 |  | 102 |

Throughout the roll-sampling program, three samples were taken from each roll. These were designated by the terms right, left, and center, and corresponded to the samples taken from the two sides and center of the roll, respectively. These terms were applied to the roll in the following manner: When the observer faced the roll and the board was unwinding over the top of the roll towards the observer, the right of the roll was on the observer's right and the left on the observer's left. The side samples, rights and lefts, were taken near but always slightly removed from the edge of the roll. The complete identity of each roll was maintained throughout.

The actual sampling technique was as follows: After selecting at random a roll of the desired grade and manufacturer, the outer laps of the roll were removed to a depth of approximately one fourth of an inch until the undamaged portion of the roll was exposed. Three full laps, or their equivalent, of undamaged board were then removed the full width of the roll for test purposes. From the innermost lap selected, a strip approximately one foot long was cut the full width of the roll and three moisture samples were taken from the strip, corresponding to the right, center, and left of the roll. Each moisture sample was cut to approximately one square foot and weighed immediately to obtain the airdry weight. Each of the laps and each of the moisture samples were carefully marked with all the necessary roll identification as to the manufacturer, date manufactured, roll number, width, weight, grade, left and right side, and the name of converter in whose warehouse the rolls were sampled. The materials were carefully wrapped and shipped by Railway Express to The Institute of Paper Chemistry at Appleton, Wisconsin.
Upon their arrival at The Institute of Paper Chemistry, the laps were cut into three sample lots of at least 20 specimens each. The specimens in each sample lot were cut to approximately 1.3 by 13 inches, thoroughly shuffled, and arranged in two groups of 10 each

Dy afternate selection. Une of the groups was used for subsequent testing and the other was stored for future reference. The 10 -specimen group selected for testing was again shuffled, and arranged in two groups of five specimens cach by alternate selection. One group was used for bursting strength and G. E. puncture test and the other group was used for basis weight, caliper, tear, tensile, stretch, and Riehle compression tests.

## MATERIALS SAMPLED

As previously mentioned, the materials tested consisted of three-lots of specimens taken from the outer laps of rolls sampled in a large number of converters' warehouses. The following summarizes the samples taken:

178 rolls of $42-\mathrm{Hb}$. D.F.B.S. Fourdrinier kraft liner
89 rolls of $.009 / 26-\mathrm{lb}$. Fourdrinier kraft corrugating medium
13 rolls of $.009 / 26-\mathrm{-lb}$. Fourdrinier bogus corrugating medium
The rolls listed above were obtained from 11 different mills. Some mills manufactured both liner and corrugating, whereas others made only liner or corrugating. The breakdown of the rolls as to manufacturers and the number sampled may be seen in Table I.

A list of the converters and the number of rolls sampled in each converter's warehouse is shown in Table II. It should be mentioned that, without the converter's co-operation, this study could not have been made and we wish to acknowledge their co-operation in this work.

TABLE II
LIST OF CONVERTERS

Converter $\quad$| Number of |
| :---: |
| Rolls Sampled |

| Allcraft Corrugated Co. | Harrison, N. J. | 3 | 3 |
| :---: | :---: | :---: | :---: |
| Allied Container Corp. | Boston, Mass. | 0 | 5 |
| Atlantic Container Corp. | Long Island, $\mathrm{N} . \mathrm{Y}$. | 4 | 0 |
| Atlas Corrugated Case Co., Inc. | Brooklyn, N. Y. | 6 | 0 |
| Ball Brothers Co. | Muncie, Ind. | 5 | 0 |
| Baltimore Paper Box Co. | Baltimore, Md. | 1 | 7 |
| Bell Fibre Products Corp. | Marion, Ind. | 6 | 0 |
| Cotonial Container Corp. | Brooklyn, N. Y. | 1 | 0 |
| Crescent Box Corporation | Philadelphia, Pa . | 5 | 5 |
| Densen-Banner Co., Inc. | Ridgefield P'ark, N. J. | 6 |  |
| Downing Box Co. | Milwaukee, Wis. | 10 |  |
| Federal Container Co. | Philadelphia, I'a. | 5 |  |
| Fort Wayne Corrugated Paper Co. | Chicago, 111. | 2 |  |
| Fort Wayne Corrugated Paper Co. | Hartford City, Ind. | 0 | 5 |
| Gaylord Container Corp. | St. Louis, Mo. | 6 |  |
| Gibraltar Corrugated Paper Co., Inc. | North Bergen, N. J. | 6 |  |
| Grand-City Container Corp. | Brooklyn, N. Y. | 2 | 2 |
| Hankins Container Co. | Cleveland, Ohio | 0 | 5 |
| Hummel \& Downing Co. | Milwaukee, Wis. | 0 | 2 |
| Inland Container Corp. | Indianapolis, Ind. | 7 | 0 |
| International Paper Co. (Container Division) | Chicago, Ill. | 7 |  |
| International Paper Co. (Container Division) | Whippany, N. J. | 5 |  |
| Interstate Container Corp. | Glendale, N. $\mathbf{Y}$. | 4 | 0 |
| Jackson Box Co. | Cincinnati, Ohio | 7 | 2 |
| Keystone lox Co. | Pittsburgh, Pa . | 0 | 5 |
| F. J. Kress Box Co. | Pittsburgh, Pa . | 10 | 0 |
| Lanzit Corrugated Box Co | Chicago, III. | 3 | 3 |
| Liberty Corrugated Container |  |  |  |
| Light Corp. | Prooklyn, N. Y. Philadelphia, Pa. | 1 9 | 0 |



## TESTING PROCEDURES

As previously mentioned, three samples of at least 20 specimens each were taken from each roll selected. The identity of these three roll samples was maintained throughout the entire testing program. The final roll values are based on the averages of the three sample lots.

Prior to testing, all of these roll samples were preconditioned for at least six hours at a relative humidity of not over $35 \%$. After the designated preconditioning period, the samples were conditioned for at least 48 hours and tested in an atmosphere at $50 \pm 2 \%$ relative humidity and a temperature of $73 \pm 3.5^{\circ} \mathrm{F}$. The tests used in this phase of the work were those currently employed and recognized in the industry. The tests performed, together with the test procedures, were as follows.

## Moisture

The airdry weight was determined by the representatives of The Institute of Paper Chemistry in the various converters' warehouses wherein the rolls were sampled. A strip approximately one foot in length, the full width of the roll, was cut from the innermost lap of those obtained from each roll sampled. This crosssectional strip was then cut into three approximately square foot specimens taken at the center and near each end of the roll. which were weighed immediately. These weighed specimens were then forwarded to The Institute of Paper Chemistry where they were dried to constant weight in an oven equipped with forced circulation and maintained at a temperature of $105 \pm 2^{\circ} \mathrm{C}$. The percentage moisture for each specimen was calculated on the ovendry basis. The final moisture value for each roll was the average of the moisture values of the three specimens taken from each roll: :

## Basis Weight

The basis weight, expressed as the weight per thousand square feet, was determined by weighing five 12 by 12 -inch conditioned'specimens from each sample on a Toledo basis-weight scale.


Figure 1. Jumbo Mullen tester.

## Caliper

The thickness determinations were made with a Cady micrometer on the specimens previously used for the basis weight determination. The machine direction was noted and care was taken to measure and record the average of the values determined at three different points on a line perpendicular to the machine direction across one end of the specimen sheet. Another series of three readings, taken at the opposite end of the specimen sheet, was recorded as a second average. In this manner two values (each being the average of three readings) for each of the five specimens per sample resulted in ten recorded values, the average of which was expressed as the caliper value for that particular sample.

## Bursting Strength

Bursting strength tests were performed with a motor-driven "Jumbo" Mullen tester equipped with a 300 -pound gage and also with a special attachment for controlling the clamping pressure on the specimen. This tester is shown in Figure 1. Two test readings were obtained on each of five specimens per sample. On each specimen one test was obtained with the diaphragm pressure applied to the wire side and one test with the pressure applied to the felt side.

## G. E. Puncture Test

The G. E. puncture tests were carried out with the new model puncture tester shown in Figure 2. TAPPI Method T $803 \mathrm{~m}-44$ was followed, using the same five specimens as were used for determination of bursting strength. Two punctures, one in each direction, were made for each specimen.

## Tensile Strength and Stretch

The Amthor tensile tester was used for simultaneously indicating the tensile breaking strength and the stretch of the test specimen. This instrument, as shown in Figure 3, is of the pendulum type, having three inde-


Figure 2. General Electric puncture tester.
pendent load-indicating ranges- 0 to 15,0 to 50 , and 0 to 200 pounds. At the start of the test the distance between the edges of the jaws of the clamps was equal to 152 mm . ( 6.0 inches). The width of the test strip was 15 mm . ( 0.59 inch ). Four test strips, two in each direction, were cut from each of the five specimens previously used for basis weight and caliper determinations. The tensile breaking strength per sample was reported as the average of the individual test specimen values expressed in pounds per inch width for each direction.
The stretch value per sample was reported as the average of the individual specimen readings expressed in percentage elongation to failure, based upon an initial test strip length of six inches.

## Elmendorf Tear

The tear values were obtained using the Elmendorf paper tester shown in Figure 4. Two test strips, one with its long axis in the machine direction and the other with its long axis perpendicular to the machine direction of the sheet, were cut from the unused portion of each of the five specimens originally used for basis weight and caliper determinations. In the text,
the term "in-machine direction" tear refers to the tear value obtained when the line of tear was parallel to the machine direction of the sheet. Similarly, the "acrossmachine direction" tear refers to the tear value obtained when the line of tear was perpendicular to the machine direction of the sheet. Only one liner test strip was torn at a time and only one tear value was recorded for each test strip. It was necessary to test four of the corrugating medium test strips simultaneously in order to obtain scale readings between 20 and 60. In this latter case five tear readings were recorded for the four-strip test specimen. The average values in both directions were reported separately.

## Riehle-Compression

The compression values were obtained by the use of a Richle Bros. hydraulic compression tester as shown


Ficure 3, Amthor tensile tester.


Figure 4. Elmendorf paper tester.
in Figure 5. Two 0.5 by 2 inch strips, one in each direction, were cut from the unused portion of each of the five specimens originally used for basis weight and caliper determinations. The compression values were reported as the averages of the individual specimen readings.


Figure 5. Riehle compression tester.

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

## PROCEDURE

The tests and procedures employed throughout this evaluation study have been described in the previous section. By virtue of the fact that samples could be obtained only from near the outermost portion of each roll, they represent the evaluation of that roll only to the extent that the sampled section was representative of the entire roll and in terms of the methods employed in this evaluation.

For the purpose of comparison of the product within a given mill and also between mills, each Fourdrinier Kraft Board Institute mill making $42-\mathrm{lb}$. D.F.B.S. Fourdrinier kraft liner has been given an arbitrarily selected code letter. This code identity has been used throughout this report. The Fourdrinier Kraft Board Institute mills producing liner have been identified in this report by the letters A to J, inclusive.

To obtain a more comprehensive and reliable insight into the variation of test values of rolls within a given mill and between mills, as well as to study the uniformity of each mill's product, it was necessary to apply statistical analysis to the test results. The application of statistical methods greatly increases the reliability of any comparison, inasmuch as a measure of the significance of the results is provided:

Statistics is that branch of mathematics which has been designed for the purpose of analyzing numerical results to determine the magnitude and the pattern of one or more of the variable characteristics of the items within the "universe" or group concerned.

The theory of statistics is based on two fundamental concepts: (1) There must exist an equality of opportunity for the chance selection of each and every possible item, and (2) nature has a precise and orderly plan for variation which is revealed whenever some variable factor is measured and the items are grouped numerically in the order of increasing magnitude. In addition, it is necessary that no secondary attributes shall influence the variable under consideration.

When all the possible items in question are subject to the influence of a large number of independent and purely random causes of variation, it is found that the values of the items tend to vary around a mean or most probable value in a given manner. If the causes of variation are truly random and truly independent, it will be found that there is a most probable or mean value which is characteristic of more items than any other given value; that small deviations from this mean value are more frequent than large deviations; and that positive deviations are as frequent as negative deviations. Such a distribution may be illustrated in an experiment in which the variation in height of a number of men is measured. If a sufficient number of men
are measured and a record is kept of the distribution of the heights (the number of men in each height class), a graph of the distribution of those heights will follow the normal distribution curve as defined by the following equation:

$$
Y=\frac{N}{\sigma \sqrt{2 \pi}} \mathrm{e}^{-\frac{-\left(\frac{x-f}{} \frac{\sigma^{2}}{\sigma^{2}}\right.}{}}
$$

in which $Y=$ the number of items at a distance.$x$ from the arithmetical mean or average;
$\pi=3.1416$;
$\mathrm{c}=2.7183$-the base of the Naperian logarithms;
$\sigma=$ the standard deviation of the array, a measure of variability;
$x=$ the individual observation value;
$\bar{x}=$ the arithmetic mean for all values of $x$ i.e., the average of all individual observation values; and
$N=$ the total number of observations made.
The standard deviation is, by definition, the square root of the mean square of all the individual deviations measured from the mean of the distribution. It may be computed by the following formula:

$$
\sigma=\sqrt{\frac{\Sigma(x-\tilde{x})^{2}}{N-1}},
$$

where $\sigma=$ the standard deviation,
$\Sigma=$ the operation of summation,
$x=$ the individual observation value,
$\bar{x}=$ the mean value of the observed results, and
$N=$ the number of observations made in the group considered-i.e., the total number of $x$ values.
This can be converted, by the application of the proper algebraic operation, to the following equation:

$$
\sigma^{2}=\frac{N \Sigma x^{2}-(\Sigma x)^{2}}{N(N-1)}
$$

This latter equation was used in the computation of the standard deviation throughout this report.
The standard deviation is most readily understood if it is thought of as a measure of the degree of dispersion or variability of the items in the universe, aggregate, or population being considered.

By integration, it is possible to determine the area under any section of the distribution curve. The area between any desired limits of $x$ is to the total area under the distribution curve as the number of items between these same limits is to the total number of items. When the limits are established as one standard
deviation $( \pm \sigma)$, the limits include $68.3 \%$ of the total number of items. If two standard deviations ( $\pm 2 \sigma$ ) are used, $95.5 \%$ of the items are included, and if three standard deviations ( $\pm 3 \sigma$ ) are used, $99.7 \%$ of all the items are included.

It should be stressed that the results of the statistical evaluation of the data presented in this report are limited by the small number of rolls which were tested for each mill. It is not to be implied that an exact analysis of a mill's production, over a period of several months, can be obtained by testing only 10 to 30 rolls. However, the results illustrate the application of statistical methods, and also indicate probable trends.

If a greater number of rolls had been included for each mill; the reliability of the statistical methods would have been increased and the results would have had greater significance. As additional surveys of these mills' production are made, a comparison between studies will indicate more reliable trends and facilitate the correlation of results.

## COMPARISON OF MILL AVERAGES.

The results of the various physical tests performed on the samples of $42-\mathrm{lb}$. D.F.B.S. Fourdrinier kraft liners have been compiled in Table III on the basis of mill averages. Complete details of the individual tests of the several rolls from each mill are given in Tables LXI-LXX in the Appendix.

The average results obtained for basis weight are shown graphically in Figure 6. The group average basis weight for all the mills participating was 42.1 pounds, which is, for all practical purposes, the same as the specified grade weight. The results indicate that Mills E and I had the highest average basis weight and Mill F the lowest. The average basis weight for all the other mills did not vary from the group average by more than $\pm 1.0$ pound.

The average caliper results are plotted in Figure 7. The average caliper value obtained for the group was 0.0150 inch. A comparison of the test results indicates
that Mill $H$ had the highestand Mill F the lowest taver erage caliper. However, all the mill averages, except that for Mill $F$, were within $\pm 0.001$ inch of the group average.

The average apparent densities in pounds per cubic foot are illustrated graphically in Figure 8. The group. average apparent density was 33.7. The highest average apparent density was obtained for Mill $F$ and the lowest for Mills G and H. The average apparent density for all the other mills did not vary from the group average by more than $\pm 0.5$ pound.
--- From the-data presented in Figure 9 it may be observed that the average moisture content for the group was $8.1 \%$ on an ovendry basis. The highest average moisture content was obtained for Mill F and the lowest for Mill G. It is interesting to note that Mill F had the lowest average caliper and basis weight but the highest average apparent density and moisture content.

The results obtained for the bursting strength test are presented graphically in Figure 10. The average bursting strength, expressed in points per pound, was 2.33. The group average bursting strength was 98 points. Mills H and I exhibited the highest and Mill F the lowest average bursting strength value.

The averages obtained for the G. E. puncture test are shown in Figure 11. The group average was 36 units, with Mill I possessing the highest and Mill F the lowest average G. E. puncture value. It may be observed that, when the group average for bursting strength is compared with the group average for the G. E. puncture, the ratio is approximately 2.7 to 1 . It should be borne in mind, however, that these results were obtained on uncombined liner samples of Fourdrinier kraft board.
The average Riehle compression test results are plotted in Figure 12. The group average of the inmachine direction was 29.0 pounds and of the acrossmachine direction 22.5 pounds. The ratio of the across-machine direction values to the in-machine direc-

TABLE III
COMPARISON OF PHYSICAI, CHARACTERISTICS BETWEEN MILLS

| Liner |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { Iasis } \\ \text { Weight, } \\ \text { lb. } \\ (12 \mathrm{x} \\ 12 / 1000) \end{gathered}$ | $\begin{gathered} \text { Caliper, } \\ 0.001 \\ \text { in. } \end{gathered}$ |  | Moisture, \% | BurstingStrength (Mullen), points | G.F. Puncture, units | $\begin{aligned} & \text { Riehle } \\ & \text { Compression, } \\ & \text { lb. } \end{aligned}$ |  | lilmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor <br> Stretch, \% |  |
| Mill | Tested |  |  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| $\wedge$ | 28 | 41.1 | 14.8 | 33.2 | 9.1 | 99 | 35 | 28.5 | 22.1 | 34.3 | 391 | 78.5 | 36.2 | 2.2 | 3.4 |
| ${ }^{13}$ | 21 | 42.9 | 15.4 | 33.4 | 8.7 | 101 | 37 | 30.6 | 23.7 | 353 | 397 | 84.1 | 38.1 | 2.2 | 3.8 |
| C | 15 | 42.7 | 14.5 . | 35.3 | 7.1 | 100 | 39 | 29.8 | 22.2 | 364 | 405 | 85.9 | 38.9 | 1.9 | 4.1 |
| D | 21 | 41.7 | 14.8 | 33.8 | 7.4 | 98 | 36 | 28.1 | 22.5 | 360 | 378 | 70.4 | 39.5 | 2.0 | 3.5 |
| E | 11 | 43.4 | 15.7 | 33.2 | 7.5 | $91^{\circ}$ | 35 | 27.5 | 20.6 | 324 | 365 | 77.1 | 34.3 | 1.8 | 3.6 |
| F | 10 | 39.7 | 13.4 | 35.6 | 10.0 | 85 | 33 | 23.3 | 18.7 | 302 | 343 | 66.7 | 33.0 | 1.9 | 3.1 |
| G | 15 | 41.9 | 15.6 | 32.2 | 7.0 | 91 | 38 | 27.4 | 23.7 | 380 | 405 | 72.3 | 41.8 | 1.7 | 3.6 |
| H | 14 | 42.6 | 15.9 | 322 | 8.0 | 108 | 37 | 30.7 | 24.5 | 386 | 407 | 75.8 | 42.7 | 2.2 | 4.1 |
| I | 22 | 43.5 | 15.3 | 34.2 | 8.4 | 109 | 41 | 30.9 | 21.8 | 408 | 465 | 85.4 | 36.8 | 2.3 | 4.5 |
| J | 21 | 41.7 | 14.7 | 34.2 | 7.7 | 93 | 32 | 30.4 | 23.7 | 301 | 355 | 74.8 | 35.9 | 2.0 | 3.2 |
| Average | e 178 | 42.1 | 15.0 | 33.7 | 8.1 | 98 | 36 | 29.0 | 22.5 | 354 | 394 | 77.8 | 37.8 | 2.1 | 3.7 |



Figure 6. Comparison of the average basis weight of 42-lb. Fourdrinier kraft liner among mills.


Figure 7. Comparison of the average caliper of 42-1b. Fourde nier kraft liner among mills.


Figure 8. Comparison of the average apparent density of $42-\mathrm{lb}$. Fourdrinier kraft liner among mills.


Figure 9. Comparison of the average moisture content of 42 lb . Fourdrinier kraft liner among.mills.


Figure 10. Comparison of the average bursting strength of 42-lb. Fourdrinier kraft liner among mills.


Figure 11. Comparison of the average General Electric puncture test of 42-lb. Fourdrinier kraft liner among mills.


Figure 12. Comparison of the average Riehle compression test of 42 -lb. Fourdrinier kraft liner among mills.


Figure 13. Comparison of the average Elmendorf tear of $42-\mathrm{lb}$. Fourdrinier kraft liner among mills.


Figure 14. Comparison of the average of Amthor tensile strength $42-\mathrm{lb}$. Fourdrinier kraft liner among mills.


Figure 15. Comparison of the average Amthor stretch of $42-\mathrm{lb}$. Fourdrinier kraft liner among mills.
tion valucs is of the magnotude of oit. the average results obtained, in both directions, for Mill le were the lowest of all the mills participating; also, the average Riehle compression for the in-machine direction for Mill F was of approximately the same order of magnitude as the group average for the across-machine direction:

The results of the Elmendorf tear test are graphically presented in Figure 13. The group average test results were 354 and 394 grams per sheet for the inmachine and across-machine directions, respectively. The ratio of the group average of the in-machine direction to the group average of the across-machine-direction is of the order of $0.9: 1$. Mills $F$ and $J$ had the lowest and Mill I the highest tear values in both directions.

The results of the Amthor tensile test are shown in Figure 14. A comparison of the results indicates that the ratio of the across-machine direction values to the in-machine direction values is of the order of $1: 2$. The group averages obtained were 77.8 and 37.8 pounds per inch width for the in- and across-machine directions, respectively. The averages for Mill $F$ were the lowest in both directions and the averages for Mill $E$ and I were the highest in the in-machine direction; however, Mills G and H were the highest in the acrossmachine direction.

The Amthor stretch results are presented in Figure 15. The group averages obtained were 2.1 and $3.7 \%$, respectively, for in- and across-machine directions. The ratio of the in-machine direction values to the across-machine direction values is approximately 6:10.

A comparison of the averages of all the strength test results indicates that Mills H and I were the highest and Mill $F$ the lowest. The averages for the group would result in a theoretical liner having the following characteristics:

| Basis weight, lb .Caliper, in. | 42.1 |
| :---: | :---: |
|  | 0.015 |
| Apparent density, lb./cu. ft . | 33.7 |
| Bursting strength, points | 98 |
|  | 36 |
| Moisture content, $\%$  <br> Riehle compression, fb . 8.1 |  |
|  |  |
| In | 29.0 |
| Across | 22.5 |
| Elmendori tear, g./sheet |  |
| In | 354 |
| Across | 394 |
| Amthor tensile, lb./in. |  |
| In | 77.8 |
| Across | 37.8 |
| Amthor stretch, \% |  |
| In | 2.1 |
| Across | 3.7 |

A comparison of the standard deviations of the mills for each test characteristic is given in Table IV. It may be noted from the results for each test characteristic that the basis weight and caliper have the lowest percentage standard deviation and the Amthor stretch the highest. The lower the percentage standard deviation, the less is the indicated variation in that particular characteristic.

In a study of this type it is often of value to know
now wheaveragequanty or portomat compares with the average quality of the same grade of board produced by other mills. With the above thought in mind, the results tabulated in Table III were treated statistically to determine if there were any significant differences in the physical characteristics obtained for one mill as compared with the average physical characteristics for the balance of the mills participating. Whether or not significant differences exist in the same test characteristic between two different groups of data can be determined by calculating the ratio of the difference of the means of each group to the-standard error- of the difference between the . same two groups.

The standard error of the difference can be readily calculated from the standard errors of the two means ${ }^{-}$ under comparison. These standard errors, in turn, can be calculated from the standard deviations listed in Table IV. The following equations are used for these calculations:

$$
\mathrm{S}: \mathrm{E} .=\frac{\sigma}{\sqrt{N}} \quad \text { or } \quad[\mathrm{S} . \mathrm{E} .]^{2}=\frac{\sigma^{2}}{N}
$$

where S. E. = standard error,
$\sigma=$ standard deviation, and
$N=$ number of items in array.

$$
[\mathrm{S} . \mathrm{E} .]_{\alpha}{ }^{2}=\frac{[\mathrm{S} . \mathrm{E} .]_{\mathrm{A}}{ }^{2}+[\mathrm{S} . \mathrm{E} .]_{\mathrm{B}}{ }^{2}+\cdots+[\mathrm{S} . \mathrm{E} .]_{\mathrm{X}}{ }^{2}}{n^{2}}
$$

where $[\mathrm{S} . \mathrm{E} .]_{\alpha}=$ standard error of a group of similar arrays, $n=$ number of arrays being considered, and $\mathrm{A}, \mathrm{B}, \cdots, \mathrm{X}=$ respective arrays under consideration. Therefore,

$$
[\mathrm{S} . \mathrm{E} .]_{\alpha}^{2}=\frac{\frac{\sigma_{\mathrm{A}}^{2}}{N_{A}}+\frac{\sigma_{\mathrm{B}}^{2}}{N_{\mathrm{B}}}+\cdots+\frac{\sigma_{\mathrm{X}}^{2}}{N_{\mathrm{X}}}}{n^{2}}
$$

$$
\left[\text { S. E. }\left.\right|_{\text {niff. }}=\sqrt{[\text { S.E. }]_{1}^{2}+[\text { S.E. }]_{2}^{2}}\right.
$$

where $[S . E .]_{\text {Diff. }}=$ standard error of the difference, and
$[\mathrm{S} . \mathrm{E} .]_{1}$ and $[\mathrm{S} . \mathrm{E} .]_{2}=$ standard errors of the items or groups of items being considcred.
These calculations are illustrated by comparing the basis weight of Mill A with that of the other mills as a group in the following manner. First, it is necessary to determine the difference of the means-i.e., the average basis weight for Mill A minus the average basis weight for Mills $B$ to $J$, inclusive. The average basis weight for Mill A was 41.1 pounds and the average for the group was 42.2 pounds. Thus, the difference of the means is -1.1 pounds, the value being negative, inasmuch as we are comparing Mill A with the group average which, in this case, is of greater magnitude.


The square of the standard error of Mill A is calculated from formula (1):

$$
\begin{equation*}
[\text { S. E. }]_{\Lambda}^{2}=\frac{\sigma_{A}^{2}}{N_{\Lambda}} \tag{1}
\end{equation*}
$$

From Table IV, $\sigma_{\mathrm{A}}$ is 1.13 and from Table III, $N_{\mathrm{A}}$ is 28; therefore,

$$
[\text { S. E. }]_{A}^{2}=(1.13)^{2} / 28 \text { or } 0.0456 \text {. }
$$

The squared form is used because it can be substituted directly into formula (3).
The standard error of the group composed of Mill B through Mill J, inclusive, is calculated by the use of formula (2):

$$
\begin{equation*}
[\mathrm{S} . \mathrm{E} .]_{a}^{2}=\frac{\frac{\sigma_{\mathrm{B}}^{2}}{N_{\mathrm{B}}}+\frac{\sigma_{\mathrm{C}}^{2}}{N_{\mathrm{C}}}+\cdots+\frac{\sigma_{\mathrm{J}}^{2}}{N_{\mathrm{J}}}}{n^{2}} . \tag{2}
\end{equation*}
$$

Substituting the appropriate values from Tables III and IV,
$[\text { S. E. }]_{a}^{2}=\frac{\frac{(1.31)^{2}}{21}+\frac{(0.785)^{2}}{15}+\cdots+\frac{(0.845)^{2}}{21}}{(9)^{2}}=0.0093$.
Since

$$
\begin{equation*}
[\mathrm{S} . \mathrm{E} .]_{\mathrm{Diff} .}=\sqrt{[\mathrm{S} . \mathrm{E} .]_{\mathrm{A}}^{2}+[\mathrm{S} . \mathrm{E} .]_{\alpha}^{2}}, \tag{3}
\end{equation*}
$$

therefore,

$$
[\mathrm{S} . \mathrm{E} .]_{\text {Diff. }}=\sqrt{(0.0456)^{2}+(0.0093)^{2}}=0.23 .
$$

From these values, the ratio of the difference of means to [S. E.] $]_{\text {Diff }}$ is:

$$
\text { Ratio }=\frac{\text { Difference of means }}{[\text { S. E. }]_{\text {Diff. }}}=\frac{-1.1}{0.23}=-4.8 .
$$

Throughout this study, it is considered that, if the magnitude of this ratio (i.e., difference of
means/[S. E.] $]_{\text {Diff. }}$. is less than 2, no significant difference exists. Reference to the appropriate table (normal variability) shows that a ratio of 2.0 indicates that there is a significant difference $95 \%$ of the time or that the probability that the difference happened by chance is $1: 19$. When the ratio is equal to 3.0 , the chance probability is greatly decreased (i.e., to about $1: 200$ ). Thus the ratio of -4.8 , obtained for the comparison of the average basis weight of Mill A with the average of the group B to J, inclusive, indicates that there is a significant difference between the average value obtained for A and the average obtained for the group $B$ to $J$, inclusive. Since the ratio is negative, it is known at once that the average value obtained for Mill A is lower than the group average.

Similarly, all the test results obtained for Mill A were compared with the group averages obtained for the group B to J, inclusive. These results are given in Table V. The results indicate that there was a significant difference in the values obtained except for bursting strength, Richle compression in both directions, Amthor tensile in the in-machine direction, and Elmendorf tear and Amthor stretch in the across-machine direction. Similarly, all the tests, in which a significant difference was indicated, were of a lower magnitude for Mill A than for the group averages obtained for Mills B to J, inclusive, except Amthor stretch in the inmachinc direction, which was slightly higher than the group average.
The results obtained when the averages for Mill B are compared with those of the balance of the group may be seen in Table VI. The results indicate that there was a significant difference in all the values obtained except G. E. puncture, Elmendorf tear in both directions, and Amthor tensile and stretch in the across-machine direction. Similarly, the values for those tests in which a significant difference was indicated were of greater magnitude than the averages obtained for the group.
A comparison of the average values obtained for

COMPARISON OF THE PHYSICAL. CHARACTERISTICS OF MILL A WITH THE B.MANCE OF THE"CROUP.
Liner

|  | Basis Weight, lb,$\begin{gathered} (12 \times 12 \\ / 1000) \end{gathered}$ | Caliper, 0.001 ln . | Burst--..- ing Strength, points | GE. <br> Puncture, units | Riehle Compression, . .. lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | ln | Across | In | Across | ln | Across |  |
| Mean of $A$ | 41.1 | 14.8 | 99 | 35 | 28.5 | 22.1 | 343 | 391 | 78.5 | 36.2 | 2.2 | 3.4 |  |
| Mean of $\alpha$ | 42.2 | 15.0 | 97 | 36 | 28.7 | 22.0 | 353 | 391 | 76.9 | 37.9 | 2.0 | 3.7 |  |
| Difference of means $(A-\alpha)$ | -1.1 | $-0.18$ | $+1.8$ | -1.72 | -0.184 | +0.151 | $-10.2$ | $-0.3$ | +1.55 | -1.64 | $+1.627$ | $-0.3171$ |  |
| Standard error of ${ }^{-}$ difference | 0.23 | 0.028 | $1.47$ | $\overline{0.481}$ | $\overline{0.352}$ | 0.248 | 4.83 | 4.40 | $\because 1.13$ | 0.414 | 0.056 | 0.220 | - - |
| Ratio: $(A-\alpha) / S E_{i}$, | -4.8 | $-6.5$ | $+1.2$ | -3.6 | -0.5 | +0.6 | -2.1 | -0.1 | +1.4 | -4.0 | +2.9 | $+1.4$ |  |
| -Significant : + | Yes. | Yes | - No | Yes . | - No. | . No | Yes. | - No | No | Yes | Yes | No |  |

Note. All mean values have been reported to the same precision as the individual test values. It will be observed that some of the intermediate values in the above table have been reported to more places than the mean values. Similarly, the difference of the means will not always correspond to the difference between the reported means, because these values have been rounded off. The mean of $\alpha$ is the mean for the balance of the group.

TABLE VI
COMPARISON OF THE PHYSICAI, CHARACTERISTICS OF MILL B WITH THE BALANCE OF THE GROUP

|  | Basis Weight, lb. $(12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E. <br> Puncture, units | Riehle Compression, lb. |  | Elmendorf <br> Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | In | Across | In | Acress | In | Across | In | Across |
| Mean of $B$ | 42.9 | 15.4 | 101 | 37 | 30.6 | 23.7 | 353 | 397 | 84.1 | 38.1 | 2.2 | 3.8 |
| Mean of $\boldsymbol{\alpha}$ | 42.0 | 15.0 | 97 | 36 | 28.5 | 21.8 | 352 | 390 | 76.3 | 37.7 | 2.0 | 3.7 |
| Difference of means $(B-\alpha)$ | +0.9 | +0.45 | +3.9 | +0.79 | +2.09 | +1.89 | +1.2 | $+6.9$ | +7.74 | +0.43 | +0.23 | +0.143 |
| Standard error of difference | 0.19 | 0.173 | 1.64 | 0.52 | 0.476 | 0.294 | 7.53 | 5.42 | 1.49 | 0.692 | 0.045 | 0.107 |
| Ratio: $(B-\alpha) / S E_{D}$ | +4.7 | +2.6 | $+2.4$ | +1.5 | +4.4 | $+6.4$ | $+0.2$ | +1.3 | $+5.2$ | +0.6 | +5.1 | +1.3 |
| Significant | Yes | Yes | Yes | No | Yes | - Yes | No | No | Yes | No | Yes | No |

TABLE: VII
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL C WITH THE BALANCE OF THE GROUP
IINER

|  | Basis Weight, lb. $(12 \times 12$ /1000) | $\quad$Burst- <br> ingCaliper, Strength,0.001 in. points |  | G.E. <br> Puncture, units | Riehle Compression, lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile $\mathrm{lb} . / \mathrm{in}$. |  | Amthor . Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $C$ | 42.7 | 14.5 | 100 |  | 39 | 29.8 | 22.2 | 364 | 405 | 85.9 | 38.9 | 1.9 | 4.1 |
| Mean of $\alpha$ | 42.1 | 15.1 | 97 | 36 | 28.6 | 22.4 | 351 | 390 | 76.1 | 37.6 | 2.0 | 3.6 |
| Difference of means $(C-\alpha)$ | +0.6 | -0.55 | +2.9 | $+3.05$ | $+1.27$ | $-3: 85$ | $+13.1$ | $+15.0$ | $+9.78$ | +1.29 | $-0.172$ | +0.43 |
| Standard error of difference | 0.22 | 0.150 | 1.63 | 0.601 | 0:443 | 0.396 | 4.54 | 7.57 | 1.26 | 0.888 | 0.059 | 0.156 |
| Ratio: $(C-\alpha) / S E_{D}$ | $+2.7^{\circ}$ | -3.7 | +1.8 | $+5.1$ | $+2.9$ | -4.7 | $+2.9$ | +2.0 | +7.8 | $+1.5$ | -2.9 | $+2.8$ |
| Significant . | Yes | Yes | No | Yes | Y'es | Yes | Yes | Yes | Yes | No | Yes | Yes |

TXBI,E VII
$\therefore x^{\prime \prime}$ :
COMHARISON OF THE PHYSICAL CHARACTERISTICS OF MILA, D WITH THE BALANCE OF THE GROUP
Liner

|  | BasisWeight,ib.$(12 \times 12$$(1000)$ | Caliper, 0.001 in. | Bursting Strength, points | Gr.E. <br> Punc- <br> ture, units | Richle Compression, (b). |  | Elmendorf 'Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\cdots$ |  |  |  |  | In | Across | $\cdots$ In | Across | Itı | $\cdots$ | In | Across |
| Mean of $D$ | 41.7 | 14.8 | 98 | 36 | 28.1 | 22.5 | 360 | 378 | 70.4 | 39.5 | 2.0 | 3.5 |
| Mean of $\alpha$ | 42.2 | 15.0 | 97 | 36 | 28.8 | 21.9 | 351 | 393 | 77.8 | 37.5 | 2.0 | 3.7 |
| Difference of means $(D-\alpha)$ | -0.5 | -0.21 | $+0.7$ | $-0.53$ | -0.73 | +0.543 | +8.8 | $-14.3$ | -7.41 | +1.93 | $-0.077$ | -0.19 |
| Standard'error of difference | 0.36 | -0.239 | 1.66 | . 0.820. | 0.457 | 0.296 | -. 3.24 | $\therefore 6.81$ | 1.15 | 0.726 | 0.055 | $0.105-$ |
| Ratio: $(l)-\alpha) / S E_{l}$, | -1.4 | -0.9 | +0.4 | -0.6 | -1.6 | +1.8 | $+2.7$ | -2.1 | -6.4 | $+2.7$ | -1.4 | $-1.8$ |
| Significant | No | No | No | No | No | No | Yes | Yes | Yes | Yes | No | No |

Note. See Note to Table V. ... -

TABLE IX
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL E WITH THE BALANCE OF THE GROUP


Note. See Note to Table V.

TABLE X
COMI'ARISON OF THE IPHYSICAL CHARACTERISTICS OF MILI F WITH THE BALANCE OF THE GROUP


Comparison of time physical characteristics of mitl g with tife balance of the quoup


Note. See Note to Table V.

TABLE XII
COMPARISON OF.THE PHYSICAL CHARACTERISTICS OF MILL H WITH THE BALANCE OF THE GROUP

| : | Basis Weight, , Ib. $(12 \times 12$ /1000) | Liner |  |  |  |  |  |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Caliper, $\begin{gathered}\text { Burst- } \\ \text { ing } \\ 0.001 \text { in. } \\ \text { pointsth }\end{gathered}$ |  | G.E. <br> I'uncture, units | $\begin{gathered} \text { Riehle } \\ \text { Compression, } \\ \text { lb. } \end{gathered}$ |  | Elmendorf <br> Tear, <br> g./sheet |  |  |  |  |  |
|  |  |  |  | In | Across | In | Across | In | Across. | In | Across |
| Mean of 11 | 42.6 | 15.9 | 108 |  | 37 | 30.7 | 245 | 386 | 407 | 75.8 | 42.7 | 2.2 | 4.1 |
| Mean of $\alpha$ | 42.1 | 14.9 | 96 | 36 | 28.5 | 21.7 | 389 | 349 | 77.2 | 37.2 | 2.0 | 3.6 |
| Difference of means ( $H-\alpha$ ) | +0.5 | +0.96 | +11.3 | +1.22 | +2.17 | +2.85 | +17.8 | +37.5 | -1.40 | +5.51 | $+0.238$ | +0.421 |
| Standard error of difference | 0.27 | 0.123 | 1.61 | 0.661 | 0.511 | 0.304 | 6.06 | 10.86 | 1.81 | 1.114 | 0.052 | 0.092 |
| Ratio: ( $I I-\alpha$ )/SE ${ }_{D}$ | +1.9 | +7.8 | +9.3 | +1.8 | +4.2 | +9.4 | +2.9 | +3.5 | -0.8 | $+4.9$ | +4.6 | +4.6 |
| Significant - | No | Yes | Yes | No | Yes | Yes | Yes | Yes | No | Yes | Yes | Yes |

Note. See Note to Table V.

Table XIII
COMPARISON OF THE PHYSICAL Characteristics of mill i with the balance of the group

|  | Basis Weight, Ib. $(12 \times 12$ /1000) | Caliper, 0.001 in | Bursting Strength points | G.E. <br> Puncture. units | Linfer |  |  |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Richle Compression, lb. |  | Elmendorf Tear, g./sheet |  |  |  |  |  |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $I$ | 43.5 | 15.3 | 109 | 41 | 30.9 | 21.8 | 465 | 408 | 85.4 | 36.8 | 2.3 | 4.5 |
| Mean of $\alpha$ | 42.0 | 15.0 | 96 | 36 | 28.5 | 22.0 | 346 | 384 | 76.2 | 37.8 | 2.0 | 3.6 |
| Difference of mean $(1-\alpha)$ | $+1.5$ | +032 | $+12.7$ | +5.39 | $+2.39$ | -0.258 | +62.3 | +82.3 | $+9.23$ | -1.02 | +0.269 | $+0.90$ |
| Standard error of difference | 0.21 | 0.085 | 1.36 | 0.413 | 0.493 | 0.291 | 4.22 | 4.84 | 0.97 | 0.358 | 0.042 | 0675 |
| Ratio: $(I-\alpha) / S E_{L}$ | $+7.1$ | +3.8 | $+9.3+$ | +13.1 | +4.8 | -0.9 | +14.8 | $+17.0$ | +9.5 | -2.8 | +6.4 | +12.0 |
| Significant | Yes | Yes | Yes | Yes | Yes | No | Yes | Yes | Yes | Yes | Yes | Yes |

Note. See Note to Table V.

| - - - | Basis Weight, lb. $(12 \times 12$ /1000) | Bursting Caliper, Strength, 0.001 in. points |  | G.E. . <br> Puncture, units | Riehle Compression, ib. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $J$ | 41.7 | 14.7 | 93 |  | 32 | 30.4 | 23.7 | 301 | 355 | 74.8 | 35.9 | 2.0 | 3.2 |
| Mean of $\alpha$ | 42.2 | 15.1 | 98 | 37 | 28.5 | 21.8 | 358 | 395 | 77.4 | 37.9 | 2.0 | 3.7 |
| Difference of mean $(I-\alpha)$ | -0.5 | -0. 38 | -5.3 | $-4.23$ | $+1.91$ | +1.91 | $-56.7$ | -40.6 | $-2.53$ | -2.02 | +0.029 | -0.56 |
| Standard error of difference | 0.21 | 0.129 | 2.68 | 0.846 | 0.352 | 0.233 | 8.44 | 9.56 | 2.15 | 0.540 | 0.048 | 0.153 |
| Ratio. ( $/-\alpha$ )/ $/ E_{f}$ ) | -2.4 | $-2.9$ | -2.0 | $-5.0$ | +5.4 | +8.2 | -6.7 | -4.2 | $-1.2$ | $-3.7$ | +0.6 | -3.6 |
| Significant | Yes- | - Yes | ${ }^{-}$Yes | Yes ${ }^{-}$ | - Yes | ${ }^{-}$Y'es | - Yes | - Yes | $\cdots \mathrm{No}$ | Yes | $\cdots \mathrm{No}$ | - Yes |

Note. See Note to Table V.

Mill C with the group average excluding C is presented in Table VII. The results indicate that there was a significant difference in all the test values except bursting strength and the Amthor tensile test in the across-machine direction. All the values in which a significant difference existed were greater than the value for the group averages with the exception of caliper, Riehle compression in the across-machine direction, and Amthor stretch in the in-machine direction.

The average test results obtained for Mill D, as compared with the average test results obtained for the remainder of the group, are given in Table VIII. The only test results which exhibited a significant difference were Elmendorf tear and Amthor tensile in both directions. This phenomenon indicates that the average quality of Mill D, as determined by these tests, was approximately the same as the average quality for the group.

A comparison of the average test values obtained for Mill E with the averages for the balance of the group may be observed in Table IX. The results indicate that a significant difference existed in all the test results except those for bursting strength, G. E. puncture, Riehle compression and Amthor tensile in the in-machine direction, and Amthor stretch in the across-machine direction. With the exception of the average caliper value, all the results wherein a significant difference existed were lower than the corresponding value for the group average.

The results of the comparison of the average test values obtained for Mill $F$ with the averages for the balance of the group may be found in Table X. The results indicate that a significant difference existed between all the average test results obtained for Mill F and the corresponding group average. All the average test values obtained for F were lower than the corresponding group average.

The comparison of the average test values obtained for Mill $G$ with the averages for the balance of the group is given in Table XI. It may be noted that the only test results in which a significant difference was
not indicated were in basis weight and Amthor stretch in the across-machine direction.
The average test values obtained for Mill H are compared with the average for the remainder of the group in Table XII. It. may be noted that basis weight, G. E. puncture, and Amthor tensile in the inmachine direction were the only test results in which a significant difference was not indicated. Both the basis weight and G. E. puncture, however, appear to be close to the borderline in respect to significance. All the test results for Mill H , wherein a significant difference was indicated, are of a greater magnitude than the corresponding group average value; thus, the average quality for Mill H , as determined by these tests, was higher than the group average.
The comparison of the average test values obtained for Mill I with the average for the balance of the group is presented in Table XIII. A significant difference is indicated in all test results except the Riehle compression in the across-machine direction. With the exception of the Amthor tensile in the across-machine direction, the average test results for Mill I, wherein a significant difference was indicated, were of a greater magnitude than the corresponding average test results of the group.
A comparison of the test averages for Mill J with the average test results obtained for the remainder of the group may be seen in Table XIV. A significant difference was indicated for all the average values except Amthor tensile and stretch in the machine-direction. Of those average results showing significant differences, all but the averages of the Richle compression in both directions, were of lower magnitude than the corresponding average values for the group.

## DISCUSSION OF INDIVIDUAL MILL TEST RESULTS FOR 42-POUND. D.F.B.S. FOURDRINIER KRAFT LINER

Mill A
The average results of the various physical tests conducted on the samples of liner rolls made by Mill $A$
are shown in Table XV. Details of the maximum and minimum values for each roll tested are given in Table LXI of the Appendix. The average basis weight was slightly lower than the grade specification of 42 pounds. The average apparent density was 33.2 pounds per cubic foot. It may also be noted that the average bursting strength was 99 points and the average G. E. puncture value was 35 units. The average moisture content was $9.1 \%$ on an ovendry basis.

In a study of this type, the interest is not solely in -the-absolute value of the average test values within a given mill or among mills, but also in the variation in the individual values which make up those averages. To say that the average of a group of test observations is 100 is of little value unless the uniformity or probability of a given variation of the values which make up this average is known.

The probability of a given variation in board from a given mill may be calculated statistically if test values, based on a sufficient number of individual specimens, are available from an adequate number of rolls from that mill. For each type of test, it is first necessary to calculate the average, and then to calculate the standard deviation as a measure of the variability among the rolls. The procedure may be illustrated for basis weight of the liner samples from Mill A.

For Mill A the average basis weight was 41.1 pounds and the standard deviation was calculated to be 1.13 pounds. Accordingly, reference to the appropriate tables (Probability Integrals) shows that a range of $41.1 \pm 1.1$ pounds or 40.0 to 42.2 pounds may be expected to contain $68.3 \%$ of the rolls of this grade produced by Mill A. In most cases it is of more interest, however, to consider the percentage of rolls which might be expected to be contained within any prespecified test value limits. Thus, assume that it is required to find the chance that the basis weight for a roll will fall within $\pm 0.5$ pound of the average basis weight. It is noted that 0.5 pound is a fraction $(0.5 / 1.13=0.44)$ equal to 0.44 of the standard deviation for the basis weight for Mill A. By referring to the appropriate tables, it is found that $3.4 \%$ of the rolls should fall within the selected limits. This indicates that Mill A has a uniformity, in respect to basis weight, such that $34 \%$ of the rolls made in the 42 -pound grade should be within the limits 40.6 to 41.6 pounds. Using the same line of procedure, it may be shown that a range of $\pm 1$ pound is equal to 0.88 of the standard deviation for Mill A, and thus the probability of the basis weight being within the limits 40.1 to 42.1 pounds is $62 \%$. (It should be noted in a precautionary way that the probability of a given test value lying within a given range is not doubled when the range is doubled.) As previously mentioned, it is fully recognized that the application of statistical methods to these data has limitations. It is included, however, to demonstrate the potentialities of its application and to predict, within limits, the variation to be expected in the physical characteristics of board made by the different mills.
Table XVI gives the standard deviations and prob-
able variations to be expected in the rolls of 42 -pound liner made by Mill A. It may be seen from these results that the chance probability or uniformity for Mill A in regard to caliper is such that the greater portion of the rolls should fall within the range of $\pm 0.001$ inch ( 0.0138 to 0.0158 inch ) of the average caliper. The uniformity of the bursting strength indicates that only three fourths of the rolls would be expected to fall within a range limit of $\pm 7.5$ points ( 91.5 to 106.5 points). On a percentage basis, the uniformity in respect to the G. E. puncture is approximately the same as that for the bursting strength. The uniformity in respect to Riehle compression, Elmendori tear, and Amthor tensile and stretch may also be observed in Table XVI. Naturally, as the arbitrarily selected limits increase, the greater will be the percentage of rolls falling within that range. The ranges used are purely arbitrary and are not intended as an attempt to specify acceptable limits. The moisture content was not treated statistically as it was felt that the secondary effects, such as warehouse storage conditions, would possibly prevent the legitimate application of statistics to the moisture data.

## Mill B

The average test results obtained on samples of liner made by Mill B are shown in Table XVII (see also Table LXII of the Appendix). The average basis weight was slightly in excess of the specified grade weight. The average caliper was 0.0154 inch and the average apparent density was 33.4 pounds per cubic foot. The average bursting strength and G. E. puncture were 101 points and 37 units, respectively. The average moisture content was $8.7 \%$ on an ovendry basis.

The statistical evaluation of these test results may be found in Table XVIII. The standard deviation for the basis weight was 1.31. The results indicate that the uniformity of basis weight for Mill B is such that only $30.0 \%$ of the rolls should be expected to fall within the range limit of $\pm 0.5$ pound ( 42.4 to 43.4 pounds), ap)proximately $55 \%$ within the range limit $\pm 1.0$ pound ( 41.9 to 43.9 pounds), and approximately $87 \%$ within the range limit of $\pm 2.0$ pounds ( 40.9 to 44.9 pounds). The standard deviation for the caliper is 0.75 and thus approximately $82 \%$ of the rolls should fall within the caliper range limit of $\pm 0.001$ inch ( 0.0144 to 0.0164 inch). The uniformity of the bursting strength as judged by the standard deviation indicates that approximately $30 \%$ of the rolls should fall within the bursting strength range limit of $\pm 2.5$ points ( 98.5 to 103.5 points), approximately $56 \%$ within the range limit of $\pm 5.0$ points ( 96 to 106 points), and approximately $76 \%$ within the range limit of $\pm 7.5$ points ( 93.5 to 108.5 points). In terms of percentage, the uniformity of the G. E. puncture is of approximately the same order of magnitude as the bursting strength. The Riehle compression, Elmendorf tear, and Amthor tensile and stretch tests showed rather large standard deviations.

TABLE XV
PHY'SICAL. CHARACTERISTICS OF 42-L.B. D.F.B.S. FOURDRINIER KRAFT LINER
Mitl $A$
Roll Averages

|  |  | _ Basis Weight, lb. ( $12 \times 12$ /1000) | $\begin{aligned} & \text { Caliper, } \\ & 0.001 \\ & \text { in. } \end{aligned}$ | Apparent Density, lb./cu.ft. | Moisture, $\%$ | Bursting Strength, points | G.E. Puncture, units | Richle Compression, lb. |  | Elmendorf. 'Tear, g./sheet |  | Amthor Tensile, $\mathrm{lb} . / \mathrm{in}$. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Date Manuf. |  |  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| 1 | 12-30-44 | 42.1 | 14.9 | 33.8 | 8.3 | 94 | 39 | 25.7 | 20.2 | 378 | 401 | 81.6 | 38.1 | 2.0 | 3.5 |
| 2 | 12-30-4.4 | 42.8 | 14.8 | 34.7 | 7.6 | (9) | 38 | 27.0 | 20.0 | 366 | 414 | 83.7 | 38.8 | 2.2 | 3.3 |
| 3 | 1-20-45 | 40.9 | 14.2 | 34.6 | 9.7 | 109 | 3.4 | 29.0 . | 21.0 | 341 | 406 | 84.6 | 35.9 | 2.7 | 3.7 |
| 4 | 1-20.45 | 41.0 | 14.1 | 34.8 | 9.2 | 110 | -35 | 28.5 | $21: 6$ | 336 | $412{ }^{-}$ | -85.3. | 37.4 | $2.9-$ | 3.6 |
| 5 | 11-15-44 | 421 | 14.3 | 35.3 | 13.2 | 107 | 36 | 25.8 | 22.7 | 387 | 415 | 76.8 | 39.8 | 2.8 | 3.5 |
| 6 | 1-26-45 | 42.1 | 15.1 | 33.4 | 10.7 | 111 | 37 | 29.2 | 23.4 | 36.3 | 417 | 85.9 | 38.3 | 2.4 | 3.7 |
| 7 | 11-15-4.4 | 40.1 . | 14.5 | 33.2 | -11.7 | $103-$ | -34 | 29.0 | 22.1 - | 351 | 396 | 78.1 | 37.6 | 2.5 | 3.4 |
| 8 | 1.16-45 | 39.2 | 14.6 | 32.2 | 8.4 | 99 | 33 | 25.9 | 20.2 | 310 | 370 | 73.8 | 36.1 | 1.7 | 2.6 |
| 9 | 1-16-45 | 38.5 | 14.5 | 31.8 | 7.9 | 90 | 31 | 27.5 | 21.2 | 334 | 366 | 72.8 | 35.7 | 2.0 | 2.8 |
| 10 | 1-15-45 | 41.4 | 14.8 | 33.5 | 7.8 | 95 | 36 | 27.5 | 21.5 | 350 | 398 | 81.0 | 36.0 | 2.0 | 2.9 |
| 11 | 1-15-45 | 41.4 | 15.5 | 32.0 | 7.2 | 92 | 35 | 28.8 | 22.3 | 384 | 407 | 82.5 | 35.2 | 2.0 | 3.7 |
| 12 | 1-15-45 | 41.1 | 15.3 | 32.2 | 6.3 | 88 | 35 | 28.1 | 21.5 | 349 | 398 | 81.7 | 34.6 | 2.0 | 3.5 |
| 13 | 1-15-45 | 41.2 | 15.3 | 32.3 | 7.0 | 93 | 37 | 27.6 | 22.0 | 377 | 418 | 82.2 | 36.0 | 1.9 | 29 |
| 14 | 7-1-44 | 40.7 | 15.1 | 32.3 | 11.3 | 98 | 35 | 31.6 | 22.9 | 355 | 382 | 70.7 | 35.4 | 1.9 | 3.7 |
| 15 | 7-1-44 | 41.3 | 15.2 | 32.6 | 12.0 | 104 | 37 | 31.6 | 22.3 | 357 | 394 | 74.0 | 33.5 | 2.3 | 3.7 |
| 16 | 7-1-14 | 40.0 | 14.6 | 32.8 | 11.8 | 96 | 33 | 31.5 | 21.8 | 350 | 380 | 69.4 | 35.1 | 2.2 | 4.2 |
| 17 | 7-1-14 | 39.1 | 14.4 | 32.5 | 10.6 | 88 | 32 | 30.0 | 22.0 | 333 | 371 | 69.4 | 33.9 | 2.1 | 3.8 |
| 18 | 2-8-45 | 41.9 | 15.3 | 32.8 | 9.1 | 104 | 34 | 29.8 | 24.4 | 339 | 404 | 80.5 | 36.9 | 2.0 | 3.7 |
| 19 | 2-8-45 | 41.2 | 15.0 | 32.9 | 8.8 | 10.4 | 32 | 28.4 | 24.7 | 336 | 382 | 86.0 | 36.2 | 2.2 | 3.6 |
| 20 | 3-12-45 | $+1.6$ | 14.9 | 33.5 | 9.6 | 99 | 32 | 31.2 | 21.3 | 319 | 373 | 84.3 | 35.0 | 2.2 | 3.5 |
| 21 | 3-11-45 | 41.2 | 14.8 | 33.4 | 8.1 | 101 | 32 | 29.2 | 22.7 | 313 | 375 | 81.2 | 35.7 | 2.0 | 3.2 |
| 22 | 3-14-45 | 42.7 | 14.9 | 34.3 | 9.9 | 100 | 36 | 27.6 | 22.3 | 321 | 370 | 77.1 | 35.2 | 2.1 | 3.3 |
| 23 | 3-15-45 | 40.4 | 14.8 | 32.7 | 7.9 | 95 | 33 | 29.4 | 22.8 | 316 | 370 | 80.7 | 33.1 | $2.0 \cdot$ | 3.5 |
| 24 | 3-15-45 | 43.3 | 15.1 | 34.4 | 10.1 | 98 | 37 | 27.7 | 226 | 331 | 404 | 74.7 | 36.1 | 2.2 | 3.4 |
| 25 | 3-14-45 | 40.6 | 15.0 | 32.4 | 8.7 | 94 | 34 | 27.1 | 23.4 | 339 | 357 | 70.6 | 37.1 | 2.1 | 2.8 |
| 26 | 3-14-45 | 42.0 | 15.3 | 329 | 8.4 | 103 | 37 | 28.8 | 23.5 | 326 | 404 | 76.9 | 37.0 | 2.3 | 3.0 |
| 27 | 11-15-44 | 40.5 | 14.8 | 32.8 | 7.6 | 95 | 33 | 28.2 | 21.4 | 325 | 373 | 74.9 | 37.4 | 2.1 | 3.3 |
| 28 | 11-15-44 | 40.0 | 14.6 | 32.8 | 6.0 | 99 | 33 | 27.5 | 21.5 | 320 | 385 | 77.3 | 37.5 | 2.0 | 3.4 |
|  | Average | 41.1 | 14.8 | 33.2 | 9.1 | 99 | 35 | 28.5 | 22.1 | 343 | 391 | 78.5 | 36.2 | 2.2 | 3.4 |

TABLE XVI
STATISTICAL EVALUATION OF PILYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

| Test values | Basis Weight, lb. $(12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E. <br> P'uncture, units | Riehle Compression, lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb ./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | Jn | Across |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 43.3 | 15.5 | 111 | 39 | 31.6 | 24.7 | 387 | 418 | 86.0 | 39.8 | 2.9 | 4.2 |
| Minimum | 38.5 | 14.1 | 88 | 31 | 25.7 | 20.0 | 310 | 357 | 69.4 | 33.1 | 1.7 | 2. |
| Average | 41.1 | 14.8 | 99 | 35 | 28.5 | 22.1 | 343 | 391 | 78.5 | 36.2 | 2.2 | 34 |
| Standard deviation | 1.13 | 0.362 | 6.26 | 2.11 | 1.65 | 1.15 | 21.8 | 18.2 | 5.19 | 1.57 | 0.279 | 0.363 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 34 | 99 | 31 | 36 | 46 | 62 | 27 | 32 | 23 | 48 | 28 | 42 |
| Range limit ( $\pm$ ) ${ }^{*}$ | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate prohability. \% | 62 | 100 | 58 | 52 | 64 | 81 | 51 | 59 | 44 | 80 | 53. | 73 |
| Range limit ( $\pm$ )* | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 92 | - | 77 | 84 | 93 | 99 | 83 | 90 | 66 | 94 | 72 | 90 |

TABLIE XVII
IMISICAL CH.ARACTIERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER
Mille 13
Roll Averages


TABLE XVIII
STATISTICAL. EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAF'I LINER


## IHYSICAI. CHARACTERISTICS.OF 42-1B D.F.B.S. FOURDRINIER KRAFI LINER

Mille C
Roll Averages

|  | - | Basis Weight, 16. | Caliper, 0.001 | Apparent | Mois- | Bursting | G. Fi. <br> Punc- | $\begin{array}{r} \mathrm{Ri} \\ \text { Comp } \end{array}$ | hle ession, |  | dorf <br> ar, heet |  | hor sile, in. |  | hor <br> h, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Manuf. | /1000) | in. | lb./cu.ft. | \% | points | units | In | Across | In | Across | In | Across | In | Across |
| 1 | 1-29-45 | 43.7 | 13.7 | 38.2 | 7.7 | 98 | 37 | 28.0 | 23.1 | 385 | 393 | 81.6 | 43.0 | 2.2 | 5.0 |
| 2 | 1-29-45 | 42.8 | 13.4 | 38.3 | 7.8 | 98 | 35 | 29.4 | 23.3 | 356 | 371 | 82.7 | 43.0 | 2.1 | 4.8 |
| 3 | 1-29-45 | 44.0 | 14.0 | 37.7 | 7.7. | 109 | 38 | 31.2 | 24.5 | 389 | 389 | 86.4 | 45.0 | 2.2 | 4.7 |
| 4 | - | 41.7 | 14.2 | 35.2 - | 8.2 | 88 | 36 | 31.2 | $22.8{ }^{\text {+ }}$ | 351 | 380 | 76.6 | 38.8 | 1.5 | 4.3 |
| 5 | - 3-8-45 | 42:6 | 14.8 | 34.5 | $-7.4$ | 104 | $41^{\circ}$ | 31.6 | -23.5 | 377 | 442 | 87.2 | 36.2 | 1.7 | 3.8 |
| 6 | 8-9-44 | 42.2 | 15.0 | 33.8 | 8.3 | 09 | 42 | 31.0 | 21.4 | 361 | 392 | 82.4 | 36.9 | 1.7 | 3.3 |
| 7 | 3-9-45 | 42.1 | 14.6 | 34.6 | 7.6 | 101 | 41 | 29.7 | 21.3 | 349 | 440 | 87.6 | 36.0 | 1.8 | 3.3 |
| . 8 | - 3-9.45 | 42.5 | 14.9 | 34.2 | -8.2 | 99 | 41 | 32.8 | 22.8 | 371 | 433 | 89.8 | 37.0 | 1.8 | 3.9 |
| 9 | 4- 4-45 | 42.1 | 15.0 | 33.7 | 5.5 | 99 | 40 | 29.9 | 21.1 | 376 | 411 | 92.0 | 35.7 | 1.9 | 4.2 |
| 10. | - 4-4-45 | 42.3 | 14.7 | 34.5 | 5.8 | 103 | 40 | 28.9 | 22.0 | 366 | 401 | 85.2 | 36.7 | 1.8 | 4.4 |
| 11 | 1-29-45 | 43.8 | 13.9 | 37.8 | 5.6 | 102 | 38 | 30.3 | 24.6 | 366 | 368 | 84.7 | 44.3 | 1.9 | 4.5 |
| 12 | 1-4-45 | 41.8 | 15.0 | 33.4 | 6.6 | 99 | 38 | 28.3 | 20.6 | 342 | 407 | 86.6 | 37.9 | 1.6 | 3.6 |
| 13 | 1-4-45 | 42.7 | 14.9 | 34.4 | 6.1 | 93 | 38 | 27.3 | 20.4 | 357 | 381 | 84.8 | 36.5 | 1.8 | 3.3 |
| 14 | 1-4-45 | 42.5 | 15.0 | 34.0 | 6.3 | 97 | 38 | 27.6 | 19.7 | 342 | 403 | 86.1 | 36.8 | 1.8 | 3.5 |
| 15 | 2-8.45 | 44.0 | 14.7 | 35.9 | 7.1 | 109 | 41 | 30.5 | 22.3 | 373 | 458 | 94.8 | 39.4 | 2.2 | 4.5 |
| Average |  | 42.7 | 14.5 | 35.3 | 7.1 | 100 | 39 | 29.8 | 22.2 | 364 | 405 | 85.9 | 38.9 | 1.9 | 4.1 |
|  |  | 4 |  |  |  |  |  |  |  |  |  |  |  |  |

TABLE XX
STATISTICAL EVALUATION OF PHYSICAL, TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER


T:ABLE XXI
PHYSICAL CHARACTERISTICS OF 42-LB. DIF.B.S. FOURDRINIER.KR.IFY LINER
Mill D
Roll Averages

|  | T- | Basis Weight, Ib. $(12 \times 12$ | Caliper, 0.001 in. | Apparent Density, lb./cu.ft. | Moisture, $\%$ | Bursting <br> Strength, points | GE. Puncture, units | Riehle Compression, lh |  | Elmendori 'Теar, \%. /sheet |  | Amthor 'Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Manuf. | /1000) |  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| 1 | 2-7-45 | 40.8 | 14.7 | 33.3 | 8.6 | 94 | 38 | 28.3 | 23.3 | 355 | - 374 | 65.3 | 419 | 1.8 | 3.1 |
| 2 | 2. 7.45 | 40.9 | 14.7 | 33.4 | 7.9 | 102 | 37 | 28.6 | 21.4 | 3.36 | 392 | 74.9 | 360 | 1.8 | 3.0 |
| 3 | 2-7-45 | 41.0 | 14.8 | 33.2 | 7.9 | 93 | 37. | 25.8 | -22.9 | 38.3 | 349 | 65.0 | 42.0 | 1.8 | 3.1 |
| 4 | 2-7-45 | 40.3 | 14.9 | 32.4 | 7.1 | 84 | 36 | 24.4 | -21.1 | 375 | 347 | 59.3 | 41.3 | 1.6 | 2.8 |
| 5 | 12-30-44 | 43.9 | 16.7 | 31.5 | 7.7 | 100 | 44 | 27.4 | 21.6 | 391 | 415 | 69.7 | 39.8 | 1.9 | 3.2 |
| 6 | 12-30-44 | 45.4 | 16.6 | 32.8 | 7.4 | 100 | 44 | 28.8 | 22.2 | 407 | 442 | 72.7 | 38.7 | 2.0 | 3.6 |
| 7. | -- | 42.4 | -153 | 33.2- | 9.4 | -97 | . 36 | 29.9 | 23.8 | . 384 | 366 | -68.5 | -42.1 | 1.8 | 3.6 |
| 8 | 8-26-44. | 40.4 | 14.4 | 33.6 | 12.4 | 102 | 34 | 29.4 | 23.4 | 34.4 | 373 | 71.5 | 40.0 | 1.5 | 3.8 |
| 9 | 1-23-45* | 42.3 | 16.0 | 31.7 | 11.7 | 101 * | $37^{\circ}$. | 30.1 | 24.7 | 369 | 406 | 70.9 | 40.3 | $1: 7$ | 3.3 |
| 10 | 3-5-45 | 38.8 | 13.3 | 349 | 4.2 | 91 | 30 | 31.4 | 23.8 | 320 | 348 | 74.0 | 37.5 | 1.9 | 4.0 |
| 11 | 3-5-45 | 39.6 | 13.0 | 36.5 | 4.3 | 95 | 30 | 31.3 | 22.7 | 334 | 341 | 76.2 | 38.5 | 1.9 | 4.3 |
| 12 | 3-12-45 | 41.6 | 14.3 | 34.8 | 7.0 | 94 | 33. | 27.0 | 24.7 | 378 | 345 | 61.5 | 46.6 | 2.0 | 3.3 |
| 13 | 3-12-45 | 39.7 | 12.8 | 37.2 | 7.4 | 104 | 32 | 27.0 | 21.8 | 332 | 335 | 70.4 | 43.7 | 2.0 | 3.5 |
| 14 | 2-12-45 | 40.8 | 14.3 | 34.2 | 8.0 | 95 | 33 | 26.1 | 20.4 | 310 | 361 | 70.8 | 33.0 | 1.9 | 3.1 |
| 15 | 2-25-45 | 42.5 | 14.7 | 34.7 | 6.0 | 102 | 35 | 27.8 | 21.4 | 366 | 399 | 75.5 | 38.5 | 2.1 | 3.1 |
| 16 | 9-26-44 | 43.4 | 14.9 | 34.9 | 6.3 | 105 | 35 | 31.1 | 23.3 | 374 | 409 | 72.3 | 41.2 | 2.2 | 4.3 |
| 17 | 2-25-45 | 41.9 | 14.5 | 34.6 | 6.6 | 105 | 34 | 26.9 | 22.5 | 357 | 382 | 74.0 | 37.5 | 2.3 | 3.2 |
| 18 | 10-11-44 | 41.9 | 16.8 | 29.9 | 8.0 | 86 | 35 | 25.9 | 20.4 | 370 | 387 | 67.6 | 34.6 | 2.0 | 3.8 |
| 19 | 2-9-45 | 43.3 | 14.6 | 35.6 | 6.7 | 110 | 36 | 28.2 | 21.4 | 360 | 402 | 74.3 | 38.7 | 2.2 | 3.7 |
| 20 | 11-3-44 | 41.0 | 15.1 | 32.6 | 5.5 | 93 | 36 | 27.8 | 22.4 | 358 | 372 | 70.4 | 39.3 | 2.3 | 4.1 |
| 21 | 2-.9-45 | 42.8 | 14.8 | 34.7 | 6.2 | 102 | 38 | 25.9 | 22.7 | 362 | 398 | 74.3 | 37.3 | 2.3 | 3.8 |
|  | verage | 41.7 | 14.8 | 33.8 | $7.4{ }^{\circ}$ | 98 | 36 | 28.1 | 22.5 | 360 | 378 | 70.4 | 39.5 | 2.0 | 3.5 |

TABLE NXII
STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-Lb. D.F.b.S. FOURDRINIER KRAFT LINER
Mill D

|  | Basis Weight, lb. $(12 \times 12$ /1000) | Caliper, 0.001 in . | Bursting Strength, points | G.E. <br> Puncture, units | Richle Compression, Ib. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 45.4 | 16.8 | 110 | 44 | 31.4 | 24.7 | 407 | 442 | 76.2 | 46.6 | 2.3 | 4.3 |
| Minimum | 38.8 | 12.8 | 84 | 30 | 24.4 | 20.4 | 310 | 335 | 59.3 | 33.0 | 1.5 | 2.8 |
| Average | 41.7 | 14.8 | 98 | 36 | 28.1 | 22.5 | 360 | 378 | 70.4 | 39.5 | 2.0 | 3.5 |
| Slandard deviation | 1.59 | 1.07 | $6.51{ }^{\circ}$ | 3.57 | 1.96 | 1.25 | 24.2 | 28.7 | 4.56 | 3.07 | 0.237 | 0.441 |
| Kange limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 24 | 65 | 30 | 22 | 39 | 58 | 24 | 21 | 26 | 26 | 33 | 35 |
| $\text { Range limit }( \pm)^{*}$ | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 47 | 94 | 56 | 33. | 56 | 77 | 46 | 40 | 49 | 48 | 60 | 64 |
| Range limit (土)* | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 79 | - | 75 | $60^{\circ}$ | 87 | 98 | 79 | 71 | 73 | 67 | 80 | 83 |

Mile C
The average test results obtained for the liner made by Mill C are given in Table XIX (see also Table LXIII of the Appendix) and the statistical evaluation of these results in Table XX. The results indicate that the average basis weight for Mill C was slightly in excess of the specified weight for this grade. The average caliper was 0.0145 inch and the average apparent density was 35.3 pounds per cubic foot. The average bursting strength and G. E. puncture values were 100 points and 39 . units, respectively.. The average mois= ture content was $7.1 \%$ on the ovendry basis.

The standard deviation for basis weight for Mill C is 0.785 . This rather low standard deviation suggests that approximately $48 \%$ of the rolls should fall within a range limit of $\pm 0.5$ pound ( 42.2 to 43.2 pounds), $80 \%$ within a range limit of $\pm 1.0$ pound ( 41.7 to 43.7 pounds), and practically all the rolls within a range limit of $\pm 2.0$ pounds ( 40.7 to 44.7 pounds). The standard deviation for the caliper is 0.537 , and thus approximately $68 \%$ of the rolls should fall within a caliper range limit of $\pm 0.0005$ inch ( 0.0140 to 0.0150 inch) and approximately $94 \%$ within the range limit of $\pm 0.001$ inch ( 0.0135 to 0.0155 inch). The uniformity of the bursting strength indicates that approximately $35 \%$ of the rolls should fall within a range limit of 2.5 points ( 97.5 to 102.5 points), $65 \%$ within the range limit of $\pm 5.0$ points ( 95 to 105 points), and approximately $84 \%$ within a range limit of $\pm 7.5$ points ( 92.5 to 107.5 points). Percentagewise, the G. E. puncture is of approximately the same order of uniformity. In gencral, the standard deviations for the Riehle compression, Elmendorf tear, and Amthor tensile and stretch are of such magnitude as to indicate considerable lack of uniformity within the low arbitrary ranges but rather good agreement within the wider arbitrarily selected ranges.

## Mile D

The average test results obtained for the liner manufactured by Mill D are shown in Table XXI (see also Table LXIV of the Appendix). The statistical evaluation of these results is given in Table XXII. The average basis weight for Mill D was, for all practical purposes, of the same order of magnitude as the specified grade weight of 42 pounds. This weight and the average caliper of 0.0148 inch resulted in an average apparent density of 33.8 pounds per cubic foot. The average bursting strength and G. E. puncture were 98 points and 36 units, respectively. The average moisture content was $7.4 \%$ on an ovendry basis.

Inasmuch as the standard deviation of the basis weight was 1.59 , it is to be expected that only $24 \%$ of the rolls would fall within a basis weight range limit of $\pm 0.5$ pound ( 41.2 to 42.2 pounds), $47 \%$ within a range limit of $\pm 1.0$ pound ( 40.7 to 42.7 pounds), and $79 \%$ within a range limit of $\pm 2.0$ pounds ( 39.7 to 43.7 pounds). On the basis of a standard deviation of
1.07 for caliper, $65 \%$ of the rolls should fall within a caliper range limit of $\pm 0.001$ inch ( 0.0138 to 0.0158 inch) and only $94 \%$ within the range limit of $\pm 0.002$ inch ( 0.0128 to 0.0168 inch). The uniformity of the bursting strength, as shown by the standard deviation of $6: 51$, indicates that only $30 \%$ - of the rolls should be expected to fall within a bursting strength range limit of $\pm 2.5$ points ( 95.5 to 100.5 points), $56 \%$ within a range limit of $\pm 5.0$ points ( 93 to 103 points), and $75 \%$ within a range limit of $\pm 7.5$ points ( 90.5 to 105.5 points). The G. E. puncture test results, with an average value of $36^{\circ}$ and a standärd deviätion of 3.57 , indicate a slightly greater probable variation than the bursting strength. The standard deviations for the Richle compression, Elmendorítar, and Amthor tensile and stretch indicate considerable nonuniformity in the narrower range limits selected.

## Mill E

The average test results obtained for the liner produced by Mill ${ }^{-}$E are given in Table XXIII (see also Table LXV of the Appendix) and the statistical evaluation of these results in Table XXIV. The average basis weight was in excess of the specified grade weight of 42 pounds. The average caliper was 0.0157 inch which results in an apparent density of 33.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 91 points and 35 units, respectively. The average moisture content was $7.5 \%$; however, as may be noted in Table XXIII, the average moisture content is based on the results obtained for only eight rolls.
The standard deviation of 0.981 for basis weight indicates that the basis weight of $39 \%$ of the rolls produced should fall within the range limit of $\pm 0.5$ pound ( 42.9 to 43.9 pounds), $69 \%$ within the range limit of $\pm 1.0$ pound ( 42.4 to 44.4 pounds), and $96 \%$ within the range limit of $\pm 2.0$ pounds ( 41.4 to 45.4 pounds). Mill E has a uniformity with respect to caliper such that $63 \%$ of the rolls should fall within the range limit $\pm 0.001$ inch ( 0.0147 to 0.0167 inch) and $93 \%$ within the range limit $\pm 0.002$ inch ( 0.0137 to 0.0177 inch ). The standard deviation of 18.6 for the bursting strength indicates extreme nonuniformity with the probable chance variation that only $31 \%$ should fall within the range limit of $\pm 7.5$ points ( 83.5 to 98.5 points). It may be observed, however, that Rolls 1 and 2 were extremely low in all test results and, since there were only 11 rolls sampled of this mill's product, the effect of these rolls is considerable. In all probability, the presence of these two rolls has distorted the uniformity far more than practical consideration would permit. If the standard deviation for bursting strength were calculated after excluding Rolls 1 and 2 , it would be 5.45 as compared with 18.6 when these two rolls are included. On the basis of statistics, however, it is not permissible to exclude these roll values.

TABLEE XXIII
PHYSICAL CHARACTERISTICS OF 42-L.B. D.F.B.S. FOURDRINIER KRAFT I, NER
Mill E:
Roll Averages

| - - | - | Hasis Weight lb. ( $12 \times 12$ <br> /1000) | Caliper, 0.001 in. | $\therefore$ Apparent Density, $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | Mois- <br> ture, \% | Bursting Strength, points | G.E. <br> Punc- <br> ture, <br> units | Richle Compression, lb . |  | Aimendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Date Manuf. |  |  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| 1 | 2-13-45 | 44.9 | 17.3 | 31.1 | 9.0 | 52 | . 28 | 22.0 | 17.5 | 274 | 278 | 54.0 | 29.9 | 1.2 | 2.7 |
| 2 | 2-13-45 | 44.6 | 17.8 | 30.1 | 5.2 | 58 | 28 | 24.3 | 18.6 | 271 | 282 | 60.5 | 29.6 | 1.3 | 2.9 |
| 3 |  | 42.5 | 14.0 | 36.4 | 8.5 | 92 | 31 | 250 | 18.7 | 314 | 349 | 75.7 | 34.5 | 1.6 | 3.7 |
| 4 | 3-20-45 | 43.8 | -16.1 | 32.6 | 9.0 | 97. | 36 | 29.7 | 21.2 | 313 | - 375 | 84.9 | 32.9 | -1.9 . | 3.7 |
| 5 | 3-21-45 | 43.0 | 16.0 | 32.2 | 6.9 | 92 | 35 | 30.4 | 20.9 | 303 | 362 | 82.3 | 33.3 | 1.7 | 3.6 |
| 6 | 3-21-45 | 43.3 | 15.9 | 32.7 | 7.5 | 98 | 34 | 28.7 | 21.7 | 317 | 380 | 88.0 | 33.2 | 1.9 | 3.8 |
| 7 | 3-20-45 | 44.2 | 15.5 | 34.2 | 6.8 | 105 | 38 | 30.9 | 22.4 | 331 | 385 | 84.3 | 33.8 | 2.0 | 3.8 |
| 8 | 3-21-45 | 41.7 | 15.4 | -32.5 | 7.3 | $104^{-}$ | 36 | 28.8 | 20.3 | 317 ${ }^{-}$ | 369 | 89.9 | 32.6 | 2.1 | 4.0 |
| 9 | 4-645. | 42.9 | 14.3 | 36.0 | , | 106 | 39 | 28.5 | 22.7 | \$62 | 404 | 78.9 | 38.4 | 2.0 | 4.0 |
| 10 | 4. 6-45* | 43.6 | 15.2 | 34.4 | * | 103 | 39 | 26.4 | 21.8 | 400 | 427 | 76.7 | 40.8 | 2.0 | 4.0 |
| 11 | 4. 6.45 | 42.4 | 15.3 | 33.3 | * | 96 | 37 | 27.5 | 21.2 | 361 | 403 ' | 72.7 | 38.5 | 1.9 | 3.8 |
|  | rage | 43.4 | 15.7 | 33.2 | 7.5 | 91 | 35 | 27.5 | 20.6 | 324 | 365 | 77.1 | 34.3 | 1.8 | 3.6 |

* No moisture samples obtained.

TABLE XXIV
STATISTICAL EVALUÁTION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAIT LINER

|  | Basis Weight, lb. ( $12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E. <br> Puncture, units | MıLL E |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, $\%$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Riehle Compression, lb. |  |  |  |  |  |  |  |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 44.9 | 17.8 | 106 | 39 | 30.9 | 22.7 | 400 | 427 | 89.9 | 40.8 | 2.1 | 4.0 |
| Minimum | 41.7 | 14.0 | 52 | 28 | 22.0 | 17.5 | 271 | 278 | 54.0 | 29.6 | 1.2 | 2.7 |
| Average | 43.4 | 15.7 | 91 | 35 | 27.5 | 20.6 | 324 | 365 | 77.1 | 34.3 | 1.8 | 3.6 |
| Standard deviation | 0.981 | 1.12 | 18.6 | 4.01 | 2.77 | 1.68 | 38.4 | 47.2 | 11.2 | 3.54 | 0.299 | 0.437 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | $7.5 *$ | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 39 | 63 | 10 | 20 | 28 | 45 | 16 | 13 | 10 | 22 | 26 | 35 |
| Range limit ( $\pm$ )* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 69 | 93 | 21 | 29 | 41 | 63 | 30 | 25 | 21 | 42 | 50 | 64 |
| Range limit ( $\pm)^{*}$ | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 96 | - | 31 | 55 | 72 | 93 | 56 | 48 | 35 | 60 | 68 | 83 |
| * Range limits we | re arbitra | ily selecte |  |  |  |  |  |  |  |  |  |  |

TABLE XXV
I'HYSICAI, CHARACTERISTICS OF 42-LR. D.F.B.S. FOURDRINIER KRAFT A.INER
Mill F
Roll Averages

|  | $\cdots$ | Basis Weight, lb. | Caliper, ent Mois- Bursting l'unc-0.001 Density, ture Strength ture, |  |  |  |  |  |  | Elmendorf Tear. $\mathrm{g} /$ /sheet |  | Amthor Tensile, lb./in. |  | $\begin{aligned} & \text { Amthor } \\ & \text { Stretch, \% } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Kıll | Manuf. | $\begin{array}{r} 12 \times 12 \\ / 1000) \end{array}$ | in. | Density, | ture, \% | Strength, points | ture, | In | Across | In | Across | In | Across | In | Across |
| 1 | 5-4-45 | 41.1 | 13.5 | 36.5 | 10:7 | 98 | 39 | 24.3 | 18.4 | 338 | 404 | 712 | 38.7 | 20 | 3.1 |
| 2 | 4-15-45 | 42.4 | 13.9 | 36.6 | 11.4 | 96 | 37 | 21.5 | 18.9 | 335 | 370 | 71.4 | 35.9 | 2.0. | 2.9 |
| 3 | 5- 5-45 | 37.5 | 13.1 | 34.3 . | 8.7 | 76 | 28 | 22.3 | 16.5 | 270 | 310 | 63.9 | 27.5 | 1.7 | 3.4 |
| $-4$ | 5- 5-45 | -41.6 | 13.5 | \$7.0 | -11.1. | 75 | 32 | - 21.6 - | 18.0 | $283-$ | -334-- | 67.0 | 29.5 | 1:8. | -3.1- |
| 5 | 5- 5-45 | 39.3 | 13.0 | 36.3 | 10.3 | 83 | 29 | 23.7 | 19.8 | 279 | 325 | 63.6 | 32.8 | 2.0 | 3.0 |
| 6 | 5- 5-45 | 39.4 | 13.4 | 35.3 | 7.8 | 78 | 31 | 23.2 | 19.7 | 292 | 320 | 61.1 | 33.8 | 20 | 3.1 |
| 7 | 5- 5-45. | 36.9 - | 12.6. | 35.1 . | 9.5 | 76 | +28 | 23.3 | 19.9 | 262 | 285 | 60.3 | 33.3 | 1.9 | 3.0 |
| 8 | 5- 4-45 | 40.0 | 13.7 | 35.0 | 10.5 | 97 | 37 | 23.4 | 19.9 | 338 | 379 | 72.0 | .35.2 | 2.0 | 3.0 |
| 9 | 5- 4-45 | - 40.5 | 13.5 | 36.0 | 10.6 | 95 | 37 | 26.9 | 19.8 | 348 | 369 | 74.0 . | 36.0 | 2.0 | 3.1 |
| 10 | 5- 5-45 | - 38.4 | 13.5 | 34.1 | 9.5 | 74 | 29 | 22.6 | 16.0 | 276 | 333 | 62.3 | 26.9 | 1.9 | 3.0 |
|  | erage | 39.7 | 13.4 | 35.6 | 10:0 | 85 | 33 | 23.3 | 18.7 | 302 | 343 | 66.7 | 33.0 | 1.9 | 31 |

TABLE XXVI
STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER


* Range limits were arbitrarily selected.

TABLE XXVII
PHISICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KR.IF゙T I,INER
Mill G
Roll Averages

|  |  | Basis Weight, (1). | $\begin{aligned} & \text { Caliper, } \\ & 0.001 \end{aligned}$ | Apparent | Mois- | Bursting | G.E. Punc- |  | hle ression, b. |  | endorf - <br> ear, sheet |  | thior asile, in. |  | thor <br> ch, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Manuf. | $\begin{gathered} (12 \times 12 \\ 1000 \end{gathered}$ |  | lb./cu.ft. | \% | points | unit | In | Across | In | Across | In ${ }^{\text {' }}$ | Across | In | Across |
| 1 | 4. 2-45 | 42.6 | 15.5 | 33.0 | 7.3 | 93 | 37 | 27.4 | 23.6 | 373 | 429 | 76.0 | 41.4 | 1.7 | 3.1 |
| 2 | 4. 2-45 | 42.5 | 15.9 | 32.1 | 4.9 | 87 | 38 | 26.7 | 23.2 | 382 | 413 | 73.5 | 40.8 | 1.4 | 2.9 |
| 3 | 4-2-45 | 42.0 -- | 15.8 | 31.9 | 7.4 | 88 | 37 | 25.7 | 22.3 | 382 | 426 | 73.0 | 41.7 | 1.6 | 3.1 |
| 4 | 4-2-45 | 41.7 | 15.7 | 31.9 | 6.8 | 85 | 37 | 26.1 | 22.0 | -392 | $420^{-}$ | 73.5 | $41.9^{-}$ | 1.5 | 2.8 |
| 5 | 4-2-45 | 42.2 | 15.9 | 31.8 | 8.1 | 92 | 38 | 25.5 | 22.0 | 390 | 423 | 74.7 | 40.7 | 1.5 | 2.8 |
| 6 | 1-22-45 | 41.2 | 16.1 | 30.7 | 5.8 | 89 | 36 | 28.8 | 21.8 | 377 | 399 | 71.5 | 37.1 | 2.0 | 4.0 |
| 7. | 1-22-45 | $41: 7$ | 16.2 | 30.9 | 7:0 | 92- | 38 | 28.1 | 23.8 | 394 | 436 | 72.3 | 40.8 . | 2.0 | 3.8 |
| 8 | 12-12-44 | 42.0 | 15.0 | 33.6 | 10.5 | 106 | 38 | 28.8 | 25.3 | 377 | 405 | 70.7 | 50.6 | 2.0 | 37 |
| 9 | 2-19-45 | 41.5 | 15.5 | 32.1 | 8.2 | 97 | 36 | 28.9 | 25.7 | - 383 | 375 | 71.6 | 44.7 | 2.0 | 4.3 |
| 10 | 2-19-45 | 41.7 | 15.2 | 32.9 | 6.3 | 95 | 35 | 27.9 | 26.2 | 381 | 382 | 70.0 | 44.4 | 2.0 | 4.2 |
| 11 | 4-2-45 | 43.3 | 15.3 | 34.0 | 6.9 | 88 | 44 | 27.4 | 23.1 | 394 | 424 | 73.9 | 37.9 | 1.8 | 4.0 |
| 12 | 4-2-45 | 40.2 | 15.3 | 31.5 | 5.8 | 91 | 39 | 28.1 | 23.7 | 364 | 407 | 70.8 | 38.6 | 1.6 | 3.6 |
| 13 | 4-2-45 | 41.6 | 15.3 | 32.6 | 5.5 | 79 | 39 | 25.6 | 22.1 | 383 | 410 | 69.7 | 35.7 | 1.4 | 3.3 |
| 14 | 11-13-44 | 42.6 | 16.0 | 31.9 | 7.3 | 88 | 36 | 28.8 | 26.8 | 382 | 358 | 70.3 | 48.4 | 1.8 | 4.1 |
| 15 | 3-13-45 | 41.0 | 15.0 | 32.8 | 7.9 | 94 | 37 | 26.6 | 24.1 | 353 | 371 | 72.5 | 42.8 | 1.8 | 4.3 |
| Average |  | 41.9 | 15.6 | 32.2 | 7.0 | 91 | 38 | $27.4 \quad 23.7$ |  | 380 | 405 | $72.3 \quad 41.8$ |  | 1.73 .6 |  |

TABLE XXVIII
STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.b.S. FOURDRINIER KRAFT LINER


Mill $F$
The average test results obtained on the liner made by Mill $F$ are reported in Table XXV (see also Table LXVI of the Appendix). The results indicate that the average basis weight is considerably lower than the specified weight for this grade. The average caliper was 0.0134 inch, which resulted in an average apparent density of 35.6 pounds per cubic foot. The average bursting strength and G. E. puncture values were 85 points and 33 units, respectively. The average moisture content was. $10.0 \%$ on an ovendry basis:

The statistical evaluation of these test results is given in Table XXVI. On the basis of a standard deviation of 1.77 for basis weight, it should be expected that only $22 \%$ of the rolls will fall within a basis.weight range limit of $\pm 0.5$ pound ( 39.2 to 40.2 pounds), $42 \%$ of the rolls within a range limit of $\pm 1.0$ pound ( 38.7 to 40.7 pounds), and $74 \%$ of the rolls within a range limit of $\pm 2.0$ pounds ( 37.7 to 41.7 pounds). The chance variation or uniformity of the caliper as determined by standard deviation indicates an expectancy of approximately all of the rolls falling within the range limit of $\pm 0.001$ inch ( 0.0124 to 0.0144 inch). The standard deviation for the bursting strength indicates that the uniformity is such that only $19 \%$ of all rolls should fall within the range limit of $\pm 2.5$ points ( 82.5 to 87.5 points) of the average obtained, $38 \%$ of the rolls within the range limit of $\pm 5.0$ points ( 80.0 to 90.0 points) and $53 \%$ within the range limit of $\pm 7.5$ points ( 77.5 to 92.5 points).. The probable variation for the G. E. puncture test appears to follow approximately the same trend as the bursting strength variation. The probable variation for Riehle compression and Amthor stretch appears to be slightly less than the variation to be expected for Elmendorf tear and Amthor tensile.

## Mill G

The average test results obtained on samples of liner made by Mill G are given in Table XXVII (see also Table LXVII of the Appendix). The average basis weight was, for all practical purposes, the same as the specified grade weight. The average caliper was 0.0156 inch and the average apparent density was 32.2 pounds per cubic foot. The average bursting strength and G.E. puncture values were 91 points and 38 units, respectively. The average moisture content was $7.0 \%$ on an ovendry basis.

The statistical evaluation of these results is given in Table XXVIII. The standard deviation for basis weight indicates that approximately $49 \%$ of the rolls should fall within a basis weight range limit of $\pm 0.5$ pound ( 41.4 to 42.4 pounds), $82 \%$ within a range limit of $\pm 1.0$ pound ( 40.9 to 42.9 pounds) and practically all the rolls produced of this grade should fall within a range limit of $\pm 2.0$ pounds ( 39.9 to 43.9 pounds). On the basis of the results obtained for caliper, it should be expected that practically all the rolls would fall within a caliper range limit of $\pm 0.001$ inch ( 0.0146 to 0.0166 inch). The standard deviation of the bursting
strength was of such magnitude that it should be expected that only $32 \%$ of the rolls should fall within a range limit of $\pm 2.5$ points ( 88.5 to 93.5 points), $59 \%$ within the range limits of $\pm 5.0$ points ( 86.0 to 96.0 points), and approximately $78 \%$ within the range limit of $- \pm 7.5$ points ( 83.5 to 98.5 points). The magnitude of the standard deviation for the G. E. puncture test indicates approximately the same probable variation as for the bursting strength. The standard deviations for the Riehle compression, Elmendorf tear, Amthor tensile and stretch indicate that the probable variation to ${ }^{-b}$ expected is quite large.--

## Mill H

The average test results obtained on the samples of . liner manufactured by Mill H are tabulated in Table XXIX (see also Table LXVIII of the Appendix). The average basis weight obtained for Mill H was slightly in excess of the specified grade weight. The average caliper was 0.0159 inch and the average apparent density was 32.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 108 points and 37 units, respectively. The average moisture content was $8.0 \%$ on an ovendry basis.

The statistical evaluation of these test results is. shown in Table XXX. The standard deviation for basis weight is of the magnitude that $40 \%$ of the rolls manufactured by Mill H in this grade should fall within a basis weight range limit of $\pm 0.5$ pound ( 42.1 to 43.1 pounds), $72 \%$ within the range limit of $\pm 1.0$ pound (41.6. to 43.6 pounds), and practically $97 \%$ within the range limit of $\pm 2.0$ pounds ( 40.6 to 44.6 pounds). On the basis of the results obtained for caliper, it should be expected that practically all the rolls should fall within $\pm 0.001$ inch ( 0.0149 to 0.0169 inch $)$ of the average caliper. The statistical evaluation of the bursting strength indicates that approximately $38 \%$ of the rolls should fall within a bursting strength range limit of $\pm 2.5$ points ( 105.5 to 110.5 points), approximately $67 \%$ within the range limit of $\pm 5.0$ points ( 103 to 113 points), and approximately $86 \%$ within the range limit of $\pm 7.5$ points ( 100.5 to 115.5 points). The variation for the G. E. puncture test exhibits relatively the same trend as the bursting strength. The standard deviations for the Riehle compression, Elmendorf tear, and Amthor tensile and stretch indicate considerable lack of uniformity in the tests.

## Mill I

The average test results obtained for the liner made by Mill I are shown in Table XXXI (see also Table LXIX of the Appendix). The average basis weight was in excess of the specified weight for this grade. The average caliper was 0.0153 . inch and the average apparent density was 34.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 109 points and 41 units, respectively. The average moisture content was $8.4 \%$ on an ovendry basis.

The statistical evaluation of these test results may

TABLE XXIX
PIISICAL CHARACTERISTICS OF 42-Lb. D.F.b.S. FOURDRINIER KRAFT LINER
Mile H
Roll Averages

| $\checkmark$ |  | Basis Weight, lb. | Caliper, | Apparent | Mois- | Bursting | G.E. Punc- | $\begin{array}{r} \mathrm{R} \\ \mathrm{Com} \end{array}$ | ehle ression, b. |  | ndorf ear, sheet |  | hor sile, /in. | $\stackrel{A n}{\text { Stre }}$ | thor <br> tch, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Date <br> Manuf. | $\begin{aligned} & (12 \times 12 \\ & / 1000) \end{aligned}$ | $\begin{aligned} & .001 \\ & \text { in. } \end{aligned}$ | Density, <br> lb./cu.ft. | $\begin{aligned} & \text { ture, } \\ & \% \end{aligned}$ | Strength, points | ture, units | In | Across | In | Across | In | Across | In | Across |
| 1 | 12-31-44 | 44.5 | 15.7 | 34.0 | 8.8 | 112 | 42 | 29.7 | 25.4 | 449 | 452 | 73.5 | 47.8 | 2.5 | 3.8 |
| 2 | 12-31-44 | 446 | 16.5 | 32.4 | 9.4 | 96 | 42 | 27.0 | 24.5 | 481 | 427 | 62.7 | 50.3 | 2.3 | 4.4 |
| 3 | 3-19-45 | 42.1 | 15.2 | 33.2 | 8.1 | 107 | 37 | 32.4 | 25.7 | 390 | 400 | 69.2 | 45.7 | 2.0 | 4.4 |
| 4 | 3-20-45 | 41.5- | 15.2 | - 32:8- | 9.0 | --103 | 35. | -29.7 | 25.4- | - 397 | 371 | 63.9 | 49.7.- | 2.0 | 4.5 |
| 5 | 3-20-45 | 42.2 | 16.4 | 30.9 | 7.1 | 108 | 35 | 34.8 | 26.1 | 340 | 405 | 80.0 | 42.5 | 2.1 | 3.7 |
| 6 | 3-20.45 | 41.6 | $15.9{ }^{\circ}$ | 31.4 | 7.7 | 105 | 36 | 31.3 | 22.8 | 339 | 391 | 79.5 | 39.1 | 2.1 | 4.0 |
| 7 | 3-20.45 | 42.4 | 16.4 | 31.0 | 6.7 | - 101 | - 37. | 32.1 | 22.7 | 346 | 405. | . 75.9 | 37.7 | 1.9 | 3.6 |
| 8 | 4-13-45 | 42.0 | 16.1 | 31.3 | 6.3 | 110 | 36 | 28.6 | 2.3 .9 | 37.3 | 389 | 80.5 | 40.9 | 2.3 | 3.9 |
| 9 | 4-13-45 | 42.3 | 15.6 | 32.5 | 8.9 | 115 | 35 | 30.9 | 24.4 | 360 | 393 | 80.9 | 41.7 | 2.4 | 4.3 |
| 10 | 4-13-45 | 42.7 | 15.8 | 32.4 | 8.8 | 111 | 38 | 30.2 | 23.8 | 378 | 400 | 80.8 | 39.2 | 2.4 | 3.8 |
| 11 | 4-13-45 | 42.9 | 15.9 | 32.4 | 8.5 | 108 | 38 | 30.5 | 23.7 | 391 | 409 | 80.0 | 41.0 | 2.3 | 4.1 |
| 12 | 4-13-45 | 42.8 | 16.1 | 31.9 | 7.8 | 107 | 38 | 30.8 | 24.8 | 375 | 406 | 82.1 | 40.2 | 2.4 | 3.8 |
| 13 | 4-13.45 | 41.9 | 15.9 | 31.6 | 8.1 | 108 | 37 | 30.1 | 25.0 | 380 | 431 | 79.1 | 41.3 | 2.3 | 4.4 |
| 14 | 4-13-45 | 42.3 | 15.6 | 32.5 | 7.4 | 114 | 36 | 31.1 | 25.4 | 406 | 420 | 73.7 | 40.3 | 2.3 | 4.2 |
| Average |  | 42.6 | 15.9 | - 32.2 | 8.0 | 108 | 37 | 30.7 | 24.5 | 386 | 407 | 75.8 | 42.7 | 2.2 | 4.1 |

TABLE XXX
STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

|  | Basis Weight, lb. ( $12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E. <br> Puncture, units | Mill H |  |  |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Riehle Compression, lb . |  | Elmendorf <br> Tear, <br> g./sheet |  |  |  |  |  |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 44.6 | 16.5 | 115 | 42 | 34.8 | 26.1 | 481 | 452 | 82.1 | . 50.3 | 2.5 | 4.5 |
| Minimum | 41.5 | 15.2 | 96 | 35 | 27.0 | 22.7 | 339 | 371 | 62.7 | 37.7 | 1.9 | 3.6 |
| Average | 42.6 | 15.9 | 108 | 37 | 30.7 | 24.5 | 386 | 407 | 75.8 | 42.7 | 2.2 | 4.1 |
| Standard deviation | 0.937 | 0.405 | 5.11 | 2.27 | 1.82 | 105 | 39.7 | 20.3 | 6.44 | 4.05 | 0.183 | 0.303 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 40 | 99 | 38 | 34 | 42 | 66 | 15 | 29 | 18 | 20 | 42 | 49 |
| Range limit (土)* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 72 | 100 | 67 | 49 | 59 | 85 | 30 | 54 | 36 | 38 | 72 | 81 |
| Kange limit ( $\pm$ )* | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 97 | - | 86 | 81 | 90 | 99 | 55 | 86 | 56 | 54 | 90 | 95 |

Man. I
Roll Averages

|  | - Date | Basis Weight, 1 b . $(12 \times 12$ | $\begin{aligned} & \text { Caliper, } \\ & 0.00 \mathrm{~L} \end{aligned}$ | $\begin{aligned} & \text { Appar- } \\ & \text { ent } \\ & \text { Density, } \end{aligned}$ | Moisture, | Bursting Strength, | G.E. Punc- |  | hle ession, b. |  | ndorf <br> ar, <br> heet |  | thor sile, in. |  | thor ch, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Manuf. | /1000) | in. | lb./cu.ft. | \% | points | units | In | Across | In | Across | In | Across | In | Across |
| 1 | 1-20-45 | 42.5 | 15.3 | 33.3 | 8.7 | 111 | 40 | 30.5 |  |  |  |  |  |  |  |
| 2 | 1-20-45 | 42.7 | 15.1 | 339 | 8.9 | 107 | 42 | 38.5 | 22.4 | 418 | 468 | 90.9 | 36.6 | 2.0 | 4.2 |
| 3 | 1-20-45 | 42.5 | 15.3 | 33.3 | 8.5 | 109 | 42 | 28.7 | 21.2 | 428 | 473 | 88.2 | 37.9 | 2.0 | 4.3 |
| 4 | 1-31-45 | 43.9 | 15.1 | 34.9 | 7.0 | 106 | 40 | 28.7 29.0 | 20.6 | 422 434 | 506 470 | 88.4 | 37.7 | 2.1 | 4.6 |
| 5 | 1-31-45 | 43.5 | 15.2 | 34.3 | 7.1 | 105 | 41 | 29.0 26.7 | 20.3 | 434 | 470 | 88.5 | 37.1 | 2.3 | 4.2 |
| -6 | -1-31-45 | 43.1 | 15.5 | - 33.4 | 6.9 | 108 | 41 |  |  |  |  | 86.3 | 35.8 | 2.2 | 4.1 |
| 7 | 1-31-45 | 43.5 | 15.5 | 33.7 | 7.0 | 104 | 41 | 29.5 30.0 | 22.5 | 401 | 462 | 85.3 | 38.0 | 2.2 | 4.3 |
| 8 | 1-31-45 | 42.1 | 152 | 33.2 | 6.5 | 102 | 31 | 39.0 29.2 | 20.4 | 408 | 487 | 87.5 | 35.3 | 2.2 | 4.3 |
| 9 | 1-30-45 | 43.4 | 15.5 | 33.6 | 10.0 | 106 | 40 | 29.2 | 21.5 | 407 | 443 | 78.6 | 36.6 | 2.0 | 4.5 |
| 10 | --1-31-45 | 43.2 | 15.5 | $33.4{ }^{-}$ | -8.9 | 109 | 40 | 29.9 29.8 | 21.9. | 411 | 442 | 81.9 | 37.1 - | 2.2 | 4.3 |
| 11 | 1-31.45 | 43.6 | 15.3 | 34.2 | 8.8 | 114 | 41 |  |  |  |  |  | 36. | 2.2 | 4.5 |
| 12 | 1-30-45 | 43.8 | 15.7 | 33.5 | 9.6 | 109 | 40 | 31.0 300 | 23.7 | 390 | 466 | 85.5 | 37.2 | 2.3 | 4.7 |
| 13 | 1-30-45 | 43.3 | 15.9 | 32.7 | 9.4 | 100 | 41 | 30.0 29.7 | 22.3 | 422 | 470 | 80.5 | 37.0 | 2.3 | 4.4 |
| 14 | 3-2-45 | 42.8 | 14.7 | 34.9 | 9.7 | 119 | 31 | 29.7 31.2 | 23.6 | 390 | 458 | 78.4 | 35.3 | 2.2 | 4.3 |
| 15 | 3-2-45 | 45.4 | 15.1 | 36.1 | 10.8 | 121 | 42 | 32.3 | 22.1 | 394 | 474 | 83.5 | 36.3 | 2.6 | 5.3 |
| 16 | 3-2-45 | 45.0 | 15.3 | 35.3 | 11.4 | 112 |  |  |  | , |  | 84.2 | 37.8 | 2.6 | 5.1 |
| 17 | 1-11-45 | 42.6: | 15.0 | $34.1{ }^{-}$ | 8.2 | 104 | 38 | 32.1 | 21.9 | 416 | 491 | 85.6 | 38.3 | 2.6 | 4.8 |
| 18 | 3-10-45 | 44.5 | 14.9 | 35.8 | 8.3 | 104 110 | 48 | 32.1 | 18.6 21.9 | 366 | 430 | 82.5 | 35.1 | 2.3 | 4.4 |
| 19 | 3-10-45 | 43.3 | 14.9 | 34.9 | 6.6 | 107 | 42 | 35.5 34.5 | 21.9 22.1 | 391 416 | 453 | 89.6 | 36.5 | 2.5 | 4.6 |
| 20 | 1-18-45 | 43.9 | 15.3 | 34.4 | 8.1 | 110 | 43 | 34.5 33.6 | 22.0 | 416 412 | 451 | 86.9 | 36.3 | 2.2 | 4.5 |
| 21 | -10-24-44 | 45.0 | 15.6 | 34.6 | 7.6 |  |  |  |  |  | 4 | 87.0 | 38.0 | 2.3 | 4.5 |
| 22 | -2-3-45 | 44.1 | 15.6 | 33.9 | 8.4 | 110 | 4 | 34.5 | 22.0 | 411 | 443 - | 92.2 | 35.4 | 2.3 | 4.4 |
|  |  |  |  |  |  | 110 | 44 | 30.3 | 24.1 | 401 | 469 | 83.4 | 37.9 | 2.2 | 4.6 |
| Average |  | 43.5 | 15.3 | 34.2 | 8.4 | 109 | 41 | 30.9 | 21.8 | 408 | 465 | 85.4 | 36.8 | 2.3 | 4.5 |

TABLE XXXII
Statisitical evaluation of physical tests on 42-Lb. D.f.b.S. Fourdrinier kraft liner

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis lb . $(12 \times 12$ | Caliper, | Bursting Strength, | G.E. <br> Puncture, | $\begin{gathered} \mathrm{R} \\ \text { Com! } \end{gathered}$ | ehle ression, b. |  | ndorf <br> ear, heet | Amth | Tensile, /in. | Amtho | Stretch, \% |
|  | /1000) | 0.001 in . | points | units | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 45.4 | 15.9 | 121 | 44 | 35.5 | 24.1 |  |  |  |  |  |  |
| Minimum | 42.1 | 14.7 | 100 | 38 | 26.7 | 18.6 | 436 | 506 430 | 92.2 78.4 | 383 | 2.6 | 5.3 |
| Average | 43.5 | 15.3 | 109 | 41 | 30.9 | 21.8 | 408 | 430 | 78.4 85.4 | 35.1 | 2.0 | 4.1 |
| Standard deviation | 0.874 | 0.290 | 4.91 | 1.46 | 2.19 | 1.8 1.25 | 408 | 465 18.7 | 85.4 3.66 | 36.8 0.996 | 23 0.179 | 4.5 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 15.8 7.5 | 18.7 | 3.66 1.5 | 0.996 | 0.179 | 0.287 |
| Approximate probability, \% | 43 | 99 | 39 | 50 | ${ }^{1.0}$ | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Range limit ( t )* | 1.0 | 2.0 | ${ }^{39} 5$ | ${ }^{50}$ |  | 58 | 36 | 31 | 32 | 68 | 42 | 52 |
| Approximate probability, \% | 75 | 100 | 69 | 1.5 | 1.5 50 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Range limit ( $\pm$ )* | 2.0 |  | 6 |  |  |  | 66 | 58 | 59 | 95 | 74 | 8.4 |
| Approximate |  |  |  | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| probability, \% | 98 | - | 87 | 96 | 83 | 98 | 94 | 89 | 83 | 99 | 91 | 96 |

TABLE XXXIII
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER ḰRAFT LINER
Mile J
Roll Averages

|  |  | Date | Basis Weight lb. $(12 \times 12$ | Caliper, $0.001$ | $\begin{aligned} & \text { Appar- } \\ & \text { ent } \end{aligned}$ | Mois- | Bursting Strength, | G.E. <br> Punc | $\begin{array}{r} \mathrm{Ri} \\ \mathrm{Comp} \end{array}$ | ression, <br> lb. |  | endorf ${ }^{--}$ <br> car, <br> sheet | A Ten lb. | thor ${ }^{*}$ sile, /in. |  | mthor etch, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Roll | Manuf. | /1000) | in. | $\mathrm{lb} / \mathrm{cu} . \mathrm{ft}$. | $\%$ | points | units | In | Across - | In | Across | In | Across | In | Across |
|  | 1 | 3-17-45 | 39.7 | 14.9 | 320 | 8.7 | 77 | 31 | 28.2 |  |  |  | In | Across |  | Across |
|  | 2 | 8-28-44 | 43.4 | 13.3 | 39.2 | 8.6 | 88 | 31 | 27.2 | 24.9 | 320 | 339 | 591 | 383 | 1.9 | 31 |
|  | 3 | 3-15-45 | 41.9 | 15.4 | 32.6 | 7.6 | 97 | . 34 | 28.9 | 21.6 23.8 | 288 319 | 344 | 70.6 | 34.3 | 17 | 2.8 |
| - | 4 | 3-15-45 | 41.5 | 15.3 | 32-5 | 8:4 | 99 | -34 | 28.9 29.5 | 23.8 24.1 | 319 324 | 378 | -76.5 | .38.2. | -2 | - 2.8 - |
|  |  |  |  | 14.6 | $33.8{ }^{\prime}$ | 8.1 | 82 | 29 | 30.2 | 22.4 | 277 | 334 | 75.5 | 38.2 | 2.0 | 27 |
|  | 6 | 2-2-45 | 41.4 | 15.2 | 32.7 | 8.4 |  | 28 |  |  |  |  | 68.8 | 34.4 | 1.6 | 2.4 |
|  | 7 | 2-20-45 | 41.2 | 146 | 33.9 | 8.0 | 8.3 | 31 | 30.0 | 24.1 | 2.47 | 294 | 64.2 | 33.5 | 2. | 24 |
|  | 8 | 2-20-45 | $40^{-5}$ | - 14.0 | 347 |  | 82 |  | 32.9 30.4 | $-22.6$ | 288 | 324 - | 69.2 | 32.0 | 20 | - $3.0{ }^{-}$ |
|  | 9 | 2-9-45 | 41.7 | 14.5 | 34.5 | ..5.7 ${ }^{\prime}$ | + 79 | 29 | -30.4 | 23.4 | 274 | 313. | 68.5 | 33.1 | 2.1 | 3.3 |
|  | 10 | 2-9-45 | 405 | 14.7 | 33.1 | 4.6 | + 78 | 28 | 32.2 29.0 | 22.7 24.3 | 236 | $291^{*}{ }^{-}$ | 68.2 | 33.6 | 1.9 | 31 |
|  | 11 | 2-25-45 | 41.9. | 15.2 | 33:1 | 7.7 |  |  |  |  | 214 | 276 | 66.8 | 34.1 | 2.0 | 25 |
|  | 12 | 4-1-45 | 42.1 | 152 | 33.2 | 6.0 |  | 34 | 30.6 | 22.7 | 290 | 370 | 75.7 | 34.3 | 2.0 | 3.0 |
|  | 13 | 4-1-45 | 41.9 | 15.1 | 33.3 | 6.0 7.5 | 83 92 | 30 30 | 29.9 31.7 | 248 | 301 | 352 | 68.6 | 34.7 | 20 | 2.3 |
|  | 14 | 4-1-45 | 41.5 | 14.9 | 33.4 | 6.2 | 87 | 30 | 31.7 29.4 | 24.9 24.2 | 298 | 331 | 67.5 | 38.6 | 2.0 | 3.0 |
|  | 15 | 2-23-45 | 41.7 | 14.9 | 33.6 | 8.2 | 100 | 30 | 29.4 | 24.2 | 302 | 339 | 69.2 | 36.6 | 18 | 2.9 |
|  | 16 | 2-25-45 | 41.2 | 14.9 | 33.2 | 7.4 |  |  |  |  |  | 38 | 77.8 | 36.9 | 2.3 | 3.2 |
|  | 17 | 3-3-45 | 42.7 | 14.6 | 35.1 | 8.4 | 103 | 30 | 31.7 | 24.3 | 318 | 361 | 80.0 | 36.2 | 2.2 | 3.1 |
|  | 18 | 3- 3-45 | 42.8 | 14.5 | 35.4 | 8.4 6.5 | 111 | 39 38 | 31.2 | 23.7 | 362 338 | 423 | 92.2 | 37.2 | 2.4 | 4.3 |
|  | 19 | 3. 3-45 | 42.2 | . 14.1 | 35.9. | .9.4. | -109 | .38 | 31.1 30.5 | 23.3 | 338 | 403. | 92.0 | 37.8 | 2.3 | 4.4 |
|  | 20 | 3-3-45 | 42.4 | 14.0 | 36.3 | 7.2 | 105 | 38 | 30.5 | 24.2 | 331 | $40)^{*}$ | 84.3 | 36.4 | 2.2 | 4.2 |
|  | 21 | 3-3-45 | 42.2 | 14.1 | 35.9 |  |  |  |  |  | 344 | 2 | 85.8 | 36.1 | 2.3 | 4.3 |
|  |  |  |  |  |  | 10 | 108 | 38 | 30.3 | 23.5 | 338 | 412 | 90.8 | 39.3 | 2.2 | 4.1 |
| . | Average |  | 41.7 | 14.7 | 34.2 | 7.7 | 93 | 32 | 30.4 | 23.7 | 301 | 355 | 74.8 | 35.9 | 2.0 | $3.2{ }^{1}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

TABLE XXXIV
S'́atistical evaluation of physical tests on 42-Lb. D.f.b.S. FOURDRINIER Kraft liner

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis Weight, lb $(12 \times 12$ | Caliper, | Bursting Strength, | G F. <br> I'uncture, | $\underset{\operatorname{ComI}}{\mathrm{R}}$ | $\begin{aligned} & \text { eble } \\ & \text { ression, } \end{aligned}$ |  | ndorf <br> ar, heet | Amtho | Tensile, in. | Amtho | Stretch, <br> \% |
| Test values | /1000) |  | points | units | In | Across | - In | Across | In. $\cdot$ | Across | In | Across |
| Maximum | 43.4 | 15.4 |  |  |  |  |  |  |  |  |  |  |
| Minimum | 39.7 | 13.3 | 177 | 39 | 33.4 | 24.9 | 362 | 423 | 92.2 | 39.3 | 2.4 |  |
| Average | 41.7 | 14.7 | 93 | 28 | 27.9 | 21.6 | 214 | 276 | 59.1 | 32.0 | 1.6 | 2.4 |
| Standard deviation | 0.845. | 0.532 | 11.7 | 3.69 | 30.4 | 23.7 | 301 | 355 | 74.8 | 35.9 | 2.0 | 3.2 |
| Range limit ( $\pm$ )* | 0.5 | . 0 | 2.5 | 1.6 | 1.43 | . 92 | 37.1 | 42.1 | 9.54 | 2.11 | 0.204 | 0.673 |
| Approximate |  | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| probability, \% | 44 | 94 | 17 | 21 |  |  |  |  |  |  |  |  |
| Range limit ( $\pm$ )* | 1.0 | 2.0 | 5.0 |  | 52 | 72 | 16 | 14 | 13 | 36 | 38 | 24 |
| Approximate |  |  | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| probability, \% | 76 | 99 | 33 |  |  |  |  |  |  |  |  |  |
| Range limit ( $\pm$ )* | 2.0 |  | 7.5 |  | 3.0 |  |  |  | 24 | 66 | 67 | 44 |
| Approximate |  | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| probability, \% | 98 | - | 48 | 58. | 96 | 99 | 58 | 52 | 40 | 84 | 86 | 63 |
| * Range limits were arbitrarily selected. |  |  |  |  |  |  |  |  |  |  |  |  |

be seen in Table XXXII. The standard deviation for the basis weight is of such magnitude that it should be expected that approximately $43 \%$ of all the rolls manufactured by Mill I should fall within a basis weight range limit of $\pm 0.5$ pound ( 43.0 to 44.0 pounds), $75 \%$ within the range limit of $\pm 1.0$ pound $\left(42.5^{\prime}\right.$ to 44.5 pounds), and approximately $98 \%$ within the range limit of $\pm 2.0$ pounds ( 41.5 to 45.5 pounds). On the basis of the results obtained for caliper, it should be expected that approximately all the rolls should fall within a caliper range limit of $\pm 0.001$ inch ( 0.0143 to 0.0163 inch ). The statistical evaluation of the results obtained for the bursting strength indicate that approximately $39 \%$ of the rolls should fall within a range limit of. $\pm 2.5$ points ( 106.5 to 111.5 points), approximately $69 \%$ within the range limit of $\pm 5.0$ points (104 to 114 points), and approximately $87 \%$ within the range limit of $\pm 7.5$ points ( 101.5 to 116.5 points). The results obtained indicate that, in terms of percentage, the rolls made by this mill should be slightly more uniform in respect to G. E. puncture than to bursting strength. The results of the Riehle compression, El-mendorf tear, and Amthor tensile and stretch indicate standard deviations of considerable magnitude.

## Mile J

The average test results obtained for the rolls of liner made by Mill J are given in Table XXXIII (see also Table LXX of the Appendix). The average basis weight obtained is practically the same as the specified
grade weight. The average caliper was 0.0147 inch and the average apparent density was 34.2 pounds per cubic foot. The average bursting strength and G. E. puncture values were 93 points and 32 units, respectively. The average moisture content was $7.7 \%$ on an ovendry básis.

The statistical evaluation of these results are reported in Table XXXIV. The magnitude of the standard deviation for basis weight indicates that approx:mately $44 \%$ of the rolls manufactured by Mill J should fall within_a_basis. weight range_limit of $\pm 0.5$ pound ( 41.2 to 42.2 pounds), approximately $76 \%$ within the range limit of $\pm 1.0$ pound ( 40.7 to 42.7 pounds) and approximately- $98 \%$ within - the - range limit of $- \pm 2.0$ pounds. ( 39.7 to 43.7 pounds). The results obtained for caliper indicate that approximately $94 \%$ of the rolls should fall within a caliper range limit of $\pm 0.001$ inch ( 0.0137 to 0.0157 inch). The standard deviation for the bursting strength is of such magnitude that it should be expected that approximately $17 \%$ of the rolls manufactured by Mill J should fall within a range limit of $\pm 2.5$ points ( 90.5 to 95.5 points), approximately $33 \%$ should fall within the range limit of $\pm 5.0$ points ( 88.0 to 98.0 points), and approximately $48 \%$ within the range limit of $\pm 7.5$ points ( 85.5 to 100.5 points). The statistical evaluation of the Riehle compression values indicates a rather low probable variation, whereas the results obtained for G. E: puncture, Elmendorf tear, Amthor tensile and stretch indicate considerable probable variation.

## EVALUATION OF THE PHYSICAL CHARACTERISTICS OF .009/26-LB. KRAFT AND BOGUS CORRUGATING MEDIUMS

## PROCEDURE

The tests and procedures employed throughout this evaluation study have been described on pages 8 to 10.

For the purpose of comparison of the characteristics of the product within a given mill and also between mills, each Fourdrinier Kraft Board Institute mill which makes $.009 / 2 \overline{6}-\mathrm{lb}$. corrugating medium has been given an arbitrarily selected code letter; they have been identified in this report by the letters $S$ to $Z$, inclusive. The corrugating medium manufactured by Mill V was a bogus medium. Consequently, the group averages have been calculated in two ways: (1) including the bogus medium and (2) excluding the bogus medium.

The test results have been given the same statistical treatment as was employed in the treatment of the 42-lb. liner.

## COMPARISON OF MILL AVERAGES

The results of the various physical tests performed on samples of $.009 / 26-\mathrm{lb}$. corrugating medium have been compiled in Table XXXV on the basis of mill averages. Complete details of the individual tests are given in Tables LXXI-LXXVIII of the Appendix.

The average results obtained for basis weight are shown graphically in Figure 16. The average basis weight for the group participating was 26.8 pounds including and 26.9 pounds excluding the bogus medium. Both of these group averages are in excess of the grade weight specified. Mill X had the highest average basis weight and Mill $V$ the lowest. The basis weight averages for all the mills were within $\pm 1$ pound of the group average.

The average caliper results are plotted in Figure 17. The average caliper value for the group was 0.010 inch, regardless of whether or not the bogus medium was included. Mill $U$ had the highest average caliper and Mills Y and Z the-lowest. All- the individual mill averages for caliper were within $\pm 0.0007$ inch of the group average caliper.

The average apparent densities, in pounds per cubic foot, are pictured graphically in Figure 18. The group average apparent density when the bogus medium was included was 32.3 pounds per cubic foot and 32.5 pounds per cubic foot when it was not included. The highest average apparent density was obtained for Mill Z and the lowest for Mill U. It is interesting to note that the mill averages for apparent density varied over a considerable range.

From the data graphically presented in Figure 19, it may be observed that the average moisture content for the group was $9.4 \%$ including the bogus medium and $9.5 \%$ when the bogus medium was not included. Mill $T$ had the highest average moisture content and Mill U the lowest. Two of the mills ( T and W ) had average moisture values in excess of $11 \%$.
From the data presented in Figure 20, it is seen that the a verage bursting strength for the group, including the bogus medium, was 62 points; it was 66 points when the bogus was not included. The bursting strength, expressed in points per pound basis weight, was 2.31 when the bogus was included and 2.45 when the bogus was not included. The highest mill average bursting strength was obtained for Mill Z and the lowest for Mill V (the bogus medium). The average bursting strength for the bogus medium was approximately $50 \%$ of the average bursting strength obtained for the other mills.

TABLE XXXV
COMPARISON OF PIIYSICAL CHARACTERISTICS BETWEEN MILLS

|  |  |  |  |  |  |  | orruga | ng Me | num |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Basis Weight lb. | Caliper, | Apparent | Mois- | $\begin{aligned} & \text { Burst- } \\ & \text { ing } \end{aligned}$ | $\begin{aligned} & \text { G.E. } \\ & \text { Punc- } \end{aligned}$ | $\begin{array}{r} \mathrm{Ri} \\ \text { Comp } \end{array}$ | chle ression, b. |  | ndorf <br> ar, <br> heet |  | nthor nsile, ./in. |  | thor <br> ch, \% |
| Mill | Tested | /1000) |  | lb./cu.ft. | \% | points | units | In | Across | In | Across | In | Across | In | Across |
| S | 10 | 27.3 | 10.1 | 32.4 | 8.5 | 68 | 20 | 19.5 | 15.5 | 268 | 276 | 52.3 | 30.4 | 1.6 | 4.7 |
| T | 10 | 27.0 | 10.0 | 32.5 | 11.8 | 57 | 20 | 15.9 | 12.8 | 237 | 261 | 45.1 | 24.2 | 1.8 | 3.7 |
| U | 21 | 26.9 | 10.7 | 30.2 | 8.4 | 65 | 20 | 19.7 | 13.5 | 238 | 266 | 53.0 | 25.7 | 2.0 | 4.8 |
| V | 13 | 25.8 | 10.1 | 30.7 | 9.2 | 32 | 11 | 12.9 | 10.3 | 121 | 134 | 31.0 | 17.2 | 1.4 | 2.4 |
| w | 13 | 26.8 | 10.1 | 31.8 | 11.1 | 69 | 19 | 17.7 | 11.5 | 228 | 300 | 56.6 | 21.8 | 2.1 | 3.8 |
| x | 14 | 27.4 | 9.8 | 33.7 | 8.7 | 68 | 21 | 17.1 | 13.1 | 250 | 281 | 52.1 | 25.3 | 2.1 | 4.3 |
| Y | 10 | 26.0 | 9.3 | 33.9 | 9.7 | 58. | 15 | 17.3 | 12.3 | 189 | 219 | 50.7 | 22.1 | 2.0 | 3.6 |
| Z | 11 | 26.8 | 9.3 | 34.7 | 9.1 | 75 | 20 | 19.9 | 15.8 | 251 | 262 | 53.8 | 33.0 | 2.0 | 4.7 |
| Group Average* 26.8 |  |  | 10.0 | 32:3 | 9.4 | 62 | 18 | 17.6 | 13.0 | 223 | 251 | 49.5 | 24.8 | 1.9 | 4.0 |
| Group Average $\dagger 26.9$ |  |  | 10.0 | 32.5 | 9.5 | 66 | 19 | 18.3 | 13.4 | 238 | 268 | 52.2 | 25.9 | 2.0 | 4.3 |
| * Including bogus from Mill V. <br> $\dagger$ Excluding bogus. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



Figure 16. Comparison of the average basis weight of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figure 17. Comparison of the average caliper of $.009 / 26-\mathrm{fb}$. corrugating medium among mills.
(Because the averages were calculated to the nearest tenth only, the average value of the caliper was the same when the bogus samples were excluded as when they were included.)


* INCLUDING BOGUS
**EXCLUDING BOGUS
Figure 18. Comparison of the average apparent density of $.009 / 26 \cdot \mathrm{lb}$. corrugating medium among mills.


Figure 19. Comparison of the average moisture content of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figure 20. Comparison of the average bursting strength of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figurf. 21. Comparison of the average General Electric puncture test of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figure 22. Comparison of the average Riehle compression test of $.009 / 26-1 \mathrm{~b}$. corrugating medium among mills.


Figure 23. Comparison of the average Elmendorf tear of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figure 24. Comparison of the average Amthor tensile strength of $.009 / 26-\mathrm{lb}$. corrugating medium among mills.


Figure 25. Comparison of the average Amthor stretch of . 009/26-1b. corrugating medium among mills.

The mill averages obtained for the C . E. puncture test are graphed in Figure 21. Because the magnitude of these results was so low that all the values fell on the extreme lower range of the indicating scale for the tester, it is doubtful if much significance can be attached to them at this time.

The average Richle compression test results are shown graphically in Figure 22. The group average was 17.6 pounds in the in-machine direction and 13.0 pounds for the across-machine direction when the bogus was-included but were 18.3 and 13.4 pounds, respectively, when the bogus medium was not included. The highest mill average was obtained for Mill $\%$ and the lowest for Mill V (the bogus medium). The across-machine direction group average, excluding the bogus medium, was approximately $3.7 \%$ greater than the in-machine direction average for the bogus medium. The ratio of the across-machine direction valucs to the in-machine direction values was, on the average, of the order of $3: 4$.

The results of the Elmendorf tear test are graphically presented in Figure 23. The group averages for each direction were 223 and 251 grams per sheet, respectively, when the bogus medium was included, and 238 and 268 grams per sheet, respectively, when the bogus medium was excluded. The highest average tear value in the in-machine direction was obtained for Mill $S$ but Mill W had the highest average tear in the acrossmachine direction. Mill $V$ had the lowest mill average tear values in both directions. The ratio of the in-machine direction values to the across-machine direction values was, in general, of the 'order of 0.9:1.

The results of the Amthor tensile test are shown graphically in Figure 24. The group averages obtained (including the bogus medium) were 49.5 and 24.8 pounds per inch width for the in-machine direction and the across-machine direction, respectively, and 52.2 and 25.9 pounds per inch width, respectively, when the bogus medium was excluded. The results indicate that Mill W had the highest average tensile value in the in-machine direction and Mill $Z$ the highest across-
machine tensile average, whereas Mill $V$ had the lowest average tensile strength for both directions. The average ratio of across-machine direction to in-machine direction was of the order of $1: 2$.

The Amthor stretch results are presented graphically in Figure 25. The group averages for the in-machine and across-machine direction stretch were 1.9 and $4.0 \%$, respectively, when the bogus medium was included, and 2.0 and $4.3 \%$, respectively, when the bogus medium was excluded. Mill $V$ had the lowest average stretch in both directions tested. The average ratio of the in-machine direction stretch to the across-machine direction was of the order of $1: 2$.

A comparison of all the strength test results indicates that the averages for Mill $Z$ were the highest and those for Mill $V$ the lowest of the group.

The standard deviations of the physical characteristics of the corrugating medium made by each mill may be seen in Table XXXVI. The results indicate that the corrugating medium of Mill S had a lower composite average standard deviation for all the tests performed than those of the other mills. It would appear, therefore, that the corrugating medium of Mill S was more uniform than the products of the other mills on the basis of this evaluation. A comparison of the group average percentage standard deviations for the various test characteristics indicates that basis weight and caliper were the least variant and Amthor stretch the most variant of all the test characteristics studied.

The average test results tabulated in Table XXXV were treated statistically to determine if there was any significant difference between the average physical characteristics obtained for a given mill and the group average physical characteristics obtained for the balance of the mills participating. Whether or not a significant difference exists in a given test characteristic between two mills or groups of mills is denoted by the magnitude (see page 24) of the ratio of the difference of the means of each mill or group to the standard error of the difference between the same two mills or groups. In this work it has been assumed that all ratios of 2 or more indicated significant differences.

TABLE XXXVI
COMPARISON OF STANDARD DEVLATIONS BETWEEN MILLS

| Corrugatina Medium |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| der | Basis |  | Bursting | G.E. | Richle Compression, lb. |  | Elmendorf Tear, g. /sheet |  | Amthor Tensile, lb./in. |  | Amthor <br> Stretch, \% |  |
| Mill | Weight, lb. | Caliper, 0.001 in . | Strength, points | Puncture, units | In | Across | In | Across | In | Across | In | Across |
| S | 0.328 | 0.301 | 291 | 0.843 | 0.783 | 0.810 | 14.8 | 119 | 2.92 | 1.70 | 0.103 | 0276 |
| - T | 1.350 | 0.827 | 6.89 | 1.62 | 1.34 | 0.932 | 28.6 | 30.7 | 4.21 | 2.23 | 0.155 | 0536 |
| U | 0.903 | 0.645 | 5.18 | 1.46 | 1.76 | 0.974 | 18.6 | 17.5 | 4.34 | 3.57 | 0.281 | 0.447 |
| $V$ | 0.889 | 0.341 | 3.64 | 1.45 | 1.17 | 1.01 | 18.7 | 18.7 | 3.70 | 2.72 | 0.224 | 0.249 |
| W | 0.910 | 0.692 | 4.54 | 1.17 | 1.62 | 0.740 | 15.2 | 17.7 | 3.69 | 0.872 | 0.350 | 0.440 |
| X | 0.881 | 0.507 | 3.14 | 1.78 | 1.25 | 0.941 | 22.9 | 24.8 | 4.88 | 2.61 | 0.133 | 0.851 |
| Y | 0.746 | 0.47 .4 | 11.0 | 2.10 | 2.80 | 1.61 | 20.8 | 25.9 | 4.90 | 2.83 | 0.157 | 0.488 |
| \% | 0.522 | 0.366 | 5.21 | 1.03 | 1.59 | 1.22 | 17.1 | 24.6 | 3.86 | 2.65 | 0.155 | 0.659 |
| Averatge | 0.816 | 0.519 | 5.31 | 1.43 | 1.54 | 1.03 | 19.6 | 21.5 | 4.06 | 2.40 | 0.195 | $0.493{ }^{\circ}$ |
| Average standard deviation, \% | 3.0 | 5.2 | 8.6 | 7.9 | 88 | 7.9 | 8.8 | 8.6 | 8.2 | 9.7 | 10.3 | 12.3 |
|  |  |  |  |  |  | 54 |  |  |  |  |  |  |

The application of this treatment to a comparison of the average results obtained for Mill S with the averages obtained for the group ' $T$ to $\%$, inclusive, may be seen in Table XXXVII. The results obtained indicate that, when the average test values of Mill $S$ are compared with the group average of Mills $\dot{\Gamma}$ to $Z$, there is a significant difference in all the test values obtained, except for the Amthor tensile in the across-machine direction. With the exception of Amthor stretch in the in-machine direction, all the average test values exhibiting significant differences were of a greater magnitude than the corresponding group values. Thus, the quality for Mill S , as determined by these tests, was significantly greater than the average quality for the group.

The results obtained when the averages for Mill 'T are compared with the average of the balance of the group may be seen in Table XXXVIII. The results indicate that there was a significant difference in all the test values except basis weight, caliper, Elmendorf tear, Amthor tensile in the across-machine direction, and Richle compression in the across-machine direction. With the exception of the average G. F. puncture value, all the test values having significant differences for Mill T were of a lower magnitude than the corresponding values for the balance of the group.

A comparison of the average values obtained for Mill $U$ with the group average excluding $U$ is presented in Table XXXIX. The results indicate that there was a significant difference in all the test values except those for basis weight and Richle compression and Amthor tensile tests in the across-machine direction. All the test values in which a significant difference existed were of a greater magnitude than the corresponding group average values.

The results of the comparison of the average test results obtained for Mill $V$ with the average test results obtained for the remainder of the group participating are given in Table XL. It may be observed that the caliper value was the only test characteristic for which a significant difference was not indicated between it and the corresponding group characteristic. All the test values for Mill V in which a significant difference was indicated were of a lower magnitude than the corresponding test values for the group.

The results of the comparison of the average test results obtained for Mill $W$ with the average test results obtained for the balance of the group are shown in Table XLI. Significant differences existed in all the test results except basis weight, caliper, Riehle compression and Elmendorf tear in the in-machine direction, and Amthor stretch in the across-machine direction.

The results obtained when the average test values for Mill $X$ were compared with the average values of the balance of the group are presented in Table XLII. The only test values in which a significant difference did not exist were caliper, Amthor tensile and stretch in the across-machine direction, and Richle compression. Similarly, all the significant values for Mill X
were greater than the average values obtained for the group.

The average test values obtained for Mill Y, and the average test results obtained for the balance of the group are given in Table XLIII. The test values in which no significant difference was indicated are bursting strength, Richle compression in both directions, and Amthor tensile in the in-machine direction. With the exception of Amthor stretch in the inmachine direction all the significant test values obtained for Mill Y were of a lower magnitude than the corresponding test values for the group.

The average test values for Mill $Z$ and the average values for the balance of the group are given in Table XLIV. The results indicate that a significant difference exists for all the test values except for basis weight and for Elmendorf tear in the across-machine direction. With the exception of caliper, all the test values for Mill \% in which a significant difference exists were of a greater magnitude than the corresponding group values.

## DISCUSSION OF INDIVIDUAL MILL TEST RESULTS FOR .009/26-LB. CORRUGATING MEDIUMS

## Mile S

The average results of the various physical tests conducted on samples of $.009 / 26-\mathrm{lb}$. kraft corrugating medium made by Mill S are shown in Table XLV (see also Table LXXI of the Appendix). It may be observed that the average basis weight was higher than the specified grade weight. The average caliper was 0.0101 in ch and the average apparent density was 32.4 pounds per cubic foot. The average bursting strength was 68 points. The average Riehle compression was 19.5 and 15.5 for the in- and across-machine directions, respectively. The average moisture content was $8.5 \%$ on an ovendry basis.

Table XLVI gives the standard deviations and the probable variation to be expected in the rolls of .009/26-lb. corrugating medium made by Mill S. These results show that the chance probability or uniformity for Mill S as regards basis weight is such that approximately $87 \%$ of the corrugating rolls 'should fall within a range limit of $\pm 0.5$ pound ( 26.8 to 27.8 pounds) and practically all the rolls should fall within a range limit of $\pm 1.0$ pound ( 26.3 to 28.3 pounds). The standard deviation of the caliper results indicates that the greater portion of the rolls should fall within a range limit of $\pm 0.001$ inch ( 0.0091 to 0.0111 inch). The uniformity of the bursting strength indicates that $61 \%$ of the rolls should fall within a range limit of $\pm 2.5$ points ( 65.5 to 70.5 points), $91 \%$ within the range limit of $\pm 5.0$ points ( 63 to 7.3 points), and practically all the rolls within the range limit of $\pm 7.5$ points ( 60.5 to 75.5 points). The standard deviation for the Richle compression is such that it should be expected that approximately $80 \%$ of the rolls should fall within a

COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL S WITH THE BALANCE OF THE GROUP
... Corrugating Medium

| Mean of $S$. <br> Mean of $\alpha^{\prime \prime}$. <br> Difference of mean $(S-\alpha)$ | Basis Weight,$\frac{-1 \mathrm{~b} \ldots}{(12 \times 12}$ |  | Bursting Strength, points | G.E. <br> Punc-ture, units | Riehle Compression, ....lb... . |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, . - lb./in.. |  | Amthor Stretch, \% |  | - $\quad$. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0.001 in . |  |  | In | Across | In | Across | In | Across | In | Across |  |  |
|  | 27.3 | 10.1 | 68 | 20 | 19.5 | 15.5 | 268 | 276 | . 523 | 30.4 | 1.6 | 4.7 |  |  |
|  | 26.7 | 9.9 | 61 | 18 | 17.2 | 12.7 | 216 | 246 | 48.9 | 24.2 | 1.9 | 3.9 |  |  |
|  | +0.63 | +0.24. | $+7.8$ | +2.5 | +2.25 | +2.74 | $+51.9$ | $+30.0$ | $+3.40$ | +6.17 | -0.29 | $+0.86$ |  |  |
| Standard error of difference | 0.143 | 0.114 | 1.15 | 0.315 | 0.312 | 0.283 | 5.19 | 4.55 | 1.03 | 0.604 | 0.0398 | 0.105 |  |  |
| Ratio: $(S-\alpha) / S E_{D}$ | +4.4 | +2.1 | $+6.8$ | $+7.9{ }^{\prime}$ | +7.2 | +9.7 | $+10.0$ | +6.6 | $+3.3$ | +1.0 | $-7.3$ | $+8.2$ |  |  |
| $\therefore$ Significant . | ' 'es. | YYes.. | Yes | _res | Yes . |  | Yes | Yes | Yes | No | Yes. | Y'es |  |  |

Note, All mean values have been reported to the same precision as individual test values. It will be observed that some of the intermediate values in the above table have been reported to more places than the mean values. Similarly the difference of the means will not always correspond to the difference between reported means, because these values have been rounded off. The mean of $\alpha$ is the mean for the balance of the group.

TABLE XXXVIII COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL T WITH THE bALANCE OF THE GROUP

|  | $\begin{aligned} & \text { Basis } \\ & \text { Weight, } \\ & \text { lb. } \\ & (12 \times 12 \\ & / 1000) \end{aligned}$ | Bursting Caliper, Strength, 0.001 in . points |  | Corrugating Medium |  |  |  |  | Amthor Tensile, 1b./in. |  | 'Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | G.E. Punc- | $\begin{aligned} & \text { Riehle } \\ & \text { Compression, } \\ & \text { lb. } \end{aligned}$ |  | Elmendorf Tear, g./sheet |  |  |  |  |  |
|  |  |  |  | units | In | Across | In | Across | In | Across | In | Across |
| Mean of $T^{\text {* }}$ | 27.0 | 10.0 | 57 | 20 | 15.9 | $12: 8$ | 237 | 261 | 45.1 | 24.2 | 1.8 | 3.7 |
| Mean of $\alpha$ | 26.7 | 9.9 | 62 | 18 | 17.7 | 13.1 | 221 | 248 | 49.9 | 25.1 | 1.9 | 4.0 |
| Difference of mean ( $T-\alpha$ ) | +0.31 | ${ }^{+}+0.09$ | -5.0 | +1.8 | -1.81 | -0.33 | +16.1 | +12.6 | -4.79 | -0.84 | -0.11 | -0.38 |
| Standard error of difference | 0.433 | 0.266 | 2.27 | 0535 | 0.462 | 0.318 | 9.26 | . 9.96 | - 1.40 | 0.753 | 0.0538 | 0.178 |
| Ratio: $(T-\alpha) / S E_{D}$ | +0.7 | +0.3 | -2.2 | +3.4 | -3.9 | -1.0 | +1.7 | +1.3 | -3.4 | -1.1 | -2.0 | -2.1: |
| Significant | No. | No | Yes | Yes | Yes | No | No | No | Yes | No | Yes | Yes |

TABLE XXXIX
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL U WITH THE BALANCE OF THE GROUP

| Corrugating Medium |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis Weight, lb . $(12 \times 12$ /1000) | Caliper, 0.001 in . | Bursting Strength, points | G.E. <br> Puncture, units | Riehle Compression, lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, $\mathrm{lb} . / \mathrm{in}$. |  | Amthor Stretch, \% |  |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $U$ | 26.9 | 10.7 | 65 | 20 | 19.7 | 13.5 | 238 | 266 | 53.0 | 25.7 | 2.0 | 4.8 |
| Mean of $\alpha$ | 26.7 | 9.8 | 61 | 18 | 17.2 | 13.0 | 221 | 247 | 48.8 | 24.8 . | 1.9 | 3.9 |
| Difference of mean $(U-\alpha)$ | $+0: 16$ | +0.91 | $+4.0$ | $+1.9$ | +2.47 | $+0.47$ | +17.5 | +18.6 | +4.16 | +0.87 | $+0.13$ | +0.92 |
| Standard error of difference | 0:219 | 0.153 | 1.33 | 0.359 | 0.426 | 0.245 | 4.66 | 4.61 | 1.05 | 0821 | 0.0650 | 0.114 |
| Ratio: $(U-\alpha) / S E_{I}$, | +0.7 | +5.9 | +3.0 | $+5.3$ | +5.8 | +1.9 | +3.8 | $+4.0$ | $+4.0$ | +1.1 | $+2.0$ | +8.1 |
| Significant | No | Yes | Yes | Yes | Yes | No | Yes | - Yes. | Yes | No | Yes | Yes |

Note: See Note to Table XXXVII.

TABLE XL
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILIV WTTH THE BALANCE OF THE GROUL
Corrugating Medium

|  | Basis Weight, lb. |  | Bursting | G.E. I'unc- | $\underset{\substack{\text { Ric } \\ \text { Compr }}}{\text { R }}$ | ehle ression, b. - |  | endorf ear, sheet | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | /1000) | 0.001 in | points | units | In | Across | In | Across | In | Across | In | Across |
| Mean of $V$ | 25.8 | 10.1 | 32 | 11 | 12.9 | 10.3 | 121 | 134 | 31.0 | 17.2 | 1.4 | 2.4 |
| Mean of $\alpha$ | 26.9 | 9.9 | 66 | 19 | 18.2 | 13.5 | 237 | 266 | 51.9 | 26.1 | 1.9 | 4.2 |
| Difference of mean . $(V-\alpha)$ | $-1.11$ | +0.20 | --33.4 | -7.8 | $-5.20$ | -3.21 | $-116.6$ | -132.3 | $-20.92$ | -8.90 | -0.52 | -1.84 |
| Standard error of Difference | 0.264 | $\bigcirc .11 \overline{3}$ | $1.23{ }^{-}$ | 0.433 | 0.373 | 0.305 | 5.65 | 5.78 | 1.12 | . 0.799 | -0.0658 | 0.091 |
| Ratio: ( $V-\alpha$ )/ $/ S E_{D}$ | -4.2 | +1.8 | -27.2 | -18.0 | -13.9 | $-10.5$ | -20.6 | -22.9 | -18.7 | -11.1 | -7.9 | -2.0 |
| Significant | Yes | No | Y'es | Yes | Yes | Yes | Yes | Yes | Yes | Yes. | ..Yes | - Yes |

TABLE XLI
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL W WITH THE BALANCE OF THE GROUP

|  | Basis Weight, lb. ( $12 \times 12$ /1000) | Corrugating Medium |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Caliper, 0.001 in | Bursting Strength, points | G.E. <br> Puncture, units | Riehle Compression, lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $\mathrm{W}^{\prime}$ | 26.8 | 10.1 | 69 | 19 | 17.7 | 11.5 | 228 | 300 | 56.6 | 21.8 | 2.1 | 3.8 |
| Mean of $\alpha$ | 26.7 | 9.9 | 61 | 18 | 17.5 | 13.3 | 222 | 243 | 48.3 | 25.4 | 1.8 | 4.0 |
| Difference of mean $(W-\alpha)$ | +0.08 | +0.17 | +8.0 | +1.1 | +0.17 | -1.79 | +5.7 | +57.3 | +8.31 | -3.57 | +0.25 | -0.24 |
| Standard error of difference | 0.269 | 0.200 | 1.43 | 0.364 | 0.484 | 0.239 | 4.79 | 5.52 | 1.12 | 0.371 | 0.0988 | 0.135 |
| Ratio: ( $W-\alpha$ ) $/ S E_{D}$ | +0.3 | +0.8 | +5.6 | +3.0 | $+0.4$ | -7.5 | +1.2 | $+10.4$ | +7.4 | -9.6 | $+2.5$ | $-1.8$ |
| Signiticance | No | No | Yes | Yes | No | Yes | No | . Yes | Yes | Yes | Yes | No |

Note. See Note to Table XXXVII.

TABLE XLII
COMIPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL X WITH THE BALANCE OF THE GROUP
Corrugating Medium

|  | Basis Weight, lb. $(12 \times 12$ /1000) | Caliper, 0.001 in . | Bursting Strength, points | G. B. <br> Puncture, units | Riehle Compression, lb. |  | Elmendorf 'Tear, g./shect |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Mean of $X$ | 27.4 | 9.8 | 68 | 21 | 17.1 | . 13.1 | 250 | 281 | 52.1 | 25.3 | 2.1 | 4.3 |
| Mean of $\alpha$ | 26.7 | 9.9 | 61 | 18 | 17.6 | 13.1 | 219 | 245 | 48.9 | 24.9 | 1.9 | 4.0 |
| Difterence of mean $(X-\alpha)$ | +0.74 | $-0.13$ | +7.2 | $+2.7$ | -0.41 | $+0.02$ | +31.2 | +35.6 | $+3.19$ | +0.36 | +0.22 | +0.31 |
| Standard error of difference | 0.254 | 0.148 | 1.09 | 0.502 | 0.383 | 0.279 | 6.50 | 7.07 | 1.37 | 0.746 | 0.0421 | 0.233 |
| Ratio: $(X-\alpha) /$ SFib | $+2.9$ | -0.9 | +6.6 | +5.4 | $-1.1$ | +0.1 | +4.8 | +5.0 | +2.3 | +0.5 | $+5.2$ | $+1.3$ |
| Significant | Yes | No | Yes | Yes | No | No | Yes | Yes | Yes | No | les | No |

Nute. See Note to Table XXXVII.

## TABLE XLIII

COMPARLSON OF THE IHYSICAL CHARACTERISTICS OF MLLL Y WITH THE BALANCE OF THE GROUP


TABLE XLIV
COMPARISON OF THE PISYICAL, CHARACTERISTICS OF MILL, Z WITH THE BALANCE OF THE GROUP

|  |  |  |  |  | Corrug | ating Mf |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis Weight, lb. |  | Bursting | G.E. Punc- |  | hle ession, | Elme $\begin{gathered} \mathrm{Te} \\ \mathrm{~g} . / \mathrm{s} \end{gathered}$ | endorf car, sheet | Amtho | Tensile, /in. | Anit Stretch | thor <br> h, \% |
|  | /1000) | 0.001 in . | points | units | In | Across | In | Across | In | Across | In | Across |
| Mean of $Z$ | 26.8 | 93. | . 75 | 20 | 19.9 | 15.8 | 251 | $262 *$ | 53.8 | 33.0 | 2.0 | 4.7 |
| Mean of $\alpha$ | 26.8 | 100 | $60^{\circ}$ | - 18 | 17.2 | 12.7 | 219 | 248 | 48.7 | 23.8 | -1.9 | 3.9 |
| Difference of mean $(Z-\alpha)$ | -0.03. | $-0.73$ | +15.7 | +1.6 | $+2.79$ | +3.05 | +32.7 | +13.5 | +5.11 | +9.18 | +0.14: | +0.81 |
| Standard error of difference | 0.185 | 0¢126 | 1.71 | 0.352 | 0.512 | 0.386 | 5.61 | 7.80 | 1.25 | 0.841 | 0.0517 | 0.206 |
| Ratio: $(Z-\alpha) / S E_{D}$ | $-0.0$ | -5.8 | +9.2 | $+4.5$ | +5.4 | $+7.9$ | $+5.8$ | +1.7 | +4.1 | $+10.9$ | +2.7 | +3:9 |
| Significance | No | Yes | Yes | Yes | Yes | Yes | Yes | No | Yes | Yes | Yes | Yes |

Note. See Note to Table XXXVII.
range limit, in both directions, of $\pm 1.0$ pound and approximately $94 \%$ within a range limit of $\pm 1.5$ pounds. The uniformity with respect to G. E. puncture, Elmendorf tear, Amthor tensile and stretch may alsobe seen in Table XLVI. Naturally, as the arbitrarily selected limits increase, the greater is the portion of rolls falling within that range. The ranges used are purely arbitrary and are not intended as an attempt to specify acceptable limits of uniformity. The moisture content was not treated statistically because it was felt that secondary effects, such as warehouse storage conditions, might cause too great an effect to permit the legitimate application of statistics.

## Mile T

The average test results obtained for the kraft corrugating medium made by Mill T are shown in Table XLVII (sec also Table LXXII of the Appendix). The average basis weight obtained was 1 pound higher than
the specified weight. The average caliper was 0.010 inch and the average apparent density was 32.5 pounds per cubic foot. The average bursting strength value was 57 points. The average Richle compression values were 15.9 and 12.8 pounds for the in- and acrossmachine directions, respectively. The average moisture content was $11.8 \%$ on an ovendry basis.

The statistical evaluation of these test results may be seen in Table XLVIII. For basis weight, the standard deviation was 1.35 , indicating that $29 \%$ of the rolls made by Mill T should fall within a range limit of $\pm 0.5$ pound ( 26.5 to 27.5 pounds), $54 \%$ within a range limit of $\pm 1.0$ pound ( 26.0 to 27.0 pounds), and approximately $86 \%$ within a range limit of $\pm 2.0$ pounds (25.0 to 29.0 pounds). The standard deviation for caliper was 0.827 ; thus, approximately $77 \%$ of the rolls of corrugating medium made by Mill $T$ might be expected to fall within a range limit of $\pm 0.001$ inch (0.009 to 0.011 inch) and approximately $98 \%$ within a

TABLE XIV
PHYSICAL CIEARACTIERISJICS OF .009/26-LR. FOURDRINIER KRAF゙T CORRUGATING MEDIUM
Mill S
Roll Averages

| - |  | Basis Weight, lb. | Caliper, | Apparent | Mois- | Bursting | G.E: Punc- | R Comp | hle ression, b. |  | ndorf ar, heet | Am <br> Ten <br> lb. | thor sile, in. | $\underset{\text { Stret }}{\text { Am }}$ | thor <br> ch, \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roll | Date <br> Manuf. | $(12 \times 12$ | in. | Density, <br> $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | $\%$ | points | ture, | In | Across | In | Across | In | Across | In | Across |
| 1 | 2-7-45 | 27.5 | 9.6 | 34.4 | 3.4 | 72 | 21 | 19.5 | 148 | 250 | 268 | 56.8 | 27.9 | 1.7 | 4.6 |
| 2 | 2-7-45 | 27.8 | 9.9 | 33.7 | 6.2 | 66 | 20 | 21.2 | 15.6 | 253 | 270 | 57.2 | 289 | 1.8 | 5.1 |
| 3 | 2-7-45 | 27.6 | 9.7 | 34.1 | 6.4 | 64 | 20 | 19.7 | 14.3 | 250 | 269 | 539 | 28.5 | 1.7 | 5.1 |
| 4 | 2-6-45 | 27., | . 10.5 | 31.0. | 11.5 | 71 | 21. | 19.7 | -. 14.4 | 281 | - 260 . | ..49.7-+ | 30.1- | 1.6 | 4.8 |
| 5 | 2-6-45 | 27.3 | 10.3 | 31.8 | 9.6 | (6) | 21 | 19.8 | 15.2 | 288 | 282 | 50.0 | 29.5 | 1.5 | 4.6 |
| 6 | 2-6-45 | 27.1 | 10.1 | 32.2 | 9.8 | 71 | 21 | 18.5 | 15.9 | 265 | 286 | 51.6 | 30.7 | 16 | 4.8 |
| 7 | 2-6-45 | 27.0 | 10.3 | 31.5 | 12.3 | 64 | 21 | 19.0 | 15.6 | 279 | 300 | 49.6 | 31.6 | 1.6 | 4.8 |
| 8 | 2-6-45- | $27.2^{-}$ | - 10.4 | -31.4 | 11.9 | 70 | $19^{-}$ | 19.4 | $16.0{ }^{\circ}$ | 287 | 285 | 49.2 | 31.0 | -1.5 | 4.9 |
| 9 | 8-9-44 | 27.7 | 10.3 | 32.3 | 4.9 | 69 | 21 | 19.4 | 16.7 | 265 | 269 | 52.2 | 33.4 | 1.5 | 4.2 |
| 10 | 8-9-44 | 26.8 | 10.1 | 31.8 | 8.5 | 67 | 19 | 18.4 | 16.4 | 263 | 261 | 52.8 | $31.9{ }^{-}$ | 1.7 | 4.5 |
| Average |  | 27.3 | 10.1 | 32.4 | 8.5 | 68 | - 20 | 19.5 | 15.5 | 268 | 276 | 52.3 | 30.4 | 1.6 | 4.7 |

TABLE XLVI
STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

|  | Mill S |  |  |  |  |  |  |  | Amthor Tensile, lb./in. |  | Amthor Stretch, $\%$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis Weight, lb. |  | Bursting | G.E. <br> Puncture, units | Riehle Compression, lb. |  | EImendorf Tear, g./sheet |  |  |  |  |  |
|  | $/ 1000)$ | $\begin{aligned} & \text { Calper, } \\ & 0.001 \text { in. } \end{aligned}$ | points |  | In | Across | In | Across | In | Across | In | Across |
| 'Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 27.8 | 105 | 72 | 21 | 21.2 | 16.7 | 288 | 300 | 572 | 33.4 | 1.8 | 5.1 |
| Minimum | 26.8 | 9.6 | 64 | 19 | 18.4 | 14.3 | 250 | 261 | 49.2 | 28.5 | 1.5 | 4.2 |
| Average | 27.3 | 10.1 | 68 | 20 | 19.4 | 15.5 | 268 | 276 | 52.3 | 30.4 | 1.6 | 4.7 |
| Standard deviation | 0.328 | 0.301 | 2.91 | $0.84,3$ | 0.783 | 0.810 | 14.8 | 11.9 | 2.92 | 170 | 0.103 | 0.275 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 87 | 90 | 61 | 77 | 80 | 78 | $3)$ | 48 | 39 | 44 | 67 | 53 |
| Kange limit (土)* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 30 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 99 | 100) | 91 | 93 | 94 | 94 | 69 | 79 | 70 | 76 | 95 | 85 |
| Kange limit ( $\pm$ ) ${ }^{*}$ | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 100 | - | 99 | 99 | 99 | 99 | 96 | 99 | 91 | 92 | 100 | 97 |

Mile 'T
Roll Averages

'TABLE XLVIII
STA'TISTICAL EVAIUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM


TABLE XLIN .
PHYSICAL CHARACTERISTICS OF 00リ/26-L.B. FOURDRINIER KRAFT CORRUGATING MEDIGM
Millu U
Koll Averages


TABLE L
STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mill U

|  | $\begin{gathered} \text { Basis } \\ \text { Weight, } \\ 1 \mathrm{~b} . \\ (12 \times 12 \\ / 1000) \end{gathered}$ | Caliper, 0.001 in . | Bursting Strength, points | G.E. <br> Puncture, units | RiehleCompression, lb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values , . Across |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 28.5 | 11.6 | 74 | 22 | 23.4 | 15.0 |  |  |  |  |  |  |
| Minimum | 25.0 | 9.4 | 54 | 17 | 16.4 | 11.8 | 276 | 295 | 59.4 | 35.7 | 2.5 | 5.8 |
| Average | 26.9 | 10.7 | 65 | 20 | 19.7 | 13.5 | 238 | 206 | 44.2 53.0 | 20.7 | 1.5 | 4.0 4.8 |
| Standard deviation | 0.903 | 0.645 | 5.18 | 1.46 | 1.76 | 0.974 | 18.6 | 206 | 53.0 4.34 |  | 2.0 0 | 4.8 |
| Range limit ( $\pm$ )* Approximate probability, \% | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 18.6 7 | 17.5 | 4.34 | 3.57 | 0.281 | 0.447 |
|  |  |  |  |  | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Range limit ( $\pm$ )* <br> Approximate probability, \% | 1.0 | 88 | 37 | 50 | 43 | 70 | 31 | 33 | 27 | 22 | 28 | 35 |
|  | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
|  | 73 | 99 | 66. | 70 | 60 | 88 | 58 | 61 |  |  |  |  |
| $\begin{gathered} \text { Range limit }( \pm)^{*} \\ \text { Approximate } \\ \text { probability, } \% \end{gathered}$ | 2.0 | - | 7.5 | 3.0 | 30 |  |  |  |  |  |  | $63$ |
|  | 97. | - | 83 | 3.0 96 | 30 91 | $\begin{array}{r}3.0 \\ \hline 99\end{array}$ | 30.0 | 300 | 5.0 | 3.0 | 0.3 | 0.6 |
|  |  |  |  |  |  |  | 89 | 91 | 75 | 60 | 72 | 82 |

- range limit of $\pm 0.002$ inch ( 0.008 to 0.012 inch). The uniformity of the bursting strength, as denoted by the standard deviation, indicates that only $28 \%$ of the rolls should fall within a range limit of $\pm 2.5$ points ( 54.5 to 59.5 points), $53 \%$ within a range limit of .$- \pm 5.0$ points ( 52.0 to 62.0 - points), and $72 \%$ within a range limit of $\pm 7.5$ points ( 49.5 to 64.5 points). The standard deviations for the Riehle compression test indicate that $55 \%$. of the rolls should fall within a range limit of $\pm 1.0$ pound in the in-machine direction, and $72 \%$ in the corresponding range limit for the -across-machine direction--Practically-all of-the- rolls should fall within a range limit of $\pm 3.0$ pounds for both directions. In general, the standard deviation for G. E. puncture, Elmendorf tear, and Amthor tensile and "stretch are of such magnitude as to indicate considerable nonuniformity.


## Mill U

The average test results obtained for kraft corrugating medium manufactured by Mill $U$ are presented in Table XLIX (see also Table LXXIII of the Appendix). The statistical evaluation of these results is given in Table L. The average basis weight for Mill U was 26.9 pounds, the average caliper was 0.0107 inch, and the average apparent density was 30.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 65 points and 20 units, respectively. The average Riehle compression values for the in- and across-machine directions were 19.7 and 13.5 pounds, respectively. The average moisture content was $8.4 \%$ on an ovendry basis.

Inasmuch as the standard deviation for basis weight was 0.903 , it is to be expected that only $42 \%$ of the rolls would fall within a range limit of $\pm 0.5$ pound (26.t to 27.4 pounds), $73 \%$ within a range limit of $\pm 1.0$ pound ( 25.9 to 27.9 pounds), and approximately $97 \%$ within a range limit of $\pm 2.0$ pounds ( 24.9 to 28.9 pounds). The standard deviation for caliper indicates that nearly $90 \%$ of the rolls should fall within a range limit of $\pm 0.001$ inch ( 0.0097 to 0.0117 inch). The uniformity of the bursting strength, as shown by the standard deviation of 5.18 , indicates that only $37 \%$ of the rolls would be expected to fall within a range limit of $\pm 2.5$ points ( 62.5 to 67.5 points), $66 \%$ within a range limit of $\pm 5.0$ points ( 60.0 to 70.0 points), and $83 \%$ within a range limit of $\pm 7.5$ points ( 57.5 to 72.5 points). For the in- and across-machine direction Riehle compression, 43 and $70 \%$ of the rolls, respectively, should fall within a range limit of $\pm 1.0$ pound, 60 and $88 \%$ within a range limit of $\pm 1.5$ pounds, and 91 and $99 \%$ within a range limit of $\pm 3.0$ pounds. The Elmendorf tear and Amthor tensile and stretch exhibit considerable variation or lack of uniformity.

## Mile V

The average test results obtained for $.009 / 26-\mathrm{lb}$. bogus corrugating medium made by Mill V are given in Table LI (see alsó Table LXXIV of the Appendix) and the statistical evaluation of these results in Table
Hitw
LII. For all practical purposes, the basis weight is the. same as the grade weight specified. The standard deviation for basis weight indicates that $42 \%$ of the rolls should fall within a range limit of $\pm 0.5$ pound (25.3 to 26.3 pounds), $74 \%$, within a range limit of $\pm 1.0$ pound (24.8-to $26: 8$ pounds), and $98 \%$ within a-range limit of $\pm 2.0$ pounds ( 23.8 to 27.8 pounds). The average caliper was 0.0101 inch with a standard deviation of 0.341 , indicating that approximately $99 \%$ of the rolls should fall within a range limit of $\pm 0.001$ inch ( 0.0091 to 0.0111 inch ). The average apparent density was 30.7 pounds per cubic foot and the average moisture content was $9.2 \%$ on an ovendry basis. The average bursting strength was 32 points and the indicated uniformity was such that $51 \%$ of the rolls should fall within a range limit of $\pm 2.5$ points ( 29.5 to 34.5 points), $83 \%$ within a range limit of $\pm 5.0$ points ( 27.0 to 37.0 points), and approximately $96 \%$ within a range limit of 7.5 points ( 24.5 to 39.5 points). The average Riehle compression values in the in- and across-machine-directions were 12.9 and 10.3 , respectively, with standard deviations indicating a probability that 80 and $86 \%$ of all the rolls would fall within a range limit of $\pm 1.5$ pounds. Approximately all the rolls should fall within'a Riehle compression range limit of $\pm 3.0$ pounds. The standard deviations for Elmendorf tear and Amthor tensile and stretch indicate that considerable variation should be expected.

## Mill W

The average test results obtained for the kraft corrugating medium made by Mill $W$ are seen in Table LIII (see also Table LXXV of the Appendix). The statistical evaluation of these results are given in Table LIV. The average basis weight was slightly above the grade weight and the standard deviation of 0.910 indicates an expectancy that $42 \%$ of the rolls should fall within the range limit of $\pm 0.5$ pound (26.3 to 27.3 pounds), $73 \%$ within a range limit of $\pm 1.0$ pound ( 25.8 to 27.8 pounds), and $97 \%$ within a range limit of $\pm 2.0$ pounds ( 24.8 to 28.8 pounds). The average caliper was 0.0101 inch and, according to the magnitude of the standard deviation, $85 \%$ of the rolls should fall within a range limit of $\pm 0.001$ inch $(0.0091$ to 0.0111 inch) and $99 \%$ within a range limit of $\pm 0.002$ inch ( 0.0081 to 0.0121 inch ). The average apparent density was 31.8 pounds per cubic foot and the average moisture content was $11.1 \%$ on an ovendry basis.

The average bursting strength was 69 points. It should be expected that $42 \%$ of the rolls should fall within a bursting strength range limit of $\pm 2.5$ points ( 66.5 to 71.5 points), $73 \%$ within a range limit of $\pm 5.0$ points ( 64.0 to 74.0 points), and $91 \%$ within a range limit of $\pm 7.5$ points ( 61.5 to 76.5 points). The average Riehle compression results in the in- and acrossmachine directions were 17.7 and 11.5 pounds, respectively. The standard deviations for the Richle compression indicate that a range limit of $\pm 1.0$ pound should include $46 \%$ of the rolls in the in-machine direc-

TABLE I.I

Mile $V$
Roll Averages

|  |  | Basis Weight, lb . | Caliper, | Apparent | Mois- | Bursting | G.E. Punc- | $\begin{aligned} & \text { Riehle } \\ & \text { Compression, } \\ & \text { Ib. } \end{aligned}$ |  | Elmendorf Tear, g./sheet |  | Anthor. Tensile, lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R | Date | $\begin{aligned} & 12 \times 12 \\ & / 1000) \end{aligned}$ | in. | Density, | $\begin{aligned} & \text { ture, } \\ & \% \end{aligned}$ | Strength, points | units | In | Across | In | Across | In | Across | In | Across |
| 1 | 1-26-45 | 26.0 | 10.4 | 30.0 | 8.4 | 31 | 8 | 12.9 | 10.0 | 95 | 112 | 30.3 | 15.2 | 1.4 | 1.9 |
| 2 | 10-21-44 | 27.3 | 9.4 | 34.8 | 8.4 | 39 | 12 | 13.1 | 10.1 | 143 | 165 | 37.6 | 18.0 | 1.8 | 2.6 |
| 3 | - | 26.4 | 10.0 | 31.7 | 10.0 | 31 | 10 | 12.9 | 9.3 | 123 | 128 | 30.3 | 16.5 | 1.5 | 2.7 |
| 4 |  | 24.3 | -9.9 | 29.4 | 11.7 - | 29 | -11- | -11.3 | - 9.0 | $101^{-}$ | -123 - - | 28.2 | 14:1 | 1.4 | 2.6 |
| 5 | - | 25.7 | 10.4 | 29.7 | 10.1 | 31 | 12 | 13.7 | 10.1 | 113 | 125 | 31.0 | 17.0 | 1.3 | 2.2 |
| 6 | - | 26.1 | 9.9 | 31.6 | 10.0 | 36 | 11 | 14.7 | 11.4 | 128 | 159 | 36.1 | 20.0 | 1.5 | 2.5 |
| 7 | . | 26.1 | 10.3 | 30.4 | . 8.5 | 31 | 13 | 12.4 | -10.3 - | 115 | 129 | 31.4 | 18.0 - | -1.2 | 2.4. |
| 8 |  | 26.9 | 9.5 | 34.0 | 5.9 | 33 | 12 | 14.4 | 9.9 | 1.33 | 157 | 35.5 | 16.4 | 1.0 | 2.5 |
| -9 | - | 25.3 | 10.1 | 30.0 | 5.5 | . 31 | 12 | 11.8 | 12.6 | 146 | 132 | 24.3 | 23.8 | 1.3 | 2.7 |
| 10 | - | 25.0 | 10.3 | 29.1 | 7.6 | 30 | 11 | 14.7 | 95 | 109 | 127 | 31.8 | 14.4 | 1.3 | 2.2 |
| 11 | - | 25.5 | 10.5 | 29.1 | 9.8 | 34 | 13 | 12.1 | 11.2 | 133 | 144 | 28.8 | 17.8 | 1.6 | 2.2 |
| 12 |  | 24.4 | 10.1 | 29.0 | 15.5 | 38 | 13 | 12.9 | 10.9 | 141 | 140 | 30.9 | 18.2 | 1.8 | 2.3 |
| 13 | - | 26.3 | 10.3 | 30.6 | 7.9 | 26 | 10 | 11.4 | 9.3 | 89 | 100 | 27.1 | 13.7 | 1.4 | 2.1 |
|  | Average | 25.8 | 10.1 | 30.7 | 9.2 | 32 | 11 | 12.9 | 10.3 | 121 | 134 | 31.0 | 17.2 | 1.4 | 2.4 |

TABLE LII
Statistical evaluation of physical tests on .009/26-Lb. boGUS CORRUGating medium
Mile $V$

|  | Basis Weight, lb. ( $12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E: <br> Puncture, units | Riehle. Compression, tb. |  | Elmendorf Tear, g./sheet |  | Amthor Tensile, lib./in. |  | Amthor Stretch, $\%$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 27.3 | 10.5 | 39 | 13 | 14.7 | 12.6 | 146 | 165 | 37.6 | 23.8 | 1.8 | 2.7 |
| Minimum | 24.3 | 9.4 | 26 | 8 | 11.3 | 9.0 | 89 | 100 | 24.3 | 13.7 | 1.0 | 1.9 |
| Average | 25.8 | 10.1 | 32 | 11 | 12.9 | 10.3 | 121 | 134 | 31.0 | 17.2 | 1.4 | 2.4 |
| Standard deviation | 0.889 | 0.341 | 3.64 | 1.45 | 1.17 | 1.01 | 18.7 | 18.7 | 3.70 | 2.72 | 0.224 | 0.249 |
| Range limit ( $\pm$ )* | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 42 | 99 | 51 | 51 | 60 | 68 | 31 | 31 | 32 | 29 | 35 | 58 |
| Range limit ( $\pm$ )* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 74 | 100 | 83 | 70 | 80 | 86 | 58 | $58$ | 58 | 54 | 63. | 89 |
| Range limit ( $\pm$ )* | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30:0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 98 | - | 96 | 96 | 99 | 99 | 89 | 89 | 82 | 73 | 82 | 98 |

## 'TABLE LIII

HHVSICAL CHARACTERIS'ILCS OF . $004 / 26-L B$. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mili. W
Roll Averages


TABLE LIV
STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM


TABLE LV
PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mile X Roll Averages


TABLE LVI
STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB: FOURDRINIER KRAFT CORRUGATING MEDIUM


TABLE ATI
PHYSICAL CHARACTERISTICS OF . $009 / 26-1 B$. FOURDRINIER KRAFT CORRUGATING MEDIUA
Mins. Y
Roll Averages

| Roll | Date Manuf. | Rasis Weight, lb. $(12 \times 12$ /1000) | $\begin{gathered} \text { Caliper, } \\ 0.001 \\ \text { in. } \end{gathered}$ |  | Moisture, \% | Bursting Strength, points | G.E. Puncture, units | RiehleCompression,lb. |  | Elmendorf Tear, g./sheet |  | Amthor <br> Tensile, <br> lb./in. |  | Amthor Stretch, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| 1 | 3-12-45 | 25.4 | 9.1 | 33.5 | 7.2 | 48 | 15 | 18.5 | 11.0 | 186 | 205 | 45.4 | 19.5 | 1.9 | 3.8 |
| 2 | 10-14-44 | 25.7 | 8.9 | 34.6 | 8.9 | 70 | 13 | 24.2 | 15.1 | 161 | 188 | 59.0 | 27.4 | 2.3 | 3.1 |
|  | 3-12-45 | 25.3 | 9.1 | 33.4 | 6.8 | 48 | 14 | 17.0 | 12.2 | 183 | 185 | 46.3 | 19.9 | 2.1 | 3.1 |
| 1 | . 3-10-45 - | 26.0 | -. 9.5.. | 32.8 | 11.7 | 72 | 17. | 16.9 | 13.7 | -194. | 243 | 55.4 | 22.3 | 2.2 | 3.7 |
| 5 | 3-10-45 | 26.8 | 9.8 | 32.8 | 7.3 | 73 | 18 | 18.7 | 13.7 | 206 | 238 | 55.5 | 21.1 | 1.9 | 4.6 |
| 6 | 3-10-45 | 27.0 | 9.8 | 33.1 | 10.5 | 65 | 18 | 16.8 | 13.1 | 238 | 270 | 54.0 | 26.6 | 2.1 | 3.7 |
| 7 | 3-12-45 | 26.1 | 9.4 | 33.3 | 10.8 | 47 | 14 | 15.7 | 11.3 | 183 | 206 | 46.6 | 19.4 | 2.0 | 3.9 |
| 8 | 3-12-45- | 27.1 | $8: 2$ | 39.6 | 12.5 | 55 | 13 | 14.9 | 10.6 | 176 | 220 | 49.6 | 224 | 2.1 | 3.8 |
| 9 | 3-12-45 | 261 | 9.2 | 34.0 | 11.1 | 51 | 13 | 10.0 | 11.9 | 180 | 219 | 49.0 | 22.1 | 1.9 | 3.3 |
| 10 | 3-12-45 | 249 | 9.5 | 31.5 | 10.1 | 48 | 13 | 14.3 | 10.0 | 182 | 214 | 45.9 | 20.2 | 1.8 | 3.0 |
|  | Average | 26.0 | 9.3 | 33.9 | 9.7 | 58 | 15 | 17.3 | 12.3 | 189 | 219 | 50.7 | 22.1 | 2.0 | 3.6 |

TABLE LVIII
STATISTICAL EVAlUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

|  |  |  |  |  | MiL | Y |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Basis Weight, ib. |  | Bursting | G.E. | $\begin{array}{r} \mathrm{R} \\ \operatorname{Comp} \end{array}$ | ehle ression, b. |  | ndorf ear. sheet | Amtho | Tensile, /in. | Amthor | Stretch, \% |
|  | /1000) | $\begin{aligned} & \text { Caliper, } \\ & 0.001 \mathrm{in} . \end{aligned}$ | points | units | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum | 27.1 | 9.8 | 73 | 18 | 24.2 | 15.1 | 238 | 270 | 59.0 | 27.4 | 2.3 | 4.6 |
| Minimum | 249 | 8.2 | 47 | 13 | 14.3 | 10.0 | 161 | 185 | 45.4 | 19:4 | 1.8 | 3.0 |
| Average | 26.0 | 9.3 | 58 | 15 | 17.3 | 12.3 | 189 | 219 | 50.7 | 22.1 | 2.0 | 3.6 |
| Standard deviation | 0.746 | 0.474 | 11.0 | 2.10 | 2.80 | 1.61 | 208 | 25.9 | 4.90 | 2.83 | 0.157 | 0.488 |
| Range limit ( $\pm$ )* | 0.5 | 10 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 50 | 97 | 18 | 37 | 28 | 46 | 28 | 23 | 24 | 27 | 48 | 32 |
| Kange limit ( $\pm$ )* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 3.0 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 82 | 99 | 35 | 52 | 41 | 64 | 53 | 44 | 46 | 52 | 80 | 59 |
| Kange limit ( $\pm$ )* | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 99 | - | 50 | 83 | 72 | 94 | 85 | 75 | 69 | 71 | 94 | 78 |

TABISE IAX
PHYSICAI, CHARACTERIS'ICS OF . $009 / 26-L B$. FOURDRINIER KRAFT CORRUGISTANG MEIMUA
Mile $Z$
Roll Averages


TABLE LX
STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mill Z

|  | Basis Weight, lb . ( $12 \times 12$ /1000) | Caliper, 0.001 in. | Bursting Strength, points | G.E. <br> Puncture, units | Riehle Compression, lb. |  | EImendorf Tear, g./sheet |  | Amthor Tensile, lb./in. |  | Amthor Stretch, $\%$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Across | In | Across | In | Across | In | Across |
| Test values |  |  |  |  |  |  |  |  |  |  |  |  |
| Mavimum | 27.9 | 10.2 | 85 | 22 | 21.4 | 17.7 | 283 | 316 | 59.5 | 35.8 | 2.3 | 5.4 |
| Minimum | 26.3 | 8.9 | 65 | 19 | 17.1 | 14.2 | 226 | 236 | 47.3 | 26.1 | 1.7 | 3.1 |
| Average | 26.8 | 9.3 | 75 | 20 | 19.9 | 15.8 | 251 | 262 | 53.8 | 33.0 | 2.0 | 4.7 |
| Standard deviation | 0.522 | 0.366 | 5.21 | 1.03 | 1.59 | 1.22 | 17.1 | 24.6 | 3.86 | 2.65 | 0.155 | 0.659 |
| Range limit ( $\pm)^{*}$ | 0.5 | 1.0 | 2.5 | 1.0 | 1.0 | 1.0 | 7.5 | 7.5 | 1.5 | 1.0 | 0.1 | 0.2 |
| Approximate probability, \% | 66 | 99 | 37 | 67 | 47 | 59 | 34 | 24 | 30 | 30 | 48 | 24 |
| Range limit ( $\pm$ )* | 1.0 | 2.0 | 5.0 | 1.5 | 1.5 | 1.5 | 15.0 | 15.0 | 30 | 2.0 | 0.2 | 0.4 |
| Approximate probability, \% | 95 | 100 | 66 | 86 | 65 | 78 | 62 | 46 | 56 | 55 | 80 | 46 |
| Kange limit ( $\pm$ * | 2.0 | - | 7.5 | 3.0 | 3.0 | 3.0 | 30.0 | 30.0 | 5.0 | 3.0 | 0.3 | 0.6 |
| Approximate probability, \% | 99 | - | . 85 | 99 | 94 | 99 | 92 | 78 | 81 | 74 | 95 | 64 |

* Range limits were arbitrarily selected.
tion and $82 \%$ in the across-machine direction. A range limit of $\pm 1.5$ pounds should include $65 \%$ in the inmachine direction and $96 \%$ in the across-machine direction, and a range limit of $\pm 3.0$ pounds should include 84 and $99 \%$, respectively. Elmendorf tear and -Amthor-tensile- and-stretch exhibited rather -large standard deviations, signifying that considerable variation should be expected.


## Mill $\mathrm{X}{ }^{*}$.

--The average-test.results obtained on samples of the kraft corrugating medium made. by Mill X are presented in Table LV (see also Table LXXVI of the Appendix). It mäà be observed that the average basis weight was 27.4 pounds. The average caliper was 0.0098 inch and the average apparent density was 33.7 pounds per cubic foot. The average bursting strength was 68 points and the average moisture $8.7 \%$ on an ovendry basis. The average Riehle compression values in the in- and across-machine directions were 17.1 and 13.1 pounds, respectively.

The statistical evaluation of these results is given in Table LVI. On the basis of a standard deviation of 0.881 for basis weight, it should be expected that $43 \%$ of the rolls should fall within a range limit of $\pm 0.5$ pound ( 26.9 to 27.9 pounds), $75 \%$ within a range limit of $\pm 1.0$ pound ( 26.4 to 28.4 pounds), and $98 \%$ within a range limit of $\pm 2.0$ pounds ( 25.4 to 29.4 pounds). With a standard deviation for caliper of 0.507 , approximately $95 \%$ of the rolls should fall within a range limit of $\pm 0.001$ inch ( 0.0088 to 0.0108 inch). Approximately $58 \%$ of the rolls. should fall within a bursting strength range limit of $\pm 2.5$ points ( 65.5 to 70.5 points), $89 \%$ within a range limit of $\pm 5.0$ points ( 63.0 to 73.0 points), and $98 \%$ within a range limit of $\pm 7.5$ points ( 60.5 to $75.5^{\prime}$ points). The standard deviation for the Riehle compression in the in-machine direction indicates that 58,77 , and $98 \%$ of the rolls should fall within range limits of $\pm 1.0, \pm 1.5$, and $\pm 3.0$ poúnds, respectively. For the across-machine direction, approximately 71,89 , and $99 \%$ of the rolls should fall within range limits of $\pm 1.0, \pm 1.5$; and $\pm 3.0^{\prime}$ pounds, respectively:

The statistical evaluation of the Elmendorf tear, Amthor tensile and stretch, and G. E. puncture indicates that, on the average, approximately $50 \%$ of the rolls should fall within the second arbitrarily selected range limit for each test.

## Mile Y

The average results obtained on samples of the kraft corrugating medium made by Mill Y are given in Table LVII (see also Table LXXVII of the Appendix). The average basis weight was $26: 0$ pounds, the average caliper 0.0093 inch, and the average apparent density was 33.9 pounds per cubic foot. The average bursting strength was 58 points, and the average Riehle compression values in the in- and across-machine directions, were 17.3 and 12.3 pounds, respectively. The average moisture content was $9.7 \%$ on an ovendry basis.

The statistical evaluation of these results is found in Table LVIII. On the basis of the standard deviation,
 it should be expected that $50 \%$ of the rolls made in : this grade by Mill Y should fall within a basis weight range limit of $\pm 0.5$ pound ( 25.5 to 26.5 pounds), $82 \%$ within a range limit of $\pm 1.0$ pound ( 25.0 to 27.0 pounds), and $99 \%$ within a range limit of $\pm 2.0$ pounds ( 24.0 to 28.0 pounds). Approximately $97 \%$ of the rollsshould fall within a caliper range limit of $\pm 0.001$. inch ( 0.0083 to. 0.0103 inch). The standard deviation for the bursting strength was 11.0 , which indicates that only $18 \%$ of the rolls should be expected to fall within a range limit of $\pm 2.5$ points ( 55.5 to 60.5 points), $35 \%$ within-"-range limit- of $\pm 5.0^{-}$points ${ }^{-}\left(53.0-\right.$ to ${ }^{-} 63: 0$ points), and $50 \%$ within a range limit of $\pm 7.5$ points ( 50.5 to 65.5 points). The standard deviations for the Riehle compression in the in- and across-machine directions indicate that 28 and $46 \%$, respectively, should fall within the range limit of $\pm 1.0$ pound, 41 and $64 \%$ within the range limit of $\pm 1.5$ pounds, and 72 and $94 \%$ within the range limit of $\pm 3.0$ pounds. The standard deviations for Elmendorf tear, G E. puncture, and Amthor tensile and stretch indicate considerable nonuniformity of these characteristics in the $.009 / 26-\mathrm{lb}$. kraft corrugating medium.

## Mile Z

The average test results obtained on samples of the kraft corrugating medium made by Mill Z are given in Table LIX (see also Table LXXVIII of the Appendix). The average basis weight was 26.8 pounds, the average caliper 0.0093 inch, and the average apparent density 34.7 pounds per cubic foot. The average moisture content was $9.1 \%$ on an óvendry basis. The average bursting strength was 75 points and the average Riehle compression values for the in- and acrossmachine directions were 19.9 and 15.8 pounds, respectively. It should be noted that Rolls Z-2 and Z-3 were made approximately the middle of 1943 and thus were substantially older than the others; however, the average results obtained for these rolls do not vary markedly from the average of the values for the other rolls.

The statistical evaluation of these results is presented in Table LX. The magnitude of the standard deviation for the basis weight indicates that $66 \%$ of the rolls should fall within the range limit of $\pm 0.5$ pound ( 26.3 to 27.3 pounds), $95 \%$ within the range limit of $\pm 1.0$ pound ( 25.8 to 27.8 pounds), and $99 \%$ within a range limit of $\pm 2.0$ pounds ( 24.8 to 28.8 pounds). Approximately $99 \%$ of the rolls should fall within a caliper range limit of $\pm 0.001$ inch ( $0: 0083$ to 0.0103 inch). The standard deviation of the bursting strength indicates that $37 \%$ of the rolls should fall within a range limit of $\pm 2.5$ points ( 72.5 to 77.5 points), $66 \%$ within a range limit of $\pm 5.0$ points ( 70.0 to 80.0 points), and $85 \%$ within a range limit of $\pm 7.5$ points ( 67.5 to 82.5 points). The standard deviations for the Riehle compression values in the in- and acrossmachine directions indicate that 47 and $59 \%$ of the rolls, respectively, should fall within a range limit of $\pm 1.0$ pound; 65 and $78 \%$ within a range limit of $\pm 1.5$ pounds, and 94 and $99 \%$ within a range limit of $\pm 3.0$ Founds. The standard deviations for Elmendorf tear, G. E. puncture, and Amthor tensile and stretch indicate the respective uniformities of these characteristics.

## SUMMARY

The results presented in this part of the baseline study are concerned with the problem of sampling, in a truly impartial cross-sectional manner, the current routine production of the co-operating mills and evalu--ating-these samples as completely as possible by means of existing board testing methods.
The second phase of the baseline study involved (1) the selection of the most representative rolls of each mill's sampled production, and (2) the fabrication of these representative rolls into corrugated combined boards and their conversion into boxes.
Because the first part of the baseline study was concerned only with the sampling and evaluation of the component parts, no conclusions regarding the relationship between the quality of component parts and the performance of combined board and boxes fabricated from these components can be made at this time.
However, the results of this phase of the study indicate that the average quality of the sampled $42-\mathrm{lb}$. D.F.B.S. Fourdrinier kraft liner and of the $.009 /$ $26-\mathrm{lb}$. kraft and bogus corrugating mediums were as follows:

|  | Liner | Corrugating <br> Medium |
| :--- | :--- | :---: |
| Basis weight, lb./1000 sq. ft. | 42.1 | 26.8 |
| Caliper, in. | 0.015 | 0.010 |
| Apparent density, lb./cu. ft. | 33.7 | 32.3 |
| Bursting strength, points | 98 | 62 |
| G. E.puncture, units | 36 | 18 |
| Moisture, $\%$ | 8.1 | 9.4 |
| Riehle compression, lb. |  |  |
| $\quad$ In | 29.0 | 17.6 |
| $\quad$ Across | 22.5 | 13.0 |


|  | Liner | Corrugating Medium |
| :---: | :---: | :---: |
| Elmendorf tear, g./sheet |  |  |
| In | 354 | 223 |
| Across | 394 | 251 |
| Amthor tensile, lb./in. . .-.--77.8 - 495 |  |  |
|  | 77.8 | 495 |
| Across | 37.8 | 24.8 |
| Amthor stretch, \% |  |  |
| In | 2.1. | $-1.9$ |
| Across | 3.7 | 4.3 |

It should be remembered that these data are based on the actual rolls sampled and on conventional test methods.

For those tests in which orientation of the specimen is specified, the approximate ratios observed in the inmachine direction and in the across-machine direction were as follows:

|  | Ratio |
| :--- | :---: |
|  | In:Across |
| Riehle compression | $4: 3$ |
| Elmendorf tear | $0.9: 1$ |
| Amthor tensile | $2: 1$ |
| Amthor stretch | $1: 2$ |

The ratio of the bursting strength to the G. E. puncture on $42-\mathrm{lb}$. D.F.B.S. Fourdrinier kraft liner was of the order of 2.7:1.

The ratio was not computed for the $.009 / 26-\mathrm{lb}$. corrugating medium since the relatively high capacity of the G. E. puncture tester did not allow sufficient subdivision of the scale to permit distinguishing between the low values obtained with any degree of accuracy.
$\square$

APPENDIX'

TABLE LXI
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURIDRINIER KRAFT LINER
Mile $A$


TABLE LXII
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER
Mill B

| Institute File No. | Roll | Basis Weight, lb.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in. |  |  | Apparent Density, b./cu.ft. | Moisture, \% |  |  | Bursting <br> Strength, points |  |  | G.E. Puncture, units |  |  | Riehle Compression, lb . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |
| 116426/28 | 1 | 432 | 41.4 | 42.2 | 16.3 | 14.9 | 15.7 |  | 32.2 | 9.5 | 8.6 | 9.0 | 117 | 78 | 101 | 37 | 32 | 34 | 35.0 | 25.0 | 29.7 |
| 116429/31 | 2 | 44.8 | 446 | 44.7 | 16.5 | 15.4 | 15.9 | 33.7 | 8.8 | 8.1 | 8.4 | 124 | 67 | 106 | 42 | 36 | 39 | 34.0 | 28.0 | 30.2 |
| 116432/34 | 3 | 44.4 | 43.6 | 44.1 | 16.0 | 14.8 | 15.5 | 34.1 | 9.3 | 8.2 | 8.9 | 126 | 88 | 105 | 38 | 34 | 36 | 33.5 | 250 | 28.7 |
| 116726/28 | 4 | 43.3 | 42.6 | 42.9 | 14.0 | 12.5 | 135 | 38.1 | 82 | 82 | 8.2 | 128 | 78 | 102 | 40 | 35 | 37 | 36.0 | 280 | 31.3 |
| 116729/31 | 5 | 41.3 | 40.8 | 41.1 | 14.1 | 13.4 | 13.8 | 35.6 | 8.7 | 8.1 | 8.4 | 119 | $70^{\prime}$ | 92 | 40 | 32 | 35 | 33.5 | 23.5 | 27.5 |
| 116735/37 | 6 | 43.0 | 41.7 | 42.4 | 16.4 | 15.5 | 16.0 | 31.8 | 9.7 | 9.3 | 9.6 | 130 | 72 | 104 | 40 | 32 | 37 | 37.0 | 26.5 | 30.0 |
| 116949/51 | 7 | 42.3 | 414 | 42.0 | 16.5 | 15.1 | 15.7 | 32.0 | 7.1 | 6.3 | 6.8 | 112 | 71 | 94 | 37 | 30 | 34 | 38.0 | 30.0 | 34.0 |
| 116952/54 | 8 | 42.6 | 41.6 | 42.2 | 15.9 | 146 | 15.3 | 33.0 | 6.9 | 5.1 | 6.0 | 120 | 76 | 96 | 37 | 32 | 35 | 37.5 | 28.0 | 339 |
| 116955/57 | 9 | 44.0 | 40.6 | 42.7 | 16.7 | 14.8 | 15.9 | 322 | 7.7 | 58 | 6.8 | 110 | 66 | 91 | 42 | 35 | 39 | 325 | 260 | 29.3 |
| 117753/55 | 10 | 45.7 | 44.0 | 45.0 | 16.8 | 15.8 | 16.4 | 32.9 | 11.3 | 10.2 | 10.8 | 119 | 84 | 104 | 42 | 37 | 40. | 335 | 280 | 31.1 |
| 117756/58 | 11 | 43.6 | 42.0 | 42.7 | 16.5 | 15.0 | 15.9 | 32.2 | 10.2 | 9.3 | 9.7 | $10{ }^{\circ}$ | 73 | 91 | 40 | 34 | 37 | 34.0 | 25.0 | 29.1 |
| 117759/61 | 12 | 45.2 | 44.8 | 45.0 | 16.8 | 15.7 | 16.2 | 33.3 | 10.3 | 9.2 | 9.7 | 119 | 80 | 103 | 44 | 38 | 40 | 34.5 | 27.5 | 31.6 |
| 117762/64 | 13 | 43.2 | 42.4 | 42.8 | 16.0 | 15.0 | 15.6 | 32.9 | 11.4 | 10.9' | 11.1 | 120 |  | 103 | 47 | 35 | 38 | 37.5 | 27.5 | 32.3 |
| 117765/67 | 14 | 44:0 | 42.8 | 43.5 | 16.2 | 15.0 | 15.7 | 33.2 | 10.3 | 9.2 | 9.7 | 120 | 87 | 106 | 42 | 35 | 39 | 39.0 | 32.0 | 35.2 |
| 117768/70 | 15 | 46.1 | 45.1 | 45.7 | 16.4 | 14.7 | 15.6 | 35.2 | 8.9 | 7.7 | 8.1 | 138 | 88 | 112 | 41 | 37 | 40 | 36.5 | 29.0 | 32.0 |
| 118017/19 | 16 | 41.9 | 41.8 | 41.8 | 15.2 , | 14.0 | 14.8 | 33.9 | 9.3 | 8.9 | 9.1 | 144 | 67 | 101 | 39 | 33 | 36 | 31.5 | 22.0 | 27.9 |
| 118020/22 | 17 | 43.4 | 41.5 | 42.3 | 15.5 | 14.5 | 15.0 | 33.8 | 10.3 | 8.9 | 9.6 | 132 | 88 | 108 | 41 | 33 | 37 | 335 | 24.5 | 30.3 |
| 118023/25 | 18 | 43.0 | 41.2 | 42.3 | 17.0 | 15.8 | 16.4 | 31.0 | 8.5 | 7.6 | 8.0 | 108 | 74 | 93 | 41 | 35 | 37 | 330 | 24.0 | 29.4 |
| 118026/28 | 19 | 43.1 | 42.4 | 42.7 | 15.5 | 14.8 | 15.1 | 33.9 | 8.3 | 7.3 | 7.7 | 134 | 94 | 111 | 39 | 33 | 36 | 35.5 | 25. | 31.3 |
| 118029/31 | 20 | 41.7 | 41.1 | 41.3 | 15.3 | 14.8 | 15.0 | $33.0{ }^{\text {t }}$ | 8.3 | 7.6 | 8.0 | 108 | 71 | 95 | 37 | 32 | 35 | 32.0 | 25.5 | 28.9 |
| 118032/34 | 21 | 41 ". 2 | 41.1 | 41.2 | 15.0 | 14.5 | 14.9 | 33.2 | 9.0 | 7.2 | 8.1 | 124 | 78 | 98 | 38 | 31 | 34 | 32.0 | 24.5 | 28.7 |
| Average |  |  |  | 42.9 |  |  | 15.4 | 33.4 |  |  | $8.7^{\prime}$ |  |  | 101 |  |  | 37 |  |  | 30.6 |

TABLF LXI
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.IB.S. FOURDRINIER KRAFT LINER
Mill $A$


TABLE LXII
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT I.INER
Mill B

|  | le Com sion, lb | s- | Elmendorf Tear, g./sheet |  |  |  |  |  | Amthor Tensile, lb./in. |  |  |  |  |  | Amthor Stretch, \% |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  |  |
| Max. | Min | Av. | Max. | Min | Av. | Max. | Min. | Av, | Max. | Min. | . iv . | Max | Min. | 八. | Max. | Min. |  | Max. |  |  | Roll |
| 285 | 19.0 | 22.6 | 408 | 288 | 337 | 456 | 352 | 412 | 93.1 | 74.2 | 83.6 | 396 | 295 | 35.4 | 2.8 | 19 | 24 | 4.6 | 24 | 3.6 | 2 |
| 28.5 | 21.5 | 25.2 | 424 | 344 | 394 | 488 | 336 | 426 | 101.6 | 81.3 | 90.0 | 51.1 | 32.7 | 420 | 2.8 | 16 | 2.1 | 4.4 | 2.0 | 3.3 3 | 2 |
| 25.5 | 19.5 | 22.6 | 392 | 312 | 356 | 456 | 360 | 395 | 84.5 | 59.1 | 776 | 40.1 | 32.2 | 36. 1 | 3.0 | 1.6 | 2.4 | 4.7 | 2.8 | 3.9 | 3 |
| 29.0 | 23.0 | 25.5 | 456 | 368 | 415 | 456 | 360 | 398 | 78.7 | 59.3 | 713 | 53.7 | 34.9 | 43.8 | 3.0 | 1.6 | 22 | 6.9 | 1.9 | 4.3 | 4 |
| 275 | 17.5 | 23.3 | 432 | 360 | 402 | 432 | 320 | 367 | 79.6 | 59.6 | 70.0 | 50.8 | 26.9 | 41.3 | 2.5 | 1.6 | 20 | 7.6 | 1.0 | 41 | 5 |
| 26.0 | 18.5 | 22.4 | 440 | 328 | 368 | 496 | 392 | 428 | 98.2 | 77.9 | 89.2 | 430 | 33.0 | 38.7 | 2.7 | 1.5 | 2.1 | 4.8 | 2.6 | 3.5 | 6 |
| 26.5 | 220 | 24.4 | 400 | 304 | 346 | 448 | 328 | 377 | 84.7 | 70.6 | 81.4 | 36.9 | 29.1 | 33.2 | 24 | 1.8 | 2.1 | 5.6 | 2.7 |  | 7 |
| 29.0 | 220 | 25.0 | 432 | 320 | 365 | 440 | 344 | 397 | 88.0 | 72.8 | 83.1 | 42.7 | 261 | 36.6 | 2.4 | 1.8 | 2.1 | 6.0 | 2.0 | 4.1 | 8 |
| 27.0 | 18.0 | 23.8 | 456 | 328 | 391 | 472 | 360 | 418 | 91.4 | 61.0 | 78.0 | 43.2 | 322 | 38.3 | 22 | 1.4 | . 1.8 | 5.1 | 1.8 | 3.8 | 9 |
| 25.5 | 19.5 | 22.5 | 400 | 312 | 365 | 448 | 344 | 416 | 99.9 | 77.9 | 89.3 | 42.5 | 33.7 | 39.4 | 2.9 | 2.1 | 25 | 4.4 | 2.4 | 3.6 | 10 |
| 25.5 | 19.5 | 22.9 | 376 | 288 | 329 | 424 | 320 | 376 | 93.1 | 69.4 | 799 | 418. | 32.3 | 37.9 | 2.3 | 1.6 | 2.0 | 4.2 | 2.0 | 3.2 | 11 |
| 27.5 | 21.5 | 24.2 | 424 | 320 | 373 | 464 | 360 | 433 | 96.5 | 77.9 | 90.1 | 44.0 | 34.7 | 393 | 2.7 | 2.11 | 2.3 | 4.2 | 2 | 3.3 | 12 |
| 28.0 | 21.0 | 23.8 | 392 | 304 | 352 | 456 | 376 | 407 | 99.9 | 67.7 | 85.7 | 422 | 23.0 | 38.7 | 2.7 | 1.6 | 2.4 | 4 | 26 | 3.5 | 13 |
| 27.0 | 22.0 | 25.2 | 384 | 304 | 345 | 464 | 368 | 407 | 99.9 | 83.0 | 914 | 44.2 | 318 | 39.5 | 28 | 2.1 | 2.4 | 4.1 | 2.1 | 3.4 | 14 |
| 29.0 | 21.0 | 25.5 | 432 | 352 | 389' | 448 | 384 | 421 | 96.5 | 71.1 | 896 | 47.1 | 381 | 42.4 | 3.0 | 2.2 | 26 | 5.4 | 2.6 | 3.8 | 15 |
|  | 18.5 | 22.1 | 34.4 | 280 | 314 | 424 | 328 | 379 | 931 | 67.7 | 831 | 40.6 | 31.8 | 35.9 | 2.7 | 20 | 23 | 6.7 | 3.1 | 5.0 | 16 |
| 26.5 | 22.0 | 24.3 . | 376 | 240 | 319 | 424 | 344 | 389 | 105.0 | 81.3 | 92.4 | 43.8 | 35.4 | 393 | 2.8 | 2.0 | 23. | 4.8 | 2.9 | 3.6 | 17 |
| 25.0 | 220 | 236 | 360 | 264 | 319 | 408 | 312 | 380 | 91.4 | 74.5 | 81.2 | 3). 4 | 27.8 | 3.39 | 24 | 1.7 | 2.1. | 50 | 20 | 3.5 | 18 |
| 27.5 | 190 | 24.7 | 368 | 296 | 332 | 416 | 352 | 381 | 982 | 77.9 | 909 | 44.2 | $3+5$ | 391 | 25 | 1.8 | 2.2 | 53 | 2.4 | 3.8 | $10^{-}$ |
| 245 | 20.0 | 22.0 | 360 | 264 | 307 | 408 | 328 | 371 | 99.9 | 66.0 | 8.35 | 415 | 284 | 34.6 | 2.5 | 2.1 | 2.3 | 6.4 | 2.7 | 4.4 | 20 |
| 25.0 | 18.5 | 21.7 | 344 | 204 | 304 | 424 | 328 | 366 | 91.4 | 72.8 | 839 | 39.1 | 28.6 | 34.8 | 2.6 | 1.7 | 22 | 5.6 | 2.0 | 43 | 21 |
| 23.7 |  |  | 353 |  |  | - $\overline{307}$ |  |  | - $\overline{84.1}$ |  |  | 38.1 |  |  | 2.2 |  |  | 3.8 |  |  |  |

TABLE LXIII
PHYSICAL CHARACTERISTICS OF 42-LIB. D.F.B.S. FOURDRINIER KRAF'T LINER
Mill C

| Institute File No. | Roll | - Basis Weight, lb.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in. |  |  | Apparent Density, lb./cu.ft. | Moisture, \% |  |  | - Bursting Strength, points |  |  | G.F. Puncture, units |  |  | Riehle Compression, lb. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. |  | Max. | Min. | Av. |
| 116360/62 | 1 | 44.6 | 42.8 | 43.7 | 14.0 | 13.4 | 13.7 |  | 38.2 | 8.0 | 7.5 | 7.7 | 122 | 79 | 98 | 41 | 34 | 37 | 34.0 | 22.0 | 28.0 |
| 116,363/65 | 2 | 43.6 | 42.1 | 42.8 | 13.8 | 12.8 | 13.4 | 38.3 | 8.2 | 7.3 | 7.8 | 119 | 76 | 98 | 38 | 33 | 35 | 37.0 | 22.5 | 29.4 |
| 116366/68 | 3 | 45.2 | 42.9 | 44.0 | 14.3 | 135 | 14.0 | 37.7 | 8.2 | 7.3 | 7.7 | 129 | 90 | 109 | 40 | 34 | 38 | 36.5 | 27.5 | 31.2 |
| 116960/62 | 4 | 42.1 | 41.2 | 41.7 | 14.8 | 13.9 | 14.2 | 35.2 | 8.7 | -7.7 | 8.2 | 107 | 75 | 88 | 42 | 33 | 36 | 34.5 | 29.0 | 31.2 |
| 116963/65 | 5 | 43.0 | 42.4 | 42.6 | 15.1 | 14.3 | 14.8 | 34.5 | 7.8 | 6.8 | 7.4 | 135 | 75 | 104 | 50 | 37 | 41 | 38.5 | 28.5 | 31.6 |
| 116975/77 | 6 | 42.5 | 41.9 | 42.2 | 15.3 | 14.7 | 15.0 | 33.8 | 8.9 | 7.9 | 8.3 | 134 | 77 | (9) | 45 | 39 | 42 | 37.5 | 27.5 | 31.0 |
| 116078/80 | 7 | 42.3 | 41.8 | 42.1 | 15.0 | 14.1 | 14.6 | 34.6 | 8.3 | 7.2 | 7.6 | 125 | 80 | 101 | 45 | 38 | 41 | 36.0 | 22.0 | 29.7 |
| 116981/83 | 8 | 42.6 | 42.4 | 42.5 | $15.2{ }^{-}$ | 14:5 | 14.9 | 34.2 | 8.5 | 7:9 | 8.2 | 118 | 80 | 99 | $43^{-}$ | 37. | $41^{\circ}$ | 37.0 | 27.5 | 32.8 |
| 117459/61 | 9 | 42.6 | 41.6 | 42.1 | 15.4 | 14.6 | 15.0 | 33.7 | 5.9 | 5.0 | 5.5 | 124 | 65 | 99 | 42 | 38 | 40 | 35.5 | 26.5 | 29.9 |
| 117462/64 | 10 | 43.0 | 41.2 | 42.3 | 15.3 | 14.0 | 14.7 | 34.5 | 6.6 | 4.9 | 5.8 | 142 | 53 | 103 | 43 | 36 | 40 | 32.5 | 25.5 | 28.9 |
| 117977/79 | 11 | 44.9 | 42.8 | 43.8 | 14.5 | 13.0 | 13.9 | 37.8 | 6.9 | 3.9 | 5.6 | 124 | 80 | 102 | 41 | 35 | 38 | 33.0 | 26.0 | 30.3 |
| 117980/82 | 12 | 42.1 | 41.6 | 41.8 | 15.2 | 14.5 | 15.0 | 33.4 | 7.5 | 5.6 | 6.6 | 120 | 78 | 99 | 40 | 35 | 38 | 33.5 | 25.5 | 28.3 |
| 117983/85 | 13 | 42.7 | 42.6 | 42.7 | 15.4 | 14.1 | 14.9 | 34.4 | 6.5 | 5.3 | 6.1 | 113 | 63 | 93 | 41 | 35 | 38 | 29.5 | 25.0 | 27.3 |
| 117986/88 | 14 | 42.7 | 42.1 | 42.5 | 15.4 | 14.6 | 15.0 | 34.0 | 6.8 | 54 | 6.3 | 133 | 78 | 97 | 42 | 34 | 38 | 32.0 | 24.0 | 27.6 |
| 117989/91 | 15 | 44.5 | 43.6 | 44.0 | 15.0 | 14.2 | 14.7 | 35.9 | 7.8 | 6.6 | 7.1 | 131 | 87 | 109 | 44 | 37 | 41 | 35.0 | 24.5 | 30.5 |
| Average |  |  |  | 42.7 |  |  | 14.5 | 35.3 |  |  | 7.1 |  |  | 100 |  |  | 39 |  |  | 29.8 |

TABLE LXIV
PHYSICAI, CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER
Mill D

| Institute File No. | Roll | Basis Weight, lb. ( $12 \times 12 / 1000$ ) |  |  | Caliper, 0.001 in. |  |  | Apparent Density, lb./cu.ft. | Moisture, \% |  |  | Bursting Strength, points |  |  | G.E. Puncture, |  |  | Riehle Compression, lb . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | $A v$. | Max. | Min. | Av. | Max. | Min. | Av. |
| 117006/08 | 1 | 41.1 | 40.3 | 40.8 | 15.0 | 14.3 | 14.7 |  | 33.3 | 8.9 | 8.3 | 8.6 | 110 | 80 | 94 | 40 | 33 | 38 | 33.5 | 24.0 | 28.3 |
| 117009/11 | 2 | 41.8 | 40.4 | 40.9 | 15.0 | 14.0 | 14.7 | 33.4 | 8.7 | 6.8 | 7.9 | 118 | 82 | 102 | 39 | 35 | 37 | 33.0 | 24.0 | 28.6 |
| 117012/14 | 3 | 41.8 | 40.2 | 41.0 | 15.1 | 14.1 | 14.8 | 33.2 | 9.1 | 6.9 | 7.9 | 118 | 63 | 93 | 40 | 35 | 37 | 29.5 | 22.0 | 25.8 |
| 117015/17 | 4 | 40.3 | 40.3 | 40.3 | 15.2 | 14.3 | 14.9 | 32.4 | 8.2 | 6.3 | 7.1 | 118 | 63 | 84 | 38 | 31 | 36 | 29.5 | 20.0 | 24.4 |
| 117018/20. | 5 | 45.4 | 42.9 | 43.9 | 17.3 | 16.2 | 16.7 | 31.5 | 8.6 | 6.7 | 7.7 | 126 | 69 | 100 | 47 | 40 | 44 | 31.0 | 25.0 | 27.4 |
| 117021/23 | 6 | 46.4 | 44.6 | 45.4 | 17.7 | 16.0 | 16.6 | 32.8 | 7.9 | 6.5 | 7.4 | 133 | 75 | 100 | 48 | 41 | 44 | 355 | 23.0 | 28.8 |
| 117054/56 | 7 | 42.9 | 41.5 | 42.4 | 15.9 | 14.8 | 15.3 | 33.2 | 11.5 | 7.6 | 9.4 | 117 | 73 | 97 | 40 | 32 | 36 | 33.5 | 25.0 | 29.9 |
| 117060/62 | 8 | 41.0 | 39.8 | 40.4 | 14.9 | 13.8 | 14.4 | 33.6 | 14.1 | 11.0 | 124 | 123 | 79 | 102 | 39 | 32 | 34 | 36.5 | 25.5 | 29.4 |
| 11706.3/6, | 9 | 42.8 | 41.8 | 42.3 | 168 | 15.4 | 16.0 | 31.7 | 12.8 | 10.5 | 11.7 | 120 | 79 | 101 | 40 | 34 | 37 | 34.0 | 26.0 | 30.1 |
| 117090/92 | 10 | 38.9 | 38.8 | 38.8 | 13.7 | 12.7 | 13.3 | 34.9 | 5.8 | 3.1 | 4.2 | 124 | 70 | 91 | 32 | 28 | 3) | 33.5 | 27.0 | 31.4 |
| 117003/95 | 11 | 40.3 | 38.9 | 39.6 | 13.5 | 12.4 | 13.0 | 36.5 | 5.3 | 3.6 | 4.3 | 120 | 71 | 95. | 33 | 28 | 30 | 36.5 | 27.0 | 31.3 |
| 117111/13 | 12 | 42.0 | 40.8 | 41.6 | 14.8 | 14.0 | 14.3 | 34.8 | 7.7 | 6.3 | 70 | 111 | 68 | 9.4 | 37 | 30 | 33 | 29.5 | 24.5 | 27.0 |
| 117114/16 | 13 | 40.3 | 39. 2 | 39.7 | 13.5 | 12.3 | 12.8 | 37.2 | 7.8 | 7.0 | 7.4 | 121 | 89 | 104 | 33. | 29 | 32 | 30.5 | 24.0 | 27.0 |
| 117123/25 | 14 | 41.6 | 40.4 | 40.8 | 15.5 | 13.9 | 14.3 | 34.2 | 8.6 | 7.1 | 8.0 | 114 | 80 | 95 | 37 | 30 | 33 | 30.0 | 22.0 | 26.1 |
| 117167/69 | 15 | 43.0 | 41.8 | 42.5 | 15.0 | 14.5 | 14.7 | 34.7 | 6.2 | 5.7 | 6.0 | 125 | 82 | 102 | 38 | 31 | 35 | 30.5 | 25.5 | 27.8 |
| 117170/72 | 16 | 44.6 | 41.6 | 43.4 | 15.8 | 14.4 | 14.9 | 34.9 | 7.1 | 5.6 | 6.3 | 130 |  | 105 | 39 | 31 | 35 | 35.0 | 26.5 | 31.1 |
| 117173/75 | 17 | 42.2 | 41.4 | 41.9 | 14.9 | 14.1 | 14.5 | 34.6 | 7.6 | 5.5 | 6.6 | 131 | 85 | 105 | 37 | 32 | 34 | 30.0 | 23.0 | 26.9 |
| 117176/78 | 18 | 43.2 | 40.4 | 41.9 | 17.9 | 15.4 | 16.8 | 29.9 | 9.0 | 6.1 | 8.0 | 104 | 64 | 86 | 38 | 32 | 35 | 29.0 | 21.5 | 25.9 |
| 117260/62 | 19 | 43.7 | 42.7 | 43.3 | 15.1 | 14.0 | 14.6 | 35.6 | 7.5 | 5.7 | 6.7 | 147 | 78 | 110 | 37 | 33 | 36 | 35.0 | 23.0 | 28.2 |
| 117266/68 | 20 | 41.2 | 40.8 | 41.0 | 15.4 | 14.5 | 15.1 | 32.6 | 5.7 | 5.1 | 5.5 | 108 | 72 | 93 | 39 | 33 | 36 | 33.0 | 24.0 | 27.8 |
| 117269/71 | 21 | 43.0 | 42.6 | 42.8 | 15.1 | 14.3 | 14.8 | 34.7 | 8.2 | 4.6 | 6.2 | 122 | 76 | 102 | 41 | 35 | 38 | 29.0 | 23.0 | 25.9 |
| Average |  |  |  | 41.7 |  |  | 14.8 | 33.8 |  |  | 7.4 |  |  | 98 |  |  | 36 |  |  | 28.1 |

TABLE LXIII
PHYSICAL. CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KKAF゙「' LINER
Mill C


TABLE LXIV
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER
Mill D

| Riehle Compres- <br> sion, lb. |  |  |
| :---: | :---: | :---: |
| Across |  |  |


| In |  |  | Across |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 408 | 288 | 355 | 392 | 336 | 374 |
| 392 | 296 | 336 | 424 | 344 | 392 |
| 424 | 328 | 383 | 408 | 320 | 349 |
| 416 | 328 | 375 | 384 | 304 | 3.47 |
| 448 | 344 | 391 | 472 | 360 | 415 |
| 480 | 336 | 407 | 512 | 392 | 442 |
| 440 | 320 | 384 | 456 | 320 | 366 |
| 376 | 312 | 3.4 | 424 | 312 | 373 |
| 536 | 288 | 369 | 456 | 336 | 406 |
| 376 | 264 | 320 | 432 | 304 | 348 |
| 400 | 288 | 334 | 384 | 296 | 341 |
| 424 | 336 | 378 | 376 | 320 | 345 |
| 368 | 280 | 332 | 368 | 288 | 335 |
| 352 | 280 | 310 | 416 | 304 | 361 |
| 400 | 344 | 366 | 448 | 360 | 399 |
| 464 | 344 | 374 | 464 | 368 | 409 |
| 400 | 328 | 357 | 424 | 344 | 382 |
| 416 | . 328 | 370 | 464 | 336 | 387 |
| 392 | 328 | 360 | 440 | 360 | 402 |
| 408 | 320 | 358 | 424 | 320 | 372 |
| 400 | 320 | 362 | 424 | 360 | 398 |
|  |  | 360 |  |  | 378 |



| Amthor Stretch, \% |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In |  |  | Across |  |  | Roll |
| Max. | Min. |  | Max. | Min. |  |  |
| 2.2 | 1.2 | 1.8 | 4.0 | 2.0 | 3.1 |  |
| 2.3 | 1.5 | 1.8 | 4.0 | 1.0 | 3.0 | 2 |
| 2.2 | 1.2 | 1.8 | 4.0 | 2.2 | 3.1 | 3 |
| 2.0 | 1.1 | 1.6 | 4.0 | 1.4 | 2.8 | 4 |
| 2.8 | 1.4 | 1.9 | 4.0 | 1.5 | 3.2 | 5 |
| 3.5 | 1.5 | 2.0 | 4.7 | 2.1 | 3.6 | 6 |
| 3.4 | 1.4 | 1.8 | 4.9 | 1.7 | 3.7 | 7 |
| 2.0 | 1.1 | 1.5 | 5.3 | 2.2 | 3.8 | 8 |
| 2.6 | 1.2 | 1.7 | 3.9 | 2.6 | 3.3 | 9 |
| 2.2 | 1.5 | 1.9 | 5.5 | 1.3 | 4.0 | 10 |
| 2.4 | 1.2 | 1.9 | 5.6 | 2.6 | 4.3 | 11 |
| 2.4 | 1.3 | 2.0 | 4.6 | 1.9 | 3.3 | 12 |
| 2.4 | 1.1 | 2.0 | 4.3 | 1.5 | 3.5 | 13 |
| 2.3 | 1.6 | 1.9 | 4.1 | 1.5 | 31 | 14 |
| 2.5 | 1.3 | 2.1 | 4.2 | 1.6 | 3.1 | 15 |
| 2.5 | 1.7 | 2.2 | 5.4 | 2.8 | 4.3 | 16 |
| 2.6 | 1.8 | 2.3 | 4.3 | 1.8 | 3.2 | 17 |
| 2.4 | 1.6 | 2.0 | 4.9 | 2.5 | 3.8 | 18 |
| 3.2 | 1.7 | 2.2 | 5.2 | 1.6 | 3.7 | 19 |
| 2.6 | 1.9 | 2.3 . | 5.5 | 1.8 | 4.1 | 20 |
| 2.6 | 1.9 | 2.3 | 4.9 | 1.8 | 3.8 | 21 |
|  |  | 2.0 |  |  | 3.5 |  |



TABLE LXVI
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER
Mill F

| Institute File No. | Roll | Basis Weight, 1b. ( $12 \times 12 / 1000$ ) |  |  | Caliper, 0.001 in. |  |  | Apparent Density, lb./cu.ft. | Moisture, \% |  |  | Bursting Strength, prints |  |  | G.E. Puncture, units |  |  | Kiehle Compression, lb |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |
| 118066/68 | 1 | 41.5 | 40.5 | 41.1 | 14.1 | 11.8 | 13.5 |  | 365 | 11.8 | 9.9 | 10.7 | 117 | 80 | 98 | 48 | 35 | 39 | 28.5 | 18.5 | 24.3 |
| 118069/71 | 2 | 429 | 41.3 | 42.4 | 14.7 | 12.1 | 13.9 | 36.6 | 12.9 | 10.3 | 11.4 | 119 | 66 | 96 | 39 | 34 | 37 | 26.0 | 17.5 | 21.5 |
| 118072/74 | 3 | 38.5 | 36.0 | 37.5 | 14.0 | 12.2 | 13.1 | 34.3 | 93 | 7.7 | 8.7 | 93 | 55 | 76 | 32 | 24 | 28 | 25.5 | 20.0 | 22.3 |
| 118075/77. | 4 | 42.8 | 40.8 | 41.6 | 14.0 | 12.7 | 13.5 | 37.0 | 12.0 | 10.2 | 11.1 | 96 | 57 | 75 | 41 | 28 | 32. | 24.0 - | 190 | 21.6 |
| 118108/10 | 5 | 40.1 | 387 | 39.3 | 13.6 | 12.3 | 13.0 | 36.3 | 11.8 | 8.8 | 10.3 | 109 | 68 | 83 | 32 | 26 | 29 | 26.5 | 19.0 | 23.7 |
| 118111/13 | 6 | 40.0 | 39.0 | 39.4 | 13.8 | 12.5 | 13.4 | 35.3 | 8.1 | 7.5 | 78 | 97 | 58 | 78 | 34 | 25 | 31 | 25.5 | 20.0 | 23.2 |
| 118114/16 | 7. | 380 | 36.2 | 36.9 | 13.1 | 12.0 | 12.6 | 35.1 | 12.6 | 7.2 | 9.5 | 93 | 58 | 76 | $30^{\circ}$ | 26 | 28 | 25.5 | 21.0 | 23.3 |
| 118117/19 | 8 | 40.5 | 39.3 | 40.0 | 14.1 | 13.0 | 13.7 | 35.0 | 11.5 | 9.3 | 10.5 | 118 |  | 97 | 41 | 32 | 37 | 28.0 | 21.0 | 23.4 |
| 118120/22 | 9 | 41.1 | 39.9 | 40.5 | 14.0 | 11.6 | 13.5 | 36.0 | 11.4 | 9.7 | 10.6 | 116 | 75 | 95 | 46. | 26 | 37 | 29.5 | 24.0 | 26.9 |
| 118123/25 | 10 | 39:1 | 37.3 | 38.4 | 14.0 | 13.1 | 13.5 | 34.1 | 10.5 | 8.5 | 9.5 | 94 | 57 | 74 | 33 | 23 | 29 | 25.5 | 18.5 | 22.6 |
| Average |  |  |  | 39.7 |  |  | 13.4 | 35.6 |  |  | 10.0 |  |  | 85 |  |  | 33 |  |  | 23.3 |

TABLE IAVVI
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER
Mill G

| Institute <br> File No. | Koll | Basis Weight, 16.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in. |  |  | Apparent Density, $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | Moisture, \% |  |  | Bursting Strength, points |  |  | G E. Puncture, unts |  |  | Riehle Compression, lb. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | A |
| 117245/47 | 1 | 42.9 | 42.0 | 42.6 | 16.1 | 14.9 | 15.5 |  | 330 | 7.7 | 6.8 | 7.3 | 114 | 66 | 93 | 40 | 34 | 37 | 30.5 | 22.0 | 27.4 |
| 117248/50 | 2 | 42.9 | 42.1 | 42.5 | 16.2 | 15.5 | 15.9 | 32.1 | 5.5 | 4.4 | 4.9 | 109 | 55 | 87 | 45 | 35 | . 38 | 30.5 | 230 | 26.7 |
| 1172.51/53 | 3 | 42.1 | 41.9 | 420 | 16.1 | 15.3 | 158 | 31.9 | 7.8 | 7.1 | 7.4 | 107 | 72 | 88 | 39 | 34 | 37 | 28.0 | 225 | 25.7 |
| 117254/56 | 4 | 424 | 41.0 | 417 | 16.1 | 15.3 | 15.7 | 31.9 , | 7.2 | 63 | 6.8 | 114 | 69 | 85 | 39 | 34 | 37 | 29.0 | 24.5 | 26.1 |
| 117257/59 | 5 | 42 S | 41.8 | 42.2 | 16.2 | 154 | 15.9 | 31.8 | 8.7 | 7.3 | 8.1 | 109 | 65 | 92 | 40 | 35 | 38 | 30.0 | 21.0 | 255 |
| 117263/65 | 6 | 41.4 | 409 | 41.2 | 16.5 | 15.6 | 16.1 | 30.7. | 7.2 | 4.3 | 5.8 | 107 | 63 | 89 | 43 . | 33 | 36 | 33.5 | 24.5 | 28 |
| 117272/74 | 7 | 41.9 | 41.5 | 41.7 | 168 | 15.9 | 16.2 | 30.9 | 84 | 6.3 | 7.0 | 113 | . 72 | 92 | 42 | 36 | 38 | 325 | 25.0 | 28. |
| 117320/22 | 8 | 426 | 41.5 | 42.0 | 15.6 | 14.1 | 15.0 | 33.6 | 10.8 | 10.3 | 105 | - 129 | 84 | 106 | 40 | 36 | . 38 | 320 | 260 | 28.8 |
| 117393/95 | 9 | 417 | 41.3 | 415 | 16.2 | 15.0 | 155 | 32.1 | 8.4 | $7.9{ }^{\circ}$ | 8.2 | 127 | 61 | 97 | 39 | 33 | 36 | 34.5 | 25.0 | 28.9 |
| 117396/98 | 10 | 42.4 | 41.3 | 417 | 16.0 | 14.8 | 15.2 | 32.9 | 8.0 | 4.0 | 63 | 122 | 60 | 95 | 38 | 32 | 35 | 38.0 | 23.5 | 27.9 |
| 117480/82 | 11 | 44.0 | 427 | 43.3 | 159 | 14.6 | 15.3 | 34.0 | 7.5 | 65 | 6.9 | 120 | 65 | 88 | 47 | 41 | 44 | 35.0 | 225 | 27.4 |
| 117483/85 | 12 | 40.4 | 39.8 | 40.2 | 16.0 | 14.8 | 15.3 | 31.5 | 63 | 5.2 | 5.8 | 122 | 68 | 91 | 42 | 35 | 39) | 330 | 25.0 | 28.1 |
| 117486/88 | 13 | 420 | 41.3 | 41.6 | 15.9 | 14.9 | 15.3 | 326 | 68 | 4.0 | 5.5 | 101 | 4) | 79 | $41^{\prime}$ | 36 | 39 | $2^{9} .0$ | 23.0 | 25. |
| 117489/91 | 14 | 432 | 41.7 | \$2.6 | 16.3 | 15.6 | 16.0 | 31.9 | 8.3 | 6.1 | 7.3 | 103 | 72 | 88 | 42 | 33 | . 36 | 32.0 | 25:5 | 28.8 |
| 117492/94 | 15', | 42.0 | 403 | 41.0 | 15.5 | 14.5 | 15.0 | 32.8 | 8.8 | 66 | 7.9 | 114 | 78 | 9.4 | 38 | 34 | 37 | 29.5 | 24.0 | 26.6 |
| Average |  |  |  | 41.9 |  |  | 15.6 | 32.2 |  |  | 7.0 |  |  | 91 |  |  | 38 |  |  | 27. |

TABLE LXV
PHISIC.V. CIAARACTERISTLCS OF 42-LB. D.F.B.S. FOURDRINIER KRAFI I.INER
Mill E.


TABLE LXVI
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER
Mill F


TABLE LXVII
PHYSICAI. CHARACTERISTICS OF $42-L B$. D F.B.S. FOURDRINIER KRAF'T LINER


| Elmendorf Tear, K / sheet |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| In |  |  | Across |  |  |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 424 | 336 | 373 | 528 | 376 | 429 |
| 432 | 320 | 382 | 456 | 360 | 413 |
| 456 | 336 | 382 | 504 | 352 | 426 |
| 440 | 352 | 392 | 480 | 384 | 420 |
| 424 | 352 | 390 | 456 | 384 | 423 |
| 416 | 320 | 377 | 440 | 360 | 399 |
| 496 | 328 | 394 | 528 | 368 | 436 |
| 416 | 344 | 377 | 464 | 368 | 405 |
| 448 | 344 | 383 | 424 | 336 | 375 |
| 448 | 336. | 381 | 440 | 344 | 382 |
| 440 | 344 | 39.4 | 472 | 360 | 424 |
| 416 | 320 | 364 | 528 | 360 | 407 |
| 440 | 320 | 383 | 448 | 376 | 410 |
| 456 | 328 | 382 | 384 | 312 | 358 |
| 384 | 328 | 353 | 432 | 328 | 371 |
|  |  | 380 |  |  | 405 |


| $\ln$ |  |  | Across |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 86.3 | 69.4 | 76.0 | 44.4 | 37.1 | 41.4 |
| 83.0 | 67.7 | 73.5 | 45.4 | 35.6 | 408 |
| 8.3 .0 | 677 | 730 | 45.2 | 35.6 | 41.7 |
| 84.7 | 66.0 | 73.5 | 45.4 | 35.6 | 41.9 |
| 86.3 | 69.4 | 74.7 | 46.2 | 35.7 | 40.7 |
| 79.6 | 643 | 71.5 | 41.8 | 32.8 | 37.1 |
| 81.3 | 62.6 | 72.3 | 45.7 | 33.7 | 40.8 |
| 77.9 | 60.1 | 70.7 | 576 | 45.4 | 50.6 |
| 79.6 | 60.9 | 71.6 | 49.9 | 37.2 | 44.7 |
| 82.3 | 565 | 70.0 | 53.2 | 33.9 | 44.4 |
| 83.5 | 61.3 | 73.9 | 427 | 33.7 | 37.9 |
| 81.9 | 60.3 | 708 | 42.7 | 308 | 38.6 |
| 81.8 | 56.4 | 69.7 | 38.4 | 31.7 | 35.7 |
| 8.3 .0 | 626 | 70.3 | 57.1 | 42.7 | 48.4 |
| 83.0 | 62.6 | 725 | 50.1 | 36.9 | 42.8 |
|  |  | 72.3 |  |  | 41.8 |


| [n |  |  | Across |  |  | Koll |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |  |
| 2.0 | 1.0 | 1.7 | 4.0 | 23 | 3.1 | 1 |
| 1.8 | 1.0 | 1.4 | 3.8 | 2.2 | 2.9 | 2 |
| 1.9 | 1.2 | 1.6 | 4.4 | 2.0 | 3.1 | 3 |
| 1.8 | 1.2 | 1.5 | 3.5 | 1.6 | 2.8 | 4 |
| 1.8 | 1.1 | 15 | 3.8 | 2.2 | 2.8 | 5 |
| 2.3 | 1.6 | 2.0 | 5.1 | 2.8 | 4.0 | 6 |
| 2.2 | 1.6 | 2.0 | 5.0 | 2.7 | 3.8 | 7 |
| 4.0 | 14 | 2.0 | 44 | 2.8 | 3.7 | 8 |
| 2.7 | 1.6 | 20 | 5.2 | 3.2 | 4.3 | 9 |
| 2.4 | 1.5 | 2.0 | 5.9 | 2.5 | 42 | 10 |
| 2.4 | 0.9 | 1.8 | 6.0 | 32 | 4.0 | 11 |
| 2.0 | 13 | 1.6 | 49 | 2.0 | 3.6 | 12 |
| 1.7 | 0.9 | 1.4 | 3.9 | 2.1 | 3.3 | 13 |
| 20 | 1.4 | 1.8 | 5.1 | 3.0 | 4.1 | 14 |
| 2.1 | 1.4 | 1.8 | 5.6 | 2.9 | 43 | $15^{\circ}$ |
|  |  | 1.7 |  |  | 3.6 |  |

TABLE LXVIII
PHYSIC.IF: CHARICCEFRISTICS OF 42-LB. D.I.B.S. FOURDRINIFR KRAFT LINER
Mill H


TABLE LXLX
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

|  |  |  | * |  |  |  |  |  | Mill I |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Riehl s | Comp on, lb. | pres- |
|  |  | Basis <br> (12 | $\begin{aligned} & \text { Weigh } \\ & \times 12 / 10 \end{aligned}$ | $\begin{aligned} & \mathrm{t}_{1} \mathrm{lb} . \\ & 000) \end{aligned}$ | Calip | $\text { er, } 0.0$ |  | Apparent |  | ture, |  | $\begin{array}{r} \mathrm{B} \\ \text { Stren } \end{array}$ | $\begin{aligned} & \text { urstir } \\ & \text { gth, } \end{aligned}$ | oints | G.E | $\begin{aligned} & \text { Punct } \\ & \text { units } \end{aligned}$ |  |  | In |  |
| Institute File No. | Roll | Max. | Min. | Av | Max. | Min. | Av. | Density, <br> lb./cu.ft. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min |  | Max. | Min. | Av. |
| 116732/34 | 1 | 43.0 | 41.8 | 42.5 | 15.9 | 149 | 15.3 | 33.3 | 9.1 | 8.3 | 8.7 | 128 | 93 | 111 | 42 | 37 | 40 | 33.5 | 23.5 | 30.5 |
| 116738/40 | 2 | 43.4 | . 41.8 | 42.7 | 159 | 14.7 | 15.1 | 33.9 | 9.4 | 8.2 | 8.9 | 137 | 90 | 107 | 45 | 40 | 42 | 33.0 | 23.0 | 28.7 |
| 116741/43 | 3 | 43.1 | 41.0 | 42.5 | 159 | 14.4 | 15.3 | 33.3 | 8.7 | 8.4 | 8.5 | 147 | 85 | 109 | 45 | 40 | 42 | 31.5 | 26.0 | . 7 |
| 116910/12 | 4 | 44.6 | 42.9 | 439 | 15.7 | 14.6 | 15.1 | 34.9 | 7.5 | 6.6 | 7.0 | 130 | 84 | 106 | 45 | 37 | 40 | 34.0 | 23.5 | 29.0 |
| 116913/15 | 5 | 44.2 | 42.6 | 43.5 | 15.8 | 14.3 | 15.2 | 34.3 | 7.7 | 6.1 | 7.1 | 124 | 86 | 105 | 45 | 37 | 41 | 31.5 | 21.5 | 26.7 |
| 116928/30 | 6 | 43.4 | 42.4 | 43.1 | 15.9 | 14.9 | 15.5 | 33.4 | 7.1 | 6.4 | 6.9 | 133 | 81 | 108 | 45 | 37 | 41 | 33.0 | 25.0 | 29.5 |
| 116943/45 | 7 | 44.2 | 42.6 | 4.3 .5 | 16.1 | 14.8 | 15.5 | 33.7 | 7.5 | 6.3 | 7.0 | 129 | 80 | 104. | 45 | 37 | 41 | 350 | 25.5 | 30.0 |
| 116946/48 | 8 | +2.6 | 413 | $42: 1$ | 15.8 | 144 | 15.2 | 33.2 | 7.0 | 6.0 | 6.5 | 129 | 76 | 102 | 42 | 37 | 39 | 32.0 | 26.0 | 29.2 29.9 |
| 117423/25 | 9 | 43.8 | 42.7 | 43.4 | 161 | 15.0 | 15.5 | 33.6 | 10.3 | 9.8 | 10.0 | 132 | 83 | 106 | 43 | 37 | 40 40 | 34.0 | 25.5 | 29.9 29.8 |
| 117426/28 | 10 | 43.7 | 42.7 | 4.3 .2 | 16.0 | 15.0 | 15.5 | 33.4 | 9.9 | 8.3 | 8.9 | 133 | 82 | 109 | 44 | 38 | 40 | 34.5 | 26.0) | 29.8 |
| 117429/31 | 11 | 44.6 | 42.7 | 43.6 | 15.9 | 138 | 15.3 | 34.2 | 90 | 8.5 | 8.8 | 131 | 96 | 114 | 43 | 38 | 41 | 35.0 | 27.0 | 31.0 |
| 117432/34 | 12 | 44.4 | 43.1 | 43.8 | 16.1 | 15.1 | 15.7 | 33.5 | 10.1 | 9.2 | 9.6 | 129 | 95 | 109 | 42 | 37 | 40 | 34.5 | 27.5 | 30.0 |
| 117435/37 | 13 | 44.0 | 42.5 | 43.3 | 16.7 | 15.1 | 15.9 | 32.7 | 10.5 | 8.0 | 9.4 | 126 | 77 | 100 | 45 | 38 | 41 39 | 33.0 | 26.0 | 29.7 31.2 |
| 117471/73 | 14 | 43.5 | 42.2 | 42.8 | 15.1 | 13.9 | 14.7 | 34.9 | 10.5 | 8.8 | 9.7 | 139 | 91 | 119 | 4.3 | 37 | 39 | 33.5 | 29.0 27.0 | 31.2 32 |
| 117474/76 | 15 | 45.9 | 45.1 | 45.4 | 15.9 | 14.5 | 15.1 | 36.1 | 11.5 | 97 | 10.8 | 147 | 94 | 121 | 46 | 39 | 42 | 39.0 | 27.0 | 32.3 |
| 117477/79 | 16 | 46.0 | 44.5 | 45.0 | $15: 7$ | 14.6 | 15.3 | 35.3 | 11.9 | 10.9 | 11.4 | 128 | 71 | 112 | 45 | 38 | 42 | 35.0 | 29.0 | 32.1 |
| 117495/97 | 17 | 42.7 | 42.4 | 42.6 | 156 | 14.4 | 15.0 | 34.1 | 9.0 | 7.6 | 8.2 | 120 | 67 | 104 | 42 | 35 | 38. | 35.0 | 30.0 | 321 |
| 117498/500 | 18 | 45.1 | 44.1 | 44.5 | 15.6 | 14.1 | 14.9 | 35.8 | 7.7 | 6.5 | 7.3 | 133 | 82 | 110 | 46 | 40 | 42 | 39.0 | 33.0 275 | 35.5 34.5 |
| 117501/03 | 19 | 43.7 | 42.6 | 43.3 | 15.2 | 14.1 | 14.9 | 34.9 | 6.7 | 6.3 | 6.6 | 142 | 91 | 107 | 478 | 38 | 42 43 | 42.0 41.0 | 275 28.0 | 34.5 |
| 117504/06 | 20 | 44.0 | 43.8 | 43.9 | 15.9 | 14.7 | 15.3 | 34.4 | 8.6 | 78 | 8.1 | 124 | 88 | 110 | 48 | 39 | 43 | 41.0 | 28.0 | 33.6 |
| 117507/09 | 21 | 45.6 | 44.0 | 45.0 | 16.4 | 15.0 | 15.6 | 34.6 | 8.5 | 6.4 | 7.6 | 143 | 85 | 108 | 46 | 40 | 43 | 40.0 | 30.0 | 34.5 |
| 117510/12 | 22. | 44.8 | 43.6 | 44.1 | 16.1 | 14.8 | 15.6 | 33.9 | 9.7 | 7.5 | 8.4 | - 141 | 81 | 110 | 49 | 41 | 44 | 37.0 | 25.0 | 30.3 |
| Average |  |  |  | 43.5 |  |  | 15.3 | 34.2 |  |  | 8.4 |  |  | $10{ }^{\circ}$ |  |  | 41 |  |  | 309 |

T:DBLE LXVIII.
PHYSICAL. CILAR.ICTERISTICS OF 42-LB. D.F B.S. FOURDRINIER KR.IFT LINER

## Mil.c. If

Richle Compres-
$\frac{\text { Across }}{-\quad \text { sion, } 1 \mathrm{~b} .-}$
27.5 5 $\begin{array}{lll}27.0 & 20.5 & 24.5\end{array}$ $\begin{array}{lll}32.0 & 21.0 & 25.7\end{array}$ $29.0 \quad 23.5 \cdot 25.4$ $\begin{array}{lll}29.5 & 23.5 & 26.1\end{array}$
$\begin{array}{lll}25.5 & 19.0 & 22.8\end{array}$ $\begin{array}{lll}25.0 & 18.0 & 22.7\end{array}$ $\begin{array}{lll}26.0 & 20.5 & 23.9\end{array}$ $\begin{array}{lll}26.5 & 21.5 & 24.4\end{array}$ $\begin{array}{lll}26.0 & 20.0 & 23.8\end{array}$
$\begin{array}{lll}26.5 & 21.0 & 23.7\end{array}$ $\begin{array}{lll}28.5 & 23.0 & 24.8\end{array}$ $\begin{array}{lll}28.0 & 22.0 & 25.0 \\ 27.0 & 23.5 & 25.4\end{array}$ $\begin{array}{lll}27.0 & 23.5 & 25.4\end{array}$
$\frac{\text { Elmendorf Tear, g./shect }}{\frac{\operatorname{In}}{\text { Max. Min. Av. Mas. Min. Av. }} \text { Across }}$
.... Amthor Tensile, tb /in

| In |  |  | Across |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 88.0 | 60.9 | 73.5 | 56.5 | 28.1 | 47.8 |
| 71.1 | 54.2 | 62.7 | 58.7 | 33.4 | 50.3 |
| 91.4 | 57.4 | 69.2 | 53.5 | 36.9 | 45.7 |
| --73:0 | 54.0 | 63.9 | 58.7 | 41.6 | 49.7 |
| 93.1 | 69.4 | 80.0 | 48.4 | 36.1 | 42.5 |
| 96.5 | 63.1 | 79.5 | 45.4 | 33.0 | 39.1 |
| 84.3 | 67.0 | 75.9 | 41.8 | -33.7 | 37.7 |
| 93.1 | 67.7 | 80.5 | 48.9 | 28.1 | 40.9 |
| 96.5 | 66.0 | 80.9 | 48.1 | 31.7 | 41.7 |
| 93.1 | 69.4 | 80.8 | 45.7 | 31.5 | 39.2 |
| 96.5 | 57.6 | 80.0 | 46.0 | 34.5 | 41.0 |
| 93.1 | 71.1 | 82.1 | 45.4 | 32.2 | 40.2 |
| 94.8 | 67.7 | 79.1 | 47.4 | 32.2 | 41.3 |
| 91.4 | 49.1 | 73.7 | 45.5 | 29.8 | 40.3 |
|  |  | 75.8 |  |  | 42.7 |

$\frac{{ }^{-} \quad \text { Amthor Stretch. \% }}{\text { In }}$
Max. Min. Av. Max. Min Av. Rell

| 2.9 | 2.0 | 2.5 | 5.2 | 1.3 | 3.8 | 1 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 3.9 | 1.6 | 2.3 | 5.8 | 2.1 | 4.4 | 2 |
| 3.3 | 1.4 | 2.0 | 5.9 | .2 .1 | 4.4 | -3. |
| 2.7 | 1.5 | 2.0 | 5.8 | 2.3 | 4.5 | 4 |
| 2.5 | 1.2 | 2.1 | 5.2 | 2.4 | 3.7 | 5 |
| 2.7 | 1.3 | 2.1 | 5.0 | 2.9 | 4.0 | 6 |
| 2.6 | 1.5 | 1.9 | 4.6 | 2.5 | 3.6 | 7 |
| 2.5 | 1.6 | 2.3 | 5.7 | 1.6 | 3.9 | 8 |
| 2.7 | 1.9 | 2.4 | 5.4 | 2.2 | 4.3 | 9 |
| 2.8 | 1.8 | 2.4 | 5.7 | 2.3 | 3.8 | 10 |
| 2.8 | 1.2 | 2.3 | 5.8 | 2.6 | 4.1 | 11 |
| 2.7 | 2.0 | 2.4 | 5.4 | 2.1 | 3.8 | 12 |
| 2.7 | 1.7 | 2.3 | 5.5 | 2.5 | 4.4 | 13 |
| 2.9 | 1.3 | 2.3 | 6.0 | 20 | 4.2 | 14 |

TABLE LXIX
PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINLER KRAFT LINER

## Mill I



| Kiehle Compres-  <br> sion,  <br> Ib.  |
| :--- | :--- | :--- |
| Mcross |


| In |  |  | Across |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 464 | 360 | 418 | 568 | 400 | 468 |
| 480 | 392 | 428 | 592 | 416 | 473 |
| 496 | 368 | 422 | 624 | 448 | 506 |
| 512 | 392 | 434 | 496 | 448 | 470 |
| 464 | 360 | 411 | 544 | 416 | 462 |
| 456 | 360 | 401 | 560 | 400 | 462 |
| 456 | 368 | 408 | 576 | 424 | 487 |
| 456 | 376 | 407 | 488 | 408 | 443 |
| 520 | 352 | 411 | 520 | 368 | 442 |
| 448 | 360 | 405 | 5.36 | 400 | 463 |
| 424 | 352 | 390 | 536 | 432 | 466 |
| 496 | 352 | 422 | 592 | 400 | 470 |
| 472 | 336 | 390 | 488 | 416 | 458 |
| 432 | 328 | 39.4 | 520 | 408 | 474 |
| 488 | 392 | 431 | 544 | 456 | 497 |
| 480 | 320 | 416 | 5.4 | 440 | 491 |
| 4.40 | 304 | 366 | 464 | 368 | 430 |
| 464 | 336 | 391 | 504 | 400 | 453 |
| 488 | 352 | 416 | 504 | 416 | 451 |
| 46.4 | 368 | 412 | 488 | 416 | 454 |
| 496 | 352 | 411 | 544 | 408 | 443 |
| 472 | 360 | 401 | 576 | 400 | 469 |
|  |  | 408 |  |  | 465 |


| In |  |  | Across |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Max. | Min. | Av. | Max. | Min. | Av. |
| 103.3 | 79.6 | 90.9 | 41.8 | 29.1 | 36.6 |
| 98.2 | 72.8 | 88.2 | 42.8 | 28.8 | 37.9 |
| 98.2 | 77.9 | 88.4 | 41.3 | 32.0 | 37.7 |
| 98.2 | 72.8 | 88.5 | 40.8 | 33.0 | 37.1 |
| 101.6 | 76.2 | 86.3 | 41.0 | 27.1 | 35.8 |
| 94.8 | 74.5 | 85.3 | 44.2 | 33.5 | 38.0 |
| 96.5 | 77.9 | 87.5 | 41.1 | 31.5 | 35.3 |
| 85.3 | 67.4 | 78.6 | 42.0 | 30.5 | 36.6 |
| 91.4 | 69.4 | 81.9 | 41.8 | 30.5 | 37.1 |
| 93.1 | 72.8 | 83.9 | 41.6 | 29.6 | 36.5 |
| 91.4 | 76.2 | 85.5 | 41.1 | 33.5 | 37.2 |
| 88.0 | 67.7 | 80.5 | 44.4 | 30.3 | 37.0 |
| 863 | 69.4 | 78.4 | 40.3 | 29.5 | 35.3 |
| 931 | 72.8 | 83.5 | 42.3 | 27.6 | 36.3 |
| 91.4 | 72.8 | 84.2 | 42.8 | 28.8 | 37.8 |
| 94.8 | 52.5 | 85.6 | 44.0 | 30.5 | 38.3 |
| 94.8 | 66.0 | 82.5 | 45.0 | 27.8 | 35.1 |
| 99.9 | 76.2 | 89.6 | 41.1 | 31.0 | 36.5 |
| 98.2 | 79.6 | 86.9 | 41.8 | 32.7 | 36.3 |
| 98.2 | 71.1 | 87.0 | 44.5 | 26.1 | 38.0 |
| 106.7 | 76.2 | 922 | 38.4 | 29.1 | 35.4 |
| 965 | 69.4 | 83.4 | 44.5 | 30.8 | 37.9 |
|  |  | 85.4 |  |  | 36.8 |



TABIAE IXX
PHYSICAI. CIIARACTERISTICS OF 42-LR. D.F.B.S. FOURDRINIER KRAFT I.INER
Mini, J


TABLE LXXI
PHYSICAL CHARACTERISTICS OF'.009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mile S

|  |  |  | Weir |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Rieh | Com sion, lb | pres- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 12/1 | 0) | Calip | er, 00 | 1 in . | Apparent |  | isture, |  | Stren | th, | ts |  | units |  |  | In |  |
| File No. | Roll | Max. | Mın. | Av. | Max. | Min. | Av. | lb./cu.ft. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |
| 117275/77 | 1 | 28.0 | 27.0 | 27.5 | 10.0 | 9.0 | 9.6 | 34.4 | 5.3 | 1.6 | 3.4 | 96 | 49 | 72 | 23 | 18 | 21 | 22.0 | 16.0 | 19.5 |
| 117278/80 | 2 | 28.1 | 27.2 | 27.8 | 10.2 | 9.4 | 9.9 | 33.7 | 7.2 | 5.2 | 6.2 | 85 | 46 | 66 | 22 | 19 | 20 | 26.0 | 17.0 | 21.2 |
| 117281/83 | 3 | 28.0 | 27.0 | 27.6 | 10.1 | 9.4 | 9.7 | 34.1 | 7.0 | 6.1 | 6.4 | 78 | 4.4 | 64 | 21 | 18 | 20 | 22.5 | 17.0 | 19.7 |
| 117323/25 | 4 | 27.6 | 26.6 | 27.1 | 10.9 | 10.0 | 10:5 | 31.0 | 12.0 | 11.1 | 11.5 | 95 | 54 | 71 | 23 | 19 | 21 | 26.0 | 14.5 | 19.7 |
| 117326/28 | 5 | 27.6 | 26.8 | 27.3 | 10.8 | 9.9 | 10.3 | 31.8 | 11.0 | 8.3 | 9.6 | 99 | 55 | 69 | 23 | 19 | 21 | 24.5 | 16.0 | 19.8 |
| 117329/31 | 6 | 28.0 | 26.2 | 27.1 | 10.7 | 9.4 | 101 | 32.2 | 10.7 | 8.9 | 9.8 | 95 | 43 | 71 | 23 | 19 | 21 | 22.0 | 16.0 | 18.5 |
| 117332/34 | 7 | 27.2 | 268 | 27.0 | 10.7 | 10.1 | 10.3 | 31.5 | 13.5 | 11.1 | 12.3 | 85 | 43 | 64 | 23 | 19 | 21 | 21.0 | 17.5 | 19.0 |
| 117335/37 | 8 | 27.6 | 26.6 | 27.2 | 10.6 | 10.1 | 10.4 | 31.4 | 12.0 | 11.8 | 11.9 | 86 | 45 | 70 | 21 | 18 | 19 | 21.5 | 17.0 | 19.4 |
| 117414/16 | 9 | 27.9 | 27.5 | 27.7 | 10.8 | 9.9 | 10.3 | 32.3 | 9.1 | 2.5 | 4.9 | 84 | 52 | 69 | 23 | 19 | 21 | 22.5 | 17.0 | 19.4 |
| 117417/19 | 10 | 27.2 | 26.4 | 26.8 | 10.5 | 9.8 | 10.1 | 31.8 | 10.0 | 7.3 | 8.5 | 84 | 50 | 67 | 21 | 18 | 19 | 20.5 | 16.0 | 18.4 |
| Average |  |  |  | 27.3 |  |  | 10.1 | 32.4 |  |  | 8.5 |  |  | 68 |  |  | 20 |  |  | 19.5 |

PHYSICAL. CHARACTERISTICS OF 42-IB. I.F.B.S. FOURDRINIER KRAFT L.INER
Mini. J


TABLE: LXXI
PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mill $S$

| Riehle Compression, lb. | Elmendorf Tear, g./sheet |  |  |  |  |  | Amthor Tensile, lb./in. |  |  |  |  |  | Amthor Stretch, \% |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Across | In |  |  | Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | Roll |
| Max. Min. Av. | Max. | Min. | Av. | Max. | Min | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |  |
| $\begin{array}{lll}16.5 & 11.5 & 14.8\end{array}$ | 284 | 222 | 250 | 298 | 244 | 268 | 63.5 | 41.6 | 56.8 | 31.0 | 24.4 | 27.9 |  |  |  |  |  |  |  |
| $\begin{array}{lll}19.0 & 13.5 & 15.6\end{array}$ | 294 | 226 | 253 | 288 | 254 | 270 | 64.3 | 49.1 | 57.2 | 32.2 | 25.4 | 28.9 28.9 | 2.0 | 1.4 | 1.7 | 6.3 | 2.9 4.0 | 4.6 | $\frac{1}{2}$ |
| 16.5111 .0 | 278 | 226 | 250 | 288 | 248 | 269 | 67.4 | 41.1 | 53.9 | 32.5 | 24.2 | 28.5 | 2.4 2.3 | 1.2 | 1.8 | 6.2 | 4.0 2.9 | 5.1 | 2 |
| $\begin{array}{llll}18.0 & 12.0 & 14.4\end{array}$ | 306 | 252 | 281 | 286 | 246 | 269 | 66.0 | 41.5 | 49.7 | 34.7 | 24.2 | 38.5 | 2.3 1.8 | 1.2 | 1.7 | 7.7 | 2.9 2.6 | 5.1 4.8 | 3 |
| $19.0 \begin{array}{lll}13.0 & 15.2\end{array}$ | 328 | 260 | 288 | 340 | 240 | 282 | 58.9 | 38.1 | 50.0 | 35.0 | 23.5 | 29.5 | 1.8 1.8 | 1.3 | 1.6 | 6.3 7.0 | 2.6 2.0 | 4.8 4.6 | 4 |
| $\begin{array}{llll}19.0 & 12.5 & 15.9\end{array}$ | 282 | 240 | 265 | 364 | 252 | 286 | 62.5 | 41.5 | 51.6 | 36.2 | 26.2 | 30.7 |  |  |  | 6.4 |  | 4.6 +8 |  |
| $\begin{array}{llll}18.0 & 13.5 & 15.6\end{array}$ | 348 | 256 | 279 | 356 | 272 | 300 | 56.7 | 39.6 | 49.6 | 36.2 | 26.2 27.1 | 30.7 31.6 | 2.0 2.0 | 1.3 1.3 | 1.6 1.6 | 6.4 | 2.6 | 4.8 | 6 |
| $\begin{array}{lll}18.0 & 13.5 & 16.0\end{array}$ | 316 | 262 | 287 | 332 | 256. | 285 | 57.1 | 41.6 | 49.2 | 34.9 | 26.7 | 31.0 | 1.9 | 1.3 | 1.6 | 6.6 | 2.6 | 4.8 | 7 |
| $\begin{array}{llll}18.5 & 14.5 & 16.7\end{array}$ | 284 | 252 | 265 | 308 | 244 | 269 | 60.1 | 40.6 | 52.2 | 37.9 | 26.2 | 31.0 33.4 | 1.9 | 1.3 | 1.5 | 6.5 | 3.0 | 4.9 4.2 | 8 9 |
| $\begin{array}{llll}19.0 & 14.0 & 16.4\end{array}$ | 320 | 228 | 263 | 300 | 234 | 261 | 60.9 | 46.2 | 52.8 | 36.7 | 26.2 26.7 | 33.4 31.9 | 1.8 1.9 | 1.1 | 1.5 | 5.3 5.6 | 2.6 3.1 | 4.2 4.5 | 9 10 |
| 15.5 |  |  | 268 |  |  | 276 |  |  | 52.3 |  |  | 30.4 |  |  | 1.6 |  |  | 4.7 |  |

## TABLE LKXH

PHYSICAI, CHARACTERISTICS OF .009/26-LR. FOURITRINIER KRANT CORRUGATLNG MEDIUM
Milf. 'T

|  |  | Basis-Weight, It.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in . |  |  | Apparent Density, $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | Moisture, \% |  |  | Bursting Strength, points |  |  | G.E. I'uncture, units |  |  | $\begin{aligned} & \begin{array}{l} \text { Riehle Compres- } \\ \text { sion, } \mathrm{lb} . \end{array} \\ & \text { In } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| File No. | Roll | Max. | Min. | Av. | Max | Min. | Av. |  | Max. | Min. | Av. | Max. | Min | $v$. | Max. | Mitr. |  | Max. | Min. | Av. |
| 118078/80 | 1 | 309 | 28.0 | 29.5 | 11.9 | 10.7 | 11.2 | 31.6 | 11.6 | 9.4 | 10.8 | 60 | 36 | 47 | 24 | 19 | 22 | 160 | 11.5 | 14.2 |
| 118081/83 | 2 | 30.0 | 29.2 | 29.5 | 13.1 | 10.7 | 11.8 | 30.0 | 13.8 | 10.8 | 12.5 | 68 | 31 | 43 | 26 | 18 | 23 | 15.5 | 11.5 | 13.7 |
| 118084/86 | 3 | 26.3 | 25.2 | 25.9 | 10.2 | 8.9 | 9.5 | 32.7 | 14.4 | 12.4 | 13.3 | 74 | 43 | 61 | 22 | 17 | 20 | 22.0 | 14.0 | 18.1 |
| 118087/89 | 4 | 26.8 | 26.4 | 26.6 | 10.1 | 9.2 | 9.5 | -33.6 | 14.2 . | -11.2 | 12.9 | 76 | 43 | . 63 | 23 | 17 | 20 | - 19.5 | 14.0 | 16.9 |
| 118000/92 | 5 | 27.7 | 26.0 | 26.6 | 10.2 | 9.4 | 9.8 | 32.6 | 13.0 | 11.8 | 12.5 | 72 | 42 | 59 | 22 | 17 | 19 | 21.0 | 13.0 | 16.7 |
| 118093/95 | 6 | 27.0 | 25.8 | 26.4 | 10.0 | 9.0 | 9.7 | 32.7 | 12.9 | 11.9 | 12.6 | 75 | 51 | 63 | 23 | 18 | 19 | 22.5 | 13.0 | 15.5 |
| 118096/98 | 7 | 28.3 | 26.3 | 27.1 | 10.4 | 9.4 | 9.9 | 32.8 | 138 | 9.1 | 10.8 | 76 | 41 | 55 | 20 | 14 | 18. | 21.0 | 13.0 | 17.1 |
| 118099/101 - | - 8- | 27.2- | 25.2 | 26.4 | 10.0 | 8.7 | -9.3- | 34.1 | $13.1{ }^{\text {- }}$ | 9.6 | '11.4 | 78 | 47 | 62 | 22 | 17 | 19 | 19.0 | 11.0 | 15.3 |
| 118102/04 | 9 | 27.0 | 24.4 | 25.9 | 10.4 | 9.0 | 9.7 | 32.0 | 12.1 | 9.5 | 10.9 | 74 | 32 | 58 | 23 | 17 | 20 | 20.0 | 11.0 | 15.9 |
| 118105/07 | 10 | 27.4 | 25.3 | 26.4 | 10.0 | 9.1 | $9.5{ }^{\text {² }}$ | 33.3 | $11.6^{-}$ | 10.0 | 10.7 |  | 49 | 60 | 20 | 15 | 18 | 22.5 | 11.0 | 15.8 |
| Average |  |  |  | 27.0 |  |  | 10.0 | 32.5 |  |  | 11.8 |  |  | 57 |  |  | 20 |  |  | 15.9 |

TABLE LXXIII
PHYSICAI. CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mille U

| Institute File No. | Roll | Basis Weight, lb. ( $12 \times 12 / 1000$ ) |  |  | Caliper, 0.001 in . |  |  | Apparent Density. lb. /cu.ft. | Moisture, \% |  |  | Bursting Strength, points |  |  | G.E. Puncture, units |  |  | Riehle Compression, lb . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min | Av. | Max | Min. | Av. |
| 116381/83 | 1 | 26.5 | 26.2 | 26.3 | 11.4 | 99 | 10.7 |  | 29.5 | 12.1 | 110 | 11.6 | 88 | 65. | 74 | 22 | 18 | 21 | 20.0 | 13.0 | 16.8 |
| 116384/86 | 2 | 25.4 | 24.5 | 25.0 | 11.5 | 9.1 | 9.7 | 30.9 | 12.0 | 10.5 | 11.3 | 90 | 52 | 70 | 19 | 17 | 18 | 20.5 | 12.5 | 16.6 |
| 117024/26 | 3 | 27.5 | 26.3 | 26.9 | 11.9 | 10.7 | 11.4 | 28.3 | 9.2 | 8.0 | 8.7 | 75 | 55 | 62 | 22 | 17 | 20 | 23.0 | 14.5 | 19.9 |
| 117027/29 | 4 | 275 | 26.4 | 26.9 | 101 | 9.4 | 9.9 | 32.6 | 9.6 | 8.1 | 9.0 | 71 | 54 | 63 | 23 | 20 | 22 | 24.5 | 18.0 | 20.1 |
| 117030/32 | 5 | 280 | 26.7 | 27.4 | 10.3 | 9.7 | 100 | 32.9 | 11.2 | 6.6 | 8.3 | 83 | 46 | 61 | 26 | 18 | 22 | 22.0 | 14.0 | 18.6 |
| 117033/35 | 6 | 27.8 | 26.8 | 27.2 | 12.2 | 107 | 11.5 | 28.4 | 11.8 | 8.1 | 9.7 | 74 | 54 | 64 | 23 | 18 | 21 | 27.0 | 16.5 | 21.5 |
| 117036/38 | 7 | 26.5 | 25.7 | 26.2 | 9.9 | 9.0 | 9.4 | 33.4 | 9.5 | 8.9 | 9.1 | 70 | 45 | 59 | 22 | 17 | 19 | 240 | 17.5 | 21.6 |
| 117513/15 | 8 | 26.8 | 247 | 26.0 | 10.8 | 9.5 | 10.1 | 30.9 | 94 | 7.9 | 8.8 | 85 | 19 | 65 | 20 | 17 | 19 | 22.5 | 17.0 | 19.3 |
| 117516/18 | 9 | 27.7 | 26.2 | 27.2 | 115 | 10.1 | 10.7 | 30.5 | 8.3 | 7.0 | 7.7 | 87 | 55 | 68 | 21 | 18 | 20 | 26.5 | 20.5 | 23.4 |
| 117519/21 | 10 | 27.7 | 26.6 | 27.1 | 11.5 | 9.9 | 10.4 | 31.3 | 100 | 9.0 | 9.4 | 84 | 55 | 68 | 22 | 16 | 19 | 24.0 | 10.5 | 22.0 |
| 117525/27 | 11 | 28.8 | 26.0 | 27.6 | 11.8 | 10.4 | 11.2 | 29.6 | 8.4 | 8.1 | 8.3 | $8)$ | 55 | 70 | 21 | 17 | 19 | 25.5 | 15.5 | 20.9 |
| 117522/24 | 12 | 28.8 | 27.9 | 28.5 | 12.0 | 11.1 | 11.6 | 29.5 | 11.0 | 7.8 | 9.5 | 89 | 49 | 66 | 2.3 | 19 | 21 | 290 | 15.5 | 21.1 |
| 117780/82 | 13 | 260 | 24.0 | 25.1 | 11.4 | 9.9 | 10.5 | 28.7 | 6.4 | 6.1 | 6.3 | 97 | 42 | 59 | 20 | 15 | 17 | 23.5 | 15.5 | $1{ }^{1} .4$ |
| 117783/85 | 14 | 28.6 | 27.2 | 27.8 | 11.5 | 10.3 | 109 | 30.6 | 7.9 | 5.5 | 6.7 | 76 | 42 | 61 | 23 | 18 | 20 | 24.0 | 18.5 | 20.5 |
| 117786/88 | 15 | 28.4 | 27.6 | 28.1 | 11.4 | 10.7 | 11.0 | 30.6 | 6.1 | 5.3 | 5.8 | 9.3 | 48 | 67 | 22 | 17 | 21 | 23.5 | 14.5 | 19.1 |
| 117789/91 | 16 | 27.5 | 26.4 | 26.8 | 10.8 | 99 | 10.4 | 30.9 | 8.0 | 6.5 | 7.4 | 83 | 23 | 64 | 25 | 18 | 20 | 21.0 | 15.0 | 18.2 |
| 117792/94 | 17 | 28.0 | 27.2 | 27.6 | 11.6 | 10.6 | 11.0 | 30.1 | 92 | 8.1 | 8.7 | 73 | 38 | 59 | 23 | 18 | 22 | 22.0 | 16.5 | 18.8 |
| 117795/97 | 18 | 26.2 | 26.0 | 26.1 | 11.2 | 9.9 | 10.3 | 30.4 | 8.7 | 6.1 | 7.6 | 70 | 43 | 54 | 21 | 17 | 19 | 220 | 14.0 | 18.1 |
| 117995/97 | 19 | 269 | 25.4 | 26.3 | 12.3 | 9.8 | 109 | 28.9 | 6.3 | 4.9 | 5.5 | 94 | 59 | 74 | 19 | 15 | 17 | 22.5 | 18.0 | 20.8 |
| 117998/8000 | 20 | 280 | 27.1 | 27.5 | 12.8 | 10.9 | 11.6 | 28.4 | 8.4 | 7.3 | 7.7 | 86 | 57 | 68 | 22 | 18 | 20 | 19.5 | 130 | 17.8 |
| 118001/03 | 21 | 27.6 | 26.8 | 27.3 | 12.0 | 10.5 | 11.4 | 28.7 | 9.1 | 7.9 | 8.7 | 86 | 50 | 69 | 23 | 18 | 20 | 21.5 | 15.0 | 18.4 |
| . ${ }^{\text {vecage }}$ |  |  |  | 26.9 |  |  | 10.7 | 30.2 |  |  | 8.4 |  |  | 65 |  |  | 20 |  |  | 19.7 |

TABLE INXIL
PHYSICAL CHARACTERISTICS OF . $00 \% / 26-L B$. FOURDRINLER KR.IFT CORRUG.ITING MEIACMI

- MitiL T


TABLE LXXIII
PHYSICAL CHARACTERISTICS OF ,009/26-LB.'FOURDRINIER KRAFT CORRUGATING MEDIUM

| Riehle Compression, lb. |  |  |  |  |  |  |  |  | Mill U |  |  |  |  |  |  |  |  |  |  |  | Roll |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Elmendorf Tear, g./sheet |  |  |  |  |  | Amthor Tensile, lb/in. |  |  |  |  |  |  |  |  |  |  |  |  |
| Across |  |  | In |  |  | Across |  |  | , In |  |  | Across |  |  | In |  |  | Across |  |  |  |
| Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. |  | Max. | Min. | Av | Max. | Min. | Av. | - Max. | Min. | Av. | Max. | Min. | Av. |  |
| 15.5 | 11.5 | 12.9 | 278 | 250 | 264 | 310 | 264 | 291 | 58.4 | 42.3 | 51.7 | 34.4 | 20.7 | 28.5 | 3.4 | 1.7 | 2.5 | 6.0 | 2.0 | 4.8 | 1 |
| 15.0 | 11.5 | 13.0 | 272 | $206^{\circ}$ | 225 | 284 | 220 | 239 | 55.9 | $41.3^{\circ}$ | 48.1. | 34.9 | 20.7 | 29.6 | 27 | 1.9 | 2.4 | 6.4 | 2.5 | 5.2 | 2 |
| 15.0 | 12.0 | 13.2 | 240 | 206 | 224 | 294 | 244 | 272 | 57.9 | 447 | 52.0 | 23.4 | 190 | 21.0 | 2.4 | 1.7 | 2.0 | 6.4 | 3.4 | 5.1 | 3 |
| 175 | 13.5 | 14.9 | 300 | 244 | 276 | 308 | 254 | 280 | 57.6 | 36.4 | 47.8 | 34.9 | 18.6 | 28.8 | 2.1 | 1.1 | 1.6 | 57 | 1.7 | 4.0 | 4 |
| 17.0 | 13.0 | 14.5 | 294 | 240 | 264 | 308 | 250 | 268 | 56.2 | 35.0 | 48.5 | 36.1 | 23.0 | 29.1 | 2.0 | 09 | 1.6 | 5.1 | 2.4 | 4.2 | 5 |
| 15.5 | 11.0 | 13.1 | 270 | 200 | 239 | 304 | 236 | 277 | 61.5 | 47.6 | 54.1 | 21.8 | 17.1 | 207. | 2.3 | 1.4 | 1.9 | 6.4 | 3.6 | 5.0 | 6 |
| 16.0 | 12.0 | 14.3 | 258 | 218 | 241 | 284 | 224 | 254 | 53.8 | 38.1 | 45.3 | 35.2 | 24.0 | 29.5 | 1.9 | 1.3 | 16 | 5.7 | 2.9 | 4.6 | 7 |
| 165 | 11.5 | 13.2 | 268 | 186 | 223 | 286 | 224 | 246 | 61.3 | 489 | 55.4 | 28.3 | 186 | 24.1 | 24 | 1.5 | 2.1 | 6.7 | 2.5 | 5.1 | 8 |
| 170 | 115 | 14.2 | 248 | 208 | 226 | 322 | 238 | 275 | 64.3 | 50.1 | 57.7 | 29.6 | 19.0 | 25.0 | 2.2 | 1.5 | 1.9 | 68 | 3.0 | 5.0 | 9 |
| 190 | 10.0 | 14.0 | 246 | 184 | 221 | 338 | 218 | 258 | 62.3 | 45.0 | 54.6 | 303 | 17.1 | 24.2 | 2.4 | 1.5 | 2.0 | 6.4 | 3.7 | 5.1 | 10 |
| 18.0 | 11.0 | 14.9 | 270 | 212 | 238 | 280 | 230 | 255 | 63.8 | 44.4 | 54.4 | 30.5 | 20.1 | 26.3 | 2.6 | 1.8 | 22 | 6.7 | 3.1 | 4.9 | 11 |
| 17.0 | 12.0 | 13.9 | 292 | 208 | 256 | 318 | 278 | 295 | 67.2 | +5.7 | 58.0 | 28.1 | 176 | 23.3 | 1.7 | 1.2 | 1.5 | 5.7 | 2.8 | 4.3 | 12 |
| 16.5 | 9.5 | 13.5 | 246 | 186 | 209 | 272 | 212 | 238 | 62.1 | 23.2 | 49.6 | 26.2 | 19.0 | 22.6 | 2.5 | 09 | 2.1 | 66 | . 3.3 | 4.9 | 13 |
| 17.5 | 11.5 | 15.0 | 248 | 206 | 229 | 308 | 256 | 283 | 67.4 | 48.6 | 57.7 | 29.0 | 21.3 | 241 | 2.5 | 1.5 | 1.9 | 7.0 | 3.6 | 5.0 | 14 |
| 15.5 | 12.0 | 13.2 | 276 | 212 | 214 | 292 | 252 | 271 | 65.5 | 47.1 | 56.5 | 31.0 | 21.8 | 266 | 2.3 | 1.7 | 20 | 5.1 | 2.9 | 4.1 | 15 |
| 18.0 | 12.0 | 14.4 | 280 | 232 | 256 | 258 | 2.30 | 24.3 | 49.8 | 38.1 | 44.2 | 42.2 | 27.4 | 35.7 | 3.0 | 1.9 | 2.5 | 7.2 | 3.4 | 5.8 | 16 |
| 14.0 | 8.5 | 11.8 | . 266 | 216 | 239 | 298 | 242 | 272 | 69.4 | 42.3 | 55.3 | 27.9 | 21.2 | 24.3 | 2.1 | 1.5 | 1.9 | 7.1 | 3.3 | 52 | 17 |
| 14.0 | 10.0 | 12.1 | 240 | 200 | 220 | 274 | 242 | 259 | 57.7 | 405 | 51.1 | 25.1 | 16.6 | 21.7 | 2.4 | 1.9 | 2.2 | 78 | 28 | 5.0 | 18 |
| 16.5 | 10.0 | 12.9 | 234 | 194 | 210 | 270 | 220 | 243 | 69.8 | 50.8 | 59.4 | 32.2 | 21.8 | 26.7 | 2.4 | 18 | 2.1 | 5.9 | 2.5 | 4.3 | 19 |
| 14.0 | 9.0 | 11.9 | 248 | 224 | 236 | 298 | 260 | 280 | 64.7 | 47.4 | 55.2 | 27.1 | 20.8 | 239 | 2.6 | 1.6 | 2.0 | 5.9 | 2.9 | 4.4 | 20 |
| 15.5 | 10.5 | 12.7 | 322 | 214 | 258 | 346 | 244 | 284 | 61.5 | 44.7 | 55.6 | 27.9 | 20.8 | 24.3. | 2.2 | 1.3 | 1.8 | 6.4 | 2.8 | 4.6 | 21 |
|  |  | 13.5 |  |  | 238 |  |  | 260 |  |  | 53.0 |  |  | 25.7 |  |  | 2.0 | - |  | 4.8 |  |

TABIEE LXXIV
PHYSICAL, CHARACTERISTICS OF $.009 / 26-\mathrm{LB}$. BOGUS CORRUGATING MEDIUM
Mill V


$\qquad$
File No. Roll Max Min. Av. ' Max. Min. Av. lb./cu.ft. Max. Min. Av. Max. Min. Av. Max. Min. Av. Max. Min. Av.


TABLE LXXV
PHYSICAL , CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

## Mile W

|  | Roll | Basis Weight, lb.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in . |  |  | Apparent Density, $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | Moisture, \% |  |  |  |  |  |  |  |  | Riehle Compression, lb. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\begin{array}{r} \text { B } \\ \text { Stren } \end{array}$ | urstin <br> th, p |  |  |  |  |  | G.E. | $\begin{aligned} & \text { Punct } \\ & \text { inits } \end{aligned}$ |  |  | In |  |
| Institute File No. |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |
| 116411/13 | 1 | 28.6 | 27.1 | 28.0 | 10.2 | 9.5 | 10.0 |  | 33.6 | 12.6 | 11.4 | 12.0 | 95 | 56 | 77 | 22 | 17 | 20 | 23.0 | 12.5 | 18.7 |
| 116414/16 | 2 | 28.3 | 27.7 | 28.0 | 10.9 | 10.1 | 10.5 | 320 | 11.8 | 10.9 | 11.4 | 89 | 52 | 70 | 22 | 18 | 20 | 240 | 14.0 | 183 |
| 116417/19 | 3 | 27.6 | 27.3 | 27.5 | 10.5 | 9.7 | 10.2 | 32.4 | 12.1 | 9.9 | 11.2 | 90 | 58 | 74 | 21 | 18 | 19 | 21.5 | 14.0 | 18.2 |
| 116420/22 | 4 | 28.0 | 26.9 | 27.4 | 11.3 | 10.5 | 11.0 | 29.9 | 11.0 | 10.2 | 10.7 | 81 | 57 | 67 | 23 | 18 | 21 | 21.0 | 12.5 | 16.4 |
| 116423/25 | 5 | 28.3 | 27.1 | 27.6 | 12.3 | 10.1 | 10.9 | 30.4 | 13.2 | 12.1 | 12.5 | 91 | 41 | 68 | 24 | 18 | 21 | 24.0 | 15.5 | 19.7 |
| 116435/37 | 6 | 26.3 | 25.5 | 25.9 | 9.3 | 8.8 | 9.0 | 34.5 | 13.9 | 12.8 | 13.2 | 100 | 62 | 74 | 20 | 17 | 18 | 20.0 | 13.0 | 16.0 |
| 116438/40 | 7 | 25.7 | 25.1 | 25.4 | 9.4 | 8.8 | 9.1 | 33.5 | 12.4 | 12.0 | 12.2 | 91 | 53 | 71 | 19 | 16 | 18 | 19.0 | 12.5 | 15.8 |
| 116441/43 | 8 | 26.4 | 25.0 | 25.7 | 9.3 | 8.7 | 9.1 | 33.9 | 10.8 | 9.0 | 10.0 | 95 | 51 | 69. | 20 | 16 | 18 | 21.0 | 14.0 | 17.3 |
| 117057/59 | 9 | 27.6 | 26.9 | 27.4 | 10.9 | 10.1 | 10.4 | 31.6 | 14.5 | 11.7 | 13.5 | 82 | 53 | 66 | 22 | 18 | 20 | 22.5 | 16.0 | 18.9 |
| 117072/74 | 10 | 26.8 | 25.5 | 26.2 | 10.9 | 9.8 | 10.4 | 30.2 | 15.0 | 13.0 | 14.3 | 93 | 47 | 62 | 22 | 16 | 19 | 24.0 | 14.5 | 20.3 |
| 117081/83 | 11 | 26.7 | 25.6 | 26.0 | 9.9 | 8.9 | 9.4 | 33.2 | 12.9 | 9.3 | 11.0 | 90 | 46 | 65 | 21 | 17 | 18 | 22.0 | 15.5 | 18.3 |
| 117747/49 | 12 | 27.7 | 26.8 | 27.2 | 11.3 | 9.9 | 10.6 | 30.8 | 6.5 | 5.8 | 6.1 | 89 | 49 | 65 | 22 | 17 | 20 | 17.5 | 11.5 | 14.9 |
| 117750/52 | 13 | 27.7 | 25.8 | 26.5 | 11.0 | 9.0 | 10.2 | 31.2 | 7.4 | 4.9 | 6.2 | 73 | 49 | 63 | 20 | 17 | 18 | 20.5 | 13.5 | 16.7 |
| Average |  |  |  | 26.8 |  |  | 10.1 | 31.8 | 11.1 |  |  | 69 |  |  |  |  | 19 |  |  | 17.7 |

TABLE LXXIV
PHYSICAL CHARACTERISTICS OF .009/26-LB. BOGUS CORRUGATING MEDIUM
Mill. $V$


TABLE LXXV
PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM Mill W

| Rieh | Com ion, lb | ores- | Elmendorf Tear, g./sheet |  |  |  |  |  | Amthor Tensile, lb./in. |  |  |  |  |  | Amthor Stretch, \% |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | Roll |
| Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |  |
| 15.0 | 10.0 | 12.4 | 276 | 218 | 240 | 356 | 270 | 315 | 74.5 | 57.6 | 64.4 | 28.8 | 19.8 | 23.6 | 2.8 | 2.0 | 2.4 | 4.7 | 2.4 | 3.7 | 1 |
| 15.5 | 10.0 | 12:0 | 250 | 224 | 236 | 350 | 274 | 316 | 69.4 | 49.1 | 61.1 | 26.9 | 17.3 | 22.1 | 2.6 | 2.0 | 2.3 | 4.6 | 1.8 | 3.4 | 2 |
| 14.0 | 10.0 | 12.1 | 250 | 206 | 229 | 370 | 286 | 323 | 64.3 | 55.9 | 60.2 | 26.4 | 17.4 | 22.3 | 2.9 | 1.8 | 2.3 | 4.4 | 2.6 | 3.5 | 3 |
| 14.0 | 8.5 | 10.9 | 296 | 242 | 260 | 364 | 276 | 371 | 62.3 | 46.7 | 54.0 | 24.4 | 16.8 | 20.5 | 2.3 | 1.5 | 1.9 | 4.5 | 2.4 | 3.2 | 4 |
| 15.0 | 10.0 | 12.5 | 288 | 218 | 249 | 354 | 274 | 301 | 64.5 | 37.1 | 51.4 | 24.4 | 17.4 | 20.8 | 2.6 | 1.4 | 2.1 | 5.3 | 3.0 | 4.1 | 5 |
| 14.0 | 8.0 | 11.5 | 238 | 202 | 214 | 330 | 256 | 293 | 67.7 | 45.4 | 59.6 | 26.2 | 17.9 | 22.4 | 2.9 | 2.2 | 2.5 | 4.9 | 3.3 | 4.1 | 6 |
| 13.0 | 7.0 | 10.3 | 232 | 194 | 213 | 338 | 262 | 292 | 67.0 | 50.3 | 56.5 | 23.2 | 19.1 | 20.9 | 2.7 | 1.8 | 2.2 | 4.9 | 2.5 | 3.6 | 7 |
| 13.0 | 7.5 | 10.7 | 254 | 200 | 226 | 372 | 270 | 310 | 68.7 | 46.6 | 55.5 | 27.3 | 19.5 | 22.6 | 3.1 | 2.1 | 2.5 | 5.1 | 2.7 | 3.7 | 8 |
| 14.5 | 10.0 | 11.9 | 238 | 190 | 215 | 336 | 274 | 300 | 59.3 | $42.7{ }^{\prime}$ | 52.9 | 25.7 | 18.6 | 22.2 | 1.5 | 0.7 | 1.2 | 5.9 | 2.5 | 3.9 | 9 |
| 12.5 | 10.0 | 11.7 | 242 | 202 | 221 | 346 | 264 | 304 | 63.7 | 40.8 | 54.2 | 24.4 | 17.6 | 20.9 | 2.4 | 1.1 | 1.9 | 3.6 | 2.2 | 3.0 | 10 |
| 15.0 | 9.0 | 11.7 | 264 | 184 | 214 | 304 | 244 | 269 | 62.8 | 45.5 | 54.8 | 25.1 | 17.6 | 22.0 | 2.4 | 1.6 | 1.9 | 6.2 | 2.9 | 4.5 | 11 |
| 12.5 | 7.5 | 10.3 | 272 | 204 | 231 | 308 | 234 | 277 | 64.7 | 42.8 | 55.3 | 24.5 | 17.3 | 21.6 | 2.2 | 1.4 | 1.9 | 6.8 | 2.6 | 4.1 | 12 |
| 14.0 | 8.5 | 11.7 | 234 | 192 | 212 | 304 | 248 | 276 | 65.0 | 48.9 | 55.8 | 24.5 | 18.6 | 21.8 | 2.4 | 1.8 | 2.1 | 5.8 | 2.9 | 4.3 | 13 |
|  |  | 11.5 |  |  | 228 |  |  | 300 |  |  | 56.6 |  |  | 21.8 |  |  | 2.1 |  |  | 3.8 |  |

Mine. X

| - - |  | Basis Weight, Lb .--$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in . |  |  | Apparent Density, lb./cu.ft. | Moisture, \% |  |  | - Bursting Strength, points |  |  | G.E. Puncture, units |  |  | Riehle Compression, lb . |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Institute <br> File No. | Rol! | Max. | Min. | Av. | Max. | Min. | Av. |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. |  | Max. | Min. | Av. |
| 117117/19 | , | 26.8 | 25.8 | 26.3 | 9.5 | 9.0 | 9.3 | 33.9 | 6.4 | 3.9 | 5.5 | 81 | 49 | 64 | 19 | 16 | 18 | 20.0 | 15.5 | 17.8 |
| 117120/22 | 2 | 28.4 | 26.2 | 27.1 | 9.9 | 9.1 | 9.5 | 34.2 | 7.5 | 6.3 | 6.7 | 83 | 52 | 67 | 21 | 17 | 19 | 23.0 | 13.0 | 18.1 |
| 117284/86 | 3 | 26.5 | 25.6 | 26.0 | 9.6 | 8.9 | 9.2 | 33.9 | 6.6 | 3.8 | 5.1 | 94 | 53 | 71 | 20 | 17 | 18 | 21.5 | 15.5 | 18.1 |
| 117287/89 | 4 | 27.1 | 25.3. | 26.4 | 9.9 | 8.9. | 9.3 | 3-4. 1 | 6.2 | 4.3 | 5.3 | . 89. | 44 | 70 | 21 | .17 | - 19 | -21.0- | 15.5 | 18.7 |
| 118051/53 | 5 | 28.4 | 26.6 | 27.4 | 11.2 | 10.2 | 10.7 | 30.7 | 8.4 | 7.5 | 7.8 | 101 | 49 | 66 | 23 | 18 | 21 | 20.0 | 15.0 | 17.7 |
| 118054/56 | 6 | 29.3 | 26.2 | 27.3 | 12.0 | 10.2 | 10.7 | 306 | 10.8 | 6.9 | 9.0 | 86 | 52 | 68 | 25 | 18 | 21 | 21.0 | 14.5 | 17.5 |
| 118057/59 | 7 | 29.2 | 26.2 | 27.3 | 9.6 | 8.9 | 9.1 | 36.0 | 9.4 | 7.5 | 8.6 | 88 | 57 | 68 | 23 | 18 | 20 | 20.0 | 15.5 | 17.2 |
| $118060 / 62$ | $8{ }^{-}$ | 29.3 | 28.9 | $29.1{ }^{+}$ | 10.6 | 9.0 | 10.1 | 34.6 | 9.8 | 8.4 | 9.1 | 75 | 48 | 63 | 26 | 21 | 24 | 18.0 | 13.0 | 15.7 |
| 118063/65 | 9 | 28.4 | 27.7 | 28.1 | 10.6 | 9.1 | 9.9 | . 34.1 | 8.7 | 7.5 | 8.2 | 94 | 57 | 68 | 25 | 20 | 23 | 19.0 | 13.0 | 16.2 |
| 118127/29 | 10 | 28.5 | 27.1 | 27.7 | 10.5 | 9.3 | 10.0 | 33.2 | 12.8 | 11.5 | 12.0 | 79 | 47 | 67 | 24 | 18 | 21 | 18.5 | 13.0 | 14.7 |
| 1181,30/32 | 11 | 284 | 27.4 | 27.8 | 10.0 | 9.2 | 9.8 | 3.4 .0 | - 11.8 | 10:4 | 11.2 | 79 | 46 | 64 | 23 | 18 | 20 | 23.0 | 14.0 | 17.4 |
| 118133/35 | 12 | 29.5 | 26.8 | 28.1 | 10.3 | 9.0 | 10.0 | 33.7 | 11.3 | 10.7 | 11.0 | 97 | 57 | 75 | 23 | 19 | 22 | 19.0 | 15.0 | 16.8 |
| 1181,36/38 | 13 | 29.5 | 27.8 | 28.5 | 9.9 | 9.0 | 9.5 | 36.0 | 11.9 | 10.4 | 11.2 | 93 | 53 | 70 | 23 | 18 | 21 | 23.0 | 16.0 | 18.8 |
| 1181,39/41 | 14 | 28.3 | 25.0 | 26.7 | 10.7 | 9.2 | 9.9 | 32.4 | 11.3 | 10.7 | 11.1 | 86 | 58 | 68 | 24 | 20 | 22 | 20.5 | 12.5 | 15.3 |
| Average |  |  |  | 27.4 |  |  | 9.8 | 33.7 |  |  | 8.7 |  |  | 68 |  |  | 21 |  |  | 17.1 |

TABLE LXXVII
PHYSICAI. CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUAI
Mine $Y$

| Institute File $\mathrm{N} \%$. | Roll | Basis Weight, th.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in . |  |  | Apparent Density, lb./cu.ft. | Moisture, \% |  |  | Bursting Strength, points |  |  | G.E. Puncture, units |  |  | Riehle Compression, lb. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | Av. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. |
| 116990/92 | 1 | 26.0 | 24.6 | 25.4 | 9.4 | 8.9 | 9.1 |  | 33.5 | 7.5 | 6.6 | 7.2 | 55 | 40 | 48 | 17 | 12 | 15 | 22.5 | 15.5 | 18.5 |
| 116993/95 | 2 | 26.0 | 25.4 | 257 | 9.1 | 8.4 | 8.9 | 34.6 | 9.9 | 7.1 | 8.9 | 82 | 58 | 70 | 14 | 12 | 13 | 27.5 | 21.0 | 24.2 |
| $116996 / 98$ | 3 | 25.8 | 25.0 | 25.3 | 9.5 | 8.9 | 9.1 | 33.4 | 10.2 | 3.9 | 6.8 | 61 | 39 | 48 | 16 | 13 | 1.4 | 20.0 | 13.5 | 17.0 |
| 117453/55 | 4 | 26.4 | 25.7 | 26.0 | 9.8 | 8.9 | 9.5 | 32.8 | 15.0 | 9.5 | 11.7 | 92 | 57 | 72 | 19 | 15 | 17 | 20.0 | 15.0 | 16.9 |
| 117456/58 | 5 | 272 | 26.0 | 26.8 | 10.6 | 9.1 | 9.8 | 32.8 | 8.0 | 6.0 | 7.3 | 98 | 58 | 73 | 19 | 15 | 18 | 23.0 | 16.0 | 18.7 |
| 118204/06 | 6 | 27.5 | 26.7 | 27.0 | 10.1 | 9.4 | 9.8 | 33.1 | 10.9 | 10.2 | 10.5 | 74 | 53 | 65 | 19 | 17 | 18 | 20.0 | 14.5 | 16.8 |
| 118207/09 | 7 | 27.1 | 25.2 | 26.1 | 9.8 | 9.0 | 9.4 | 33.3 | 12.3 | 10.0 | 10.8 | 53 | 39 | 47 | 16 | 12 | 14 | 19.0 | 12.5 | 15.7 |
| 118210/12 | 8 | 27.6 | 26.5 | 27.1 | 8.5 | 7.9 | 8.2 | 39.6 | 12.7 | 12.2 | 12.5 | 65 | 46 | 55 | 14 | 12 | 13 | 18.5 | 13.0 | 14.9 |
| 118213/15 | 9 | 26.8 | 25.5 | 26.1 | 9.5 | 9.0 | 9.2 | 34.0 | 11.8 | 10.1 | 11.1 | 58 | 42 | 51 | 18 | 12 | 13 | 19.0 | 13.5 | 16.0 |
| 118216/18 | 10 | 25.3 | 24.4 | 24.9 | 9.9 | 9.1 | 9.5 | 31.5 | 11.2 | 9.2 | 10.1 | 57 | 32 | 48 | 14 | 12 | 13 | 16.5 | 12.5 | 14.3 |
| Average |  |  |  | 26.0 |  |  | 9.3 | 33.9 |  |  | 9.7 |  |  | 58 |  |  | 15 |  |  | 17.3 |

TABLE LXXVIII
PHYSICAL CHARACTIERISTICS OF . $009 / 26-L B$. FOURDRINIER KRAFT CORRUGATING MEDILIM
Mile \%

| Institute File No. | Roll | Basis Weight, H.$(12 \times 12 / 1000)$ |  |  | Caliper, 0.001 in |  |  | Apparent Density, $\mathrm{lb} . / \mathrm{cu} . \mathrm{ft}$. | Moisture, \% |  |  | Bursting Strength, points |  |  | G.F. Puncture, units |  |  | Riehle Compression, lb. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | In |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Max. | Min. | $A v$. |  |  |  | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Iv. | Max. | Min. | Av. |
| 116931/33 | 1 | 26.7 | 26.2 | 265 | 9.8 | 8.9 | 9.2 |  | 34.6 | 9.0 | 8.0 | 8.4 | 89 | 55 | 70 | 20 | 17 | 19 | 23.0 | 18.0 | 20.2 |
| $116034 / 36$ | 2 | 27.9 | 26.2 | 27.3 | 9.4 | 8.6 | 8.9 | 36.8 | 8.1 | 7.5 | 7.8 | 105 | 56 | 78 | 20 | 17 | 19 | 33.0 | 18.0 | 21.4 |
| 116937/39 | 3 | 28.1 | 26.5 | 27.4 | 10.7 | 9.7 | 10.2 | 32.2 | 8.9 | 8.6 | 8.7 | 77 | 50 | 65 | 25 | 20 | 22 | 21.0 | 14.5 | 17.1 |
| 116940/42 | 4 | 28.1 | 27.5 | 27.9 | 10.3 | 9.0 | 9.5 | 35.2 | 10.1 | 8.3 | 9.1 | 104 | 43 | 85 | 22 | 20 | 21 | 33.0 | 16.0 | 21.0 |
| 1174.38/40 | 5 | 27.0 | 25.9 | 26.5 | 9.8 | 8.8 | 9.3 | 34.2 | 8.8 | 6.0 | 7.5 | 99 | 50 | 73 | 22 | 18 | 20 | 26.0 | 17.5 | 21.3 |
| 117.4.1/43 | 6 | 272 | 25.9 | 26.5 | 9.6 | 8.7 | 9.1 | 34.9 | 10.1 | 8.8 | 9.5 | 102 | 36 | 77 | 20 | 17 | 19 | 24.0 | 15.5 | 20.8 |
| 11744/46 | 7 | 26.8 | 25.7 | 26.4 | 9.5 | 8.7 | 9.0 | 35.2 | 9.6 | 8.5 | 9.1 | 98 | 60 | 79 | 22 | 17 | 19 | 24.0 | 17.0 | 20.9 |
| 117447/49 | $8 \cdot$ | 26.9 | 25.5 | 26.4 | 9.5 | 8.7 | 9.0 | 35.2 | 10.6 | 9.5 | 9.9 | 96 | 62 | 75 | 21 | 17 | 19 | 24.0 | 16.0 | 20.1 |
| 117450/52 | 9 | 27.0 | 25.9 | 26.6 | 9.8 | 8.6 | 9.0 | 35.5 | 12.5 | 9.6 | 10.9 | 98 | 48 | 78 | 22 | 18 | 19 | 25.0 | 15.5 | 20.8 |
| 117465/67 | 10 | 26.9 | 26.4 | 26.6 | 9.9 | 9.0 | 9.4 | 33.9 | 10.5 | 7.3 | 8.6 | 8.4 | 56 | 74 | 22 | 17 | 19 | 22.0 | 15.5 | 18.5 |
| 117468/70 | 11 | 26.5 | 26.0 | 26.3 | 10.1 | 9.0 | 9.4 | 336 | 11.7 | 9.3 | 10.8 | 92 | 49 | 73 | 23 | 18 | 20 | 21.5 | 13.0 | 17.2 |
| Average |  |  |  | 268 |  |  | 9.3 | 34.7 |  |  | 9.1 |  |  | 75. |  |  | 20 |  |  | 19.9 |

TABLE LXXYI

- PHSSIC.NL CHARACTERISTICS OF ,OO9/26-LB. FOURDRINIER KRAFT CORKUGATLNG MEIMLMM.


PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEI)IUM
Minle $Y$

| Rieh | le Com sion, lb | pres- | Elmendorf Tear, g./sheet |  |  |  |  |  | Amthor Tensile, lb./in. |  |  |  |  |  | Amthor Stretch, \% |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | In |  |  | Across |  |  | Redl |
| Max. | Min. | Av. | Max. | Min. | $A v$. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min. | Av. | Max. | Min | Av. | Max | Min. | Av |  |
| 120 | 8.5 | 11.0 | 240 | 164 | 186 | 232 | 170 | 205 | 51.6 | 37.6 | 45.4 | 22.3 | 14.7 | 19.5 | 2.8 | 1.6 | 1.9 | 6.0 | 24 | 3.8. | 1 |
| 17.5 | 12.0 105 | 15.1 12.2 | 200 | 136 168 | 161 183 | 216 | 170 | 188 | 64.3 50.8 | 52.0 | 59.0 | 30.5 | 24.0 | 27.4 | 32 | 2.0 | 2.3 | 4.4 | 23 | 3.1 | 2 |
| 16.0 | 11.5 | 13.7 | 220 | 174 | 194 | 260 | 160 | 185 | 50.8 62.3 | 41.3 430 | 46.3 55.4 | 22.0 | 17.1 | 19.9 | 2.5 | 15 | 21 | 39. | 20 | 3.1 | 3 |
| $16.0{ }^{\text {2 }}$ | 11.5 | 13.7 . | 236 | 190 | 206 | 280 | 192 | 238 | 64.5 | 45.5 | 55.4 | 22.7 | 19.1 | 21.1 | 2.5 | 1.6 | 2.2 1.9 | 5.4 6.0 | 2.6 34 | 3.7 4.6 | 5 |
| 15.5 13.0 | 10.0 9.5 | 13.1 | 258 | 202 | 238 | 300 | 240 | 270 | 63.0 | $49.8{ }^{\text {' }}$ | 540 | 31.3 | 21.7 | 26.6 | 2.5 | 1.6 | 2.1 | 5.4 | 2.2 | 37 | 6 |
| 12.5 | 9.0 | 10.6 | 214 | 148 | 183 | 224 | 192 | 206 | 53.8 | 40.8 | 46.6 | 22.2 | 17.6 | 19.4 | 2.4 | 1.6 | 2.0 | 5.4 | 2.7 | 39 | 7 |
| 14.0 | 9.0 | 11.9 | 200 | 164 | 180 | 274 | 188 | 219 | 54.5 | 42.0 | 49.6 49.0 | 25.6 | 20.1 | 22.4 | 2.4 | 1.6 | 21 | 4.7 | 3.0 | 3.8 | 8 |
| 12.5 | 8.5 | 10.0 | 200 | 162 | 182 | 230 | 176 | 214 | 52.3 | 37.6 | 459 | 21.8 | 19.3 17.4 | 20.2 | 24 2.2 | 1.3 | 19 1.8 | 4.2 3.8 |  | 3.3 3.0 | 9 10 |
|  |  | 12.3 |  |  | 189 |  |  | 219 |  |  | 50.7 |  |  | 22.1 |  |  | 2.0 |  |  | 3.6 | - |

TABLE LXXVIII
PHYSICAI, CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM
Mini $Z$


