# STUDY OF PAPER BOARD QUALITY AS RELATED TO

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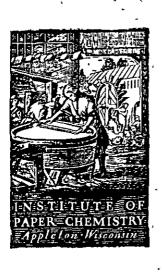
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# FIBER BOX PERFORMANCE

## **REPORT NUMBER I**

Baseline Studies 1. The Evaluation of Current Kraft Liners and Corrugating Mediums





## FOURDRINIER KRAFT BOARD INSTITUTE, INC.

# STUDY OF PAPER BOARD QUALITY AS RELATED TO FIBER BOX PERFORMANCE

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REPORT NUMBER I

Baseline Studies 1. The Evaluation of Current Kraft Liners and Corrugating Mediums

## REPORT TO

FOURDRINIER KRAFT BOARD INSTITUTE, INC.

Appleton, Wisconsin

## THE INSTITUTE OF PAPER CHEMISTRY

OCTOBER, 1945

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7.

BASELINE STUDIES. I. THE EVALUATION OF CURRENT KRAFT LINERS AND CORRUGATING MEDIUMS

#### GENERAL INTRODUCTION

Project 1108 of The Institute of Paper Chemistry is.a long range program of research and development, -which has as its objective the development of the basic information needed for improving the measurement and control of the quality of box components and box performance. It was apparent that an objective scientific approach to this problem would require the development of more adequate means of evaluating the quality of boxes and box components. In other words, it is necessary to create reliable "yardsticks" for the selection of raw materials, for the control of manufacturing and converting variables, for the facilitation of design, and for the measurement and prediction of performance.

The broad outline of procedure for the development of basic information was as follows:

I. Review of literature and previous experience

II. Review of existing test methods

III. Review of available box performance data

IV. Instrumentation or improvement of present testing methods and the development of new methods

- V. Research, testing and development (including field observation of performance and analysis of field hazards) on materials and methods of fabrication related to physical properties and design of
  - A. Paperboard
  - B. Combined board

C. Boxes

VI. Interpretation and application of results

This study was undertaken in 1944 in co-operation with the Fourdrinier Kraft Board Institute, whose membership was composed of the following organizations:

The Brown Paper Mill Company, Inc.

The Chesapeake Corporation

Hummel-Ross Fibre Corporation

International Paper Company, Southern Kraft Division

National Container Corporation

St. Joe Paper Company

Union Bag & Paper Corporation

West Virginia Pulp & Paper Company

These mills produce a substantial percentage of the kraft liner and corrugating board made in this country.

#### INTRODUCTION TO BASELINE STUDY

Essential to any long-range program of this nature is the establishment of a baseline for reference throughout the course of the study. It was decided, therefore, that an index of the quality of the current production of the co-operating mills should be established as a baseline. This baseline was to be determined as accurately as was feasible within the limitations imposed by existing testing techniques and by wartime operating conditions in the paperboard-industry. The baseline study was to be undertaken as early as possible. However, some of the work under Sections I, II, III, and IV outlined above was to be pursued concurrently with the baseline study. The procedure for the establishment of the baseline was divided into two phases.

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The first phase of the baseline study was concerned with the problem of sampling, in a truly impartial cross-sectional manner, the current routine production of the co-operating mills and evaluating these samples as completely as possible by means of existing board testing methods. It is with this phase of the baseline study that the present report is primarily concerned.

As it would have been almost impossible to determine the quality index for each grade currently manufactured by the various mills, it was decided to base the index on 42-lb. D.F.B.S. (dry finish both sides) kraft liner and .009/26-lb. corrugating medium production.

The selection of sample rolls was to be done by representatives of The Institute of Paper Chemistry from converters' warehouse stocks, rather than at the producing mills. The producing mills had no previous knowledge or control of the time or place of sampling or of the identity or quantity of their product sampled. Samples from the selected rolls were evaluated in the laboratories of The Institute of Paper Chemistry. The rolls thus sampled were set aside for subsequent use by The Institute of Paper Chemistry in the second phase of the baseline study.

Phase two of the baseline study involved (1) the selection of the most representative rolls of each mill's sampled production, and (2) the fabrication of these representative rolls into corrugated combined boards and their conversion into boxes. The corrugating operation and the conversion into boxes were to be carried out by an impartial boxmaker under carefully controlled, but normal, conditions of manufacture and according to a predetermined schedule of component combinations. Evaluation of the combined board and boxes produced was then to be carried out at The Institute of Paper Chemistry by means of conventional board and box testing methods.

The purpose of this phase of the baseline study was threefold. First, it would provide information concerning the deviation in test values which may be obtained with a given group of component parts under closely controlled conditions of corrugating and box making. Second, it would provide a further means of comparing the quality of board from the various mills. Third, it would provide additional data required for the establishment of the current quality index—namely, data on combined board and boxes.

In order to complete the baseline study within a reasonable period of time, it was necessary to limit the variables of combination and box design. Accordingly, it was decided that the corrugated board should be "B" flute with starch adhesive and that the combined board should be converted into R.S.C. 24 No.  $2\frac{1}{2}$  can size domestic can boxes with stitched joints.

## SUMMARY

This report covers the first phase of a baseline study which, in turn, is a part of a long-range investigation of paperboard and fiber-box performance.

The results of this phase of the study indicate that the average quality of the sampled 42-lb. D.F.B.S. Fourdrinier kraft liner and of .009/26-lb. kraft and bogus corrugating mediums were as follows:

	Liner	Corrugating Medium
Basis weight, lb./1000 sq. ft.	42.1	26.8
Caliper, in.	0.015	0,010
Apparent density, lb./cu. ft.	33.7	32.3
Bursting strength, points	98	62
G. E. puncture, units	36	18
Moisture, %	8.1	· 9.4
Richle compression, lb.		
In	29.0	17.6
Across	22.5	13.0

6

and the A	مشتغتشيه المستح	- Separate	Corrugating	2010
	- ( • · · ·	" Liner	Medium	•
Elmendorf tear, g./she	et			
In	•	354	223	
Across		394	251	
Amthor tensile, lb./in.				
In		77.8	49.5	
Across		37.8	24.8	
Amthor stretch, %	-			
In		2.1	1.9	•
Across		3.7	4.3	

It should be remembered that these data are based on the actual rolls sampled and on conventional test methods.

- For those tests in-which-orientation of the specimen is specified, the approximate ratios observed in the in-machine direction and in the across-machine direction were as follows:

Ratio
In:Acros
4:3
0.9:1
2:1
1:2

The ratio of the bursting strength to the G. E. puncture test on 42-lb. D.F.B.S. Fourdrinier kraft liner was of the order of 2.7:1.

The ratio was not computed for the .009/26-lb. corrugating medium since the relatively high capacity of the G. E. puncture tester did not allow sufficient subdivision of the scale to permit distinguishing between the low values obtained with any degree of accuracy.

## SAMPLING PROCEDURE

The materials tested were 42-lb. D.F.B.S. (dry finish both sides) Fourdrinier kraft liners and .009/26-lb. kraft and bogus Fourdrinier corrugating mediums. All the component rolls from which the samples were obtained were manufactured by member mills of the Fourdrinier Kraft Board Institute. Inasmuch as some of the members of the Fourdrinier Kraft Board Institute operate more than one mill, it was decided to establish the baseline of current production by giving equal representation to each mill, rather than to each parent company, in the cross-sectional sampling. In this way, the coverage of the field was substantially complete in respect to the quality of board produced by individual mills, as well as within a given company.

The component samples were obtained by three members of the staff of The Institute of Paper Chemistry from full rolls selected at random in a large number of converters' warchouses. An attempt was made to secure sample rolls produced during the first quarter of 1945. Wherever possible, the production period covered by this sampling was narrow enough to be considered current, yet broad enough to eliminate the day-to-day variation in each mill's operation.

At the beginning of this program, each Fourdrinier Kraft Board Institute member submitted a complete list of customers to The Institute of Paper Chemistry. The co-operating converters were chosen by The Institute of Paper Chemistry from these customer lists, partly on the basis of geographic location and partly by the necessity of adequately sampling grades of each mill's production.

The collection of random rolls of liner and corrugating medium proved to be a difficult and laborious task. The hand-to-mouth supply of most converters, caused by the shortage of materials, made it necessary to search more widely and more diligently than had been anticipated. The sampling program was started on March 19, 1945 and completed on May 26, 1945, during which time a total of 280 rolls had been sampled and set aside in 41 converters' warehouses.

The original program called for the sampling of five rolls, selected at random, of each grade of each mill's production in each of four converters' warehouses. The samples from each of the 20 rolls per mill per grade would give a cross-sectional view of the current production for each mill for the grades selected. As may be observed from Table I, it was necessary in some cases to modify the number of rolls sampled because of the scarcity of materials. This was especially true with respect to the corrugating mediums, as additional government restrictions regarding the use of .009/26-lb. kraft corrugating medium went into effect soon after this program of sampling was initiated.

-	•	TA	BLĖ I	•
3	NUMBE	R OF ROLLS	SELECTED PER	R MILL
42	-lb, D.F.	B.S. Liner	.009/26-lb. Co	rugating Medium
Mill	1 1	Roll Samples	Mill	Roll Samples
A		28	5	10
В		21	Т	10
••• C		- 15	U	- 21
D		21	v	13*
E		11	W	13
F		10	х	14
G	-	15	• Y	10
н		14	. 2	iĭ
I		22		
J		21		
	Tota	178		102
* Rome	modium			

\* Bogus medium.

Throughout the roll-sampling program, three samples were taken from each roll. These were designated by the terms right, left, and center, and corresponded to the samples taken from the two sides and center of the roll, respectively. These terms were applied to the roll in the following manner: When the observer faced the roll and the board was unwinding over the top of the roll towards the observer, the right of the roll was on the observer's right and the left on the observer's left. The side samples, rights and lefts, were taken near but always slightly removed from the edge of the roll. The complete identity of each roll was maintained throughout.

The actual sampling technique was as follows: After selecting at random a roll of the desired grade and manufacturer, the outer laps of the roll were removed to a depth of approximately one fourth of an inch until the undamaged portion of the roll was exposed. Three full laps, or their equivalent, of undamaged board were then removed the full width of the roll for test purposes. From the innermost lap selected, a strip approximately one foot long was cut the full width of the roll and three moisture samples were taken from the strip, corresponding to the right, center, and left of the roll. Each moisture sample was cut to approximately one square foot and weighed immediately to obtain the airdry weight. Each of the laps and each of the moisture samples were carefully marked with all the necessary roll identification as to the manufacturer, date manufactured, roll number, width, weight, grade, left and right side, and the name of converter in whose warehouse the rolls were sampled. The materials were carefully wrapped and shipped by Railway Express to The Institute of Paper Chemistry at Appleton, Wisconsin.

Upon their arrival at The Institute of Paper Chemistry, the laps were cut into three sample lots of at least 20 specimens each. The specimens in each sample lot were cut to approximately 13 by 13 inches, thoroughly shuffled, and arranged in two groups of 10 each by alternate selection. One of the groups was used for subsequent testing and the other was stored for future reference. The 10-specimen group selected for testing was again shuffled, and arranged in two groups of five specimens each by alternate selection. One group was used for bursting strength and G. E. puncture test and the other group was used for basis weight, caliper, tear, tensile, stretch, and Riehle compression tests.

## MATERIALS SAMPLED

As previously mentioned, the materials tested consisted of three lots of specimens taken from the outer laps of rolls sampled in a large number of converters' warehouses. The following summarizes the samples taken:

178 rolls of 42-lb. D.F.B.S. Fourdrinier kraft liner

89 rolls of .009/26-lb. Fourdrinier kraft corrugating medium 13 rolls of .009/26-lb. Fourdrinier bogus corrugating medium

The rolls listed above were obtained from 11 different mills. Some mills manufactured both liner and corrugating, whereas others made only liner or corrugating. The breakdown of the rolls as to manufacturers and the number sampled may be seen in Table I.

A list of the converters and the number of rolls sampled in each converter's warehouse is shown in Table II. It should be mentioned that, without the converter's co-operation, this study could not have been made and we wish to acknowledge their co-operation in this work.

## TABLE II

#### LIST OF CONVERTERS

Converter	Num Rolls S	ber of ampled	
Converter		Liner	Corru- gating
Allcraft Corrugated Co.	Harrison, N. J.	3	3
Allied Container Corp.	Boston, Mass.	0	3 5
Atlantic Container Corp.	Long Island, N. Y.	4	0
Atlas Corrugated Case Co., Inc.	Brooklyn, N. Y.	6 5	0
Ball Brothers Co.	Muncie, Ind.	5	0
Baltimore Paper Box Co.	Baltimore, Md.	1	7
Bell Fibre Products Corp.	Marion, Ind.	6	0
Colonial Container Corp.	Brooklyn, N. Y.	1	0
Crescent Box Corporation	Philadelphia, Pa.	5	0 5 5 6
Densen-Banner Co., Inc.	Ridgefield Park, N. J.	. 6	5
Downing Box Co.	Milwaukee, Wis.	10	6
Federal Container Co.	Philadelphia, Pa.	5 2	0
Fort Wayne Corrugated Paper Co.	Chicago, Ill.		6
Fort Wayne Corrugated Paper Co.	Hartford City, Ind.	0·	5
Gaylord Container Corp.	St. Louis, Mo.	6	0
Gibraltar Corrugated Paper Co.,			
Inc.	North Bergen, N. J.	6	3
Grand-City Container Corp.	Brooklyn, N. Y.	2	3 2 5 2
Hankins Container Co.	Cleveland, Ohio	0	5
Hummel & Downing Co.	Milwaukee, Wis.	0	2
Inland Container Corp.	Indianapolis, Ind.	7	0
International Paper Co. (Con-			
tainer Division)	Chicago, Ill.	· 7	7
International Paper Co. (Con-			
tainer Division)	Whippany, N. J.	5	5
Interstate Container Corp.	Glendale, N. Y.	4	0
Jackson Box Co.	Cincinnati, Ohio	7	2
Keystone Box Co.	Pittsburgh, Pa.	0	5 0 2 5 0
F. J. Kress Box Co.	Pittsburgh, Pa.	10	
Lanzit Corrugated Box Co.	Chicago, Ill.	3	3
Liberty Corrugated Container			
Corp.	Brooklyn, N. Y.	1	0
Light Corrugated Box Corp.	Philadelphia, Pa.	9	0

Converter		Num	ber of ampled	المينية. من	, r ,	ېنام
Converter	-	Liner	Corru- gating			
Manufacturers Corrugated Box						
Co., Inc.	Brooklyn, N. Y.	3	_0			
Menasha Wooden Ware Corp.	Menasha, Wis.	3 6	_0 0		•	-
National Box & Specialty Co.	Sheboygan, Wis.	12	4			
National Container Corp. (Long						
Island City Division)	Long Island, N. Y.	10	10			
Owens-Illinois Glass Co.	Gas City, Ind.	3	2			
Pomeroy Manufacturing Co., Inc.	Vincennes, Ind.	5	2 5			
Scharff-Koken Manufacturing Co.	St. Louis, Mo.	Ĝ	0			
Schiffenhaus Bros. Corrugated	,					
	Newark, N J	5	3	•	-	
Superior Paper Products Co.	Pittsburgh, Pa.	2	0			
U. S. Corrugated-Fibre Box Co.	Indianapolis, Ind.	3	0			
David Weber & Co.	Philadelphia, Pa.	ð	2			

#### TESTING PROCEDURES

As previously mentioned, three samples of at least 20 specimens each were taken from each roll selected. The identity of these three roll samples was maintained throughout the entire testing program. The final roll values are based on the averages of the three sample lots.

Prior to testing, all of these roll samples were preconditioned for at least six hours at a relative humidity of not over 35%. After the designated preconditioning period, the samples were conditioned for at least 48 hours and tested in an atmosphere at  $50\pm2\%$  relative humidity and a temperature of  $73\pm3.5^{\circ}$  F. The tests used in this phase of the work were those currently employed and recognized in the industry. The tests performed, together with the test procedures, were as follows.

#### MOISTURE

The airdry weight was determined by the representatives of The Institute of Paper Chemistry in the various converters' warehouses wherein the rolls were sampled. A strip approximately one foot in length, the full width of the roll, was cut from the innermost lap of those obtained from each roll sampled. This crosssectional strip was then cut into three approximately square foot specimens taken at the center and near each end of the roll, which were weighed immediately. These weighed specimens were then forwarded to The Institute of Paper Chemistry where they were dried to constant weight in an oven equipped with forced circulation and maintained at a temperature of  $105 \pm 2^{\circ}$  C. The percentage moisture for each specimen was calculated on the ovendry basis. The final moisture value for each roll was the average of the moisture values of the three specimens taken from each roll.

#### **BASIS WEIGHT**

The basis weight, expressed as the weight per thousand square feet, was determined by weighing five 12 by 12-inch conditioned specimens from each sample on a Toledo basis-weight scale.

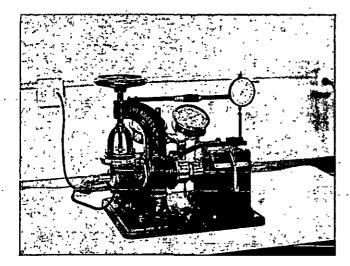


FIGURE 1. Jumbo Mullen tester.

#### CALIPER

The thickness determinations were made with a Cady micrometer on the specimens previously used for the basis weight determination. The machine direction was noted and care was taken to measure and record the average of the values determined at three different points on a line perpendicular to the machine direction across one end of the specimen sheet. Another series of three readings, taken at the opposite end of the specimen sheet, was recorded as a second average. In this manner two values (each being the average of three readings) for each of the five specimens per sample resulted in ten recorded values, the average of which was expressed as the caliper value for that particular sample.

#### BURSTING STRENGTH

Bursting strength tests were performed with a motor-driven "Jumbo" Mullen tester equipped with a 300-pound gage and also with a special attachment for controlling the clamping pressure on the specimen. This tester is shown in Figure 1. Two test readings were obtained on each of five specimens per sample. On each specimen one test was obtained with the diaphragm pressure applied to the wire side and one test with the pressure applied to the felt side.

#### G. E. PUNCTURE TEST

The G. E. puncture tests were carried out with the new model puncture tester shown in Figure 2. TAPPI Method T 803 m-44 was followed, using the same five specimens as were used for determination of bursting strength. Two punctures, one in each direction, were made for each specimen.

#### TENSILE STRENGTH AND STRETCH

The Amthor tensile tester was used for simultaneously indicating the tensile breaking strength and the stretch of the test specimen. This instrument, as shown in Figure 3, is of the pendulum type, having three inde-

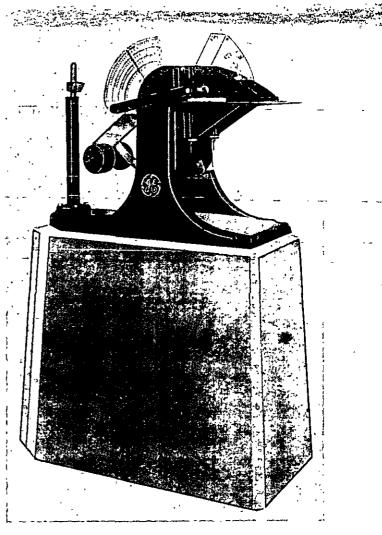


FIGURE 2. General Electric puncture tester.

pendent load-indicating ranges—0 to 15, 0 to 50, and 0 to 200 pounds. At the start of the test the distance between the edges of the jaws of the clamps was equal to 152 mm. (6.0 inches). The width of the test strip was 15 mm. (0.59 inch). Four test strips, two in each direction, were cut from each of the five specimens previously used for basis weight and caliper determinations. The tensile breaking strength per sample was reported as the average of the individual test specimen values expressed in pounds per inch width for each direction.

The stretch value per sample was reported as the average of the individual specimen readings expressed in percentage elongation to failure, based upon an initial test strip length of six inches.

#### Elmendorf Tear

The tear values were obtained using the Elmendorf paper tester shown in Figure 4. Two test strips, one with its long axis in the machine direction and the other with its long axis perpendicular to the machine direction of the sheet, were cut from the unused portion of each of the five specimens originally used for basis weight and caliper determinations. In the text, the term "in-machine direction" tear refers to the tear value obtained when the line of tear was parallel to the machine direction of the sheet. Similarly, the "acrossmachine direction" tear refers to the tear value obtained when the line of tear was perpendicular to the machine direction of the sheet. Only one liner test strip was torn at a time and only one tear value was recorded for each test strip. It was necessary to test four of the corrugating medium test strips simultaneously in order to obtain scale readings between 20 and 60. In this latter case five tear readings were recorded for the four-strip test specimen. The average values in both directions were reported separately.

#### RIEHLE COMPRESSION

The compression values were obtained by the use of a Richle Bros. hydraulic compression tester as shown

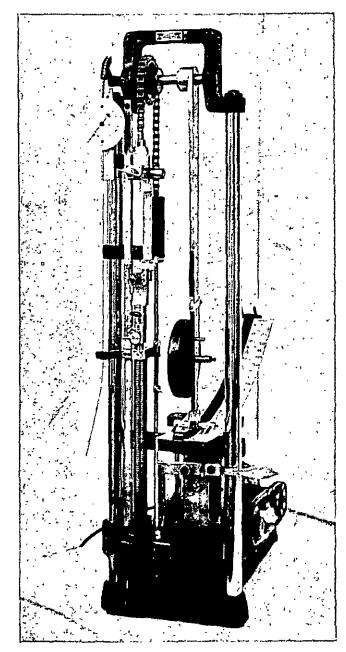


FIGURE 3, Amthor tensile tester.

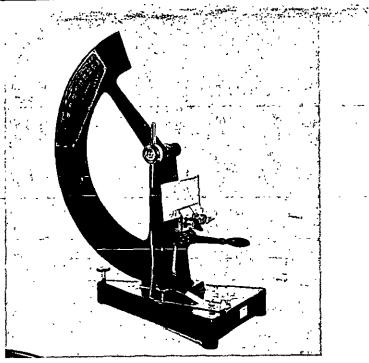


FIGURE 4. Elmendorf paper tester.

in Figure 5. Two 0.5 by 2 inch strips, one in each direction, were cut from the unused portion of each of the five specimens originally used for basis weight and caliper determinations. The compression values were reported as the averages of the individual specimen readings.

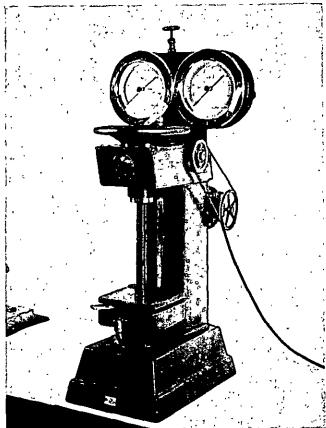


FIGURE 5. Riehle compression tester.

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### PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

#### PROCEDURE

The tests and procedures employed throughout this evaluation study have been described in the previous section. By virtue of the fact that samples could be obtained only from near the outermost portion of each roll, they represent the evaluation of that roll only to the extent that the sampled section was representative of the entire roll and in terms of the methods employed in this evaluation.

For the purpose of comparison of the product within a given mill and also between mills, each Fourdrinier Kraft Board Institute mill making 42-lb. D.F.B.S. Fourdrinier kraft liner has been given an arbitrarily selected code letter. This code identity has been used throughout this report. The Fourdrinier Kraft Board Institute mills producing liner have been identified in this report by the letters A to J, inclusive.

To obtain a more comprehensive and reliable insight into the variation of test values of rolls within a given mill and between mills, as well as to study the uniformity of each mill's product, it was necessary to apply statistical analysis to the test results. The application of statistical methods greatly increases the reliability of any comparison, inasmuch as a measure of the significance of the results is provided.

Statistics is that branch of mathematics which has been designed for the purpose of analyzing numerical results to determine the magnitude and the pattern of one or more of the variable characteristics of the items within the "universe" or group concerned.

The theory of statistics is based on two fundamental concepts: (1) There must exist an equality of opportunity for the chance selection of each and every possible item, and (2) nature has a precise and orderly plan for variation which is revealed whenever some variable factor is measured and the items are grouped numerically in the order of increasing magnitude. In addition, it is necessary that no secondary attributes shall influence the variable under consideration.

When all the possible items in question are subject to the influence of a large number of independent and purely random causes of variation, it is found that the values of the items tend to vary around a mean or most probable value in a given manner. If the causes of variation are truly random and truly independent, it will be found that there is a most probable or mean value which is characteristic of more items than any other given value; that small deviations from this mean value are more frequent than large deviations; and that positive deviations are as frequent as negative deviations. Such a distribution may be illustrated in an experiment in which the variation in height of a number of men is measured. If a *sufficient* number of men are measured and a record is kept of the distribution of the heights (the number of men in each height class), a graph of the distribution of those heights will follow the normal distribution curve as defined by the following equation:

$$Y = \frac{N}{\sigma\sqrt{2\pi}} e^{-i\frac{(x-\hat{x})^2}{\sigma^2}}$$

in which Y = the number of items at a distance x from

- the arithmetical mean or average;
- $\pi = 3.1416;$
- e=2.7183-the base of the Naperian logarithms;
- $\sigma$  = the standard deviation of the array, a measure of variability;
- x = the individual observation value;
- - i.e., the average of all individual observation values; and
- N = the total number of observations made.

The *standard deviation* is, by definition, the square root of the mean square of all the individual deviations measured from the mean of the distribution. It may be computed by the following formula:

$$\sigma = \sqrt{\frac{\Sigma(x-\bar{x})^2}{N-1}},$$

where  $\sigma =$  the standard deviation,

- $\Sigma$  = the operation of summation,
- x = the individual observation value,
- $\bar{x}$  = the mean value of the observed results, and
- N = the number of observations made in the group considered—i.e., the total number

of x values. This can be converted, by the application of the

$$\sigma^2 = \frac{N\Sigma x^2 - (\Sigma x)^2}{N(N-1)}$$

proper algebraic operation, to the following equation:

This latter equation was used in the computation of the standard deviation throughout this report.

The standard deviation is most readily understood if it is thought of as a measure of the degree of dispersion or variability of the items in the universe, aggregate, or population being considered.

By integration, it is possible to determine the area under any section of the distribution curve. The area between any desired limits of x is to the total area under the distribution curve as the number of items between these same limits is to the total number of items. When the limits are established as one standard deviation  $(\pm \sigma)$ , the limits include 68.3% of the total number of items. If two standard deviations  $(\pm 2\sigma)$  are used, 95.5% of the items are included, and if three standard deviations  $(\pm 3\sigma)$  are used, 99.7% of all the items are included.

It should be stressed that the results of the statistical evaluation of the data presented in this report are limited by the small number of rolls which were tested for each mill. It is not to be implied that an exact analysis of a mill's production, over a period of several months, can be obtained by testing only 10 to 30 rolls. However, the results illustrate the application of statistical meth--ods, and also indicate probable trends.

If a greater number of rolls had been included for each mill, the reliability of the statistical methods would have been increased and the results would have had greater significance. As additional surveys of these mills' production are made, a comparison between studies will indicate more reliable trends and facilitate the correlation of results.

#### COMPARISON OF MILL AVERAGES-

The results of the various physical tests performed on the samples of 42-lb. D.F.B.S. Fourdrinier kraft liners have been compiled in Table III on the basis of mill averages. Complete details of the individual tests of the several rolls from each mill are given in Tables LXI-LXX in the Appendix.

The average results obtained for basis weight are shown graphically in Figure 6. The group average basis weight for all the mills participating was 42.1 pounds, which is, for all practical purposes, the same as the specified grade weight. The results indicate that Mills E and I had the highest average basis weight and Mill F the lowest. The average basis weight for all the other mills did not vary from the group average by more than  $\pm 1.0$  pound.

The average caliper results are plotted in Figure 7. The average caliper value obtained for the group was 0.0150 inch. A comparison of the test results indicates

that Mill H had the highest and Mill F the lowest average caliper. However, all the mill averages, except that for Mill F, were within  $\pm 0.001$  inch of the group average.

The average apparent densities in pounds per cubic foot are illustrated graphically in Figure 8. The group average apparent density was 33.7. The highest average apparent density was obtained for Mill F and the lowest for Mills G and H. The average apparent density for all the other mills did not vary from the group average by more than  $\pm 0.5$  pound.

--- From the data presented in Figure 9 it may be observed that the average moisture content for the group was 8.1% on an ovendry basis. The highest average moisture content was obtained for Mill F and the lowest for Mill G. It is interesting to note that Mill F had the lowest average caliper and basis weight but the highest average apparent density and moisture content.

The results obtained for the bursting strength test are presented graphically in Figure 10. The average bursting strength, expressed in points per pound, was 2.33. The group average bursting strength was 98 points. Mills H and I exhibited the highest and Mill F the lowest average bursting strength value.

The averages obtained for the G. E. puncture test are shown in Figure 11. The group average was 36 units, with Mill I possessing the highest and Mill F the lowest average G. E. puncture value. It may be observed that, when the group average for bursting strength is compared with the group average for the G. E. puncture, the ratio is approximately 2.7 to 1. It should be borne in mind, however, that these results were obtained on uncombined liner samples of Fourdrinier kraft board.

The average Riehle compression test results are plotted in Figure 12. The group average of the inmachine direction was 29.0 pounds and of the acrossmachine direction 22.5 pounds. The ratio of the across-machine direction values to the in-machine direc-

## TABLE III COMPARISON OF PHYSICAL CHARACTERISTICS BETWEEN MILLS

LINER

Rolls		Basis Weight, lb. (12 x	Caliper, 0.001	Appar- ent Density,	Mois- ture,	Bursting Strength (Mullen).	G.E. Punc- ture,	Comp	Riehle Compression, lb.		Elmendorf Tear, g./sheet		Amthor Tensile, lb./in.		Amthor Stretch, %	
Mill			in.	lb./cu.ft.	%	points	units	In	Across	In	Across	In	Across	In	Across	
A B C D E	28 21 15 21 11	41.1 42.9 42.7 41.7 43.4	14.8 15.4 14.5 14.8 15.7	33.2 33.4 35.3 33.8 33.2	9.1 8.7 7.1 7.4 7.5	99 101 100 98 91	35 37 39 36 35	28.5 30.6 29.8 28.1 27.5	22.1 23.7 22.2 22.5 20.6	343 353 364 360 324	391 397 405 378 365	78.5 84.1 85.9 70.4 77.1	36.2 38.1 38.9 39.5 34.3	2.2 2.2 1.9 2.0 1.8	3.4 3.8 4.1 3.5 3.6	
F G H I J	10 15 14 22 21	$   \begin{array}{r}     39.7 \\     41.9 \\     42.6 \\     43.5 \\     41.7   \end{array} $	13.4 <sup>-</sup> 15.6 15.9 15.3 14.7	35.6 32.2 32 2 34.2 34.2	10.0 7.0 8.0 8.4 7.7	85 91 108 109 93	33 38 37 41 32	23.3 27.4 30.7 30.9 30.4	18.7 23.7 24.5 21.8 23.7	302 380 386 408 301	343 405 407 465 355	66.7 72.3 75.8 85.4 74.8	33,0 41,8 42,7 36,8 35,9	1.9 1.7 2.2 2.3 2.0	3.1 3.6 4.1 4.5 3.2	
Averag	e 178	42.1	15.0	33.7	8.1	98	36	29.0	22.5	354	394	77.8	37.8	2.1	3.7	

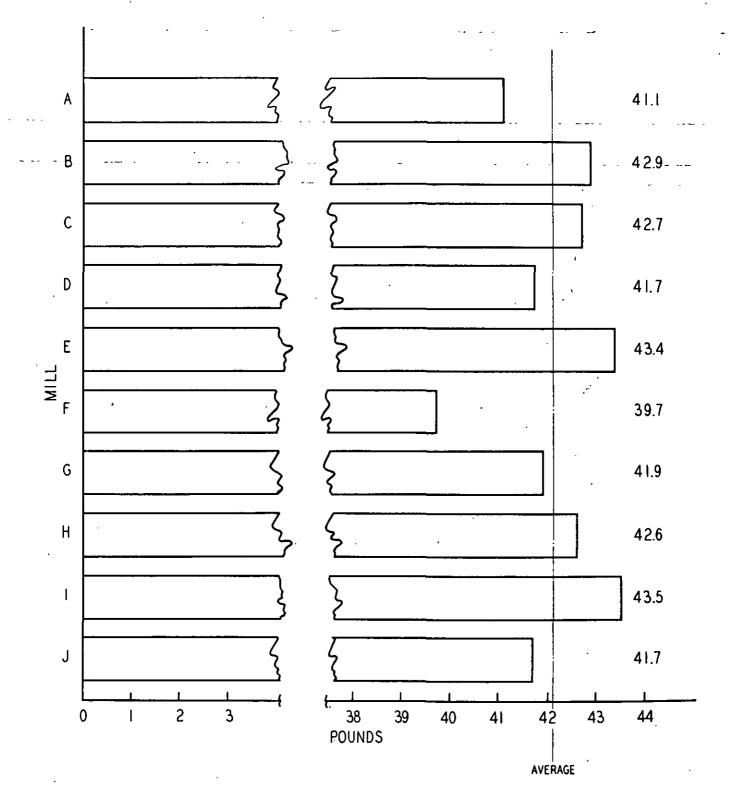


FIGURE 6. Comparison of the average basis weight of 42-lb. Fourdrinier kraft liner among mills.

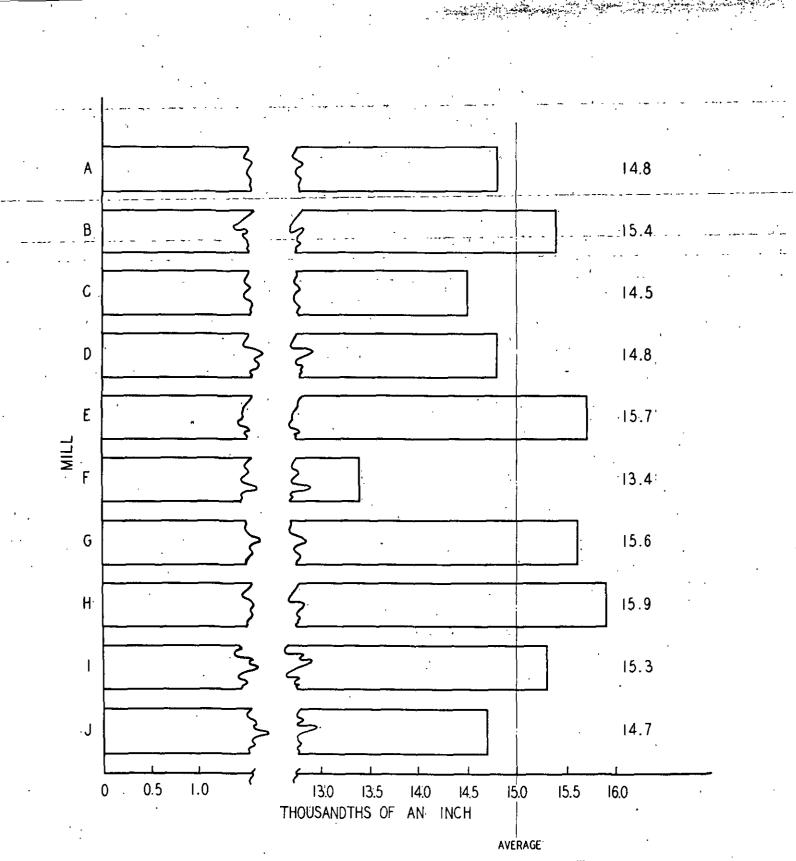
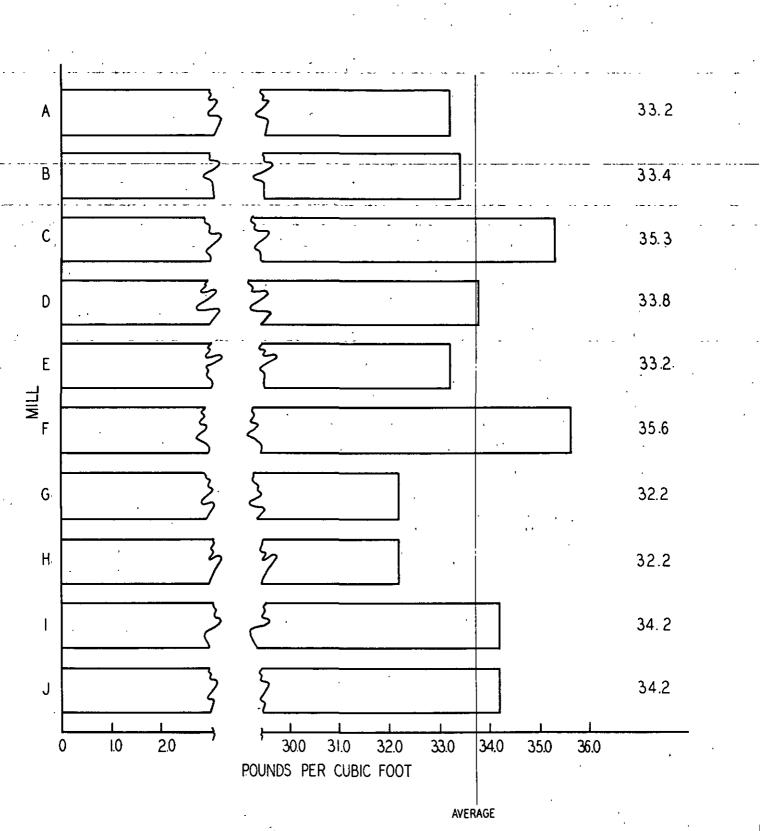


FIGURE 7. Comparison of the average caliper of 42-lb. Fourdr nier kraft liner among mills.



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FIGURE 8. Comparison of the average apparent density of 42-lb. Fourdrinier kraft liner among mills.

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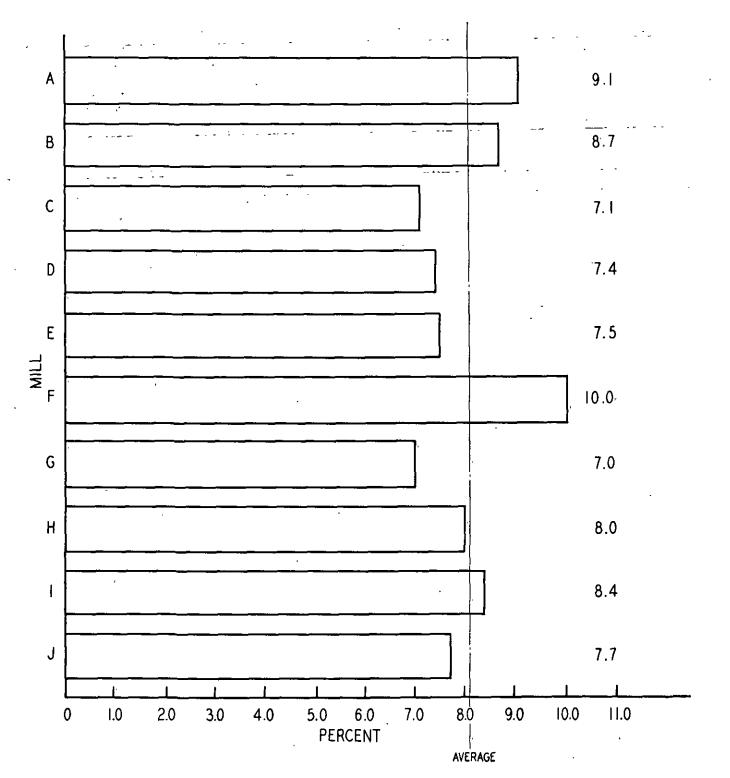


FIGURE 9. Comparison of the average moisture content of 42-lb. Fourdrinier kraft liner among mills.

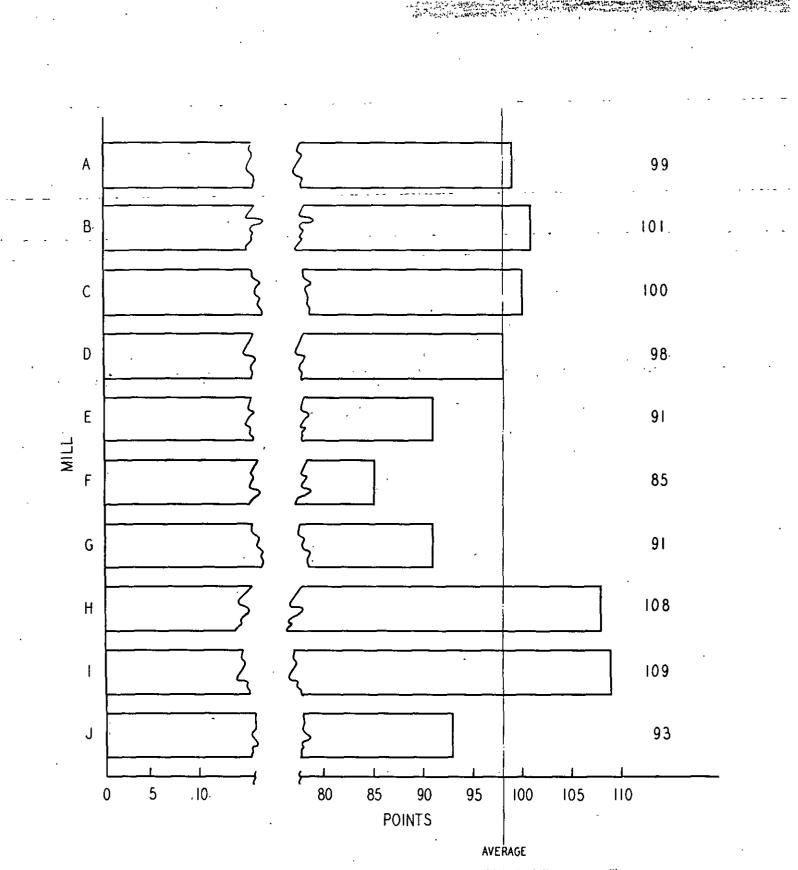
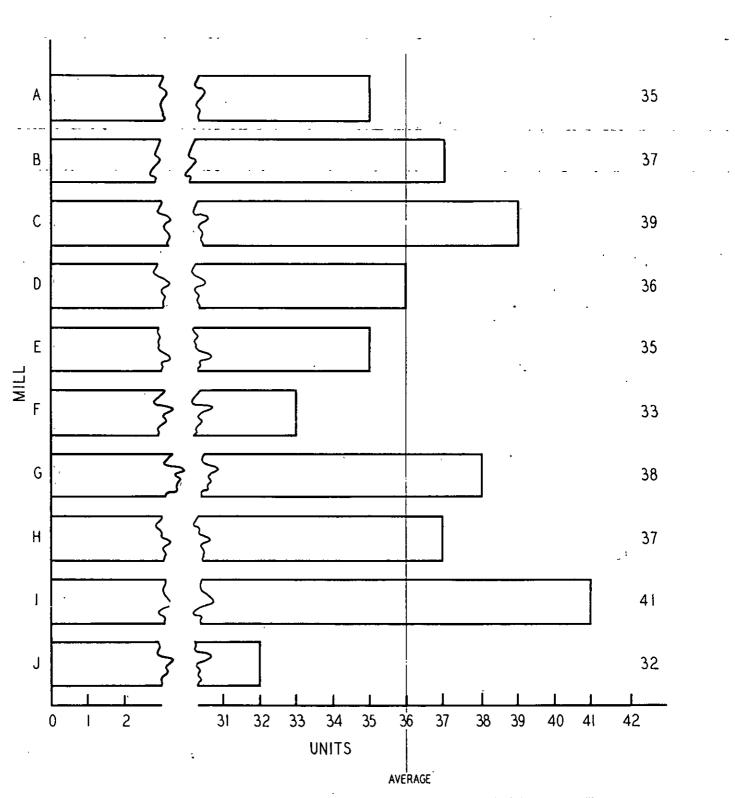


FIGURE 10. Comparison of the average bursting strength of 42-lb. Fourdrinier kraft liner among mills.



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FIGURE 11. Comparison of the average General Electric puncture test of 42-lb. Fourdrinier kraft liner among mills.

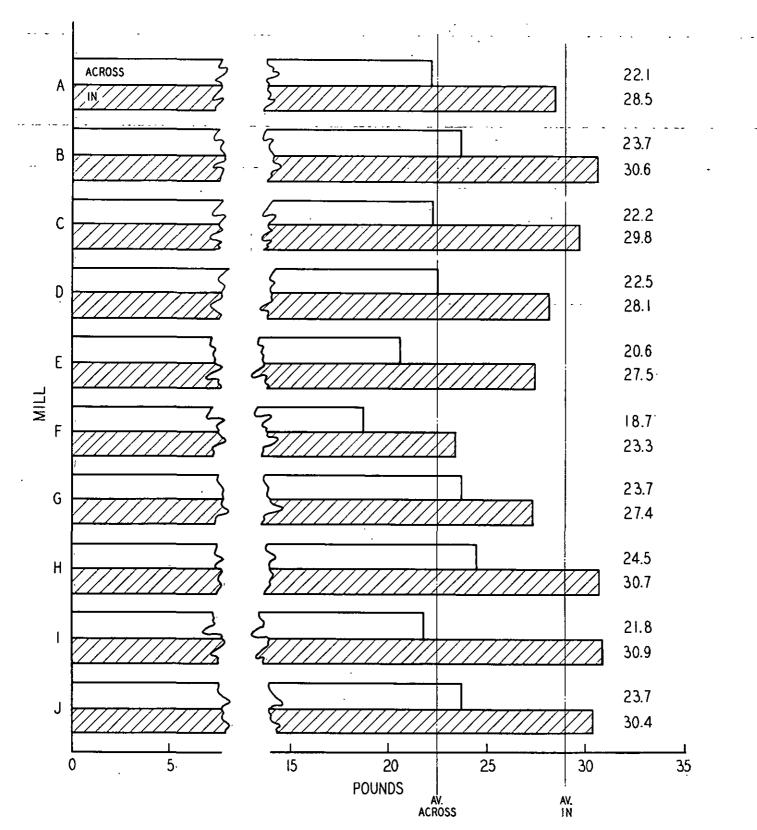


FIGURE 12. Comparison of the average Richle compression test of 42-lb. Fourdrinier kraft liner among mills.

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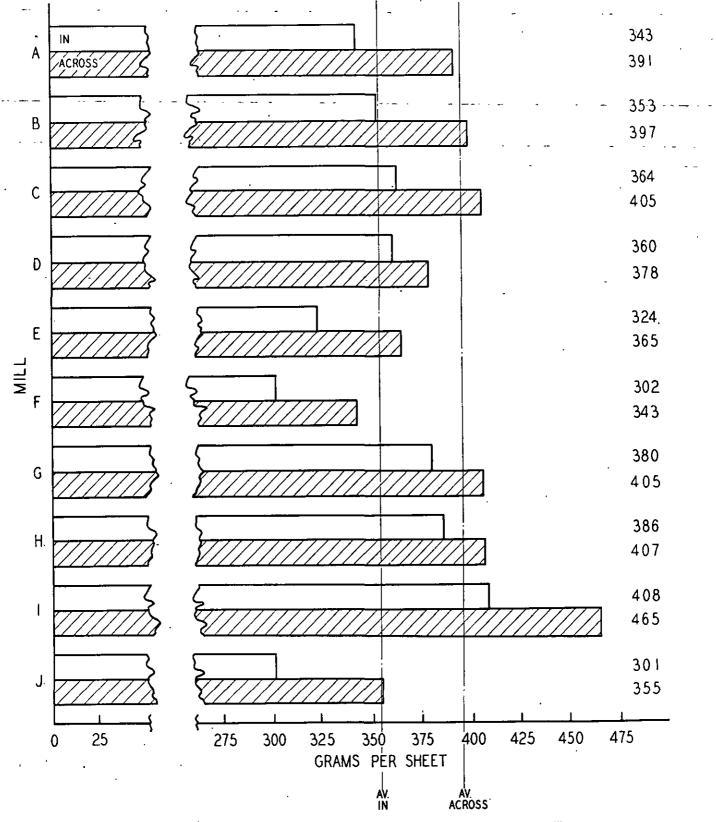


FIGURE 13. Comparison of the average Elmendorf tear of 42-lb. Fourdrinier kraft liner among mills.

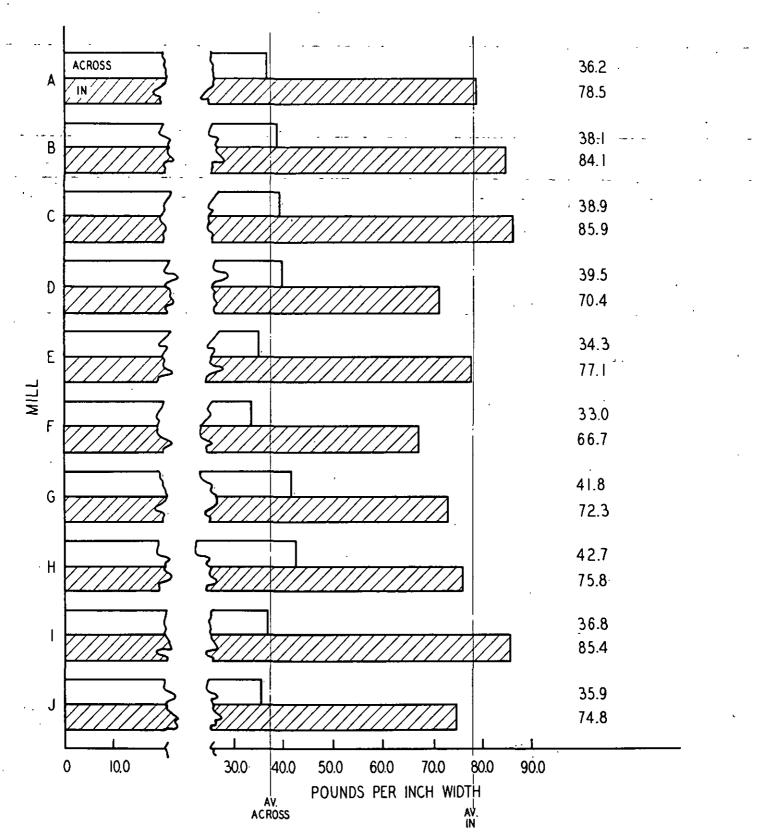


FIGURE 14. Comparison of the average of Amthor tensile strength 42-lb. Fourdrinier kraft liner among mills.

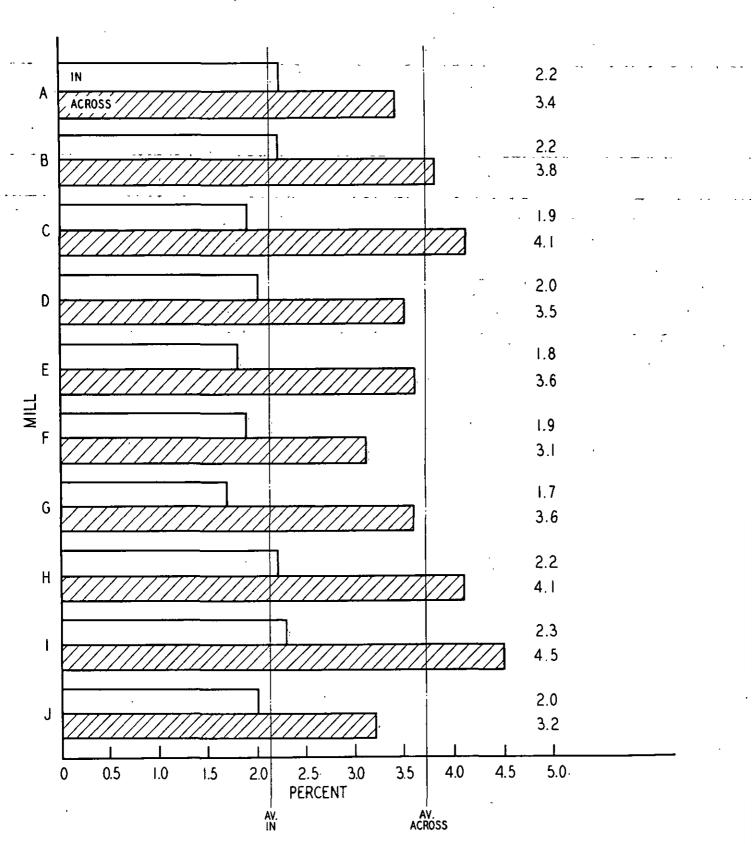


FIGURE 15. Comparison of the average Amthor stretch of 42-lb. Fourdrinier kraft liner among mills.

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tion values is of the magnitude of 5:4. The average results obtained, in both directions, for Mill F were the lowest of all the mills participating; also, the average Riehle compression for the in-machine direction for Mill F was of approximately the same order of magnitude as the group average for the across-machine direction:

The results of the Elmendorf tear test are graphically presented in Figure 13. The group average test results were 354 and 394 grams per sheet for the inmachine and across-machine directions, respectively. The ratio of the group average of the in-machine direction to the group average of the across-machine-direction is of the order of 0.9:1. Mills F and J had the lowest and Mill I the highest tear values in both directions.

The results of the Amthor tensile test are shown in Figure 14. A comparison of the results indicates that the ratio of the across-machine direction values to the in-machine direction values is of the order of 1:2. The group averages obtained were 77.8 and 37.8 pounds per inch width for the in- and across-machine directions, respectively. The averages for Mill F were the lowest in both directions and the averages for Mill C and I were the highest in the in-machine direction; however, Mills G and H were the highest in the acrossmachine direction.

The Amthor stretch results are presented in Figure 15. The group averages obtained were 2.1 and 3.7%, respectively, for in- and across-machine directions. The ratio of the in-machine direction values to the across-machine direction values is approximately 6:10.

A comparison of the averages of all the strength test results indicates that Mills H and I were the highest and Mill F the lowest. The averages for the group would result in a theoretical liner having the following characteristics:

Basis weight, lb.	42.1
Caliper, in.	0.015
Apparent density, lb./cu. ft.	33.7
Bursting strength, points	98
G. E. puncture, units	36
Moisture content, %	8.1
Richle compression, lb.	
In	29.0
Across	22.5
Elmendorf tear, g./sheet	
In	354
Across	394
Amthor tensile, lb./in.	
In	77.8
Across	37.8
Amthor stretch, %	
In	2.1
Across	3'.7

A comparison of the standard deviations of the mills for each test characteristic is given in Table IV. It may be noted from the results for each test characteristic that the basis weight and caliper have the lowest percentage standard deviation and the Amthor stretch the highest. The lower the percentage standard deviation, the less is the indicated variation in that particular characteristic.

In a study of this type it is often of value to know

now the average quality of board made more multi-series in compares with the average quality of the same grade of board produced by other mills. With the above thought in mind, the results tabulated in Table III were treated statistically to determine if there were any significant differences in the physical characteristics obtained for one mill as compared with the average physical characteristics for the balance of the mills participating. Whether or not significant differences exist in the same test characteristic between two different groups of data can be determined by calculating the ratio of the difference of the means of each group to the standard error of the difference between the . same two groups.

The standard error of the difference can be readily calculated from the standard errors of the two meansunder comparison. These standard errors, in turn, can be calculated from the standard deviations listed in Table IV. The following equations are used for these calculations:

S. E. 
$$= \frac{\sigma}{\sqrt{N}}$$
 or  $[S. E.]^2 = \frac{\sigma^2}{N}$ 

where S. E. = standard error,

 $\sigma$  = standard deviation, and N = number of items in array.

 $[S. E.]_{\alpha}^{2} = \frac{[S. E.]_{A}^{2} + [S. E.]_{B}^{2} + \cdots + [S. E.]_{X}^{2}}{n^{2}}$ 

where  $[S. E.]_{\alpha}$  = standard error of a group of similar arrays,

n = number of arrays being considered, and A, B,  $\cdots$ , X = respective arrays under consideration. Therefore,

$$[S. E.]_{\alpha}^{2} = \frac{\frac{\sigma_{A}^{2}}{N_{A}} + \frac{\sigma_{B}^{2}}{N_{B}} + \dots + \frac{\sigma_{X}^{2}}{N_{X}}}{n^{2}} \cdot [S. E.]_{\alpha}^{2} + \sqrt{[S. E.]_{1}^{2} + [S. E.]_{2}^{2}},$$

where [S. E.]<sub>Diff.</sub>=standard error of the difference, and

[S. E.]<sub>1</sub> and [S. E.]<sub>2</sub>=standard errors of the items or groups of items being considered.

These calculations are illustrated by comparing the basis weight of Mill A with that of the other mills as a group in the following manner. First, it is necessary to determine the difference of the means—i.e., the average basis weight for Mill A minus the average basis weight for Mills B to J, inclusive. The average basis weight for Mills A was 41.1 pounds and the average for the group was 42.2 pounds. Thus, the difference of the means is -1.1 pounds, the value being negative, inasmuch as we are comparing Mill A with the group average which, in this case, is of greater magnitude.

#### TABLE IV COMPARISON OF STANDARD DEVIATIONS BETWEEN MILLS

LINER	
-------	--

a		Bas Weig		Bursting		Comp	chle ression, b.	т	iendorf 'ear, /sheet		Tensile, ./in.		nthor .ch, %
N	Mill	· lb.	0.001		units	In	Across	In	Across	In	Across	In	Across
	A	1.13			2.11	1.65	1.15	21.8	18.2	5.19	1.57	0.279	0.363
	B.	1,31	0.7	51 6.42	2.02	2.06	1.24	32.6	21.5	6.34	2.90	0.190	0.446
	С	0.78	5 0.5	37 5.38	2.08	1.60	1.47	14.6	27.4	4.37	3.27	0.219	0.584
	D	1.59	1.0	7 6.51	3.57	1.96	1.25	24.2	28.7	4.56	3.07	0.237	0.441
	C D E	0.98	1 1.1	2 18.6	4.01	2.77	1.68	38.4	47.2	11.2	3.54	0.299	0.437
	F	1.77			4.35	1.55	1.46	33.5	<sup></sup> 36.4	5.09 -	3.87	0.106	0:134
	G	0.75	3 0.3	94 6.08	2.09	1.25	1.63	11.1	23.6	1.84	4.01	0.229	0.556
	H	0.93	7 0.4	05 5.11	2.27	1.82	1.05	39.7	20.3	644	4.05	0.183	0.303
	I		4 0.2	90 4.91	1.46	2.19	1.25	15.8	18.7	3.66	0.996	0.179	0.287
	J	0.8			3.69	1.43	0.920	37.1	42.1	9.54	2.11	-0.204	0.673
Ave		1.1( andard	0.5	84 8.13	2.77	1.83	1.31	26.9	28.4	5.82	2.94	0.213	0.422
	eviatio		3.9	8.3	7.7	6.3	5.8	7.6	7.2	7.5	7.8	10.1	11.4

The square of the standard error of Mill A is calculated from formula (1):

$$[S. E.]_{A}^{2} = \frac{\sigma_{A}^{2}}{N_{A}}$$
 (1)

From Table IV,  $\sigma_A$  is 1.13 and from Table III,  $N_A$  is 28; therefore,

$$[S. E.]_{A}^{2} = (1.13)^{2}/28$$
 or 0.0456.

The squared form is used because it can be substituted directly into formula (3).

The standard error of the group composed of Mill B through Mill J, inclusive, is calculated by the use of formula (2):

$$[S. E.]_{\alpha}^{2} = \frac{\frac{\sigma_{\rm R}^{2}}{N_{\rm B}} + \frac{\sigma_{\rm C}^{2}}{N_{\rm C}} + \dots + \frac{\sigma_{\rm J}^{2}}{N_{\rm J}}}{n^{2}}.$$
 (2)

Substituting the appropriate values from Tables III and IV,

$$[S. E.]_{\alpha}^{2} = \frac{\frac{(1.31)^{2}}{21} + \frac{(0.785)^{2}}{15} + \cdots + \frac{(0.845)^{2}}{21}}{(9)^{2}} = 0.0093.$$

Since

S. E. 
$$]_{\text{Diff.}} = \sqrt{[S. E.]_{A}^{2} + [S. E.]_{\alpha}^{2}},$$
 (3)

therefore,

S. E.]<sub>Diff.</sub> = 
$$\sqrt{(0.0456)^2 + (0.0093)^2} = 0.23$$
.

From these values, the ratio of the difference of means to  $[S. E.]_{Diff.}$  is:

Ratio = 
$$\frac{\text{Difference of means}}{[\text{S. E.]}_{\text{Diff.}}} = \frac{-1.1}{0.23} = -4.8.$$

Throughout this study, it is considered that, if the magnitude of this ratio (i.e., difference of

means/[S. E.]<sub>Diff.</sub>) is less than 2, no significant difference exists. Reference to the appropriate table (normal variability) shows that a ratio of 2.0 indicates that there is a significant difference 95% of the time or that the probability that the difference happened by chance is 1:19. When the ratio is equal to 3.0, the chance probability is greatly decreased (i.e., to about 1:200). Thus the ratio of -4.8, obtained for the comparison of the average basis weight of Mill A with the average of the group B to J, inclusive, indicates that there is a significant difference between the average value obtained for A and the average obtained for the group B to J, inclusive. Since the ratio is negative, it is known at once that the average value obtained for Mill A is lower than the group average.

Similarly, all the test results obtained for Mill A were compared with the group averages obtained for the group B to J, inclusive. These results are given in Table V. The results indicate that there was a significant difference in the values obtained except for bursting strength, Richle compression in both directions, Amthor tensile in the in-machine direction, and Elmendorf tear and Amthor stretch in the across-machine direction. Similarly, all the tests, in which a significant difference was indicated, were of a lower magnitude for Mill A than for the group averages obtained for Mills B to J, inclusive, except Amthor stretch in the inmachine direction, which was slightly higher than the group average.

The results obtained when the averages for Mill B are compared with those of the balance of the group may be seen in Table VI. The results indicate that there was a significant difference in all the values obtained except G. E. puncture, Elmendorf tear in both directions, and Amthor tensile and stretch in the across-machine direction. Similarly, the values for those tests in which a significant difference was indicated were of greater magnitude than the averages obtained for the group.

A comparison of the average values obtained for

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL A WITH THE BALANCE OF THE GROUP LINER

	Basis Weight, lb		Burst- ing Strength,	G E. Punc-	_	hle ession, o.	Elmer Te g./sl	ar,		Tensile, /in		thor ch, %	 -
		0.001 in.		ture, units	In	Across	In	Across	In	Across	ln	Across	
Mean of A	41.1	14.8	99	35	28.5	22.1	343	391	78.5	36.2	2.2	3.4	
Mean of $\alpha$	42.2	15.0	97	36	28.7	22.0	353	391	76.9	37.9	2.0	3.7	
Difference of means $(A - \alpha)$	-1.1	-0.18	+1.8	-1.72	-0.184	+0.151	-10.2	-0.3	+1.55	-1.64	+1.627	→0.3171	
Standard error of <sup>-</sup> difference	0.23	0.028	1.47	0.481	0.352	0.248	4,83	4.40	1.13	0.414	0.056	0.220	
Ratio: $(A - \alpha)/SE_D$	-4.8	-6.5	+1.2	-3.6	-0.5	+0.6	-2.1	-0.1	+1.4	-4.0	+2.9	+1.4	
-Significant -	Yes .	Yes	- No	Yes .	- No.	No	Yes	No	No	Yes	Yes	No	 _

NOTE. All mean values have been reported to the same precision as the individual test values. It will be observed that some of the intermediate values in the above table have been reported to more places than the mean values. Similarly, the difference of the means will not always correspond to the difference between the reported means, because these values have been rounded off. The mean of  $\alpha$  is the mean for the balance of the group.

#### TABLE VI

#### COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL B WITH THE BALANCE OF THE GROUP

			•			LINER						
	Basis Weight, 1b. (12 x 12	Calinan	Burst- ing	G.E. Punc-	Comp	ehle ression, b.	. T	endorf 'ear, sheet		τ Tensile, ./in.		nthor tch, %
		0.001 in.	Strength, points	ture, units	· In	Across	In	Acress	In	Across	In	Across
Mean of <b>B</b>	42.9	15.4	101	37	30.6	23.7	353	397	84.1	38.1	2.2	3.8
Mean of $\alpha$	42.0	15.0	97	36	28.5	21.8	. 352	390	76.3	37.7	2.0	3.7
Difference of means $(B-\alpha)$	5 +0.9·	+0.45	+3.9	+0.79	+2.09	+1.89 <sup>.</sup>	+1.2	+6.9	+7.74	+0.43	+0.23	+0.143
Standard error of difference	0.19	0.173	1.64	0.52	0.476	0.294	7.53	5.42	1.49	0.692	0.045	0.107
Ratio: $(B - \alpha)/SE_D$		+2.6	+2.4	+1.5	+4.4	+6.4	+0.2	+1.3	+5.2	+0.6	+5.1	+1.3
Significant	Yes	Yes	Yes	No	Yes	· Yes	No	No	Yes	No	Yes	No

NOTE. See Note to Table V.

#### TABLE VII

## COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL C WITH THE BALANCE OF THE GROUP

						LINER						
	Basis Weight, lb.		Burst- ing Strength,	G.E. Punc-	Comp	ehle ression, lb.	1	iendorf Fear, /sheet		or Tensile )./in.		nthor tch, %
		0.001 in.		ture, units	In	Across	In	Across	In	Across	In	Across
Mean of C	42.7	14.5	100	39	29.8	22.2	364	405	85.9	38.9	1.9	4.1
Mean of <i>a</i>	42.1	15.1	97	36	28.6	22.4	351	390	76.1	37.6	2.0	3.6
Difference of mean $(C-\alpha)$	s +0.6	-0.55	+2.9	+3.05	+1.27.	-3:85	+13.1	+15.0	+9.78	+1.29	-0.172	+0.43
Standard error of difference	0.22	0.150	1.63	0.601	0:443	0.396	4.54	7.57	1.26	0.888	0.059	0.156
Ratio: $(C-\alpha)/SE_L$	→ +2.7 <sup>′</sup>	-3.7	+1.8	+5.1	+2.9	-4.7	+2.9	+2.0	+7.8	+1.5	-2.9	+2.8
Significant ·	Yes	Yes	No	Yes	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes

NOTE. See Note to Table V.

# TABLE VIII

	Basis Weight, lb. (12 x 12	Caliner	Burst- ing Strength,	G.E. Punc-		LINER thle ression,	Т	endorf ear, sheet		Tensile, ./in.	Am Stret	thor ch, %
	/1000)	0.001 in.		ture, units	In	Across	In	Across	In	Across	În	Across
Mean of D	41.7	14.8	98	36	28.1	22.5	360	378	70.4	39.5	2.0	3.5
Mean of <i>a</i>	42.2	15.0	97	36	28.8	21.9	351	393	77.8	37.5	2.0	3.7
Difference of mean $(D-\alpha)$	-0.5	-0.21	+0.7	-0.53	-0.73	+0.543	· +8.8	-14.3	-7,41	+1.93	-0.077	-0.19
Standard error of difference	0.36	0.239	1.66	. 0.820.	0.457	0.296		. 6.81-	. 1,15	0.726	- 0.055	0.105
Ratio: $(D-\alpha)/SE$		-0.9	+0.4	-0.6	-1.6	+1.8	+2.7	-2.1	-6.4	+2.7	1.4	-1.8
Significant	No	No	No	No	No	No	Yes	Yes	Ves	Yes	No	No
Note. See Note to	-Table V.			<b>, .</b>			<u></u>	•	-		-	

TABLE IX

#### COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL E WITH THE BALANCE OF THE GROUP

						LINER		•				
	Basis Weight, lb. (12 r 12	Caliper,	Burst- ing	G.E. Punc- ture.	Comp	chle ression, b.	Elme T g.			, r Tensile, o./in.		mthor etch, %
	/1000)	0.001 in.		units	In	Across	In	Across	 In	Across	In	Across
Mean of $E$	43.4	15.7	91	35	27.5	20.6	324	365	77.1	34.3	1.8	3.6
Mean of $\alpha$	42.0	14.9	98	36	28.8	22.1	355	394	77.1	38.1	2.0	3.7
Difference of mean $(E-\alpha)$	+1.4	+0.78	-6.8	-1.73	-1.37	-1.5	-31.6	-29.1	-0.02	-3.77	-0.266	-0:054
Standard error of difference	0.31	0.342	5.64	1.231	0.847	0.519	11.77	14.4	3,41	1.10	0,092	0.138
Ratio: $(E-\alpha)/SE$	o -4.7	+2.3	-1.2	-1.4	-1.6	-2.9	-2.7	-2.0	0.0	-3.4	-2.9	-0.4
Significant	Yes	Yes	No	No	No	Yes	Yes	Yes	No	Yes	Yes	No
_												

NOTE. See Note to Table V.

						LINER						
	Basis Weight, Ib. (12 x 12	Calinar	Burst- ing	G.E. Punc-	Comp	chle pression, lb.	1	endorf Fear, 'sheet		or Tensile, ./in.		nthor tch, %
		0.001 in.	Strength, points	ture, units	In	Across	[n	Across	In	Across	In	Across
Mean of F	39.7	13.4	85	33	23.3	18.7	302	343	66.7	33.0	1.9	3.1
Mean of $\alpha$	42.4	15.2	99	37	29.3	22.3	358	396	78.3	38.2	2.0	3.8
Difference of mear $(F-\alpha)$	-2.7	-1.82	-13.9	-3.88	-6.03	-3.66	-55.8	-53.5	-11.57	-5.28	-0.102	-0.684
Standard error of difference	0.57	0.131	3.38	1.39	0.516	0.473	10.83	11.76	1.70	1.252	0.038	0.061
Ratio: $(F-\alpha)/SE_{i}$	o −4.7	-13.9	-4.1	-2.8	-11.7	-7.7	-5.2	-4.5	-6.8	-4.2	-2.7	-11.2
Significant	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Ves	Yes	Yes	Yes

#### TABLE X

#### COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL F WITH THE BALANCE OF THE GROUP

NOTE. See Note to Table V.

# TABLE XI COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL G WITH THE BALANCE OF THE GROUP

· , .

	Basis Weight, Ib.		Burst-	G.E. Punc-		hle ression, b.	ï	endorf 'ear, 'sheet		r Tensile, ./in.		1thor tch, %		
	(12 x 12 /1000)	0.001 in.		ture, units	In	Across	In	Across	ĺn	Across	In	Across		
Mean of,G	41.9	15.6	<b>9</b> 1	38	27.4	23.7	380	405	72.3	41.8	1.7	3.6	••••	
Mean of <i>α</i>	42.1	14.9	98	36	28.9	21.8	349	390	77.6	37.3	2.1	3 7		
Difference of mean $(G-\alpha)$	-0.2	+0.63	-7.1	+1.64	-1.5	+1.92	+31.3	+15.7	-5.36	+4.57	-0.313	-0.095		
Standard error of difference	0.22	0.116	1.79	0.602	0.362	0.435	3.82	6.67	0.75	1.07	0.062	0.149		
Ratio: $(G-\alpha)/SE_D$	-0.9	+5.4	-4.0	+2.7	-4.1	+4.4	+8.2	+2.4	-7.1	+4.3	-5.1	-0.6		
Significant	No	Yes	Yes	Yes <sup>-</sup>	- Yes	- Yes	* * Ves	Yes	' Ves	Ves *	– Yes	- No		

## TABLE XII

## COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL H WITH THE BALANCE OF THE GROUP

						LINER						
	Basis Weight, Ib. (12 x 12		Burst- ing Strength	G.E. Punc-	Comp	ehle ression, lb.		endorf Fear, /sheet		· r Tensile, ./in.		thor ch, %
	/1000)			, ture, units	In	Across	In	Across	In	Across.	In	Across
Mean of <i>H</i>	42.6	15.9	108	37	30.7	24 5	386	407	75.8	42.7	2.2	4.1
Mean of <i>a</i>	42.1	. 14.9	96	36	28.5	21.7	389	349	77.2	37.2	2.0	3.6
Difference of mean $(H-\alpha)$	ıs +0.5	+0.96	+11.3	+1.22	+2.17	+2.85	+17.8	+37.5	-1.40	+5.51	+0.238	+0.421
Standard error of difference	0.27	0.123	1.61	0,661	0.511	0.304	6.06	10.86	1.81	1.114	0.052	0.092
Ratio: $(H-\alpha)/SE$	D +1.9 ·	+7.8 <sup>°</sup>	+9.3	+1.8	+4.2	+9.4	+2.9	+3.5	-0.8	+4.9	+4.6	+4.6
Significant	No	Yes	Yes	No	Yes	s Yes	Yes	s Yes	No	Yes	Yes	Yes
NOTE. See Note to	Table V.						-					

TABLE ATT
COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL I WITH THE BALANCE OF THE GROUP
LINER

	Basis Weight, Ib. (12 x 12	Celiner	Burst- ing	G.E. Punc-		Richle pression, lb.		iendorf Fear, /sheet		or Tensile, Ib./in.		mthor etch, %
	$(12 \times 12)$ (1200)		Strength . points	i, ture. units	In Across		In	Across	In	Across	In	Across
Mean of I	43.5	15.3	109	41	30.9	21.8	465	408	85.4	36.8	2.3	4.5
Mean of $\alpha$	42.0	15.0	96	36	28.5	22.0	346	384	76.2	37.8	2.0	3.6
Difference of mean $(l-\alpha)$	+1.5	+0 32	+12.7	+5.39	+2.39	-0.258	+62.3	+82.3	+9.23	-1.02	+0.269	+0.90
Standard error of difference	0.21	0.085	1.36	0.413	0,493	0.291	4.22	4.84	0.97	0:358	0.042	0 075
Ratio: $(I-\alpha)/SE_D$	+7.1	+3.8	+9.3	+13.1	+4.8	-0.9	+14.8	+17.0	+9.5	-2.8	+6.4	+12.0
Significant	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes	Yes	Yes	Yes	Yes
NOTE. See Note to	Table V.				1							

#### TABLE XIV

COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL J WITH THE BALANCE OF THE GROUP

	Basis Weight, lb. (12 x 12	· ·	Burst- ing Strength,	G.E. Punc- ture,	Compr	ehle ession, b.	Te	endorf ar, sheet	Amthor lb.	Tensile, /in.	Amt	hor 2h, % •
		0.001 in.		units	In	Across	In	Across	In	Across	In	Across
Mean of J	41.7	14.7	93	32	30.4	23.7	301	355	74.8	35.9	2.0	3.2
Mean of $\alpha$	42.2	15.1	98	37	28.5	21.8	358	395	77.4	37.9	2.0	3.7
Difference of mean $(J-\alpha)$ Standard error of	-0.5	-0.38	- <u>5</u> .3	-4.23	+1.91	+1.91	-56.7	-40.6	-2.53	-2.02	+0.029	-0.56
difference	0,21	0.129	2.68	0,846	0.352	0.233	8.44	9.56	2.15	0.540	0.048	0.153
Ratio. $(J - \alpha)/SE_D$	-2.4	-2.9	-2.0	-5.0	+5.4	+8.2	-6.7	-4.2	-1.2	-3.7	+0.6	-3.6
Significant	Yes	. <sup>–</sup> Yes	Yes	Yes <sup>-</sup>	- Yes	-Yes	Yes	· Yes	No	Yes	•	Yes

NOTE. See Note to Table V.

Mill C with the group average excluding C is presented in Table VII. The results indicate that there was a significant difference in all the test values except bursting strength and the Amthor tensile test in the across-machine direction. All the values in which a significant difference existed were greater than the value for the group averages with the exception of caliper, Riehle compression in the across-machine direction, and Amthor stretch in the in-machine direction.

The average test results obtained for Mill D, as compared with the average test results obtained for the remainder of the group, are given in Table VIII. The only test results which exhibited a significant difference were Elmendorf tear and Amthor tensile in both directions. This phenomenon indicates that the average quality of Mill D, as determined by these tests, was approximately the same as the average quality for the group.

A comparison of the average test values obtained for Mill E with the averages for the balance of the group may be observed in Table IX. The results indicate that a significant difference existed in all the test results except those for bursting strength, G. E. puncture, Riehle compression and Amthor tensile in the in-machine direction, and Amthor stretch in the across-machine direction. With the exception of the average caliper value, all the results wherein a significant difference existed were lower than the corresponding value for the group average.

The results of the comparison of the average test values obtained for Mill F with the averages for the balance of the group may be found in Table X. The results indicate that a significant difference existed between all the average test results obtained for Mill F and the corresponding group average. All the average test values obtained for F were lower than the corresponding group average.

. The comparison of the average test values obtained for Mill G with the averages for the balance of the group is given in Table XI. It may be noted that the only test results in which a significant difference was not indicated were in basis weight and Amthor stretch in the across-machine direction.

The average test values obtained for Mill H are compared with the average for the remainder of the group in Table XII. It may be noted that basis weight, G. E. puncture, and Amthor tensile in the inmachine direction were the only test results in which a significant difference was not indicated. Both the basis weight and G. E. puncture, however, appear to be close to the borderline in respect to significance. All the test results for Mill H, wherein a significant difference was indicated, are of a greater magnitude than the corresponding group average value; thus, the average quality for Mill H, as determined by these tests, was higher than the group average.

The comparison of the average test values obtained for Mill I with the average for the balance of the group is presented in Table XIII. A significant difference is indicated in all test results except the Riehle compression in the across-machine direction. With the exception of the Amthor tensile in the across-machine direction, the average test results for Mill I, wherein a significant difference was indicated, were of a greater magnitude than the corresponding average test results of the group.

A comparison of the test averages for Mill J with the average test results obtained for the remainder of the group may be seen in Table XIV. A significant difference was indicated for all the average values except Amthor tensile and stretch in the machine direction. Of those average results showing significant differences, all but the averages of the Richle compression in both directions, were of lower magnitude than the corresponding average values for the group.

#### DISCUSSION OF INDIVIDUAL MILL TEST RESULTS FOR 42-POUND D.F.B.S. FOURDRINIER KRAFT LINER

Mill A

The average results of the various physical tests conducted on the samples of liner rolls made by Mill A are shown in Table XV. Details of the maximum and minimum values for each roll tested are given in Table LXI of the Appendix. The average basis weight was slightly lower than the grade specification of 42 pounds. The average apparent density was 33.2 pounds per cubic foot. It may also be noted that the average bursting strength was 99 points and the average G. E. puncture value was 35 units. The average moisture content was 9.1% on an ovendry basis.

In a study of this type, the interest is not solely in -the absolute value of the average test values within a given mill or among mills, but also in the variation in the individual values which make up those averages. To say that the average of a group of test observations is 100 is of little value unless the uniformity or probability of a given variation of the values which make up this average is known.

The probability of a given variation in board from a given mill may be calculated statistically if test values, based on a sufficient number of individual specimens, are available from an adequate number of rolls from that mill. For each type of test, it is first necessary to calculate the average, and then to calculate the standard deviation as a measure of the variability among the rolls. The procedure may be illustrated for basis weight of the liner samples from Mill A.

For Mill A the average basis weight was 41.1 pounds and the standard deviation was calculated to be 1.13 pounds. Accordingly, reference to the appropriate tables (Probability Integrals) shows that a range of  $41.1 \pm 1.1$  pounds or 40.0 to 42.2 pounds may be expected to contain 68.3% of the rolls of this grade produced by Mill A. In most cases it is of more interest, however, to consider the percentage of rolls which might be expected to be contained within any prespecified test value limits. Thus, assume that it is required to find the chance that the basis weight for a roll will fall within  $\pm 0.5$  pound of the average basis weight. It is noted that 0.5 pound is a fraction (0.5/1.13=0.44) equal to 0.44 of the standard deviation for the basis weight for Mill A. By referring to the appropriate tables, it is found that 34% of the rolls should fall within the selected limits. This indicates that Mill A has a uniformity, in respect to basis weight, such that 34% of the rolls made in the 42-pound grade should be within the limits 40.6 to 41.6 pounds. Using the same line of procedure, it may be shown that a range of  $\pm 1$  pound is equal to 0.88 of the standard deviation for Mill A, and thus the probability of the basis weight being within the limits 40.1 to 42.1 pounds is 62%. (It should be noted in a precautionary way that the probability of a given test value lying within a given range is not doubled when the range is doubled.) As previously mentioned, it is fully recognized that the application of statistical methods to these data has limitations. It is included, however, to demonstrate the potentialities of its application and to predict, within limits, the variation to be expected in the physical characteristics of board made by the different mills.

Table XVI gives the standard deviations and prob-

able variations to be expected in the rolls of 42-pound liner made by Mill A. It may be seen from these results that the chance probability or uniformity for Mill A in regard to caliper is such that the greater portion of the rolls should fall within the range of  $\pm 0.001$ inch (0.0138 to 0.0158 inch) of the average caliper. The uniformity of the bursting strength indicates that only three fourths of the rolls would be expected to fall within a range limit of  $\pm 7.5$  points (91.5 to 106.5) points). On a percentage basis, the uniformity in respect to the G. E. puncture is approximately the same as that for the bursting strength. The uniformity in respect to Riehle compression, Elmendorf tear, and Amthor tensile and stretch may also be observed in-Table XVI. Naturally, as the arbitrarily selected limits increase, the greater will be the percentage of rolls falling within that range. The ranges used are purely arbitrary and are not intended as an attempt to specify acceptable limits. The moisture content was not treated statistically as it was felt that the secondary effects, such as warehouse storage conditions, would possibly prevent the legitimate application of statistics to the moisture data.

#### Mill B

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The average test results obtained on samples of liner made by Mill B are shown in Table XVII (see also Table LXII of the Appendix). The average basis weight was slightly in excess of the specified grade weight. The average caliper was 0.0154 inch and the average apparent density was 33.4 pounds per cubic foot. The average bursting strength and G. E. puncture were 101 points and 37 units, respectively. The average moisture content was 8.7% on an ovendry basis.

The statistical evaluation of these test results may be found in Table XVIII. The standard deviation for the basis weight was 1.31. The results indicate that the uniformity of basis weight for Mill B is such that only 30.0% of the rolls should be expected to fall within the range limit of  $\pm 0.5$  pound (42.4 to 43.4 pounds), approximately 55% within the range limit  $\pm 1.0$  pound (41.9 to 43.9 pounds), and approximately 87% within the range limit of  $\pm 2.0$  pounds (40.9 to 44.9 pounds). The standard deviation for the caliper is 0.75 and thus approximately 82% of the rolls should fall within the caliper range limit of  $\pm 0.001$  inch (0.0144 to 0.0164 inch). The uniformity of the bursting strength as judged by the standard deviation indicates that approximately 30% of the rolls should fall within the bursting strength range limit of  $\pm 2.5$  points (98.5 to 103.5 points), approximately 56% within the range limit of  $\pm 5.0$  points (96 to 106 points), and approximately 76% within the range limit of  $\pm 7.5$  points (93.5 to 108.5 points). In terms of percentage, the uniformity of the G. E. puncture is of approximately the same order of magnitude as the bursting strength. The Richle compression, Elmendorf tear, and Amthor tensile and stretch tests showed rather large standard deviations.

#### TABLE XV

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

#### MILL A Roll Averages

<u></u> .	-		- Basis . Weight, lb.	Caliper		Mois-	Bursting	G.E. Punc-	Comp	ichle ression, b.	- Te	endorf ear, sheet	Ter	thor nsile, /in.		thor ch, %
	Roll	Date Manuf.	(12 x 12 /1000)	0.001 in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across	In	Across	ln	Across
	1 2 3 4	12-30-44 12-30-44 1-20-45 1-20-45	42.1 42.8 40.9 -41.0	14.9 14.8 14.2 14.1	33.8 34.7 - 34.6 - 34.8	9.4	94 99 110 110	39 38 34 35	25.7 27.0 29.0 -28.5	2176 ~	378 366 341 ~336	401 414 406 412 <sup>-</sup>	81.6 83.7 84.6 85.3	38.1 38.8 35.9 37.4 39.8	2.0 2.2 2.7 2.9- 2.8	3.5 3.3 3.7 -3 <del>.</del> 6 3.5
	5 6 7 8 9 10	11-15-44 1-26-45 11-15-44 1-16-45 1-16-45 1-15-45	42 1 42.1 40.1- 39.2 38.5 41.4	14.3 15.1 14.5 14.6 14.5 14.8	35.3 33.4 33.2 32.2 31.8 33.5	13.2 10.7 -11.7 8.4 7.9 7.8	107 111 103 99 90 95	36 37 34 33 31 36	25.8 29.2 29.0 25.9 27.5 27.5	22.7 23.4 22.1 - 20.2 21.2 21.5	387 363 - 351 310 334 350	415 417 396 370 366 - 398	76.8 85.9 78.1 73.8 72.8 81.0	39.8 38.3 37.6 36.1 35.7 36.0	2.4 2.5. 1.7 1.9 2.0	3.7 3.4 2.6 2.8 2.9
	10 11 12 13 14 15	1-15-45 1-15-45 1-15-45 1-15-45 7-1-44 7-1-44	41.4 41.1 41.2 40.7 41.3	15.5 15.3 15.3 15.1 15.2	32.0 32.2 32.3 32.3 32.3 32.6	7.2 6.3 7.0 11.3 12.0	92 88 93 98 104	35 35 37 35 37	28.8 28.1 27.6 31.6 31.6	22.3 21.5 22.0 22.9 22.3	384 349 377 355 357	407 398 418 382 394	82.5 81.7 82.2 70.7 74.0	35.2 34.6 36.0 35.4 33.5	2.0 2.0 1.9 1.9 2.3	3.7 3.5 2.9 3.7 3.7
•	16 17 18 19 20	7-1-44 7-1-44 2-8-45 2-8-45 3-12-45	40.0 39.1 41.9 41.2 41.6	14.6 14.4 15.3 15.0 14.9	32.8 32.5 32.8 32.9 33.5	11.8 10.6 9.1 8.8 9.6	96 88 104 104 99	33 32 34 32 32	31.5 30.0 29.8 28.4 31.2	21.8 22.0 24.4 24.7 21.3	350 333 339 336 319	380 371 404 382 373	69.4 69.4 80.5 86.0 84.3	35.1 33.9 36.9 36.2 35.0	2.2 2.1 2.0 2.2 2.2	4.2 3.8 3.7 3.6 3.5
	21 22 23 24 25	3-11-45 3-14-45 3-15-45 3-15-45 3-14-45	41.2 42.7 40.4 43.3 40.6	14.8 14.9 14.8 15.1 15.0	33.4 34.3 32.7 34.4 32.4	8.1 9.9 7.9 10.1 8.7	101 100 95 98 94	32 36 33 37 34	29.2 27.6 29.4 27.7 27.1	22.7 22.3 22.8 22.6 23.4	313 321 316 331 339	375 370 370 404 357	81.2 77.1 80.7 74.7 70.6	35.7 - 35.2 33.1 36.1 37.1	2.0 2.1 2.0 2.2 2.1	3.2 3.3 3.5 3.4 2.8
	26 27 28	3-14-45 11-15-44 11-15-44	$42.0 \\ 40.5 \\ 40.0$	15.3 14.8 14.6	32 9 32.8 32.8	8.4 7.6 6.0	103 95 99	37 33 33	28.8 28.2 27.5	23.5 21.4 21.5	326 325 320	404 373 385	76.9 74.9 77.3	37.0 37.4 37.5	2.3 2.1 2.0	3:0 3:3 3:4
	l	lverage	41.1	14.8	33.2	9.1	99	35	28.5	22.1	343	391	78.5	36.2	2.2	3.4

#### TABLE XVI

## STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

					MIL	L A						
	Basis Weight, lb.		Bursting	G.E.	Comp	ehle ression, lb.	Т	endorf ear, sheet		Tensile, /in.		Stretch,
	$(12 \times 12)/(1000)$	Caliper, 0.001 in.	points	Puncture, units	In	Across	In	Across	_ In	Across	In	Across
Test values Maximum Minimum Average	43.3 38.5 41.1	15.5 14.1 14.8	111 88 99	39 31 35	31.6 25.7 28.5	$24.7 \\ 20.0 \\ 22.1$	- 387 310 343	418 357 391	86.0 69.4 78.5	39.8 33.1 36.2	2.9 1.7 2.2	4.2 2.6 3 4
Standard deviation	1.13	0.362	6.26	2.11	1.65	1.15	21.8	18.2	5.19	1.57	0.279	0:363
Range limit (±)* Approximate probability, %	0.5 <sub>.</sub> 34	1.0 99	2.5 . 31	1.0 36	1.0 46	1.0 62	7.5 27	7.5 32	1.5 23	1.0 48	0.1 28	0.2 42
Range limit (±)* Approximate	1.0	2.0	5.0	1.5	1.5	1.5	15.0	15.0	3.0	2.0	0.2	0.4
probability, %	62	100	58	52	64	81	51	59	44	80	53.	73
Range limit (±)* Approximate	2.0		7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0,3 - 72	0.6 90
probability, %	92		77	84	93	99	83	90	66	94	14	

\* These range limits were arbitrarily selected.

### TABLE XVII

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

### Mill B Roll Averages

		-	Weight, lb.	Caliper	Appar- ent	`. Mois-	Bursting	G.E. Punc-	Comp	iehle ression, lb.	Те	ndorf ar, heet	Ter	thor sile, /in		nthor tch, %
	Roll	Date Manuf.	(12 x 12 /1000)	0.001 in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across ·	In	Across	In	Across
	1	1-29-45	42.2	15.7	32.2	9.0	101	34	29.7	22.6	337	412	83.6	35.4	2.4	3.6
	2	10-17-44	44.7	15.9	33.7	8.4	106	39	30.2	25.2	394	426	90.0	42.0	2.1	3.3
	3	1-29-45	44.1	15.5	34.1	8.9	105	36	28.7	22.6	356	395	77.6	36.1	2.4	3.9
	-4	3-25-45		13:5	3871	8.2	102		31.3	25:5	415	398	- 71.3	43.8		
	5	3-25-45	41.1	13.8	35.6	8.4	92	35	27.5	23.3	402	367	70.0	41.3	2.0	4.1
	6	12-29-44	42.4	16.0	31.8	9.6	104	37	30.0	22.4	368	428	89.2	38.7	2.1	3 5
	7	2-14-45	-42.0	15.7	32.0	6.8	94 -	. 34	34.0	24.4	346	377	81.4	33.2	2.1	4.1
-	8	2-14-45	42.2	15.3	33.0	6.0	96	35	33.9	25.0	365	397	83.1	36.6	2.1	4.1
	9	2-14-45	42.7	15.9	32.2	6.8		39	29.3	23.8	391	418	78.0	38.3	1.8	3.8
	10	9-25-44	45.0	16.4	32.9	10.8	104	40	31.1	22.5	365	416	89.3	39.4	2.5	3.6
-	11	9-15-44	42.7	15.9	32.2	9.7	91	37	29.1	22.9	329	376	79.9	37.9	2.0	3.2
	12	9-15-44	45.0	16.2	33.3	9.7	103	40	31.6	24.2	373	433	90.1	39.3	2.3	3.3
	13	9-25-44	42.8	15.6	32.9	11.1	103	38	32.3	23.8	352	407	85.7	38.7	2.4	3.5
		9-25-44	43.5	15.7	33.2	9.7	106	39	35.2	25.2	345	407	91.4	39.5	2.4	3.4
	. 14 15	9-25-44	45.7	15.6	35.2	8.1	112	40	32.0	25.5	389	421	89.6	42.4	2.6	38
	16	4-45	41.8	14.8	33.9	9.1	101	36	27.9	22.1	314	379	83.1	35.9	2.3	5.0
	17	4-45	41.8	15.0	33.8	9.6	108	37	30.3	24.3	319	389	92.4	39.3	2.3	3.6
	18	4-45	42.3	16.4	31.0	8.0	93	37	29.4	23.6	319	380	81.2	33.9	2.1	3.5
	19	4-45	42.3	15.1	33.9	7.7	- nii	36	31.3	24.7	332	381	90.9	39.1	2.2	3.8
	20	4-45	41.3	15.0	33.0	8.0	95	35	28.9	22.0	307	371	83.5	34.6	2.3	4.4
										21.7	304	366	83.9	34.8	2.2	4.3
	21	4-45	41.2	14.9	33.2	8.1	98	34	28.7	21.1	304	500	03.9	01.0		
	i	\verage	42.9	15.4	33.4	8.7	101	37	30.6	23.7	353	397	84.1	38.1	2.2	3.8

#### TABLE XVIII

STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

					Mil	l B						
	Basis Weight, lb.	~ "	Bursting	G.E.	Comp	ehle ression, lb.	T	endorf ear, sheet		Tensile, /in.	Amthor	Stretch,
	(12 x 12 /1000)	Caliper, 0.001 in.	Strength, points	Puncture, units	ſn	Across	In	Across	In	Across	ľn	Across
Test values Maximum Minimum Average Standard deviation Range limit (±)*	45.7 41.1 42.9 1.31 0.5	16.4 13.5 15 4 0.75 1.0	111 91- 101 6.42 2.5	40 34 37 2.02 1.0	35.2 27.5 30.6 2.06 1.0	25.5 21.7 23.7 1.24 1.0	415 304 353 32.6 7.5	433 367 397 21.5 7.5	92.4 70.0 84.1 6.34 1.5	43.8 33.2 38.1 2.90 1.0	2.6 1.8 2.2 0.19 0.1	5.0 3.2 3.8 0.45 0.2
Approximate probability, % Range limit (±)*	30 1.0	82 2	30 5.0	38 1.5	38 <sup>.</sup> 1.5	58 1.5	18 15.0	27 15.0	19 3.0	27 2.0	40 0.2	34 0.4
Approximate probability, % Range limit (±)*	55 2.0	99 	56 7.5	54 3.0	53 3.0	77 3.0	35 30.0	52 30.0	36 5.0	51 3.0	71 0.3	63 0,6
Approximate probability, %	87		76	86	86	98	64	84	77	70	89	82

\* Range limits were arbitrarily selected.

## TABLE XIX

## PHYSICAL CHARACTERISTICS OF 42-LB D.F.B.S. FOURDRINIER KRAFT LINER

MILL C Roll Averages

.

	- Date	Basis Weight, lb. (12 x 12	Caliper, 0.001	Appar- ent Density,	Mois- ture,	Bursting Strength,	G.E. Punc- ture,	- Comp	ehle ression, lb.	Т	endorf ear, sheet	Ten	thor isile, /in.		thor ch, %
Roll	Manuf.	/1000)	in.	lb./cu.ft.	%	points	units	In	Across	In	Across	In	Across	In	Across
1 2 3 4 5-	1-29-45 1-29-45 1-29-45 	43.7 42.8 44.0 41.7 42.6	13.7 13.4 14.0 14.2 14.8	38.2 38.3 37.7 35.2 34.5	7.7 7.8 7.7 8.2 -7.4	98 98 109 88 104 -	37 35 38 36 41	28.0 29.4 31.2 -31.2 -31.6	23.1 23.3 24.5 22.8 -23.5	385 356 389 351 377	393 371 389 380 442	81.6 82.7 86.4 76.6 87.2	43.0 43.0 45.0 38.8 -36.2	2.2 2.1 2.2 1.5 1.7	5.0 4.8 4.7 4.3 3.8
6 7 .8 9 10 · ·	8- 9-44 3- 9-45 - 3- 9-45 4- 4-45 4- 4-45	42.2 42.1 - 42.5 42.1 42.3	15.0 14.6 14.9 15.0 14.7	33.8 34.6 34.2 - 33.7 34.5	8.3 7.6 - 8.2 5.5 5.8	09 101 99 99 103	42 41 41 40 40	31.0 29.7 32.8 29.9 28.9	21.4 21.3 22.8 21.1 22.0	361 349 371 376 366	392 440 433 411 401	82.4 87.6 89.8 92.0 85.2	36.9 36.0 37.0 35.7 36.7	1.7 1.8 1.8 1.9 1.8	3.3 3.3 3.9 4.2 4.4
11 12 13 14 15	1-29-45 1- 4-45 1- 4-45 1- 4-45 2- 8-45	43.8 41.8 42.7 42.5 44.0	13.9 15.0 14.9 15.0 14.7	37.8 33.4 34.4 34.0 35.9	5.6 6.6 6.1 6.3 7.1	102 99 93 97 109	38 38 38 38 41	30.3 28.3 27.3 27.6 30.5	24.6 20.6 20.4 19.7 22.3	366 342 357 342 373	368 407 381 403 458	84.7 86.6 84.8 86.1 94.8	44.3 37.9 36.5 36.8 39.4	1.9 1.6 1.8 1.8 2.2	4.5 3.6 3.3 3.5 4.5
A	verage	42.7	14.5	35.3	7.1	100	39	29.8	22.2	364	405	85.9	38.9	1.9	4.1

	-					E XX						
	STICAL	EVALUAT	TION OF P	HYSICAL	TESTS	ON, 42-L1	B. D.F.B.	S. FOURI	ORINIER	KRAFT	LINER	
*					Мп	.r. C						
	Basis Weight, Ib. (12 x 12	Caliper,	Bursting Strength.	G.E. Puncture,	Comp	iehle oresșion; lb.	Т	endorf ear, sheet		r Tensile, ./in.		· Stretch, %
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average Standard deviation	44.0 41.7 42.7 0.785	15.0 13.4 14.5 0.537	109 88 100	42 35 39	32.8 27.3 29.8	24.6 19.7 22.2	389 342 364	458 368 405	94.8 76.6 85.9	45.0 36.0 38.9	2.2 1.5 1.9	5.0 3.3 4.1
Range limit (±)* Approximate probability, %	0.785	0.337 1.0 94	5.38 2.5 35	2.08 1.0 37	1.60 1.0 47	1.47 1 0 50	14.6 7.5	27.4 7.5	4.37 1.5	3.27 1.0	0.219 0.1	0.584 0.2
Range limit (±)* Approximate	1.0	2.0	5.0	1.5	1.5	1.5	39 15.0	21 15.0	27 3.0	24 2.0	35 0.2	27 0.4
probability, % Range limit (±)* Approximate	80 2.0	99 —-	65 7.5	53 3.0	65 3.0	69 <sup>,</sup> 3.0	70 30.0	$\frac{42}{30.0}$	51 5.0	46 3.0	64 0.3	50 0,6
probability, %	99		84	85	94	96	96	72	75	64	83	70

\* Range limits were arbitrarily selected.

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## TABLE XXI

## PHYSICAL CHARACTERISTICS OF 42-LB, D:F.B.S. FOURDRINIER-KRAFT LINER

MILL D Roll Averages

•	T- • Date	Basis Weight, Ib. (12 x 12	- Caliper 0.001	Appar- , ent Density,	Mois- ture,	Bursting Strength,	G E. Punc- ture,	Comp	ehle ression, lb	Т	endorf 'ear, 'sheet	Tei	thor nsile, ./in.		nthor ch, %		
· Roll	Manuf.	/1000)	in.	lb./cu.ft.	%	points	units	In	Across	In	Across	ĺn	Across	In	Across		
1 2 3 4 5	2- 7-45 2- 7-45 2- 7-45 2- 7-45 12-30-44	40.8 40.9 - 41.0 40.3 43.9	14.7 14.7 14.8 14.9 16.7	33.3 33.4 33.2 32.4 31.5	8.6 7.9 7.9 7.1 7.7	94 102 93 	38 37 37 36 44	28.3 28.6 25.8 24.4 27.4	23.3 21.4 22.9 21.1 21.6	355 336 383 375 391	- 374 392 349 347 415	65.3 74.9 65.0 59.3 69.7	41 9 36 0 - 42.0 41.3 39.8	1.8 1.8 1.8 1.6 1.9	3.1 3.0 3.1 2.8 3.2	·	•
- 6. 7. 	12-30-44 8-26-44 1-23-45 3- 5-45	45.4 42.4 40.4 42.3 38.8	16.6 15 3 14.4 16.0 13.3	32.8 33.2- 33.6 31.7 34.9	7.4 9.4 12.4 11.7 4.2	100 -97 102 101 " 91	44 36 34 37 30	28.8 29.9 29.4 30.1 31.4	22.2 23.8 23.4 24.7 23.8	407 384 344 369 320	442 366 373 406 348	72.7 -68.5 71.5 70.9 74.0	38.7 -42.1 40.0 40.3 37.5	2.0 1.8 1.5 1.7 1.9	3.6 - 3.7 - 3.8 - 3.3 - 4.0	- <u>-</u>	• •
11 12 13 14 15	3- 5-45 3-12-45 3-12-45 2-12-45 2-25-45	39.6 41.6 39.7 40.8 42.5	13.0 14.3 12.8 14.3 14.7	36.5 34.8 37.2 34.2 34.7	4.3 7.0 7.4 8.0 6.0	95 94 104 95 102	30 33 32 33 35	31.3 27.0 27.0 26.1 27.8	22.7 24.7 21.8 20.4 21.4	334 378 332 310 366	341 345 335 361 399	76.2 61.5 70.4 70.8 75.5	38.5 46.6 43.7 33.0 38.5	1.9 2.0 2.0 1.9 2.1	4.3 3.3 3.5 3.1 3.1		
16 17 18 19 20	9-26-44 2-25-45 10-11-44 2- 9-45 11- 3-44	43.4 41.9 41.9 43.3 41.0	14.9 14.5 16.8 14.6 15.1	34.9 34.6 29.9 35.6 32.6	6.3 6.6 8.0 6.7 5.5	105 105 86 110 93	35 34 35 36 36	31.1 26.9 25.9 28.2 27.8	23.3 22.5 20.4 21.4 22.4	374 357 370 360 358	409 382 387 402 372	72.3 74.0 67.6 74.3 70.4	41.2 37.5 34.6 38.7 39.3	2.2 2.3 2.0 2.2 2.3	4.3 3.2 3.8 3.7 4.1		
21 /	2- <u>9</u> -45 Verage	42.8 41.7	14.8 14.8	34.7 33.8	6.2 7.4	102 98	38 36	25.9 28.1	22.7 22.5	362 360	398 378	'74.3 70.4	37.3 39.5	2.3 2.0	3.8 3.5		

TABLE XXII

## STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill	D
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	Basis Weight, lb. (12 x 12	Caliper,	Bursting Strength	G.E. Puncture,	Comp	iehle pression, lb.	Т	endorf ear, sheet		r Tensile, /in.		Stretch,
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
Test values												
Maximum	45.4	16.8	110	44	31.4	24.7	407	442	76.2	46.6	2.3	4.3
Minimum	38.8	12.8	84	30	24.4	20.4	310	335	59.3	33.0	1.5	2.8
Average	41.7	14.8	98	36	28.1	22.5	360	378	70.4	39.5	2.0	3.5
Standard deviation	1.59	1.07	6.51	3.57	1.96	1.25	24.2	28.7	4.56	3.07	0.237	0.441
Range limit (±)* Approximate	0.5	1.0	2.5	1.0	1.0	1.0	7.5	7.5	1.5	1.0	0.1	0.2
probability, %	24	65	30	22	39	58	24	21	26	26	33	35
Range limit $(\pm)^*$ Approximate	1.0	2.0	5.0	1.5	1.5	1.5.	15.0	15.0	3.0	2.0	0.2	0.4
probability, %	47	94	56	33.	56	77	46	40	49	48	60	64
Range limit (±)* Approximate	2.0	-	7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0.3	0.6
probability, %	79		75	60.	87	98	79	71	73	67	80	83

\* Range limits were arbitrarily selected.

#### Mill C

The average test results obtained for the liner made by Mill C are given in Table XIX (see also Table LXIII of the Appendix) and the statistical evaluation of these results in Table XX. The results indicate that the average basis weight for Mill C was slightly in excess of the specified weight for this grade. The average caliper was 0.0145 inch and the average apparent density was 35.3 pounds per cubic foot. The average bursting strength and G. E. puncture values were 100 points and 39 units, respectively. The average moisture content was 7.1% on the ovendry basis.

The standard deviation for basis weight for Mill C is 0.785. This rather low standard deviation suggests that approximately 48% of the rolls should fall within a range limit of  $\pm 0.5$  pound (42.2 to 43.2 pounds), 80% within a range limit of  $\pm 1.0$  pound (41.7 to 43.7 pounds), and practically all the rolls within a range limit of  $\pm 2.0$  pounds (40.7 to 44.7 pounds). The standard deviation for the caliper is 0.537, and thus approximately 68% of the rolls should fall within a caliper range limit of  $\pm 0.0005$  inch (0.0140 to 0.0150 inch) and approximately 94% within the range limit of  $\pm 0.001$  inch (0.0135 to 0.0155 inch). The uniformity of the bursting strength indicates that approximately 35% of the rolls should fall within a range limit of 2.5 points (97.5 to 102.5 points), 65% within the range limit of  $\pm 5.0$  points (95 to 105 points), and approximately 84% within a range limit of  $\pm 7.5$  points (92.5 to 107.5 points). Percentagewise, the G. E. puncture is of approximately the same order of uniformity. In general, the standard deviations for the Riehle compression, Elmendorf tear, and Amthor tensile and stretch are of such magnitude as to indicate considerable lack of uniformity within the low arbitrary ranges but rather good agreement within the wider arbitrarily selected ranges.

#### Mill D

The average test results obtained for the liner manufactured by Mill D are shown in Table XXI (see also Table LXIV of the Appendix). The statistical evaluation of these results is given in Table XXII. The average basis weight for Mill D was, for all practical purposes, of the same order of magnitude as the specified grade weight of 42 pounds. This weight and the average caliper of 0.0148 inch resulted in an average apparent density of 33.8 pounds per cubic foot. The average bursting strength and G. E. puncture were 98 points and 36 units, respectively. The average moisture content was 7.4% on an ovendry basis.

Inasmuch as the standard deviation of the basis weight was 1.59, it is to be expected that only 24% of the rolls would fall within a basis weight range limit of  $\pm 0.5$  pound (41.2 to 42.2 pounds), 47% within a range limit of  $\pm 1.0$  pound (40.7 to 42.7 pounds), and 79\% within a range limit of  $\pm 2.0$  pounds (39.7 to 43.7 pounds). On the basis of a standard deviation of

1.07 for caliper, 65% of the rolls should fall within a caliper range limit of  $\pm 0.001$  inch (0.0138 to 0.0158 inch) and only 94% within the range limit of  $\pm 0.002$ inch (0.0128 to 0.0168 inch). The uniformity of the bursting strength, as shown by the standard deviation of 6:51, indicates that only 30% of the rolls should be expected to fall within a bursting strength range limit of  $\pm 2.5$  points (95.5 to 100.5 points), 56% within a range limit of  $\pm 5.0$  points (93 to 103 points), and 75% within a range limit of  $\pm 7.5$  points (90.5 to 105.5 points). The G. E. puncture test results, with an average value of 36 and a standard deviation of 3.57, indicate a slightly greater probable variation than the bursting strength. The standard deviations for the Richle compression, Elmendorí tear, and Amthor tensile and stretch indicate considerable nonuniformity in the narrower range limits selected.

#### Mill E

The average test results obtained for the liner produced by Mill E are given in Table XXIII (see also Table LXV of the Appendix) and the statistical evaluation of these results in Table XXIV. The average basis weight was in excess of the specified grade weight of 42 pounds. The average caliper was 0.0157 inch which results in an apparent density of 33.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 91 points and 35 units, respectively. The average moisture content was 7.5%; however, as may be noted in Table XXIII, the average moisture content is based on the results obtained for only eight rolls.

The standard deviation of 0.981 for basis weight indicates that the basis weight of 39% of the rolls produced should fall within the range limit of  $\pm 0.5$ pound (42.9 to 43.9 pounds), 69% within the range limit of  $\pm 1.0$  pound (42.4 to 44.4 pounds), and 96% within the range limit of  $\pm 2.0$  pounds (41.4 to 45.4 pounds). Mill E has a uniformity with respect to caliper such that 63% of the rolls should fall within the range limit  $\pm 0.001$  inch (0.0147 to 0.0167 inch) and 93% within the range limit  $\pm 0.002$  inch (0.0137 to 0.0177 inch). The standard deviation of 18.6 for the bursting strength indicates extreme nonuniformity with the probable chance variation that only 31%should fall within the range limit of  $\pm 7.5$  points (83.5) to 98.5 points). It may be observed, however, that Rolls 1 and 2 were extremely low in all test results and, since there were only 11 rolls sampled of this mill's product, the effect of these rolls is considerable. In all probability, the presence of these two rolls has distorted the uniformity far more than practical consideration would permit. If the standard deviation for bursting strength were calculated after excluding Rolls 1 and 2, it would be 5.45 as compared with 18.6 when these two rolls are included. On the basis of statistics, however, it is not permissible to exclude these roll values.

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## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

MILL E Roll Averages

	-	Basis Weight, lb.	Caliper,		Mois-	Bursting	G.E. Punc-	Comp	ehle ression, b.	· • Te	endorf ear, - sheet	Ter	thor sile, - /in.		nthor ich, %
Roll	Date Manuf.	(12 x 12 /1000)	0.001 in.	Density, lb./cu. ft.	ture, %	Strength, points	ture, units	In	Across	[n	Across	In	Across	In	Across
1	2-13-45	44.9	17.3	31.1	9.0	52	. 28	22.0	17.5	274	278	54.0	29.9	1.2	2.7
$\tilde{2}$	2-13-45	44.6	17.8	30.1	5.2	58	28	24.3	18.6	271	282	60.5	29.6	1.3	2.9
3		42.5	14.0	36.4	8.5	92	.31	25 0	18.7	314	349	75.7	34.5	1.6	3.7
- 4	3-20-45	43.8	- 16.1	32.6.	9.0_	97	_ 36	29.7	21.2	313	_ 375	84.9	32.9	_1.9.	3.7 _
5	3-21-45	43.0	16.0	32.2	6.9	92	35	30.4	20.9	303	362	82.3	33.3	1.7	3.6
6	3-21-45	43.3	15.9	· 32.7	7.5	98	34	28.7	21.7	317	380	88.0	33.2	1.9	3.8
7	3-20-45	44.2	15.5	34.2	6.8	105	38	30.9	22.4	331	385	84.3	33.8	2.0	3.8
8	3-21-45	41.7	15.4	-32.5	7.3	104	36	28.8	20.3	317 -	369	89.9	32.6	2.1	-4.0
- Ģ	4- 6-45	42.9	14.3	36.0	*	106	39	28.5	22.7	362	404	78.9	38.4	2.0	4.0
10	4- 6-45	43.6	15.2	34.4	*	<sup>-</sup> 103	- 39	26.4	21.8	400	427	76.7	40.8	2.0	4.0
11	4- 6-45	42.4	15.3	33.3	*	96	37	27.5	21.2	361	403 '	72.7	38.5	1.9	3.8
	Average	43.4	15.7	33.2	7.5	91	35	27.5	20.6	324	365	77.1	34.3	1.8	3.6

No moisture samples obtained.

TABLE XXIV STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

					Мџ	LЕ					,	
	Basis Weight, lb.	a ľ	Bursting	G.E.	Comp	iehle ression, lb.	Te	endorf ear, sheet		r Tensile, ./in.		Stretch,
	(12 x 12 /1000)	Caliper, 0.001 in.	Strength, points	Puncture, units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average Standard deviation Range limit (±)* Approximate	44.9 41.7 43.4 0.981 0.5	17.8 14.0 15.7 1.12 1.0	106 52 91 18.6 2.5	39 28 35 4.01 1.0	30.9 22.0 27.5 2.77 1.0	22.7 17.5 20.6 1.68 1.0	400 271 324 38.4 7.5	427 278 365 47.2 7.5	89.9 54.0 77.1 11.2 1.5	40.8 29.6 34.3 3.54 1.0	2.1 1.2 1.8 0.299 0.1	4.0 2.7 3.6 0.437 0.2
probability, % Range limit (±)* Approximate	39 1.0	63 2.0	10 5.0	20 1.5	28 1.5	45 1.5	16 15.0	13 15.0	10 3.0	22 2.0	26 0.2	35 0.4
probability, % Range limit (±)* Approximate	69 2.0	93 	21 7.5	29 3.0	41 3.0	63 3.0	30 30.0	25 30.0	21 5.0	42 3.0	50 0.3	64 0.6
probability, %	96	—	31	55	72	93	56	48	35	60	68	83

\* Range limits were arbitrarily selected.

#### TABLE XXV

## PHYSICAL CHARACTERISTICS OF 42-LB, D.F.B.S. FOURDRINIER KRAFT LINER

#### MILL F Roll Averages

F	-	 Date	Basis . Weight, lb. (12 x 12	Caliper, 0.001		Mois-	Bursting	G.E. Punc-	Compi	hle ession, o.	Те	ndorf ar, sheet	Ter	nthor nsile, /in.		thor ch, %	
	Roll	Manuf.	/1000)	in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across	In	Across	In	Across	
	1 2 3 · 4- 5	5- 4-45 4-15-45 5- 5-45 5- 5-45 5- 5-45	41.1 42.4 37.5 - 41.6 - 39.3	13.5 13.9 13.1 13.5 13.0	36.5 36.6 34.3. 37.0 36.3	10:7 11.4 8.7 -11-1 10.3	98 96 76 75 83	39 37 28 32 29	24.3 21.5 22.3 21-6 23.7	18.4 18.9 16.5 18.0 19.8	338 335 270 283- 279	404 370 310 -334 325	71 2 71.4 63.9 - 67.0 63.6	38.7 35.9 27.5 29.5 32.8	2 0 2.0. 1.7 1 <del>.</del> 8- 2.0	3.1 2.9 3.4 -3.1- 3.0	÷ .
-	6 7 8 9 - 10	5- 5-45 5- 5-45 - 5- 4-45 5- 4-45 5- 5-45	39_4 36_9_ 40_0 40_5 38_4	13.4 12.6_ 13.7 13.5 13.5	35.3 35.1 35.0 36.0 34.1	7.8 9.5_ 10.5 10.6 9.5	78 76 97 95 74	31 -28 - 37 37 29	23.2 - 23.3 23.4 26.9 22.6	19.7 19.9 19.9 19.8 16.0	292 262 338 348 276	320 285 379 369 333	61.1 -60.3 72.0 74.0. 62.3	33.8 33.3 35.2 36.0 26.9	2 0 1.9 2.0 2.0 1.9	3.1 3.0 3.0 3.1 3.0	
	Λ	lverage	39.7	13.4	35.6	10:0	85	33	23.3	18.7	302	343	66.7	33.0	1.9	31	

TABLE XXVI STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

				Mu	LL F					,	
Basis Weight, Ib.	Caliner	Bursting	G.E.	Comp	pression,	Т	ear,				r Stretch, %
/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
42.4 36.9 39.7	13.9 12.6 13.4	98 74 85	39 28 33	24.3 21.5 23.3	19.9 16.0 18.7	348 262 302	404 `285 343	74.0 60,3 66.7	38.7 26.9 33.0	2.0 1.7 1.9	3.4 2.9 3.1
1,77 0.5	0.374 1.0	10.3 2.5	4,35 1.0	1.55 1.0	1.46 1.0	33.5 7.5	$\frac{36.4}{7.5}$	5.09 1.5	3.87 1.0	0.106 0.1	0.134 0:2
22	99	19	18	48	50	17	17	23	21	65	86
1.0 42	2.0 100	5.0 38	1.5 27	1.5 67	1.5 70	15.0 35	15.0 32	3.0 44	2.0 40	0.2 94	0.4 99
2.0 74		7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0.3	0.6
	Weight, b (12 x 12 /1000) 42.4 36.9 39.7 1.77 0.5 22 1.0 42	Weight, Ib         Caliper, (12 x 12         Caliper, Caliper, 0.001 in.           42.4         13.9         36.9         12.6           39.7         13.4         1.77         0.374           0.5         1.0         22         99           1.0         2.0         42         100           2.0	Weight, Ib. (12 x 12)         Bursting Caliper, 0.001 in.         Bursting Strength, points           42.4         13.9         98           36.9         12.6         74           39.7         13.4         85           1.77         0.374         10.3           0.5         1.0         2.5           22         99         19           1.0         2.0         5.0           42         100         38           2.0          7.5	Weight, Ib. (12 x 12)         Caliper, O.COI in.         Bursting Strength, points         G.E. Puncture, units           42.4         13.9         98         39           36.9         12.6         74         28           39.7         13.4         85         33           1.77         0.374         10.3         4.35           0.5         1.0         2.5         1.0           22         99         19         18           1.0         2.0         5.0         1.5           42         100         38         27           2.0          7.5         3.0	Basis Weight, Ib (12 x 12 (1000)Caliper, 0.001 in.Bursting Strength, pointsG.E. Puncture, unitsComp $42.4$ $36.9$ $12.6$ $39.7$ $13.9$ $13.4$ $98$ $85$ $33$ $39$ $24.3$ $21.5$ $33.23.3$ $24.3$ $21.5$ $33.23.3$ $1.77$ $0.5$ $0.374$ $1.0$ $10.3$ $2.5$ $4.35$ $1.0$ $1.55$ $1.0$ $22$ $299$ $1.0$ $99$ $18$ $1.0$ $48$ $1.0$ $1.5$ $1.5$ $42$ $1.0$ $100$ $38$ $27$ $27$ $67$ $2.0$	Weight, Ib. (12 x 12       Bursting Caliper, (1000)       Bursting Strength, points       G.E. Puncture, units       Compression, Ib.         42.4       13.9       98       39       24.3       19.9         36.9       12.6       74       28       21.5       16.0         39.7       13.4       85       33       23.3       18.7         1.77       0.374       10.3       4.35       1.55       1.46         0.5       1.0       2.5       1.0       1.0       1.0 <sup>+</sup> 22       99       19       18       48       50         1.0       2.0       5.0       1.5       1.5       1.5         42       100       38       27       67       70         2.0        7.5       3.0       3.0       3.0	Basis Weight, Ib.Bursting Strength, pointsG.E. Puncture, unitsRiehle Compression, Ib.Elm T g./ $42.4$ 13.9 $36.9$ 98 $12.6$ $39.7$ 39 $13.4$ 24.3 $85$ $33$ 19.9 $21.5$ 348 $262$ $33$ 26.3 $21.5$ 19.9 $16.0$ $262$ $39.7$ 348 $302$ $1.77$ $0.374$ 0.3 $2.5$ 4.35 $1.0$ 1.55 $1.0$ 1.46 $1.0$ 33.5 $1.0$ $22$ $29$ $1.0$ 99 $1.0$ 18 $1.5$ 48 $1.5$ 50 $1.5$ 17 $1.5$ $22$ $2.0$ 99 $-$ 19 $1.0$ 18 $1.5$ 48 $1.5$ 1.55 $1.5$ 1.50 $1.5$ $42$ $2.0$ 100 $-$ 38 $27$ 27 $67$ $3.0$ 3.0 $3.0$ 30.0	Basis Weight, Ib.Bursting Dot 12 x 12 (1000)Bursting Caliper, 0.001 in.G.E. Puncture, pointsRiehle 	Basis Weight, lb. (12 x 12 (2000)Bursting Strength, pointsG.E. Puncture, unitsRiehle Compression, lb.Elmendorf Tear, g./sheetAmtho lb42.4 36.9 39.713.9 13.498 85 3339 24.3 21.5 16.0 23.324.3 19.9 262 262 285 262 285 285 262 285 60.3 66.774.0 10.0 262 285 262 285 262 285 260.3 262 285 66.7Amtho lb42.4 36.9 39.713.4 13.485 85 3339 24.3 21.5 16.0 23.3 18.7262 302 262 285 262 285 285 60.3 302 343 66.774.0 66.742 1.0 2.00.3 2.5 1.01.05 1.61.46 1.0 1.0 7.53.6.4 7.55.09 1.522 1.0 2.099 5.0 1.518 1.5 1.548 1.517 17 17 23 1.523 1.522 2.0 2.099 5.0 1.51.5 1.51.50 1.515.0 15.03.0 3.042 2.0 - -100 7.538 3.027 3.067 3.0 3.030.0 30.030.0 30.05.0	Basis Weight, Ib.Bursting Strength, pointsG.E. Puncture, unitsRiehle Compression, Ib.Elmendorf Tear, g./sheetAmthor Tensile, ib./in.42.413.9 36.098 12.639 7424.3 28 21.519.9 16.0348 262 262 285 302404 60.3 262 285 30274.0 60.3 262 285 60.3 26.9 302 34374.0 60.7 38.7 302 302 34374.0 60.7 38.7 302 302 34374.0 60.7 38.7 302 302 34374.0 60.7 38.7 302 302 34374.0 60.7 38.7 302 302 34374.0 60.7 38.7 302 302 34374.0 60.7 30.0 30.0 30.038.7 302 34374.0 60.7 30.0 30.030.4 30.0 30.074.0 38.7 302 302 34374.0 60.7 30.038.7 302 34374.0 60.7 30.038.7 302 34374.0 60.7 30.030.0 3.02022 42 1.099 2.019 5.018 1.5 1.5 1.548 1.5 1.5 1.517 17 17 23 21 21 21 21 21 22 22 22 23 22 23 24.1 2.021 24.1 23 21 21 21 21.038 27 27 27 27 27 27 27 27 27 27 27 27 27 23 2244 20 2.044 20 20 2033.0 2030.0 2030.0 2030.0 20	Basis Weight, lb. (12 x 12 (2000)Bursting D.0001 in.G.E. Strength, pointsRiehle functure, unitsElmendorf rear, g./sheetAmthor Tensile, ib./in.Amthor Amthor Tensile, ib./in.Amthor Amthor ib./in.42.4 36.9 36.9 39.713.9 13.498 85 3339 24.3 28 21.5 33 23.3 18.724.3 262 262 285 302 23.3 18.710.4 302 348 302 348 302 343 302 343 302 343 36.474.0 38.7 2.0 3.26.9 1.7 302 343 302 343 302 343 36.474.0 38.7 2.0 3.26.9 1.7 302 343 302 343 302 343 36.420.0 3.87 0.106 0.1 1.91.77 22 1.0 2.00.3 2.5 1.01.05 1.51.46 1.0 1.0 1.035.5 1.5 1.5 1.530.0 3.030.0 3.020.0 2.00.1622 42 2.099 19 1.018 1.5 1.5 1.548 1.5 1.517 17 17 17 23 24 1.021 65 1.065 1.0 0.1'24 2.0100 - 7.538 3.027 3.067 3.0 3.030.0 30.030.0 30.05.0 3.03.0 0.3

\* Range limits were arbitrarily selected.

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#### TABLE XXVII

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER

MILL G Roll Averages

• •	Date	Basis <sup></sup> Weight, lb. (12 x 12	Caliper, 0.001	Appar- ent Density,	Mois-	Bursting	G.E. Punc-		ehle ression, b.	Т	endorf - ear, sheet	Ter	thor isile, /in.		nthor ich, %
Roll	Manuf.	/1000)	in.	lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	Ín	Across	In '	Across	In	Acros
1	4- 2-45	42.6	15.5	33.0	7.3	93	37	27.4	23.6	373	429	76.0	41.4	1.7	3.1
2	4-2-45	42.5	15.9	32.1	4.9	87	38	26.7	23.2	382	413	73.5	40.8	1.4	2.9
 .3.	4- 2-45	<u>42.0</u>	15.8	31.9	7.4	88	37	25.7	22.3	382	426	73.0	41.7	1.6	3.1
4	4-2-45	41.7	15.7	31.9	6.8	85	37	26.1	22.0	~392	420	73.5	'41.9 °	1.5	2.8
5	4- 2-45	42.2	15.9	31.8	8.1	92	38	25.5	22.0	390	423	74 7	40.7	1.5	2.8
6	1-22-45	41.2	16.1	30.7	5.8	89	36	28.8	21.8	377	399	71.5	37.1	2.0	4.0
-7-	1-22-45	41:7 -	16.2	- 30.9	7:0	92-	38 -	28.1	23.8	- 394	436	72.3	40.8	- 2.0	3.8
8	12-12-44	42.0	15.0	33.6	10.5	106	38	28.8	25.3	377	405	70.7	50.6	2.0	37
9	2-19-45	41.5	15.5	32 1	8.2	97	36 -	28.9	25.7	- 383	375	71.6	44.7	2.0	4.3
10	2-19-45	41.7	15.2	32.9	6.3	95	35	27.9	26.2	381	382	70.0	44.4	2.0	4.2
11	4-2-45	43.3	15.3	34.0	6.9	88	44	27.4	23.1	394	424	73.9	37.9	1.8	4.0
12	4-2-45	40.2	15.3	31.5	5.8	91	39	28.1	23.7	364	407	70.8	38.6	1.6	3.6
13	4-2-45	41.6	15.3	32.6	5.5	79	39	25.6	22.1	· 383	410	69.7	35.7	1.4	3.3
14	11-13-44	42.6	16.0	31.9	7.3	88	36	28.8	26.8	382	358	70.3	48.4	1.8	4.1
15	3-13-45	41.0	15.0	32.8	7.9	94	37	26.6	24.1	353	371	72.5	42.8	1.8	4.3
А	verage	41.9	15.6	32.2	7.0	91	38	27.4	23.7	380	405	72.3	41.8	1.7	3.6

TABLE XXVIII

# STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER MILL G

	Caliper, 0.001 in.	Bursting Strength, points	G.E. Puncture, units	Riehle Compression, lb.		Elmendorf Tear, g./sheet		Amthor Tensile, lb./in.		Amthor Stretch, %	
				In	Across	In	Across	In	Across	In	Across
43.3 40.2 41.9 0.753 0.5	16.2 15.0 15.6 0.394 1.0	106 79 91 6.08 2.5	44 35 38 2.09 1.0	28.9 25.5 27.4 1.25 1.0	26.8 21.8 23.7 1.63 1.0	394 353 380 11.1 7.5	436 358 405 23.6 7.5	76.0 69.7 72.3 1.84 1.5	50.6 35.7 41.8 4.01 1.0	2.0 1.4 1.7 0.229 0.1	4.3 2.8 3.6 0.556 0.2
49 1.0	99 2.0	32 5.0	37 1.5	58 1.5	46 1.5	50 15.0	25 15.0	59 3.0	20 2.0	34 0.2	28 0.4
82 2.0 99	100 	59 7.5 78	53 3.0 85	77 3.0 98	64 3.0 93	82 30.0 <sup>.</sup> 99	48 30.0 80	90 5.0 99	38 3.0 55	62 0.3 81	53 0.6 72
	Weight, lb. (12 x 12 /1000) 43.3 40.2 41.9 0.753 0.5 49 1.0 82 2.0	Weight, lb. (12 x 12 Caliper, /1000) 0.001 in. 43.3 16.2 40.2 15.0 41.9 15.6 0.753 0.394 0.5 1.0 49 99 1.0 2.0 82 100 2.0 —	Weight, lb.         Bursting Strength, points           (12 x 12 (1000)         Caliper, 0.001 in.         Bursting Strength, points           43.3         16.2         106 40.2           43.3         16.2         106 79 41.9           0.753         0.394         6.08 0.5           0.5         1.0         2.5           49         99         32 1.0         2.0           82         100         59 2.0         7.5	Weight, lb. (12 x 12Caliper, Caliper, 0.001 in.Bursting Strength, pointsG.E. Puncture, units43.316.21064440.215.0793541.915.691380.7530.3946.082.090.51.02.51.0499932371.02.05.01.58210059532.0-7.53.0	Weight, lb. ( $12 \times 12$ Caliper, Components         Bursting Strength, points         G.E. Puncture, units         Components           43.3         16.2         106         44         28.9           40.2         15.0         79         35         25.5           41.9         15.6         91         38         27.4           0.753         0.394         6.08         2.09         1.25           0.5         1.0         2.5         1.0         1.0           49         99         32         37         58           1.0         2.0         5.0         1.5         1.5           82         100         59         53         77           2.0         -         7.5         3.0         3.0	Weight, lb. (12 x 12Bursting Caliper, 0.001 in.Bursting Strength, pointsG.E. Puncture, unitsCompression, lb.43.316.21064428.926.840.215.0793525.521.841.915.6913827.423.70.7530.3946.082.091.251.630.51.02.51.01.01.04999323758461.02.05.01.51.51.582100595377642.0-7.53.03.03.0	Weight, lb. (12 x 12 (1000)Compression, Bursting Strength, Puncture, unitsCompression, lb.Tr g./s43.316.21064428.926.839440.215.0793525.521.835341.915.6913827.423.73800.7530.3946.082.091.251.6311.10.51.02.51.01.01.07.5499932375846501.02.05.01.51.51.515.08210059537764822.0-7.53.03.03.030.0	Weight, lb. (12 x 12Bursting Caliper, (1000)Bursting Strength, pointsG.E. Puncture, unitsCompression, lb.Tear, g./sheet43.316.21064428.926.8394.43640.215.0793525.521.835335841.915.6913827.423.73804050.7530.3946.082.091.251.6311.123.60.51.02.51.01.01.07.57.549993237584650251.02.05.01.51.51.515.015.0821005953776482482.0-7.53.03.03.030.030.0	Weight, lb. (12 x 12Bursting Strength, pointsG.E. Puncture, unitsCompression, lb.Tear, g./sheetAmthor lb.43.316.21064428.926.8 $394 \cdot 436$ 76.040.215.0793525.521.8 $353$ 35869.741.915.6913827.423.738040572.30.7530.3946.082.091.251.6311.123.61.840.51.02.51.01.01.07.57.51.54999323758465025591.02.05.01.51.51.515.015.03.082100595377648248902.0-7.53.03.03.030.05.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Weight, lb. (12 x 12Bursting Strength, pointsG.E. Puncture, unitsCompression, lb.Tear, g./sheetArnthor Tensile, lb./in.Amthor Marthor In43.316.21064428.926.839443676.050.62.040.215.0793525.521.835335869.735.71.441.915.6913827.423.738040572.341.81.70.7530.3946.082.091.251.6311.123.61.844.010.2290.51.02.51.01.01.07.57.51.51.00.149993237584650255920341.02.05.01.51.51.515.015.03.02.00.2821005953776482489038622.0-7.53.03.03.030.05.03.00.3

\* Range limits were arbitrarily selected.

#### MILL F

The average test results obtained on the liner made by Mill F are reported in Table XXV (see also Table LXVI of the Appendix). The results indicate that the average basis weight is considerably lower than the specified weight for this grade. The average caliper was 0.0134 inch, which resulted in an average apparent density of 35.6 pounds per cubic foot. The average bursting strength and G. E. puncture values were 85 points and 33 units, respectively. The average moisture content was 10.0% on an ovendry basis.

The statistical evaluation of these test results is given in Table XXVI. On the basis of a standard deviation of 1.77 for basis weight, it should be expected that - MILL H only 22% of the rolls will fall within a basis weight range limit of  $\pm 0.5$  pound (39.2 to 40.2 pounds), 42% of the rolls within a range limit of  $\pm 1.0$  pound (38.7 to 40.7 pounds), and 74% of the rolls within a range limit of  $\pm 2.0$  pounds (37.7 to 41.7 pounds). The chance variation or uniformity of the caliper as determined by standard deviation indicates an expectancy of approximately all of the rolls falling within the range limit of  $\pm 0.001$  inch (0.0124 to 0.0144 inch). The standard deviation for the bursting strength indicates that the uniformity is such that only 19% of all rolls should fall within the range limit of  $\pm 2.5$  points (82.5 to 87.5 points) of the average obtained, 38% of the rolls within the range limit of  $\pm 5.0$  points (80.0 to 90.0 points) and 53% within the range limit of  $\pm 7.5$  points (77.5 to 92.5 points). The probable variation for the G. E. puncture test appears to follow approximately the same trend as the bursting strength variation. The probable variation for Riehle compression and Amthor stretch appears to be slightly less than the variation to be expected for Elmendorf tear and Amthor tensile.

# MILL G

The average test results obtained on samples of liner made by Mill G are given in Table XXVII (see also Table LXVH of the Appendix). The average basis weight was, for all practical purposes, the same as the specified grade weight. The average caliper was 0.0156 inch and the average apparent density was 32.2 pounds per cubic foot. The average bursting strength and G. E. puncture values were 91 points and 38 units, respectively. The average moisture content was 7.0% on an ovendry basis.

The statistical evaluation of these results is given in Table XXVIII. The standard deviation for basis weight indicates that approximately 49% of the rolls should fall within a basis weight range limit of  $\pm 0.5$ pound (41.4 to 42.4 pounds), 82% within a range limit of  $\pm 1.0$  pound (40.9 to 42.9 pounds) and practically all the rolls produced of this grade should fall within a range limit of  $\pm 2.0$  pounds (39.9 to 43.9 pounds). On the basis of the results obtained for caliper, it should be expected that practically all the rolls would fall within a caliper range limit of  $\pm 0.001$  inch (0.0146 to 0.0166 inch). The standard deviation of the bursting

strength was of such magnitude that it should be expected that only 32% of the rolls should fall within a range limit of  $\pm 2.5$  points (88.5 to 93.5 points), 59% within the range limits of  $\pm 5.0$  points (86.0 to 96.0 points), and approximately 78% within the range limit of  $\pm 7.5$  points (83.5 to 98.5 points). The magnitude of the standard deviation for the G. E. puncture test indicates approximately the same probable variation as for the bursting strength. The standard deviations for the Riehle compression, Elmendorf tear, Amthor tensile and stretch indicate that the probable variation to be expected is quite large.

المحافظ بالمحمد الأميسي والمستعاد والمتعلم معداته معلوهم والمحافظ والمحافظ والمحافظ والمستعار

The average test results obtained on the samples of . liner manufactured by Mill H are tabulated in Table XXIX (see also Table LXVIII of the Appendix). The average basis weight obtained for Mill H was slightly in excess of the specified grade weight. The average caliper was 0.0159 inch and the average apparent density was 32.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 108 points and 37 units, respectively. The average moisture content was 8.0% on an ovendry basis.

The statistical evaluation of these test results isshown in Table XXX. The standard deviation for basis weight is of the magnitude that 40% of the rolls manufactured by Mill H in this grade should fall within a basis weight range limit of  $\pm 0.5$  pound (42.1 to 43.1 pounds), 72% within the range limit of  $\pm 1.0$  pound (41.6 to 43.6 pounds), and practically 97% within the range limit of  $\pm 2.0$  pounds (40.6 to 44.6 pounds). On the basis of the results obtained for caliper, it should be expected that practically all the rolls should fall within  $\pm 0.001$  inch (0.0149 to 0.0169 inch) of the average caliper. The statistical evaluation of the bursting strength indicates that approximately 38% of the rolls should fall within a bursting strength range limit of  $\pm 2.5$  points (105.5 to 110.5 points), approximately 67% within the range limit of  $\pm 5.0$  points (103 to 113) points), and approximately 86% within the range limit of  $\pm 7.5$  points (100.5 to 115.5 points). The variation for the G. E. puncture test exhibits relatively the same trend as the bursting strength. The standard deviations for the Riehle compression, Elmendorf tear, and Amthor tensile and stretch indicate considerable lack of uniformity in the tests.

### MILL I

The average test results obtained for the liner made by Mill I are shown in Table XXXI (see also Table LXIX of the Appendix). The average basis weight was in excess of the specified weight for this grade. The average caliper was 0.0153 inch and the average apparent density was 34.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 109 points and 41 units, respectively. The average moisture content was 8.4% on an ovendry basis.

The statistical evaluation of these test results may

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# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

# MILL H Roll' Averages

Roll	Date	Basis Weight, lb. (12 x 12	Caliper, 0.001	Appar- , ent Density,	Mois- ture,	Bursting Strength,	G.E. Punc-	Comp	iehle pression, lb.	้า	endorf 'ear, 'sheet	Те	thor nsile, ./in.		nthor etch, %
Ron	Manuf.	/1000)	in.	lb./cu.ft.	%	points	ture, units	In	Across	In	Across	In	Across	In	Across
1 2 3 4 5	12-31-44 12-31-44 3-19-45 - 3-20-45 3-20-45	44.5 44 6 42.1 41.5- 42.2	15.7 16.5 15.2 15.2 16.4	34.0 32.4 33.2 32.8- 30.9	8.8 9.4 8.1 9.0 7.1	112 96 107 103 108	42 42 37 35- 35	29.7 27.0 32.4 - 29.7 34.8	25.4 24:5 25.7 25.4 — 26.1	449 481 390 - 397 340	452 427 400 371 405	73.5 62.7 69.2 63.9 80.0	47.8 50.3 45.7 49:7 42.5	2.5 2.3 2.0 - 2.0 - 2.1	3.8 4.4 4.4 4.5 - 3.7
6 7 9 10	3-20-45 3-20-45 4-13-45 4-13-45 4-13-45 4-13-45	41.6 42.4 42.0 42.3 42.7	15.9 16.4 16.1 15.6 15.8	31.4 31.0 31.3 32.5 32.4	7.7 6.7 6.3 8.9 8.8	105 - 101 110 115 . 111	36 - 37 - 36 35 38	31.3 32.1 28.6 30.9 30.2	22.8 22.7 23.9 24.4 23.8	339 346 373 360 378	391 405 389 393 400	79.5 .75.9 80.5 .80.9 .80.8	39.1 37.7_ 40.9 41.7 39.2	$2.1 \\ 1.9 \\ 2.3 \\ 2.4 \\ 2.4 \\ 2.4$	4.0 3.6 3.9 4.3 3.8
11 12 13 14	4-13-45 4-13-45 4-13-45 4-13-45	42.9 42.8 41.9 42.3	15.9 16.1 15.9 15.6	32.4 31.9 31.6 32.5	8.5 7.8 8.1 7.4	108 107 108 114	- 38 38 37 36	30.5 30.8 30.1 31.1	23.7 24.8 25.0 25.4	391 375 380 406	409 406 431 420	80.0 82.1 79.1 73.7	41.0 40.2 41.3 40.3	$2.3 \\ 2.4 \\ 2.3 \\ 2.3 \\ 2.3$	4.1 3.8 4.4 4.2
ł	verage	42.6	15.9	32.2	8.0	108	37	30.7	24.5	386	407	75.8	42.7	2.2	4.1
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TABLE XXX

# STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

M	TLT.	H	

	Basis Weight, Ib. (12 x 12	Caliper,	Bursting Strength,	G.E. Puncture.	Comp	iehle ression, lb.	T	nendørf ear, sheet		r Tensile, ./in.		Stretch,
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average	44.6 41.5 42.6	16.5 15.2 15.9	115 96 108	42 35 37	34.8 27.0 30.7	26.1 22.7 24.5	481 339 386	452 371 407	82.1 62.7 75.8	- 50.3 37.7 42.7	$2.5 \\ 1.9 \\ 2.2$	$4.5 \\ 3.6 \\ 4.1$
Standard deviation Range limit $(\pm)^*$	0.937 0.5	0.405	5.11 2.5	2.27 1.0	1.82 1.0	1 05 1.0	39.7 7.5	20.3 7.5	75.8 6.44 1.5	4.05	0.183 0.1	0,303 0.2
Approximate probability, %	40	99	38	34	42	66	15	29	18	20	42	49
Range limit (±)* Approximate probability, %	1.0 72	2.0 100	5.0 67	1.5 49	1.5 59	1.5 85	15.0 30	15.0 54	3.0 36	2.0 38	0.2 72	0.4 81
Range limit (±)* Approximate probability, %	2.0 97	_	7.5 86	3.0 81	3.0 90	3.0 99	30.0 55	30.0 86	5.0 56	3.0 54	0.3 90	0.6 95

\* Range limits were arbitrarily selected.

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PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill I
<b>Roll Averages</b>

	Date	Basis Weight, lb. (12 x 12	Caliper, 0.001	Appar- ent Density,	Mois- ture,	Bursting Strength,	G.E. Punc- ture,	Comp	ehle ression, b	Т	endorf ear, sheet	Ter	ithor isile, /in.		othor tch, %
	anuf.	/1000)	in.	lb./cu.ft.	%	points	units	In	Across	In	Across	In	Across	In	Across
2 1- 3 1- 4 1- 5 1-	20-45 20-45 20-45 31-45 31-45	$\begin{array}{r} 42.5 \\ 42.7 \\ 42.5 \\ 43.9 \\ 43.5 \end{array}$	15.3 15.1 15.3 15.1 15.2	33 3 33 9 33.3 34.9 34.3	8.7 8.9 8.5 7.0 7.1	111 107 109 106 105	40 42 42 40 41	30.5 28.7 28.7 29.0 26.7	22.4 21.2 20.6 20.8 20.3	418 428 422 434 411	468 473 506 470 462	90.9 88.2 88.4 88.5 86.3	36.6 37.9 37.7 37.1 35.8	$2.0 \\ 2.0 \\ 2.1 \\ 2.3 \\ 2.2$	4.2 4.3 4.6 4.2 4.1
7 1 8 1 9 1 101	31-45 31-45 31-45 30-45 31-45	43.143.542.143.4-43.2	15.5 15.5 15.2 15.5 15.5	33.4 33.7 33.2 33.6 33.4	-6.9 7.0 6.5 10.0 8.9	108 104 102 106 109	41 41 39 40 40	29.5 30.0 29.2 29.9 29.8	22.5 20.4 21.5 21.9 20.4	401 408 407 411 405	462 487 443 442 463	85.3 87.5 78.6 81.9 83.9	38.0 35.3 36.6 37.1- 36.5	2.2 2.2 2.0 2.2 2.2	4.3 4.3 4.5 - 4.3 4.5
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	31-45 30-45 30-45 2-45 2-45	43.6 43.8 43.3 42.8 45.4	15.3 15.7 15.9 14.7 15.1	34.2 33.5 32.7 34.9 36.1	8.8 9.6 9.4 9.7 10.8	114 109 100 119 121	41 40 41 39 42	31.0 30.0 29.7 31.2 32.3	23.7 22.3 23.6 22.1 22.2	390 422 390 394 431	466 470 458 474 497	85.5 80.5 78.4 83.5 84.2	37.2 37.0 35.3 36.3 37.8	2.3 2.3 2.2 2.6 2.6	4.7 4.4 4.3 5.3 5.1
17 1-1 18 3-1 19 3-1 20 1-1 21 -10-2	2-45 11-45 10-45 10-45 18-45 24-44 3-45	45.0 42.6 44.5 43.3 43.9 45.0 44.1	15.3 15.0 14.9 14.9 15.3 15.6 - 15.6	35.3 34.1 35.8 34.9 34.4 34.6	11.4 8.2 7.3 6.6 8.1 7.6	112 104 110 107 110 * 108*	42 38 42 42 43 43	32.1 32.1 35.5 34.5 33.6 34.5	21.9 18.6 21.9 22.1 22.0 22.0	416 366 391 416 412 411	491 430 453 451 454 443 -	85.6 82.5 89.6 86.9 87.0 92.2	38.3 35.1 36.5 36.3 38.0 35.4	2.6 2.3 2.5 2.2 2.3 2.3	4.8 4.4 4.6 4.5 4.5 4.4
Averaj		44.1	15.0	33.9 34.2	8.4 8.4	110 109	44 41	30.3 30.9	24.1 21.8	401 408	469 465	83.4 85.4	37.9 36.8	2.2 2.3	4.6 4.5

TABLE XXXII

# STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

					Mn	LL I						
,	Basis Weight, lb. (12 x 12	Caliper,			Com	iehle pression, lb.	Т	endorf ear, sheet		r Tensile, ./in.		r Stretch, %
	/1000)	0.001 in.	points	Puncture, units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average Standard deviation Range limit (±)* Approximate	45.4 42.1 43.5 0.874 0.5	15.9 14.7 15.3 0.290 1.0	121 100 109 4.91 2.5	44 38 41 1.46 1.0	35.5 26.7 30.9 2.19 1.0	24.1 18.6 21.8 1.25 1.0	434 366 408 15.8 7.5	\$06 430 465 18.7 7.5	92.2 78.4 85.4 3.66 1.5	38 3 35.1 36.8 0.996 1.0	2.6 2.0 2 3 0.179 0.1	5.3 4.1 4.5 0.287 0.2
probability, % Range limit (±)* Approximate	43 1.0	99 2.0	39 5.0	50 1.5	35 1.5	58 1,5	36 15.0	31 15.0	32 3.0	68 2.0	42 0.2	52 0.4
probability, % Range limit (±)* Approximate	75 2.0	100	69 7.5	70 3.0	50 3.0	77 3.0	66 30.0	58 30.0	59 5.0	95 3.0	74 0.3	84 0.6
probability, % * Range limits we	98		87	96	83	98	94	89	83	99	91	96

Range limits were arbitrarily selected.

# TABLE XXXIII

# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill J Roll Averages

								1000 110	ages			•							
		Date	(12 x 12	'Caliper,	Density,	Mois- ture,	Bursting Strength,	G.E. Punc- ture,	Comp	ehle ression, b.	T	endorf ~ ~ car, · sheet	Ter	thor * sile, /in.		thor ch, %		<b>-</b> -	
	Roll	Manuf.	/1000)	in.	lb /cu.ft.	%	points	units	In	Across -	In	Across	In	Across	 In	Across			
	1 2 3 4	3-17-45 8-28-44 3-15-45 3-15-45_	39.7 43.4 41.9 - 41.5	14.9 13.3 15.4 -15.3-	32 0 39.2 32.6 	8.7 8.6 7.6 8-4	77 88 97 99	31 31 -34	28.2 27.9 28.9	24.9 21.6 23.8	320 288 319	339 344 378	59 1 70.6 _76.5_	38 3 34.3 	1.9 1 7 2.0	3 1 2.8 2 8	•		
	5	8-26-44	41.1 -	14.6	33.81	8.1	82	29	-29.5- 30.2	24.1 22.4	324 277	368 334	75.5 68.8	38.2 34.4	2.0	2 7 2.4			
		2- 2-45 2-20-45 2-20-45	41.4 41 <u>.2</u> 40.5	15.2 _14.6_ 14.0	32.7 33.9	$\frac{8.4}{8.0}$	78 83		30.0 - 32.9	24.1 -22.6 -	247 · 288- ·	- 324 -	64.2 69.2	$\frac{33.5}{32.0}$	$-\frac{2.1}{2.0}$	$-\frac{2}{3.0}$	- • <b>-</b>		
-	9 10	2- 9-45 2- 9-45 -	40.5	14.5 14.7	$     34 7 \\     34.5 \\     33.1 $	9.1 - 5.7 4.6	82 - 79 - 78	30 - 29 - 28	30.4 32.2 29.0	23.4 -22.7 24.3	274 1236 214	313 291 276	$\frac{68.5}{68.2}$	33.1 33.6	- 2.1 1.9	$3.3 \\ 3.1$			
	11 12 13 14 15	2-25-45 4- 1-45 4- 1-45 4- 1-45 2-23-45	41.9 <sup>,</sup> 42.1 41.9 41.5 41.7	15.2 <sup>-</sup> 15 2 15.1 14.9 14.9	3371 33.2 33.3 33.4 33.6	7.7 6.0 7.5 6.2 8.2	96 83 92 - 87 - 100	34 30 30 30 31	30.6 29.9 31.7 29.4 33.4	22.7 24 8 24.9 24.2 24.2 24.4	290 301 298 302 318	370 352 331 339	66.8 75.7 68.6 67.5 69.2	34.1 34.3 34.7 38.6 36.6	2.0 2.0 2.0 2.0 1.8	2 5 3.0 2.3 3.0 2.9	ı		ļ
	16 17 18 19 20	2-25-45 3- 3-45 3- 3-45 3- 3-45 3- 3-45	41.2 42.7 42.8 42.2 42.4	14.9 14.6 14.5 _14.1 14.0	33.2 35.1 35.4 35.9. 36.3	7.4 8.4 6.5 .9.4. 7.2	103 106 111 109 105	30 39 38 -38 -38 -38	31.7 31.2 31.1 - 30:5 - 30.0	24.3 23.7 23.3 23.2 24.8	318 362 338 331 - 344	381 361 423 403 400	77.8 80.0 92.2 92.0 84.3	36.9 36.2 37.2 37.8 36.4	$2.3 \\ 2.2 \\ 2.4 \\ -2.3 \\ 2.2 \\ 2.2$	3.2 3.1 4.3 4.4 4.2		<b></b> -	
	21	3- 3-45	42.2	14.1	35.9	10.2	108	38	30.3	23.5	344 338	412 412	85.8 90.8	36.1 39.3	2.3 2.2	4.3 4.1	•		
	A	verage	41.7	14.7	34.2	7.7	93	32	30.4	23.7	301	355	74.8	35.9	2.0	3.2			
	-			•												•			

TABLE XXXIV

STATISTICAL EVALUATION OF PHYSICAL TESTS ON 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

												•
•					$\mathbf{M}_{1}$	ır J				*		
, -	Basis Weight, Ib (12 x 12	Caliper,	Bursting Strength,	G E. Puncture,	Com	iehle pression, lb.	Т	endorf ear, sheet	Amthor lb	• Tensile, /in.		r Stretch, %
Test values	/1000)	0.001 in.	points '	units	In	Across	· In	Across	In	Across	In	Across
Maximum Minimum Average Standard deviation Range lmit (±)* Approximate	0.5	15.4 13.3 14.7 0.532 <sup>.</sup> 1.0	111 77 93 11.7 2.5	39 . 28 32 3.69 1.0	33, 427, 930, 41, 431, 0	24.9 21.6 23.7 .92 1.0	362 214 , 301 37.1 7.5	423 276 355 42.1 7.5	92.2 59.1 74.8 9.54 1.5	39.3 32.0 35.9 2.11 1.0	2.4 1.6 2.0 0.204 0.1	4.4 2.3 3.2 0.673 0.2
probability, % Range limit (±)* Approximate	44 1.0	94 2.0	17 5.0	21 1.5	52 1.5	72 1.5	16 15.0	14 15.0	13 3.0	36 2.0	. 38 0.2	$24 \\ 0.4$
probability, % Range limit (±)* Approximate	76 2.0	99 	33 7.5	32 3.0	71 3.0	90 3.0	31 30.0	28 30.0	24 5,0	66 3.0	67 0.3	44 0.6
probability, % * Range limits we	98 re arbitrar	 ilv selected	-48 I	58-	96	99	58	52	40	84	86	63

be seen in Table XXXII. The standard deviation for the basis weight is of such magnitude that it should be expected that approximately 43% of all the rolls manufactured by Mill I should fall within a basis weight range limit of  $\pm 0.5$  pound (43.0 to 44.0 pounds), 75% within the range limit of  $\pm 1.0$  pound (42.5 to 44.5 pounds), and approximately 98% within the range limit of  $\pm 2.0$  pounds (41.5 to 45.5 pounds). On the basis of the results obtained for caliper, it should be expected that approximately all the rolls should fall within a caliper range limit of  $\pm 0.001$  inch (0.0143 to 0.0163 inch). The statistical evaluation of the results obtained for the bursting strength indicate that approximately 39% of the rolls should fall within a range limit of  $\pm 2.5$  points (106.5 to 111.5 points), approxi-. mately 69% within the range limit of  $\pm 5.0$  points (104 to 114 points), and approximately 87% within the range limit of  $\pm 7.5$  points (101.5 to 116.5 points). The results obtained indicate that, in terms of percentage, the rolls made by this mill should be slightly more uniform in respect to G. E. puncture than to bursting strength. The results of the Riehle compression, Elmendorf tear, and Amthor tensile and stretch indicate standard deviations of considerable magnitude.

# Mill J

The average test results obtained for the rolls of liner made by Mill J are given in Table XXXIII (see also Table LXX of the Appendix). The average basis weight obtained is practically the same as the specified

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grade weight. The average caliper was 0.0147 inch and the average apparent density was 34.2 pounds per cubic foot. The average bursting strength and G. E. puncture values were 93 points and 32 units, respectively. The average moisture content was 7.7% on an ovendry basis.

The statistical evaluation of these results are reported in Table XXXIV. The magnitude of the standard deviation for basis weight indicates that approximately 44% of the rolls manufactured by Mill J should fall\_within\_a\_basis\_weight range\_limit\_of\_±0.5\_pound (41.2 to 42.2 pounds), approximately 76% within the range limit of  $\pm 1.0$  pound (40.7 to 42.7 pounds) and approximately 98% within the range limit of  $\pm 2.0$ pounds (39.7 to 43.7 pounds). The results obtained for caliper indicate that approximately 94% of the rolls should fall within a caliper range limit of  $\pm 0.001$  inch (0.0137 to 0.0157 inch). The standard deviation for the bursting strength is of such magnitude that it should be expected that approximately 17% of the rolls manufactured by Mill J should fall within a range limit of ±2.5 points (90.5 to 95.5 points), approximately 33% should fall within the range limit of  $\pm 5.0$ points (88.0 to 98.0 points), and approximately 48%within the range limit of  $\pm 7.5$  points (85.5 to 100.5 points). The statistical evaluation of the Riehle compression values indicates a rather low probable variation, whereas the results obtained for G. E. puncture, Elmendorf tear, Amthor tensile and stretch indicate considerable probable variation.

EVALUATION OF THE PHYSICAL CHARACTERISTICS OF .009/26-LB. KRAFT AND BOGUS CORRUGATING MEDIUMS

# PROCEDURE

The tests and procedures employed throughout this evaluation study have been described on pages 8 to 10.

For the purpose of comparison of the characteristics of the product within a given mill and also between mills, each Fourdrinier Kraft Board Institute mill which makes .009/26-lb. corrugating medium has been given an arbitrarily selected code letter; they have been identified in this report by the letters S to Z, inclusive. The corrugating medium manufactured by Mill V was a bogus medium. Consequently, the group averages have been calculated in two ways: (1) including the bogus medium and (2) excluding the bogus medium.

The test results have been given the same statistical treatment as was employed in the treatment of the 42-lb. liner.

# COMPARISON OF MILL AVERAGES

The results of the various physical tests performed on samples of .009/26-lb. corrugating medium have been compiled in Table XXXV on the basis of mill averages. Complete details of the individual tests are given in Tables LXXI-LXXVIII of the Appendix.

The average results obtained for basis weight are shown graphically in Figure 16. The average basis weight for the group participating was 26.8 pounds including and 26.9 pounds excluding the bogus medium. Both of these group averages are in excess of the grade weight specified. Mill X had the highest average basis weight and Mill V the lowest. The basis weight averages for all the mills were within  $\pm 1$  pound of the group average. The average caliper results are plotted in Figure 17. The average caliper value for the group was 0.010 inch, regardless of whether or not the bogus medium was included. Mill U had the highest average caliper and Mills Y and Z the lowest. All the individual mill averages for caliper were within  $\pm 0.0007$  inch of the group average caliper.

The average apparent densities, in pounds per cubic foot, are pictured graphically in Figure 18. The group average apparent density when the bogus medium was included was 32.3 pounds per cubic foot and 32.5 pounds per cubic foot when it was not included. The highest average apparent density was obtained for Mill Z and the lowest for Mill U. It is interesting to note that the mill averages for apparent density varied over a considerable range.

From the data graphically presented in Figure 19, it may be observed that the average moisture content for the group was 9.4% including the bogus medium and 9.5% when the bogus medium was not included. Mill T had the highest average moisture content and Mill U the lowest. Two of the mills (T and W) had average moisture values in excess of 11%.

From the data presented in Figure 20, it is seen that the average bursting strength for the group, including the bogus medium, was 62 points; it was 66 points when the bogus was not included. The bursting strength, expressed in points per pound basis weight, was 2.31 when the bogus was included and 2.45 when the bogus was not included. The highest mill average bursting strength was obtained for Mill Z and the lowest for Mill V (the bogus medium). The average bursting strength for the bogus medium was approximately 50% of the average bursting strength obtained for the other mills.

#### TABLE XXXV

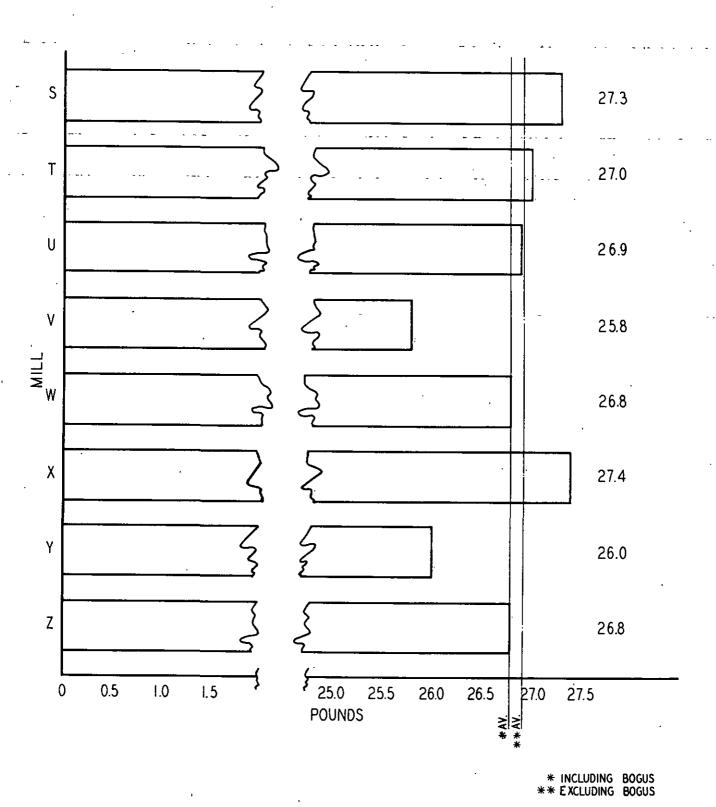
# COMPARISON OF PHYSICAL CHARACTERISTICS BETWEEN MILLS

#### CORRUGATING MEDIUM

	Rolls	Basis Weight, lb. (12 x 12	Caliper, 0.001		Mois-		G.E. Punc-	Comp	ehle ression, b.	Te	ndorf ar, sheet	Т	nthor ensile, o./in.		nthor tch, <u>%</u>
Mill	Tested	/1000)	0.001 in.	Density, lb./cu.ft.	ture,. %	Strength, points	ture, units	In	Across	In	Across	In	Across	In	Across
S T V W X	10 10 21 13 13 14	27.3 27.0 26.9 25.8 26.8 27.4	10.1 10.0 10.7 10.1 10.1 9.8	32.4 32.5 30.2 30.7 31.8 33.7	8.5 11.8 8.4 9.2 11.1 8.7	68 57 65 32 69 68	20 20 20 11 19 21	19.5 15.9 19.7 12.9 17.7 17.1	15.5 12.8 13.5 10.3 11.5 13.1	268 237 238 121 228 250	276 261 266 134 300 281	52.3 45.1 53.0 31.0 56.6 52.1	30.4 24.2 25.7 17.2 21.8 25.3	1.6 1.8 2.0 1.4 2.1 2.1	4.7 3.7 4.8 2.4 3.8 4.3
Y Z	10 11	26.0 26.8	9.3 9.3	33.9 34.7	9:7 9:1	58. 75	15 20	17.3 19.9	12.3 15.8	189 251	219 262	50.7 53.8	22.1 33.0	$\begin{array}{c} 2.0\\ 2.0\end{array}$	3.6 4.7
	p Averag p Averag		10.0 10.0	32:3 32.5	9.4 9.5	62 66	18 19	17.6 18.3	13.0 13.4	223 238	251 268	49.5 52.2	24.8 25.9	1,9 2.0	4.0 4.3

\* Including bogus from Mill V.

† Excluding bogus.



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FIGURE 16. Comparison of the average basis weight of .009/26-lb. corrugating medium among mills.

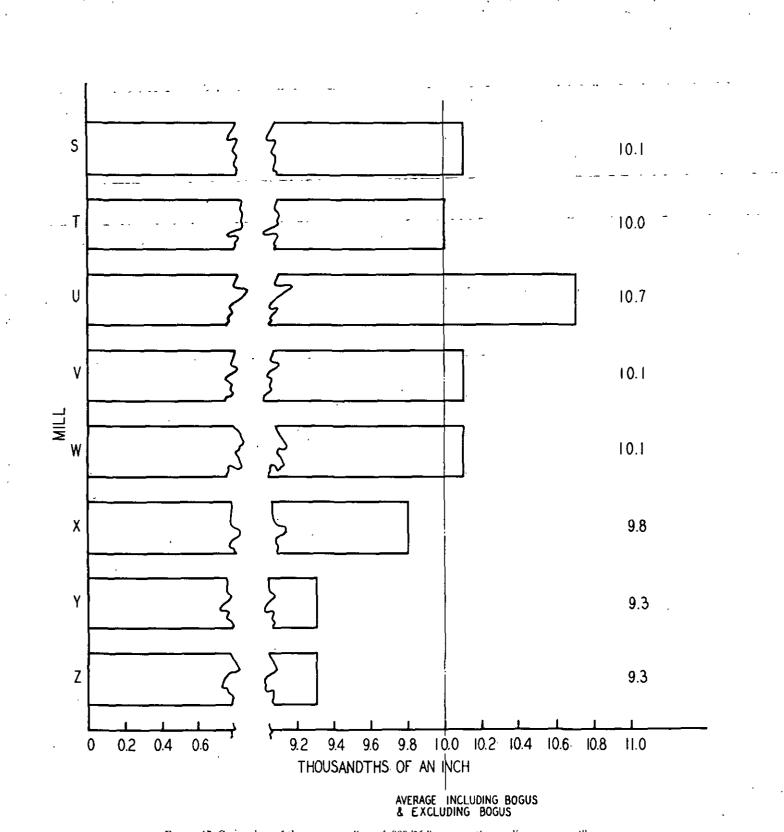
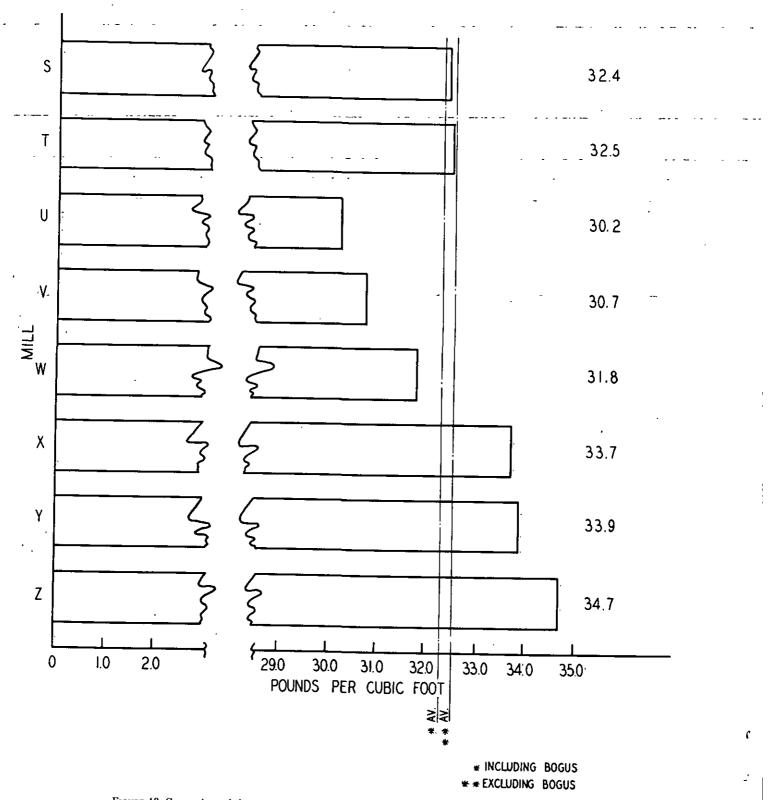


FIGURE 17. Comparison of the average caliper of .009/26-lb. corrugating medium among mills.

(Because the averages were calculated to the nearest tenth only, the average value of the caliper was the same when the bogus samples were excluded as when they were included.)



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FIGURE 18. Comparison of the average apparent density of .009/26-lb. corrugating medium among mills.

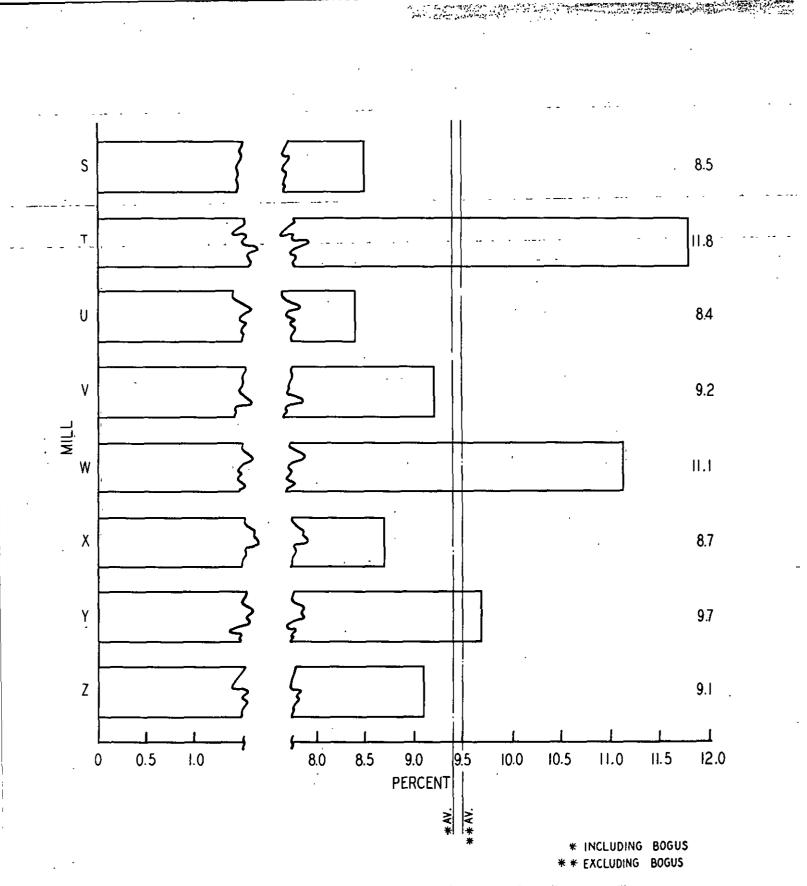


FIGURE 19. Comparison of the average moisture content of .009/26-lb, corrugating medium among mills.

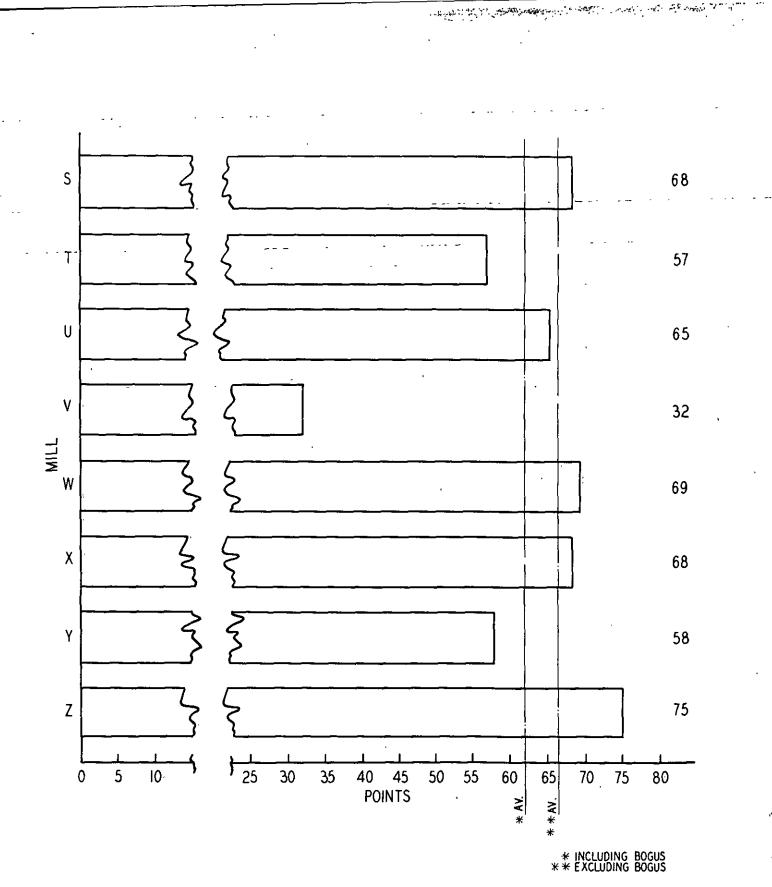


FIGURE 20. Comparison of the average bursting strength of .009/26-lb. corrugating medium among mills.

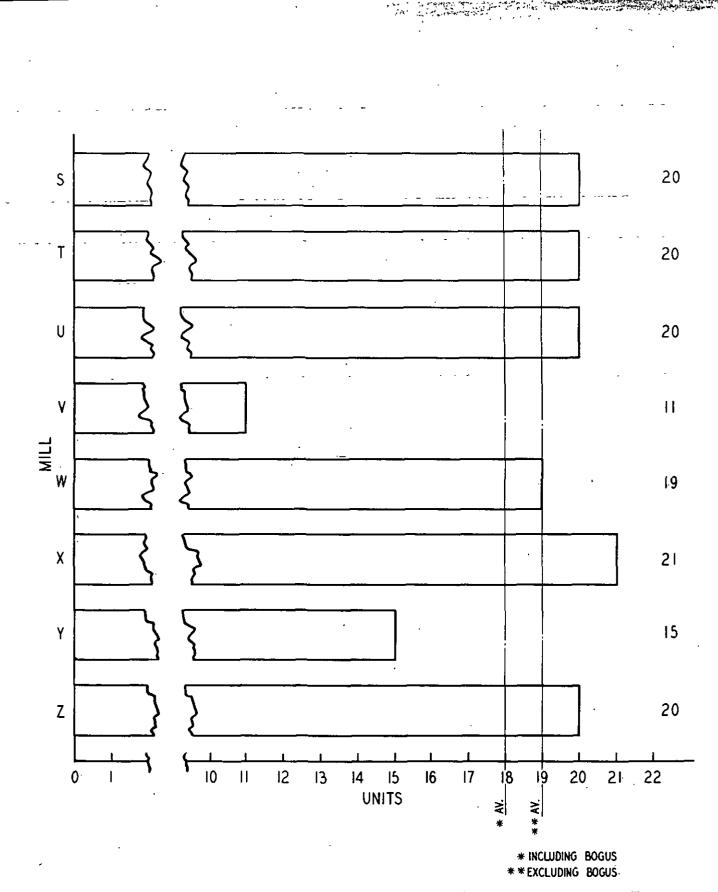
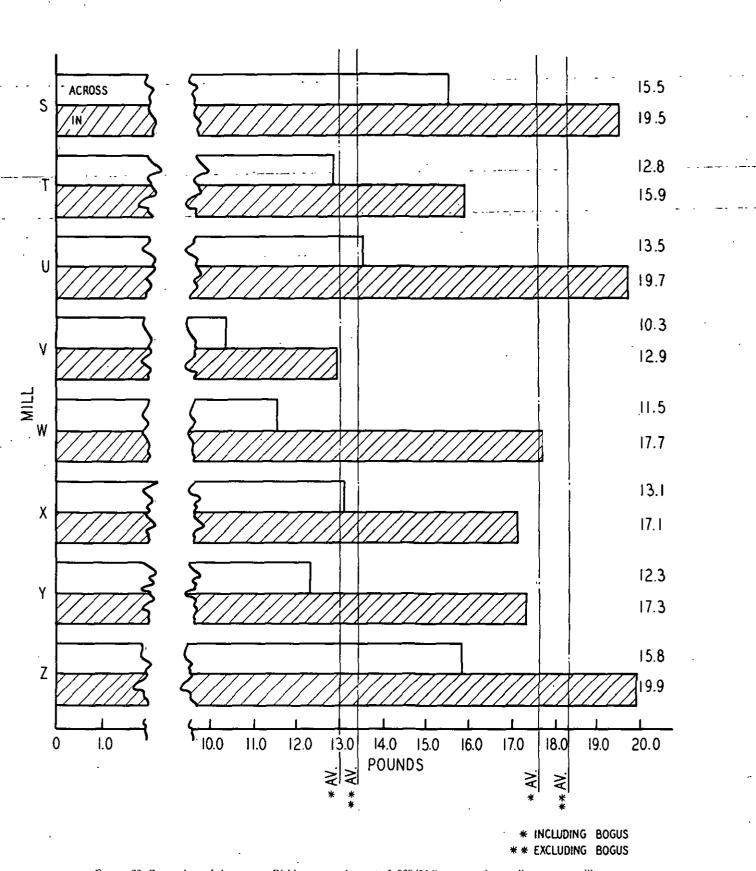
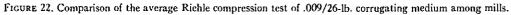


FIGURE 21. Comparison of the average General Electric puncture test of .009/26-lb. corrugating medium among mills.



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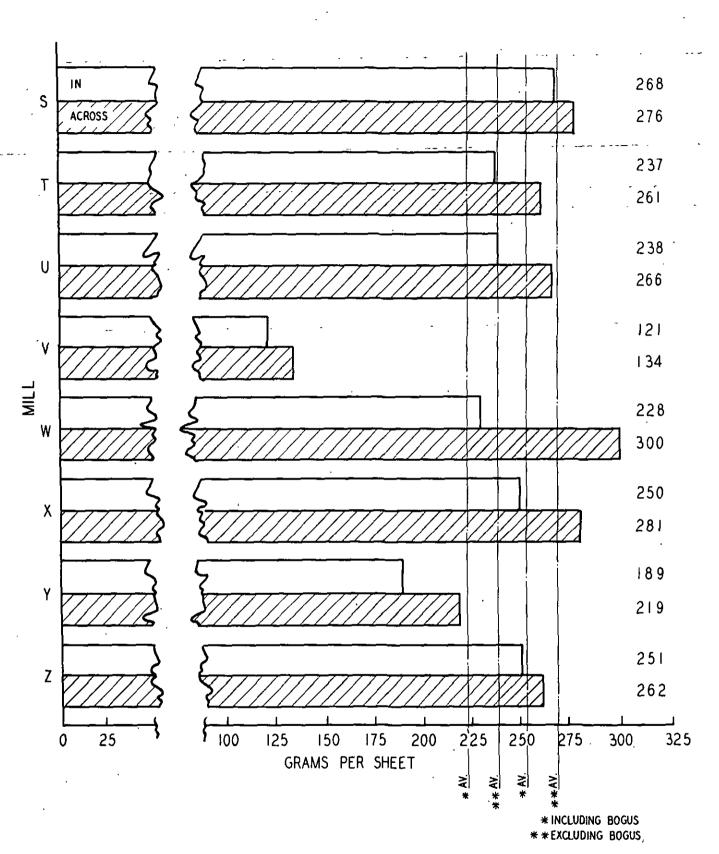
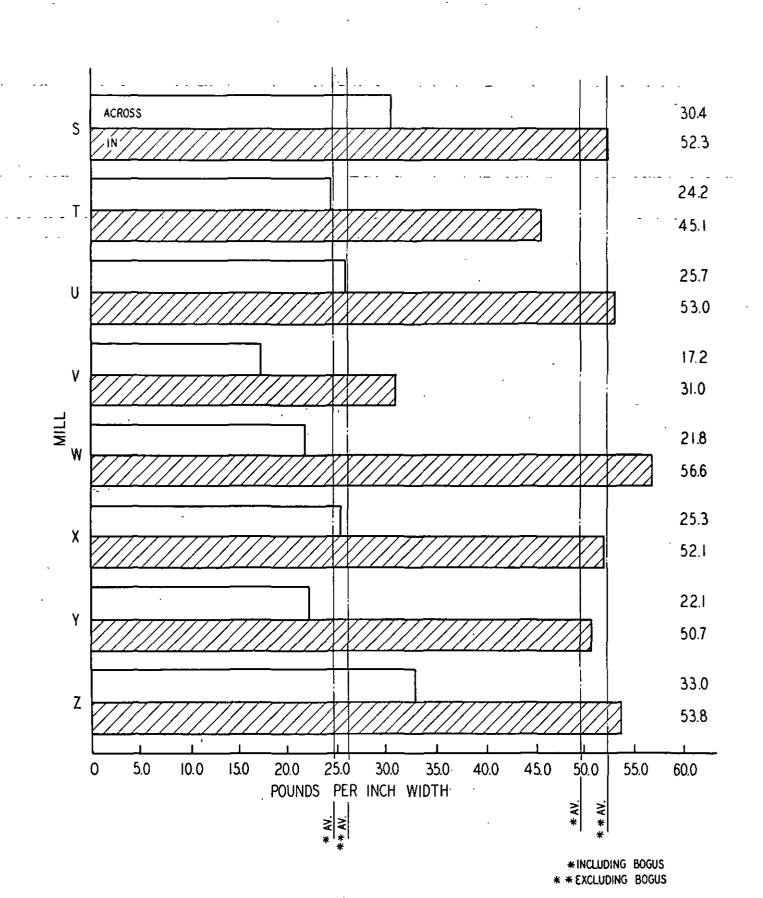


FIGURE 23. Comparison of the average Elmendorf tear of .009/26-lb. corrugating medium among mills.

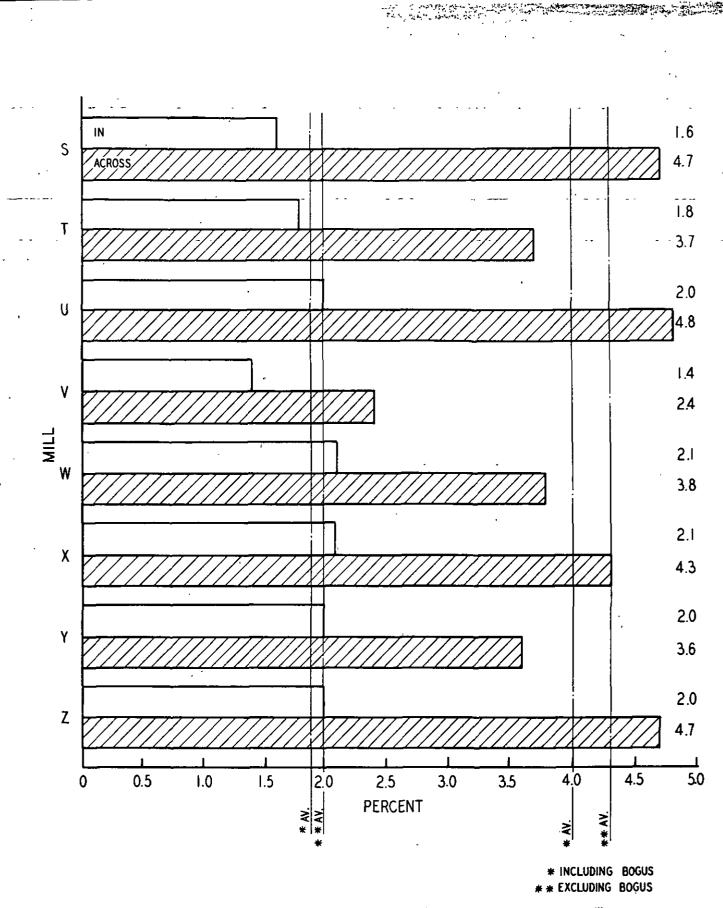


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FIGURE 24. Comparison of the average Amthor tensile strength of .009/26-lb. corrugating medium among mills.



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FIGURE 25. Comparison of the average Amthor stretch of .009/26-lb. corrugating medium among mills.

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The mill averages obtained for the G. E. puncture test are graphed in Figure 21. Because the magnitude of these results was so low that all the values fell on the extreme lower range of the indicating scale for the tester, it is doubtful if much significance can be attached to them at this time.

The average Richle compression test results are shown graphically in Figure 22. The group average was 17.6 pounds in the in-machine direction and 13.0 pounds for the across-machine direction when the bogus was-included but were 18.3 and 13.4 pounds, respectively, when the bogus medium was not included. The highest mill average was obtained for Mill Z and the lowest for Mill V (the bogus medium). The across-machine direction group average, excluding the bogus medium, was approximately 3.7% greater than the in-machine direction average for the bogus medium. The ratio of the across-machine direction values to the in-machine direction values was, on the average, of the order of 3:4.

The results of the Elmendorf tear test are graphically presented in Figure 23. The group averages for each direction were 223 and 251 grams per sheet, respectively, when the bogus medium was included, and 238 and 268 grams per sheet, respectively, when the bogus medium was excluded. The highest average tear value in the in-machine direction was obtained for Mill S but Mill W had the highest average tear in the acrossmachine direction. Mill V had the lowest mill average tear values in both directions. The ratio of the in-machine direction values to the across-machine direction values was, in general, of the 'order of 0.9:1.

The results of the Amthor tensile test are shown graphically in Figure 24. The group averages obtained (including the bogus medium) were 49.5 and 24.8 pounds per inch width for the in-machine direction and the across-machine direction, respectively, and 52.2 and 25.9 pounds per inch width, respectively, when the bogus medium was excluded. The results indicate that Mill W had the highest average tensile value in the in-machine direction and Mill Z the highest acrossmachine tensile average, whereas Mill V had the lowest average tensile strength for both directions. The average ratio of across-machine direction to in-machine direction was of the order of 1:2.

The Amthor stretch results are presented graphically in Figure 25. The group averages for the in-machine and across-machine direction stretch were 1.9 and 4.0%, respectively, when the bogus medium was included, and 2.0 and 4.3%, respectively, when the bogus medium was excluded. Mill V had the lowest average stretch in both\_directions tested. The average ratio of the in-machine direction stretch to the across-machine direction was of the order of 1:2.

A comparison of all the strength test results indicates that the averages for Mill Z were the highest and those for Mill V the lowest of the group.

The standard deviations of the physical characteristics of the corrugating medium made by each mill may be seen in Table XXXVI. The results indicate that the corrugating medium of Mill S had a lower composite average standard deviation for all the tests performed than those of the other mills. It would appear, therefore, that the corrugating medium of Mill S was more uniform than the products of the other mills on the basis of this evaluation. A comparison of the group average percentage standard deviations for the various test characteristics indicates that basis weight and caliper were the least variant and Amthor stretch the most variant of all the test characteristics studied.

The average test results tabulated in Table XXXV were treated statistically to determine if there was any significant difference between the average physical characteristics obtained for a given mill and the group average physical characteristics obtained for the balance of the mills participating. Whether or not a significant difference exists in a given test characteristic between two mills or groups of mills is denoted by the magnitude (see page 24) of the ratio of the difference of the means of each mill or group to the standard error of the difference between the same two mills or groups. In this work it has been assumed that all ratios of 2 or more indicated significant differences.

		TABLE	E XXXVI	•	
COMPARISON	OF	STANDARD	DEVIATIONS	BETWEEN	MILLS

CORRUGATING MEDIUM

	Basis	0.1	Bursting	G.E.	Comp	chle ression, lb.	Te	endorf ear, sheet		Tensile, ./in.		thor tch, %
Mill	Weight, lb.	Caliper, 0.001 in.	Strength, points	Puncture,— units	In	Across	In	Across	In	Across	In	Across
S T U V W	0.328 1.350 0.903 0.889 0.910	0.301 0.827 0.645 0.341 0.692	2 91 6.89 5.18 3.64 4.54	0.843 1.62 1.46 1.45 1.17	0.783 1.34 1.76 1.17 1.62	0.810 0.932 0.974 1.01 0.740	14.8 28.6 18.6 18.7 15.2	11 9 30.7 17.5 18.7 17.7	2.92 4.21 4.34 3.70 3.69	1.70 2.23 3.57 2.72 0.872	$\begin{array}{c} 0.103 \\ 0.155 \\ 0.281 \\ 0.224 \\ 0.350 \end{array}$	$\begin{array}{c} 0 & 276 \\ 0 & 536 \\ 0 & 447 \\ 0 & 249 \\ 0 & 440 \end{array}$
X Y Z	0.881 0.746 0.522	$\begin{array}{c} 0.507 \\ 0.474 \\ 0.366 \end{array}$	3.14 11.0 5.21	1.78 2.10 1.03	1.25 2.80 1.59	0.941 1.61 1.22	22.9 20.8 17.1	24.8 25.9 24.6	4.88 4.90 3.86	2.61 2.83 2.65	0.133 0.157 0.155	0.851 0.488 0.659
Average	0.816	0.519	5.31	1.43	1.54	1.03	19:6	21.5	4.06	2.40	0.195	0.493
Average standard deviation, %	3.0	5.2	8.6	7.9	88	7.9	8.8	8.6	8.2	9.7	10.3	12.3

The application of this treatment to a comparison of the average results obtained for Mill S with the averages obtained for the group T to Z, inclusive, may be seen in Table XXXVII. The results obtained indicate that, when the average test values of Mill S are compared with the group average of Mills T to Z, there is a significant difference in all the test values obtained, except for the Amthor tensile in the across-machine direction. With the exception of Amthor stretch in the in-machine direction, all the average test values exhibiting significant differences were of a greater magnitude than the corresponding group values. Thus, the quality for Mill S, as determined by these tests, was significantly greater than the average quality for the group.

The results obtained when the averages for Mill T are compared with the average of the balance of the group may be seen in Table XXXVIII. The results indicate that there was a significant difference in all the test values except basis weight, caliper, Elmendorf tear, Amthor tensile in the across-machine direction, and Richle compression in the across-machine direction. With the exception of the average G. E. puncture value, all the test values having significant differences for Mill T were of a lower magnitude than the corresponding values for the balance of the group.

A comparison of the average values obtained for Mill U with the group average excluding U is presented in Table XXXIX. The results indicate that there was a significant difference in all the test values except those for basis weight and Riehle compression and Amthor tensile tests in the across-machine direction. All the test values in which a significant difference existed were of a greater magnitude than the corresponding group average values.

The results of the comparison of the average test results obtained for Mill V with the average test results obtained for the remainder of the group participating are given in Table XL. It may be observed that the caliper value was the only test characteristic for which a significant difference was not indicated between it and the corresponding group characteristic. All the test values for Mill V in which a significant difference was indicated were of a lower magnitude than the corresponding test values for the group.

The results of the comparison of the average test results obtained for Mill W with the average test results obtained for the balance of the group are shown in Table XLI. Significant differences existed in all the test results except basis weight, caliper, Riehle compression and Elmendorf tear in the in-machine direction, and Amthor stretch in the across-machine direction.

The results obtained when the average test values for Mill X were compared with the average values of the balance of the group are presented in Table XLII. The only test values in which a significant difference did not exist were caliper, Amthor tensile and stretch in the across-machine direction, and Riehle compression. Similarly, all the significant values for Mill X were greater than the average values obtained for the group.

The average test values obtained for Mill Y, and the average test results obtained for the balance of the group are given in Table XLIII. The test values in which no significant difference was indicated are bursting strength, Richle compression in both directions, and Amthor tensile in the in-machine direction. With the exception of Amthor stretch in the inmachine direction all the significant test values obtained for Mill Y were of a lower magnitude than the corresponding test values for the group.

The average test values for Mill Z and the average values for the balance of the group are given in Table XLIV. The results indicate that a significant difference exists for all the test values except for basis weight and for Elmendorf tear in the across-machine direction. With the exception of caliper, all the test values for Mill Z in which a significant difference exists were of a greater magnitude than the corresponding group values.

# DISCUSSION OF INDIVIDUAL MILL TEST RESULTS FOR .009/26-LB. CORRUGATING MEDIUMS

Mill S

The average results of the various physical tests conducted on samples of .009/26-lb. kraft corrugating medium made by Mill S are shown in Table XLV (see also Table LXXI of the Appendix). It may be observed that the average basis weight was higher than the specified grade weight. The average caliper was 0.0101 inch and the average apparent density was 32.4 pounds per cubic foot. The average bursting strength was 68 points. The average Riehle compression was 19.5 and 15.5 for the in- and across-machine directions, respectively. The average moisture content was 8.5% on an ovendry basis.

Table XLVI gives the standard deviations and the probable variation to be expected in the rolls of .009/26-lb. corrugating medium made by Mill S. These results show that the chance probability or uniformity for Mill S as regards basis weight is such that approximately 87% of the corrugating rolls should fall within a range limit of  $\pm 0.5$  pound (26.8 to 27.8 pounds) and practically all the rolls should fall within a range limit of  $\pm 1.0$  pound (26.3 to 28.3 pounds). The standard deviation of the caliper results indicates that the greater portion of the rolls should fall within a range limit of  $\pm 0.001$  inch (0.0091 to 0.0111 inch). The uniformity of the bursting strength indicates that 61% of the rolls should fall within a range limit of  $\pm 2.5$ points (65.5 to 70.5 points), 91% within the range limit of  $\pm 5.0$  points (63 to 73 points), and practically all the rolls within the range limit of  $\pm 7.5$  points (60.5 to 75.5 points). The standard deviation for the Richle compression is such that it should be expected that approximately 80% of the rolls should fall within a

# TABLE XXXVII

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL S WITH THE BALANCE OF THE GROUP

		•			Corrug	ATING MED	IUM						
···	Basis Weight,	) Calina	Burst- ing Strength	G.E. Punc	Compi	chle ression,	Te	endorf ear, sheet		Tensile, /in	Amt Stretc		, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
ц	/1000)	0.001 in.	points	, ture, units	In	Across	, In	Across	In	Across	In	Across	i
Mean of S	27 3	10.1	68	20	19.5	15.5	268	276	52 3	30.4	1.6	4.7	
Mean of $\alpha$	26.7	9.9	61	18 .	17.2	12.7	216	246	48.9	24.2	1.9	3.9	,
Difference of mean $(S-\alpha)$ Standard error of	+0.63	+0.24.	+7.8	+2.5	+2.25	+2.74	+51.9	+30.0	+3.40	+6.17	-0.29	+0.86	
difference	0.143	0,114	1.15	0.315	0.312	0.283	5.19	4.55	1.03	0.604	0.0398	0.105	
Ratio: $(S-\alpha)/SE_D$	+4.4	+2.1	+6.8	+7.9'	+7.2	+9.7	+10.0	+6.6	+3.3	+1.0	7.3	+8.2	
Significant	Yes	Yes	Yes	_Yes	_Yes	Yes	Yes	Yes	Yes	No	Yes		

NOTE. All mean values have been reported to the same precision as individual test values. It will be observed that some of the intermediate values in the above table have been reported to more places than the mean values. Similarly the difference of the means will not always correspond to the difference between reported means, because these values have been rounded off. The mean of  $\alpha$  is the mean for the balance of the group.

#### TABLE XXXVIII

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL T WITH THE BALANCE OF THE GROUP CORRUGATING MEDIUM

		-										
	Basis Weight, lb.	Caliper,	Burst- ing Strongth	G.E. Punc-	் Comp	ehle pression, lb.		endorf Fear, /sheet		ior Tensile, b./in.		nthor tch, %
		0.001 in.		, ture, units ·	In	Across	In	Across	In	Across	In	Across
Mean of $T$	27.0	10.0	57	20	· 15.9	12:8	237	261	45.1	24.2	1.8	3.7
Mean of $\alpha$ ,	26.7	· 9.9	62	18 ·	17.7	13.1	221	248	49.9 ·	25.1	1.9	4.0
Difference of mea $(T-\alpha)$		+0.09	-5.0	+1.8	-1.81	-0.33	+16.1	+12.6	-4.79	-0.84	-0.11	-0.38
Standard error of difference	0.433	0.266	2.27	0 535	0.462	0.318	9.26	9.96	- 1.40	0.753	0.0538	0.178
Ratio: $(T-\alpha)/SE$	E <sub>D</sub> +0.7	+0.3	2.2	+3.4	-3.9	-1.0	+1.7	+1.3	-3.4	1.1	-2.0	-2.1
Significant	No	No	Yes	Yes	Yes	No	No	No	Yes	No	Yes	Yes

NOTE. See Note to Table XXXVII.

# TABLE XXXIX

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL U WITH THE BALANCE OF THE GROUP CORRUGATING MEDIUM

	Basis Weight, lb. (12 x 12	Caliper,	ing	G.E. Punc- ture,	Comp	ehle ession, b.	Т	endorf ear, sheet		Tensile, /in.	Am Strete	thor h, %
•		0.001 in.		units	In	Across	In	Across	In	Across	In	Across
Mean of $U$	26.9	10.7	65	20	19.7	13.5	238	266	53.0	25.7	2.0	4.8
Mean of $\alpha$	26.7	9.8	61	18	17.2	13.0	221	247	48.8	24.8 ·	1.9	3.9
Difference of mean $(U-\alpha)$	+0:16	+0.91	+4.0	+1.9	+2.47	+0.47	+17.5	+18.6	+4.16	+0.87	+0:13	+0.92
Standard error of difference	0:219	0.153	1.33	 0.359	0.426	0.245	4.66	4.61	1.05	0 821	0.0650	0.114
Ratio: $(U - \alpha)/SE_i$ Significant	o +0.7 No	+5.9 Yes	+3.0 Yes	+5.3 Yes	+5.8 Yes	+1.9 No	+3.8 Yes	+4.0 ⊷ Yes	+4.0 Yes	+1.1 No	+2.0 Yes	+8.1 Yes

NOTE: See Note to Table XXXVII.

0.746

No

+0.5

1.37

+2.3

Yes

+5.2

Yes

+1.3

No

0.0421 0.233

# TABLE XL

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL V WITH THE BALANCE OF THE GROUP

	Basis Weight, Ib.	Calinan	Burst- ing	G.E. Punc-	Comp	ichle oression, lb	Т	endorf ear, sheet		r Tensile, ./in		thor ch, %	-	
		0.001 in	Strength . points	, ture, . units	In	Across	In	Across	In	Across	In	Across		
Mean of V	25.8	10.1	32	11	12.9	10.3	121	134	31.0	17.2	1.4	2.4		
Mean of $\alpha$	26.9	9.9	66	19	18.2	13.5	237	266	51.9	26.1	1.9	4.2		
Difference of mean $(V-\alpha)$	-1.11	+0.20	33.4	-7.8	-5.20	-3.21	-116.6	-132.3	-20.92	-8.90	-0.52	-1.84		
Standard error of Difference	0.264	0.113	1.23	0.433	0.373	0.305	5.65	5.78	1.12	0.799	0.0658	0.091		
Ratio: $(V - \alpha)/SE_i$	<b>-4.2</b>	+1.8	-27.2	-18.0	-13.9	-10.5	-20.6	-22.9	-18.7	-11.1	-7.9	-2.0		
Significant	Yes	No	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes _	Yes	Ves .		
NOTE. See Note to	Table XX	xxvII.	-		•									

#### TABLE XLI

# COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL W WITH THE BALANCE OF THE GROUP

				CORRUG	ATING MED	IUM					
Basis Veight, 15.	Calinar	Burst- ing	G.E. Punc-	Compr	ession,	Т	ear,				
			units	In	Across	In	Across	In	Across	In	Across
26.8	10.1	69	19	17.7	11.5	228	300 ·	56.6	21.8	2.1	3.8
26.7	9.9	61	18	17.5	13.3	222	243	48.3	25.4	1.8	4,0
+0.08	+0.17	+8.0	+1.1	+0.17	-1.79	+5.7	+57.3	+8.31	-3.57	+0.25	-0.24
0.269	0,200	1.43	0.364	0.484	. 0.239	4.79	5.52	1.12	0.371	0.0988	0,135
+0.3	+0.8	+5,6	+3.0	+0.4	-7.5	+1.2	+10.4	+7.4	-9.6	+2.5	-1.8
No	No	Yes	Yes	No	Yes	No	.Yes	Yes	Yes	Yes	No
	/eight, 1b. 2 x 12 1000) 26.8 26.7 -0.08 0.269 ⊢0.3	reight, lb.       2 x 12       Caliper, 1000)       0.001 in.         26.8       10.1       26.7       9.9         -0.08       +0.17       0.269       0.200         +0.3       +0.8       +0.8       +0.8	Peright,         Burst- ing           1b.         ing           2 x 12         Caliper, Strength, 1000)           0.001 in.         points           26.8         10.1         69           26.7         9.9         61           -0.08         +0.17         +8.0           0.269         0.200         1.43           +0.3         +0.8         +5.6	Peright,         Burst- ing         G.E. Punc- 1000)           2 x 12         Caliper, Strength, points         ture, units           26.8         10.1         69         19           26.7         9.9         61         18           -0.08         +0.17         +8.0         +1.1           0.269         0.200         1.43         0.364           +0.3         +0.8         +5.6         +3.0	Peright,       Burst- ing       G.E. Punc- lb.       Comprise $2 \times 12$ Caliper, Strength, 1000)       ture, 0.001 in.       in $26.8$ 10.1       69       19       17.7 $26.7$ 9.9       61       18       17.5 $-0.08$ $+0.17$ $+8.0$ $+1.1$ $+0.17$ $0.269$ $0.200$ $1.43$ $0.364$ $0.484$ $+0.3$ $+0.8$ $+5.6$ $+3.0$ $+0.4$	reight, lb.Burst- ing pointsG.E. Punc- unitsCompression, lb.2 x 12 1000)Caliper, Strength, pointsture, unitsInAcross26.8 26.710.1 9.969 61 1817.7 17.511.5 13.3-0.08 -0.08 +0.17 +0.17+8.0 +1.1 +0.17 +1.1 +0.17 +0.3 +0.8 +5.6 +3.0 +0.4-7.5	Pright,       Burst-ing       G.E.       Compression,       Transform         1b.       ing       Punc-       ib.       g./s         2 x 12       Caliper, Strength,       ture,       In       Across       In         26.8       10.1       69       19       17.7       11.5       228         26.7       9.9       61       18       17.5       13.3       222         -0.08       +0.17       +8.0       +1.1       +0.17       -1.79       +5.7         0.269       0.200       1.43       0.364       0.484       0.239       4.79         +0.3       +0.8       +5.6       +3.0       +0.4       -7.5       +1.2	reight, lb.Burst- ing Punc- Lo.Compression, lb.Tear, g./sheet2 x 12 1000)Caliper, Strength, pointsture, unitsInAcrossInAcross26.8 26.710.1 9.969 6119 1817.7 17.511.5 13.3228 222300 243-0.08 -0.08+0.17 +8.0+1.1 +1.1+0.17 +0.17 -1.79-1.79 +5.7 +5.7 +57.3+57.3 -52 +0.30.269 -0.2000.200 1.431.43 0.3640.484 +0.4 -7.50.239 +1.2 +1.2 +10.4	reight, lb.Burst- ing punc- 1000)G.E. punc- unitsCompression, lb.Tear, g./sheetAmthor lb.2 x 12 1000)Caliper, pointsStrength, unitsture, unitsIn 1000AcrossIn AcrossAmthor lb.26.8 26.710.1 9.969 6119 1817.7 17.511.5 13.3228 222300 24356.6 48.3-0.08 -0.08+0.17 +8.0+1.1 +1.1+0.17 +0.17 -1.79-1.79 +5.7 +5.7 +57.3+8.31 +8.310.269 -0.2000.200 +0.81.43 +5.60.484 +3.0 +0.40.239 -7.54.79 +1.2 +10.45.52 +7.4	reight, lb.Burst- ing Punc- 2 x 12G.E. Punc- unitsCompression, lb.Tear, g./sheetAmthor Tensile, lb./in.2 x 12Caliper, Strength, pointsture, unitsInAcrossInAcross26.810.1691917.711.522830056.621.826.79.9611817.513.322224348.325.4-0.08+0.17+8.0+1.1+0.17-1.79+5.7+57.3+8.31-3.570.2690.2001.430.3640.4840.2394.795.521.120.371+0.3+0.8+5.6+3.0+0.4-7.5+1.2+10.4+7.4-9.6	reight, lb.Burst- ing Punc- 2 x 12G.E. Punc- unitsCompression, lb.Tear, g./sheetAmthor Tensile, lb./in.Amt Stretc26.810.1691917.711.522830056.621.82.126.810.1691917.711.522830056.621.82.126.79.9611817.513.322224348.325.41.8-0.08+0.17+8.0+1.1+0.17-1.79+5.7+57.3+8.31-3.57+0.250.2690.2001.430.3640.4840.2394.795.521.120.3710.0988+0.3+0.8+5.6+3.0+0.4-7.5+1.2+10.4+7.4-9.6+2.5

NOTE. See Note to Table XXXVII.

COMPA	RISON O	<b>F THE P</b>	HYSICAI	CHAR	ACTERIS	TICS OF	MILL X	WITH TH	IE BALAN	CE OF T	HE GRO	JP
					Corru	gating Me	DIUM					
	Basis Weight, lb. (12 x 12	Caliner	Burst- ing Strength.	G.E. Punc- ture.	Comp	iehle pression, lb.	Т	iendorf 'ear, 'sheet		Tensile, /in.		thor ch, %
		0.001 in.		units	In	Across	,In	Across	 In	Across	In	Across
Mean of $X$	27.4	9.8	68	21	17.1	. 13.1	250	281	52.1	25.3	2.1	4.3
Mean of $\alpha$	26.7	9.9	61	18	17.6	13.1	219	245	48.9	24.9	1.9	4.0
Difference of mea $(X-\alpha)$	n +0.74	-0.13	+7.2	+2.7	-0,41	+0.02	+31.2	+35.6	+3.19	+0.36	+0.22	+0.31

+0.1

0.279

No

7.07

Yes

+5.0

6.50

+4.8

Yes

# TABLE XLII

NOTE, See Note to Table XXXVII.

Ratio:  $(X-\alpha)/SE_D + 2.9 = -0.9$ Significant Ves No

Yes

Standard error of difference

Significant

0.254 0.148

No

1.09

+6.6

Yes

+5.4

Yes

0.502

-1.1

No

0.383

COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL Y WITH THE BALANCE OF THE GROUP

						Corrug	ATING MEI	DIUM		•						
	n der – 11. ann a 18 dimension	Basis Weight, lb.	Caliper.	Burst- ing	G.E . Punc-	Rie Compr Il	,	Т	endorf ear, sheet	Amthor lb.	Tensile, /in	Ami Streto				•
			0.001 in.		ture, units	In	Across	In	Across	In	Across	In	Across	· ·		
	Mean of Y	26.0	9.3	58	15	17.3	12.3	189	219	50.7	22.1	2.0	3.6	•		
	Mean of $\alpha$	26.8	10 0	62	19	17.5	13 2	228	254	49.1	25.4	1,9	4.0			
	Difference of mean $(Y - \alpha)$	0.82	-0 75	-4.3	-39	-0.23	-0.95	-38.6	-35 3	+1.54	-3.27	+0.18	-0.44		•	
<u>.</u>	Standard error of difference	0.254	0.161	3 52	0.679	0.897	0.520	6.91	8.53	1.61	0.929	0.0543	0 164			
	Ratio: $(Y - \alpha)/SE_D$	-3.2	-4.7	1.2	5.7	-0.3	-t.8	-5.6	-4.1	+1.0	-3.5	+3.3	-2.7			
	Significant.	Yes.	Yes	No		No	No	Yes	Yes	No	Yes	Yes	Yes			_
	NOTE Cas Note to '	ren 1997 Pable VI	· ·····					•								

TABLE XLIV

#### COMPARISON OF THE PHYSICAL CHARACTERISTICS OF MILL Z WITH THE BALANCE OF THE GROUP

2	,				CORRUG	ATING MEI	NUM	,				
	Basis Weight, Ib.	Caliper.	Burst- ing	G.E. Punc-	Comp	chle ression, b.	Т	endorf ear, sheet		r Tensile, ./in.		thor ch, %
		0.001 in.		, ture, units	In	Across	In	Across	In	Across	In	Across
Mean of Z	26.8	93.	.75	20	19.9	15.8	251	262	53.8	33.0	2.0	4.7
Mean of $\alpha$	26.8	10 0	60·	- 18	17.2	12.7	219	248	48.7	23.8	× 1′, 9	3.9
Difference of mean $(Z-\alpha)$		-0.73	+15.7	+1.6	+2.79	+3.05	+32.7	+13.5	+5.11	+9.18	-+-0:14	+0.81
Standard error of difference	0.185	0:126	1. <b>71</b>	0.352	0.512	0.386	5.61	7.80	1.25	0.841	0.0517	0.206
Ratio: $(Z-\alpha)/SE_D$	-0.0	-5.8	+9.2	+4.5	+5.4	+7.9	+5.8	+1.7	+4.1	+10.9	+2.7	+3.9
Significance	No	Yes	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes	Yes	Yes
NOTE. See Note to '								1				

range limit, in both directions, of  $\pm 1.0$  pound and approximately 94% within a range limit of  $\pm 1.5$ pounds. The uniformity with respect to G. E. puncture, Elmendorf tear, Amthor tensile and stretch may also be seen in Table XLVI. Naturally, as the arbitrarily selected limits increase, the greater is the portion of rolls falling within that range. The ranges used are purely arbitrary and are not intended as an attempt to specify acceptable limits of uniformity. The moisture content was not treated statistically because it was felt that secondary effects, such as warehouse storage conditions, might cause too great an effect to permit the legitimate application of statistics.

MILL T

The average test results obtained for the kraft corrugating medium made by Mill T are shown in Table XLVII (see also Table LXXII of the Appendix). The average basis weight obtained was 1 pound higher than the specified weight. The average caliper was 0.010 inch and the average apparent density was 32.5 pounds per cubic foot. The average bursting strength value was 57 points. The average Riehle compression values were 15.9 and 12.8 pounds for the in- and across-machine directions, respectively. The average moisture content was 11.8% on an ovendry basis.

The statistical evaluation of these test results may be seen in Table XLVIII. For basis weight, the standard deviation was 1.35, indicating that 29% of the rolls made by Mill T should fall within a range limit of  $\pm 0.5$  pound (26.5 to 27.5 pounds), 54% within a range limit of  $\pm 1.0$  pound (26.0 to 27.0 pounds), and approximately 86% within a range limit of  $\pm 2.0$  pounds (25.0 to 29.0 pounds). The standard deviation for caliper was 0.827; thus, approximately 77% of the rolls of corrugating medium made by Mill T might be expected to fall within a range limit of  $\pm 0.001$  inch (0.009 to 0.011 inch) and approximately 98% within a

۰.

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

#### Mill S Roll Averages

						1	xon Avera	.ges										
	_	Basis Weight, lb.	Caliper,		Mois-	Bursting	G.E. Punc-	Comp	ehle ression, lb.	Т	endorf ear, sheet	Am Ten lb.,	thor sile, /in.	Am Stret	thor ch, %		• -	
Roll	Date Manuf.	(12 x 12 /1000)	0.001 in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across	In	Across	In	Across			•
$     \begin{array}{r}       1 \\       2 \\       3 \\       - 4 \\       5     \end{array} $	2-7-45 2-7-45 2-7-45 - 2-6-45 2-6-45	27.5 27.8 27.6 27.1_ 27.3	9.6 9.9 9.7 10.5 10.3	34.4 33.7 34.1 31.0 31.8	3.4 6.2 6.4 11.5 9.6	72 66 64 71 69	21 20 20 21 21	19.5 21.2 19.7 19.7 19.8	14 8 15.6 14.3 14.4 15.2	250 253 250 281 288	268 270 269 269 282	56.8 57.2 53 9 49.7_ 50.0	27.9 28.9 28.5 - 30.1- 29.5	1.7 1.8 1.7 1.6- 1.5	4.6 5.1 5.1 -4.8 4.6	-	••••	_
6 7 8 9 10	2-6-45 2-6-45 2-6-45 8-9-44 8-9-44	27.1 27.0 27.2 27.7 26.8	10.1 10.3 - 10:4 10.3 10.1	32.2 31.5 -31.4 32.3 31.8	9.8 12.3 11.9 4.9 8.5	71 70 69 67	21 21 19 21 19	18.5 19.0 19.4 19.4 18.4	15.9 15.6 16.0 16.7 16.4	265 279 287 265 263	286 300 285 269 261	51.6 49.6 49.2 52.2 52.8	30.7 31.6 31.0 33.4 31.9	$     \begin{array}{r}       1 & 6 \\       1.6 \\       1.5 \\       1.5 \\       1.7 \\       1.7 \\     \end{array} $	$\begin{array}{c} 4.8 \\ 4.8 \\ 4.9 \\ 4.2 \\ 4.5 \end{array}$	·		-
Aver	age '	27.3	10.1	32.4	8.5	68	· 20	19.5	15.5	268	276	52.3	30.4	1.6	4,7			•

STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM MILL S .

TABLE XLVI

	Basis Weight, Ib. (12 x 12		Bursting	G.E.	Comp	chle ression, b.	T	endorf ear, sheet		r Tensile, ./in.		Stretch, %
	/1000)	Caliper, 0.001 in.	Strength, points	Puncture, units	In	Across	In	Across	In	Across	' In	Across
Test values Maximum Minimum	27.8 26.8	10 5 9.6	72 64	21 19	21.2	16.7 14.3	288 250	300 261	572 492	33.4 28.5	1.8 1.5	$5.1 \\ 4.2$
Average	27.3	10.1	68	20	19.4	15.5	268	276	52.3	30.4	1.6	4.7
Standard deviation	0.328	0.301	2.91	0.843	0.783	0.810	14.8	11.9	2.92	1 70	0.103	0.276
Range limit (±)* Approximate	0.5	1.0	2.5	1.0	1.0	1.0	7.5	7.5	1.5	1.0	0.1	0.2
probability, %	87	99	61	77	80	78	39	48	39	44	67	53
Range limit $(\pm)^*$ Approximate	1.0	2.0	5.0	1.5	1.5	1.5	15.0	15.0	3 0	2.0	0.2	0,4
probability, %	99	100	91	93	94	94	69	79	70	76	95	85
Range limit $(\pm)^*$ Approximate	2.0	—	7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0.3	0,6
probability, %	100	—	99	99	99	99	96	99	91	92	100	97

\* Range limits were arbitrarily selected.

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

## MILL T **Roll Averages**

								100111100	inges .			-					
	na - giunte≠	Date	Basis Weight, lb. (12 x 12	Caliper,	-Appar- ent Density,	Mois-	Bursting Strength,	Punc-	Comp	ehle ression, - lb.			• Ter	thor sile; /in.		thor ch, %	* + +=== *-= *
	Roll	Manuf.	/1000)	in	lb./cu.ft.		points	units	In	Across	In	Ácross	In	Across	In	Across	
	1 2 3 4	5- 1-45 5- 1-45 5- 2-45 5- 2-45	29.5 29.5 25.9 26.6	11.2 11.8 9.5 9.5	31 6 30.0 32.7 33.6	10.8 12.5 13 3 12.9	47 43 61 63	22 23 20 20	14.2 13.7 18.1 16.9	11.6 11.2 13.8 12.2	293 284 225 224	326 304 231 238	39.0 37.1 46.0 48.7	21.4 19.2 24.9 25.6	1.7 1.6 1.5 1.7	3.2 2.6 3.9 3.8	
	6 7 8 9 10	- 5-+2-45- 5- 2-45 3-31-45 5-2-45 5- 2-45 -5- 2-45	25 9	9.7 9.9	$\begin{array}{c} 32.7\\ 32.8 \end{array}$	-12.5 12.6 10.8 -11.4 10.9 10.7	63 55 62 58 60	20	15.5 17.1	12.9	226	266 248 259 -244 246 245 ~-	47.7 42.5	24.1	2.0 1.9 1.8 1.9 1.9 1.8	4.0 3.0 4.0 4.1 3.8 4.2	
•	Averag	ge .	27.0 -	10.0	32.5	11.8	57	20	15.9	12.8	· 237	261	45.1	24.2	1.8	3.7	

TABLE XLVIII

# STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

					Mı	ll T	,	Ĺ	•			
	Basis Weight, lb. (12 x 12	Caliper,	Bursting Strength,	G.E. Puncture,	Com	lichle pression, lb.	Т	endorf ear, sheet		r Tensile, ./in.		Stretch,
	/1000)	0.001 in	points	units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average Standard deviation	29.5 25.9 27.0 1.35	11.8 9.3 10.0 0.827	63 43 57 6.89	23 18 20. 1.62	18.1 13.7 15.9 1.34	14.1 11.2 12 8 0.932	293 211 237 28 .6	326 231 261 30.7	49.4 37.1 45.1 4.21	26 7 19.2 24.2 2.23	2.0 1.5 1.8 0.155	4 2 2.6 3.7 0.536
Range limit (±)* Approximate probability, %	0.5 29	1:0 77	2.5 28	1.0 46	1.0 55	1.0 72	75 21	7.5	1.5 28	1.0 35	0.1 48	0.2 29
Range limit $(\pm)^*$ Approximate	1.0	2.0	5.0	1.5	1'.5	15	15.0	15.0	30	2.0	0.2	0:4
probability, % Range limit (±)* Approximate	54 2.0	98 	53 7.5	65 3.0	74 30	89 3.0	$\frac{40}{30.0}$	38 30,0	52 5.0	63 3.0	80 0.3	55 0.6
probability, %	86		72	94	98	100	71	67	79	82	95	74

\* Range limits were arbitrarily selected

# TABLE XLIX .

# PHYSICAL CHARACTERISTICS OF 009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

# Mill U

Roll <i>i</i>	lverages
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7. 11	Date	Basis Weight, lb. (12 x 12	Caliper, 0 001	Density,	Mois- ture,	Bursting Strength,	G.E. Punc- ture,	Comp	iehle <sup>-</sup> pression, lb.	Т	endorf ear, sheet	Tei	mthor nsile, ./in.		athor tch, %	
Roll	Manuf.	/1000)	in.	ib /cu.ft.	%	points	units	In	Across	, In	Across	In	Across	In	Across	
	1-30-45 1-30-45 10- 2-44	26.3 25.0 26.9	10.7 9.7 11.4	29.5 30.9 28.3	11.6 11.3 	74 70 62	21- 18 20	16.8 16.6 19.9	12.9 · 13.0 13.2_	264 225 224	291 239 272	51.7 48.1 52.0-	28.5 29.6 - 21 0	2.5 2.4 -2.0	4 8 5 2 5-1	
5	<sup></sup> 11-23-44 11-23-44	26:9 27.4	- <u>9</u> ,9 10.0	32.6 32.9	9.0 8.3	63 · 61	22 22	$\frac{20.1}{18.6}$	14,9 14,5	276 264	280 268	$47.8 \\ 48.5$	28 8 29.1	1.6	4 0 4.2	
6 	10- 2-44 - 11-23-44 12-11-44 12-11-44 12-11-44	27.2 -26.2 26.0 27.2 - 27.1	11 5 - 9:4 - 10.1 - 10.7 - 10.4	28 4 - 33:4 - 30.9 30.5 31.3	9.7 -9.1 8.8 7.7 9.4	64 59 65 68 68	21 - 19 19 20 19	21 5 21-6 19.3 23.4 22.0	-13.1 14.3 13.2 14.2 14.0	239 241 223 226 221	277 254 246 275 258	54.1 45.3 55.4 57.7	20.7 29.5 24.1 25 0	1.9 1.6 2.1 1.9	.5.0 4 6 . 5.1 5.0	
11 12 13 14 15	10-16-44 11- 1-44 11- 1-44 11- 1-44 11- 1-44	27.6 28.5 25.1 27 8 28.1	11.2 11.6 10.5 10.9 11.0	29.6 29.5 28.7 30:6 30.6	8.3 9.5 6.3 6.7 5.8	70 66 59 61 67	19 21 17 20 21	20.9 21.1 19.4 20.5 19.1	14.9 13.9 13.5 15.0 13.2	238 256 209 229 244	255 295 238 283 271	.54.6 54.4 58.0 49.6 57.7	24.2 26.3 23.3 22.6 24.1	2.0 2.2 1.5 2.1 1.9	5.1 4.9 4.3 4.9 5.0	*
16 17 18 19 20 21	3-18-45 11- 1-44 11- 6-44 9-20-44 10- 4-44 10- 4-44	26.8 27.6 26.1 26.3 27.5 27.3	10.4 11.0 10.3 10.9 11.6 11.4	30.9 30.1 30.4 28.9 28.4 28.7	7.4 8.7 7.6 5.5 7.7 8 7	64 59 54 74 68 69	20 22 19 17 20 20	18.2 18.8 18.1 20.8 17.8 18.4	13.2 14.4 11.8 12.1 12.9 11.9 12.7	256 239 220 210 236	243 272 259 243 280	56.5 44.2 55.3 51.1 59.4 55.2	26.6 35.7 24.3 21.7 26.7 23.9	2.0 2.5 1.9 2.2 2.1 2.0	4.1 5.8 5.2 5.0 4.3 4.4	۰.
Avera	ge ,	26.9	10.7	30.2	8.4	65	20	19.7	13.5	248 238	284 266	55.6 53.0	24.3 25.7	1.8 2.0	4.6 4.8	

TABLE L

STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

					MII	l U		•				
• • •	Basis Weight, lb. (12 x 12	Caliper,	Bursting Strength	G.E. Puncture,	Com	iehle pression, lb.	Т	endorf ear, sheet		r Tensile, ./in.		r Stretch, %
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
Test values						1			•			
Maximum Minimum Average	28.5 25.0 26.9	11.6 9.4 10.7	74 54 65	22 17 20	23.4 16.6 19.7	15.0 11.8 13.5	276 209	295 238	59.4 44.2	35.7 20.7	2.5 1.5	$\begin{array}{c} 5.8 \\ 4.0 \end{array}$
Standard deviation	0,903	0.645	5.18	1.46	1.76	0.974	238	206	53.0	25.7	2.0	4.8
Range limit (±)* Approximate	0.5	1.0	2.5	1.40	1.0	1.0	18.6 7.5	17.5 7.5	4.34 1.5	3.57 1.0	0.281 0.1	0.447 0.2
probability, %	42	88	37	50	43	70	31	33	27	22	00	
Range limit $(\pm)^*$ Approximate	1.0	2.0	5.0	1.5	1.5	1.5	15.0	15.0	3.0	2.0	28 0.2	35 0.4
probability, %	73	99	66	70	60	88	58	61	51	42	50	()
Range limit (±)* Approximate	2.0		7.5	3.0	30	3.0	30.0	30 0	5.0	42 3.0 ,	52 0.3	63 0.6
probability, % * Range limits we	97.	-	83 `	96	91	99	89	91	75	60	72	82

ige limits were arbitrarily selected:

 $_{-}$  range limit of  $\pm 0.002$  inch (0.008 to 0.012 inch). The uniformity of the bursting strength, as denoted by the standard deviation, indicates that only 28% of the rolls should fall within a range limit of  $\pm 2.5$  points (54.5 to 59.5 points), 53% within a range limit of  $\pm 5.0$  points (52.0 to 62.0 points), and 72% within arange limit of.  $\pm 7.5$  points (49.5 to 64.5 points). Thestandard deviations for the Riehle compression test indicate that 55% of the rolls should fall within a range limit of  $\pm 1.0$  pound in the in-machine direction, and 72% in the corresponding range limit for the across-machine direction-Practically-all of the rolls should fall within a range limit of  $\pm 3.0$  pounds for both directions. In general, the standard deviation for G. E. puncture, Elmendorf tear, and Amthor tensile and stretch are of such magnitude as to indicate considerable nonuniformity.

# Mill U

The average test results obtained for kraft corrugating medium manufactured by Mill U are presented in Table XLIX (see also Table LXXIII of the Appendix). The statistical evaluation of these results is given in Table L. The average basis weight for Mill U was 26.9 pounds, the average caliper was 0.0107 inch, and the average apparent density was 30.2 pounds per cubic foot. The average bursting strength and G. E. puncture were 65 points and 20 units, respectively. The average Riehle compression values for the in- and across-machine directions were 19.7 and 13.5 pounds, respectively. The average moisture content was 8.4%on an ovendry basis.

Inasmuch as the standard deviation for basis weight was 0.903, it is to be expected that only 42% of the rolls would fall within a range limit of  $\pm 0.5$  pound (26.4 to 27.4 pounds), 73% within a range limit of  $\pm 1.0$  pound (25.9 to 27.9 pounds), and approximately 97% within a range limit of  $\pm 2.0$  pounds (24.9 to 28.9) pounds). The standard deviation for caliper indicates that nearly 90% of the rolls should fall within a range limit of  $\pm 0.001$  inch (0.0097 to 0.0117 inch). The uniformity of the bursting strength, as shown by the standard deviation of 5.18, indicates that only 37%of the rolls would be expected to fall within a range limit of  $\pm 2.5$  points (62.5 to 67.5 points), 66% within a range limit of  $\pm 5.0$  points (60.0 to 70.0 points), and 83% within a range limit of  $\pm 7.5$  points (57.5 to 72.5 points). For the in- and across-machine direction Riehle compression, 43 and 70% of the rolls, respectively, should fall within a range limit of  $\pm 1.0$  pound, 60 and 88% within a range limit of  $\pm 1.5$  pounds, and 91 and 99% within a range limit of  $\pm 3.0$  pounds. The Elmendorf tear and Amthor tensile and stretch exhibit considerable variation or lack of uniformity.

#### Mill V

The average test results obtained for .009/26-lb. bogus corrugating medium made by Mill V are given in Table LI (*see also* Table LXXIV of the Appendix) and the statistical evaluation of these results in Table

LII. For all practical purposes, the basis weight is the, same as the grade weight specified. The standard deviation for basis weight indicates that 42% of the rolls should fall within a range limit of  $\pm 0.5$  pound (25.3) to 26.3 pounds), 74% within a range limit of  $\pm 1.0$ -pound (24.8-to 26.8 pounds), and 98%-within a-range limit of  $\pm 2.0$  pounds (23.8 to 27.8 pounds). The average caliper was 0.0101 inch with a standard deviation of 0.341, indicating that approximately 99% of the rolls should fall within a range limit of  $\pm 0.001$  inch (0.0091 to 0.0111 inch). The average apparent density was 30.7 pounds per cubic foot and the average moisture content was 9.2% on an ovendry basis. The average bursting strength was 32 points and the indicated uniformity was such that 51% of the rolls should fall within a range limit of  $\pm 2.5$  points (29.5 to 34.5 points), 83% within a range limit of  $\pm 5.0$  points (27.0 to 37.0 points), and approximately 96% within a range limit of 7.5 points (24.5 to 39.5 points). The average Richle compression values in the in- and acrossmachine-directions were 12.9 and 10.3, respectively, with standard deviations indicating a probability that 80 and 86% of all the rolls would fall within a range limit of  $\pm 1.5$  pounds. Approximately all the rolls should fall within a Riehle compression range limit of  $\pm 3.0$  pounds. The standard deviations for Elmendorf tear and Amthor tensile and stretch indicate that considerable variation should be expected.

# Mill W

The average test results obtained for the kraft corrugating medium made by Mill W are seen in Table LIII (see also Table LXXV of the Appendix). The statistical evaluation of these results are given in Table LIV. The average basis weight was slightly above the grade weight and the standard deviation of 0.910 indicates an expectancy that 42% of the rolls should fall within the range limit of  $\pm 0.5$  pound (26.3 to 27.3 pounds), 73% within a range limit of  $\pm 1.0$  pound (25.8 to 27.8 pounds), and 97% within a range limit of  $\pm 2.0$  pounds (24.8 to 28.8 pounds). The average caliper was 0.0101 inch and, according to the magnitude of the standard deviation, 85% of the rolls should fall within a range limit of  $\pm 0.001$  inch (0.0091) to 0.0111 inch) and 99% within a range limit of  $\pm 0.002$  inch (0.0081 to 0.0121 inch). The average apparent density was 31.8 pounds per cubic foot and the average moisture content was 11.1% on an ovendry basis.

The average bursting strength was 69 points. It should be expected that 42% of the rolls should fall within a bursting strength range limit of  $\pm 2.5$  points (66.5 to 71.5 points), 73\% within a range limit of  $\pm 5.0$ points (64.0 to 74.0 points), and 91% within a range limit of  $\pm 7.5$  points (61.5 to 76.5 points). The average Riehle compression results in the in- and acrossmachine directions were 17.7 and 11.5 pounds, respectively. The standard deviations for the Richle compression indicate that a range limit of  $\pm 1.0$  pound should include 46% of the rolls in the in-machine direc-

# TABLE LI

# PHYSICAL CHARACTERISTICS OF .009/26-LB. BOGUS CORRUGATING MEDIUM

MILL V Roll Averages

							1000 1100	anges							,			
- n - 11		Basis Weight, lb. (12 x 12	 Caliper, 0.001		Mois-	, Bursting Strength,	G.E. Punc-	Comp	ehle . ression, lb.	T	endorf . car, sheet	Te	othor. nsile, /in.		nthor tch, %			1
Roll	Date Manuf.	/1000)		Density, lb./cu.ft.	ture, %	points	ture, units	ĺn	Across	In	Across	In	Across	In	Across			
1	1-26-45 10-21-44	26.0 27.3	$10.4^{\circ}$ 9.4	30.0 34.8	8.4 8.4	31 39	8 12	$12.9 \\ 13.1$	10,0 10,1	95 143	112 165	30.3 37.6	15.2 18.0	$1.4 \\ 1.8$	1.9 2.6			
2 3 1	10-21-44 —	26.4 24.3	10.0 -9.9	31.7 29.4	10.0 11.7	31	10	12.9	9.3 • 9.0	123 101-	128	30.3	16.5 14 <del>.</del> 1	1.5	2.7		- •	-
5	-	25.7	10.4	29.7	10.1	31	12	13.7	10.1	113	125	31.0	17.0	1.3	2.2			
- <sup>6</sup> 7		26.1 .26.1	9.9 10.3_		10.0 . 8.5		11 13	14.7 12.4	11.4 _10.3 _	128 115	159 129	36.1 31.4	20.0 18.0	1.5	2.5			
8 _9 10		$26.9 \\ 25.3 \\ 25.0$	9,5 10,1 10,3	34_0 30_0 29_1	5.9 5.5 7.6	33 - 31 - 30	12 12 11	14.4 11.8 14.7	9.9 12.6 9.5	133 146 109	157 132 127	35.5 24.3 31.8	$16.4 \\ 23.8 \\ 14.4$	$1.0 \\ 1.3 \\ 1.3$	2.5 2.7 2.2	<b>,</b> ·		
11	-	25.5	10.5	29.1	9.8	34	13	12.1	11.2	133	144	28.8	17.8	1.6	2.2			
12 13	_	24,4 26,3	10.1 10.3	29.0 30.6	15.5 7.9	38 26	13 10	$\begin{array}{c} 12.9 \\ 11.4 \end{array}$	$\begin{array}{c} 10.9 \\ 9.3 \end{array}$	141 89	140 100	30.9 27.1	18.2 13.7	$\begin{array}{c} 1.8 \\ 1.4 \end{array}$	2.3 2.1			
Ĩ	Verage	25.8	10.1	30.7	9.2	32	11	12.9	10.3	121	134	31,0	17.2	1.4	2.4			

TABLE LU

# STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. BOGUS CORRUGATING MEDIUM

					Мп	l V						
	Basis Weight, lb.	<b>C</b> -1'	Bursting	G.E.	Comp	iehle - ression, lb.	T	endorf ear, sheet		r Tensile, ./in.	Amthor	Stretch, %
	(12 x 12 /1000)	Caliper, 0.001 in.	Strength, points	Puncture, units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average	27.3 24.3 25.8	10.5 9.4 10.1	39 26 32	13 8 11	14.7 11.3 12.9	12.6 9.0 10.3	146 89 121	165 100 134	37.6 24.3 31.0	23.8 13.7 17.2	$1.8 \\ 1.0 \\ 1.4$	2.7 1.9 2.4
Standard deviation	0.889	0.341	3.64	1.45	1.17	1.01	18.7	18.7	3.70	2.72	0.224	0.249
Range limit (±)* Approximate probability, %	0.5 42	1.0 99	2.5 51	1.0 51	1.0 60	1,0 68	7.5 31	7.5 31	1.5 32	1.0 29	0.1 35	0.2 58
Range limit (±)* Approximate	1.0	2.0	5.0	1.5	1.5	1.5	15.0	15.0	3.0	2.0	0.2	0.4
probability, % Range limit (±)*	$\frac{74}{2.0}$	100	83 7.5	70 3.0	80 3.0	86 3.0	58 30:0	$\frac{58}{30.0}$	58 5.0	54 3.0	63 0.3	89 0.6
Approximate probability, %	98		96	96	<del>9</del> 9	99	89	89	82	73	82	98

\* Range limits were arbitrarily selected.

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

M	IILL W
Roll	Averages

	,					,	·		and Ben		. '						
		una ma a seconda da se Da ta	Basis Weight,- lb. (12 x 12	Caliper, 0.001		Mois-	Bursting	G.E. <sup>-</sup> Punc-	* Comp	ehle ression,** h.		endorf ear, sheet	Ter	thor silė, – – /in.		nthor tch, %	<b>b</b> a <b>a</b> a
	Roll	Date Manuf.	/1000)	in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across	In	Across	In	Across	
	1.3 2	2- 1-45 11-11-44	$\begin{array}{c} 28.0\\ 28.0\end{array}$	10.0 10.5	33.6 32.0	12.0 11.4	· 77 70	20 20	18.7 18.3	$12.4 \\ 12.0$	240 236	315 316	64.4 61.1	23.6 22.1	2'.4 2.3	3.7 3.4	•
	3 4	11-11-44 12-28-44	27.5 27.4	10.2	32.4 29.9	11.2 _10.7	74 67	19 21	18.2 16.4_	12.1	229 260 · .	323 321	60.2 _54.0.	22.3 -20.5	2.3 . 1.9	3.5	منبع ومغاد المر
	5 6	12-28-44 2-27-45	27.6 25.9	10.9 9,0	30.4 34.5	12.5 13.2	68 74	21 18	19.7 16.0	12.5 11.5	249 214	301 293	51.4 596	20 8 22.4	2.1 2.5	4 1 4.1	
	- 8	2-27-45		9.1 - 9:1 -	33.5 33 <sup>.</sup> 9-	12.2 10.0-	71 	18 18	15.8 17.3-	10.3	213	292 310 <sup>-</sup>	56.5 55.5	20.9	2.2		
	10	12-17-44 12-17-44	27 4 26.2	10.4 10.4	31.6 30.2	13.5 14.3 -	- 66 - 62	20 19	$\frac{18.9}{20.3}$	$\frac{11.9}{11.7}$	215 221	300 304	52.9 54.2	22.2 20.9	1.2 1.9	$-\frac{3}{3.0}$	•
	11 12 13	2-28-45 2- 3-45 2- 3-45	26.0 27.2 26.5	· 9.4 10.6 10.2	33.2 30.8 31.2	. 11.0 6.1 , 6.2	65 65 63	18 20 18	$18.3 \\ 14.9 \\ 16.7$	11.7 10.3 11.7	214 231 212	269 277 276	54.8 55.3 55.8	22.0 21.6 21.8	1.9 1.9 2.1	4.5 4.1 4.3	
• '	) A	verage .	26 8	10.1	31.8	11.1	69	19	17.7	11.5	228	300	56.6	21.8	2.1	3.8	

TABLE LIV

STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

					·	MIL	l W			-			
	·	Basis Weight, lb.	0.1	Bursting	G.E.	Comp	iehle ression, lb.	T	endorf ear, sheet		Tensile, ./in.		Stretch,
		(12 x 12 /1000)	Caliper, 0.001 in.	Strength, points	Puncture, units	In	Across	In	Across	 In	Across	In	Across.
	Test values Maximum Miminum Average	28.0 25.4 26.8	11.0 9.0 10.1	77 62 69	21 18 19	20.3 14.9 17.7	12.5 10.3 11.5	260 212 228	323 <sup>°</sup> 269 300	64.4 51.4 56.6	23.6 205 21.8	2.5 1.2 2.1	4.5 3.0 3.8
•	Standard deviation	0.910	0.692	4.54	1.17	1.62	, 0.740	15.2	17.7	3.69	0.872	0.350	0.440
	Range limit (±)* 'Approximate	0.5	1.0	2.5	1.0	1.0	1.0	7.5	7.5	1.5	1.0	0.1	0.2
	probability, %	42	85	42	60	46	82	38	32	32	75	23	35
	Range limit (±)* Approximate	1.0	2.0	5.0	1.5	1.5	1.5	15.0	15.0	3.0	2.0	0.2	0.4
1	probability, %	73	99	73	80	65	96	68	60	58	98	43	64
	Range limit $(\pm)^*$ Approximate	2.0-		7.5	30	3.0	3.0	30.0	30.0	5.0'	3.0	0.3	0.6
	probability, %	97	—	91	99	84	99	95	91	82	99	61	83

\* Range limits were arbitrarily selected.

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM Mill X

					1			,	Roll Ave	rages			۰.					
	•	-	Date	Basis Weight, Ib. (12 x 12	Caliper, 0 001	Appar- ent Density,		Bursting	G.E. Punc-	Comp	ehle ression, lb.	- T.	endorf. ear, sheet		thor		ithor ich, %	ی میں اور
		Roll	Manuf.	/1000)	in.	lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	[n	Across	In	Across	In	Across	
		1 . 2 3	3-14-45 3-14-45 3-13-45	26.3 • 27 1 26.0	9.3 9.5 9.2	33.9 34.2 33.9	5.5 6.7 5.1	64 67 71	18 19 18	17.8 18.1 18.1	13.8 12.9 13.4	231 236 221	253 261 242	51.8 51.9 53.9	23.6 23.0 23.3	2.0 1.9 2.0	4.2 4.2 4.5	
		4 5		26.4 27.4	9_3 10_7	34.1 30.7	5.3- 7.8	70 66	<u>1</u> 9 21	18.7- 17.7	13:8 12.6	219- 249	246 298	56:7* 54.8	23.8 22.4	2.2-	4.8	· · · ·
		6 7	11-27-44 3-13-45-		10 7 9.1	30.6 	9.0 _8.6	68 68	21 20	17.5 17.2	12.4 . 13.9		290 - 265	55.2 - 48.5-	22.5 29.6-	1.9 - 2.3	4.4 -4.9	
-	-		- 3-30-45 3-30-45 10-15-44	29.1 28.1 27.7	10.1 9.9 10.0	34.6 34.1 33 2	9.1 8.2 12 0	63 68 67	24 23 21	15.7 16.2 14.7	14.1 13.9 10.8	302 289 256	320 - 310 300	$40.6 \\ 45.8 \\ 50.5$	30-1 29.3 25.5	$2.0 \\ 2.2 \\ 2.2 \\ 2.2$	2.4 2.9 4.7	·
		- 11 12 13 14	9-12-44 9-15-44 9-20-44 6-27-44	27.8 28.1 28.5 26.7	0.8 10.0 9.5 9.9	34.0 33.7 36.0	11.2 11.0 11.2	- 64 75 70 68	20 · 22 21 22	17.4 16.8 18.8	13.5 12.4 13.9	261 250 250	295 297 288	$56.2 \\ 56.4 \\ 58.1 \\ 40.1$	25.0 25.3 24.9	2.1 2.2 2.1	5.4 3.8 5.4 3.7	
, ,	•		0-27-44 Average	20.7	9.9 9.8	32.4· 33.7	11.1 8.7	68	,27 21	15.3 17.1	12.2 13.1	245 250	266. 281	49.1 52.1	25.3 25.3	2.0 2.1	3.7 4.3	
								· .										L

TABLE LVI

STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB: FOURDRINIER KRAFT CORRUGATING MEDIUM

									•			
· · · ·	-				MIL	L X						
1	Basis Weight, Ib. (12 x 12	Caliper.	Bursting	G.E. Puncture,	Comp	iehle pression, b.	Т	endorf ear, sheet		r Tensile, )./in.		r Stretch, %
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	 In	Across
Test values	• /		-									
Maximum	29.1	10.7	75	24	18.8	14.1	302	320	58.1	30.1	2.3	5.4
` Minimum	26.0	9.1	63	18	14.7	10.8	219	242	40.6	22.4	1.9	2.4
Average	27.4	9.8	68	21	17.1	13.1	250	281	52.1	25.3	2.1	4.3
<ul> <li>Standard deviation</li> </ul>	0.881	0.507	3.14	1.78	1 25	0.941	22.9	24.8	4.88	2.61	0.133	0.851
Range limit (±)* Approximate	0.5	1.0	2.5	1.0	1.0	1.0	7.5	7.5	1.5	1.0	0.1	0.2
probability, %	43	95	58	42	58	71	26	· 24	24	30	55	19
Range limit $(\pm)^*$ Approximate	1.0	2.0	5.0	1.5	.1.5	1.5	15 0	15.0	3.0	2.0	0.2	0.4
probability, %	75	100	89	60	77	89	49	45	46	56	87	36
Range limit (±)* Approximate	2.0	—	7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0.3	0.6
probability, %	98	—	98	91	98	99	81 •	77	69	75	98	52
* D 11 1.	1 * .		1									

\* Range limits were arbitrarily selected.

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# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

MILL Y Roll Averages

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	-			Caliper,		Mois-	Bursting		Comp	ehle ression, b.	- T	endorf ear, sheet	Tei	ithor nsile, /in.		nthor tch, %	<i>.</i>
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Roll	-		-					In	Across	In	Across	In	Across	In	Across	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1	3-12-45	25.4	9.1	33.5	7.2	48	15	18.5	11.0	186	205	45.4	19.5	1.9	3.8	•
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2	10-14-44	25.7	8.9	34.6	8.9	70	13	24.2	15.1	161	188	59.0	27.4	2.3	3.1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3	3-12-45	25.3	9.1	33.4	6.8	48	14	17.0	12.2	183	185	46.3	19.9	2.1	3.1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	. 3-10-45 _		9.5.	. 32.8	11.7	72	17.	. 16.9	13.7	. 194	243	55.4	22.3	2.2	3.7	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	3-10-45	26.8	9.8	32.8	7.3	73	18	18.7	' 13.7	206	238	55.5	21.1	1.9	4.6	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6	3-10-45	27.0	9.8	33.1	10.5	65	18	16.8	13.1	238	270	54.0	26.6	2.1	3.7	
9       3-12-45       26 1       9.2       34.0       11.1       51       13       16.0       11.9       180       219       49.0       22.1       1.9       3.3         10       3-12-45       24 9       9.5       31.5       10.1       48       13       14.3       10.0       182       214       45.9       20.2       1.8       3.0	7	3-12-45	26.1	9.4	33.3	10.8	47	14	15.7	11.3	183	206	46.6	19.4	2.0	3.9	
10  3-12-45  24  9  9.5  31.5  10.1  48  13  14.3  10.0  182  214  45.9  20.2  1.8  3.0  -	8	3-12-45	27.1	8.2	39.6	12.5	55	13 -	14.9	10.6	176	220 -	49.6	22 4	2.1	3.8	
10 3-12-45 24 9 9.5 31.5 10.1 48 13 14.3 10.0 182 214 45.9 20.2 1.8 3.0	9	3-12-45	26 1	9.2	34.0	11.1	51	13	16.0	11.9	180	219	49.0	22.1	1.9	3.3	
Average 26.0 9.3 33.9 9.7 58 15 17.3 12.3 189 219 50.7 22.1 2.0 3.6	10	3-12-45				10.1	48	13	14.3	10.0	182	214	45.9	20.2	1.8	3.0	-
	2	Average	26.0	9.3	33.9	9.7	58	15	17.3	12.3	189	219	50.7	22.1	2.0	3.6	

TABLE LVIII STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM MILL Y

					MILL	L 1						
	Basis Weight, lb. (12 x 12	Caliper,	Bursting Strength,	G.E. Puncture.	Comp	ehle ression, lb.	Т	endorf <sup>.</sup> ear, sheet		Tensile, ./in.		Stretch,
	/1000)	0.001 in.	points	units	In	Across	In	Across	In	Across	In	Across
Test values Maximum Minimum Average Standard deviation Range limit $(\pm)^*$	27.1 24.9 26.0 0.746 0.5	9.8 8.2 9.3 0.474 1 0	73 47 58 11.0 2.5	18 13 15 2.10 1.0	24.2 14.3 17.3 2.80 1.0	15.1 10.0 12.3 1.61 1.0	238 161 189 20 8 7.5	270 185 219 25.9 7.5	59.0 45.4 50.7 4.90 1.5	27,4 19:4 22.1 2.83 1.0	2,3 1,8 2,0 0,157 0,1	4.6 3.0 3.6 0.488 0.2
Approximate probability, %	50	97	18	37	28	46	28	23	24	27	48	32
Range limit (±)* Approximate probability, %	1.0 82	2.0 99	5.0 35	1.5 52	1.5 41	1.5 64	15.0 53	15.0 44	3.0 46	2.0 52	0.2 80	0.4 59
Range limit $(\pm)^*$ Approximate	2.0	—	7.5	3.0	3.0	3.0	30.0	30.0	5.0	3.0	0.3	0.6
probability, %	99	_	50	83	72	94	85	75 .	69	71	94	78

\* Range limits were arbitrarily selected.

# TABLE LIX

1. B. B.

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

# M1LL Z Roll Averages

					• •											
• ••			Caliper,	Appar- ent	Mois-		G.E. Punc-	Comp	chle - ression, lb.	Т	endorf ear, /sheet	Ter	thor · isile, ./in.	• An	nthor tch, %	
Roll	Date Manuf.	(12 x 12 <sup>.</sup> /1000)	0.001 in.	Density, lb./cu.ft.	ture, %	Strength, points	ture, units	In	Across	In	Across	In	Across	 In	Across	
1	7-21-44	26.5	9.2	34.6	84	70	19	20.2	16.9	265	248	50.5	33.7	1.9	5.0	
2	8-12-43	27 3	8.9	36.8	7.8	78	19	21.4	15.8	256	269	54 5	35 7	2.0	4.0	
3	5-11-43	27.4	10.2	32.2	8.7	65	22	17.1	14.2	283	316	50.8	26.1		3.1	
 4-	10-30-44	27.9	9.5	35.2 -	9-1-		21	21.0	15.4	257	- 295	59.5	33.0	2.0	5.1	
5	2-26-45	26.5	9.3	34 2	75	73	20	21.3	17.6	252	243	+ 55.5	34.5	2.1	4.8	
6	2-26-45	26.5	9.1	. 34.9	9.5	77	19	20.8	17.7	244	236	53.4	35.8	2.3	5.3	
+ 7	2-26-45	26.4	9.0	_ 35.2	9.1_		. 19	- 20.9	16.2	226	·247 ·	- 578	- 31.1	2.1	4.9	-
 8	2-26-45	26 4	9.0	35.2	9,9	75	19	20.1	15.0	231	254	55.9	33.6	2.0	5.4	
. 9	2-26-45	. 26.6	9,0	35.5	10.9	78	19 -	20.8	15.4	231	- 241	57 1°	32.4	1.9	- 4.9 · ·	
10	7-21-44	26.6	9.4	33.9	8.6	74	19	18.5	15.0	257	268	49.4	33.8	1.9	4.4	
11	7-21-44	26.3	9.4	33.6	10.8	73	20	17.2	14.2	262	260	47.3	33.1	2.1	4.8	
А	verage	26.8	9.3	34.7	9.1	75	20	19.9	15.8	251	262	53.8	33.0	<sup>1</sup> 2.0	4.7	

TABLE LX

STATISTICAL EVALUATION OF PHYSICAL TESTS ON .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

Mr		~ <b>/</b>
-1211	ᇿ	6

	Basis Weight, Ib. (12 x 12	Caliper,	Bursting Strength,	G.E. Puncture,	Comp	ehle ression, b.	Te	endorf ear, sheet		Tensile, /in.	Amthor Stretch,		
	/1000)	0.001 in.	points	units	· In	Across	In	Across	In	Across	 In	Across	
Test values Maximum Minimum	27.9 26.3	10.2 8.9	85 65	22 19	21.4 17.1	17.7 14.2	283 226	316 236	59.5 47.3	35.8 26.1	2.3	$5.4 \\ 3.1$	
Average Standard deviation	26.8	9.3	75	20 1.03	19.9 1.59	15.8 1.22	251	262	53.8	33.0	2.0 0.155	4.7 0.659	
Range limit $(\pm)^*$	$0.522 \\ 0.5$	0.366 1.0	5.21 2.5	1.03	1.0	1.0	17.1 7.5	$\begin{array}{r} 24.6 \\ 7.5 \end{array}$	3.86 1.5	$\begin{array}{c} 2.65 \\ 1.0 \end{array}$	0.155	0.059	
probability, %	66	99	37	67	47	59	34	24	30	30	48	24	
Range limit (±)* Approximate	1.0	2.0	5.0	1.5	1,5	1.5	15,0	15.0	30	2.0	0.2	0.4	
probability, %	95	100	66	86	65	78	62	46	56	55	80	46	
Range limit (±)* Approximate	2.0		7.5	3.0	3,0	3.0 '	30.0	30,0	5.0	3.0	0.3	0.6	
probability, %	99	—	,85	99	94	99	92	78	81	74	95	64	

\* Range limits were arbitrarily selected.

tion and 82% in the across-machine direction. A range limit of  $\pm 1.5$  pounds should include 65% in the inmachine direction and 96% in the across-machine direction, and a range limit of  $\pm 3.0$  pounds should include 84 and 99%, respectively. Elmendorf tear and Amthor tensile and stretch exhibited rather largestandard deviations, signifying that considerable variation should be expected.

# Mill X

--The average-test results obtained on samples of the kraft corrugating medium made by Mill X are presented in Table LV (see also Table LXXVI of the Appendix). It may be observed that the average basis weight was 27.4 pounds. The average caliper was 0.0098 inch and the average apparent density was 33.7 pounds per cubic foot. The average bursting strength was 68 points and the average moisture 8.7% on an ovendry basis. The average Riehle compression values in the in- and across-machine directions were 17.1 and 13.1 pounds, respectively.

The statistical evaluation of these results is given in Table LVI. On the basis of a standard deviation of 0.881 for basis weight, it should be expected that 43%of the rolls should fall within a range limit of  $\pm 0.5$ pound (26.9 to 27.9 pounds), 75% within a range limit of  $\pm 1.0$  pound (26.4 to 28.4 pounds), and 98% within a range limit of  $\pm 2.0$  pounds (25.4 to 29.4 pounds). With a standard deviation for caliper of 0.507, approximately 95% of the rolls should fall within a range limit of  $\pm 0.001$  inch (0.0088 to 0.0108 inch). Approximately 58% of the rolls should fall within a bursting strength range limit of  $\pm 2.5$  points (65.5 to 70.5 points), 89% within a range limit of  $\pm 5.0$  points (63.0 to 73.0 points), and 98% within a range limit of  $\pm 7.5$ points (60.5 to 75.5 points). The standard deviation for the Riehle compression in the in-machine direction indicates that 58, 77, and 98% of the rolls should fall within range limits of  $\pm 1.0$ ,  $\pm 1.5$ , and  $\pm 3.0$  pounds. respectively. For the across-machine direction, approximately 71, 89, and 99% of the rolls should fall within range limits of  $\pm 1.0$ ,  $\pm 1.5$ , and  $\pm 3.0$  pounds, respectively:

The statistical evaluation of the Elmendorf tear, Amthor tensile and stretch, and G. E. puncture indicates that, on the average, approximately 50% of the rolls should fall within the second arbitrarily selected range limit for each test.

## Mill Y

The average results obtained on samples of the kraft corrugating medium made by Mill Y are given in Table LVII (see also Table LXXVII of the Appendix). The average basis weight was 26.0 pounds, the average caliper 0.0093 inch, and the average apparent density was 33.9 pounds per cubic foot. The average bursting strength was 58 points, and the average Riehle compression values in the in- and across-machine directions, were 17.3 and 12.3 pounds, respectively. The average moisture content was 9.7% on an ovendry basis. within a range limit of  $\pm 2.5$  points (72.5 to 77.5 points), 66% within a range limit of  $\pm 5.0$  points (70.0 to 80.0 points), and 85% within a range limit of  $\pm 7.5$ points (67.5 to 82.5 points). The standard deviations for the Riehle compression values in the in- and acrossmachine directions, were 17.3 and 12.3 pounds, respectively. The average moisture content was 9.7% on an ovendry basis.

The statistical evaluation of these results is found in Table LVIII. On the basis of the standard deviation,

it should be expected that 50% of the rolls made in this grade by Mill Y should fall within a basis weight range limit of  $\pm 0.5$  pound (25.5 to 26.5 pounds), 82%within a range limit of  $\pm 1.0$  pound (25.0 to 27.0 pounds), and 99% within a range limit of  $\pm 2.0$  pounds (24.0 to 28.0 pounds). Approximately-97% of the rollsshould fall within a caliper range limit of  $\pm 0.001$ , inch (0.0083 to 0.0103 inch). The standard deviation for the bursting strength was 11.0, which indicates that only 18% of the rolls should be expected to fall within a range limit of  $\pm 2.5$  points (55.5 to 60.5 points), 35%within a range limit of ±5.0 points (53.0 to 63.0 points), and 50% within a range limit of  $\pm 7.5$  points (50.5 to 65.5 points). The standard deviations for the Riehle compression in the in- and across-machine directions indicate that 28 and 46%, respectively, should fall within the range limit of  $\pm 1.0$  pound, 41 and 64% within the range limit of  $\pm 1.5$  pounds, and 72 and 94% within the range limit of  $\pm 3.0$  pounds. The standard deviations for Elmendorf tear, G E. puncture, and Amthor tensile and stretch indicate considerable nonuniformity of these characteristics in the .009/26-lb. kraft corrugating medium.

## Mill Z

The average test results obtained on samples of the kraft corrugating medium made by Mill Z are given in Table LIX (see also Table LXXVIII of the Appendix). The average basis weight was 26.8 pounds, the average caliper 0.0093 inch, and the average apparent density 34.7 pounds per cubic foot. The average moisture content was 9.1% on an ovendry basis. The average bursting strength was 75 points and the average Riehle compression values for the in- and acrossmachine directions were 19.9 and 15.8 pounds, respectively. It should be noted that Rolls Z-2 and Z-3 were made approximately the middle of 1943 and thus were substantially older than the others; however, the average results obtained for these rolls do not vary markedly from the average of the values for the other rolls.

The statistical evaluation of these results is presented in Table LX. The magnitude of the standard deviation for the basis weight indicates that 66% of the rolls should fall within the range limit of  $\pm 0.5$ pound (26.3 to 27.3 pounds), 95% within the range limit of  $\pm 1.0$  pound (25.8 to 27.8 pounds), and 99% within a range limit of  $\pm 2.0$  pounds (24.8 to 28.8 pounds). Approximately 99% of the rolls should fall within a caliper range limit of  $\pm 0.001$  inch (0.0083 to 0.0103 inch). The standard deviation of the bursting strength indicates that 37% of the rolls should fall within a range limit of  $\pm 2.5$  points (72.5 to 77.5 points), 66% within a range limit of  $\pm 5.0$  points (70.0 to 80.0 points), and 85% within a range limit of  $\pm 7.5$ points (67.5 to 82.5 points). The standard deviations for the Riehle compression values in the in- and acrossmachine directions indicate that 47 and 59% of the rolls, respectively, should fall within a range limit of  $\pm 1.0$  pound, 65 and 78% within a range limit of  $\pm 1.5$ rounds. The standard deviations for Elmendorf tear, G. E. puncture, and Amthor tensile and stretch indicate the respective uniformities of these characteristics.

SUMMARY

The results presented in this part of the baseline study are concerned with the problem of sampling, in a truly impartial cross-sectional manner, the current routine production of the co-operating mills and evaluating-these samples as completely as possible by means of existing board testing methods.

The second phase of the baseline study involved (1) the selection of the most representative rolls of each mill's sampled production, and (2) the fabrication of these representative rolls into corrugated combined boards and their conversion into boxes.

Because the first part of the baseline study was concerned only with the sampling and evaluation of the component parts, no conclusions regarding the relationship between the quality of component parts and the performance of combined board and boxes fabricated from these components can be made at this time.

However, the results of this phase of the study indicate that the average quality of the sampled 42-lb. D.F.B.S. Fourdrinier kraft liner and of the .009/ 26-lb. kraft and bogus corrugating mediums were as follows:

	Liner	Corrugating Medium
Basis weight, lb./1000 sq. ft.	42.1	26.8
Caliper, in.	0.015	0.010
Apparent density, lb./cu. ft.	33.7	32.3
Bursting strength, points	98	62
G. E. puncture, units	36	18
Moisture, %	8.1	9.4
Riehle compression, lb.		
In	29.0	. 17.6
Across	22.5	13.0

	Liner	Corrugating Medium
Elmendorf tear, g./sheet		
In	354	223
Across	394	251
Amthor tensile, lb./in.		
In	77.8	— 495°
Across	37.8	24.8
Amthor stretch, %		
In	2.1	1.9
Across	3.7	4.3

It should be remembered that these data are based on the actual rolls sampled and on conventional test methods.

For those tests in which orientation of the specimen is specified, the approximate ratios observed in the inmachine direction and in the across-machine direction were as follows:

	Ratio
<b>-</b> .	In:Across
Riehle compression	4:3
Elmendorf tear	0.9:1
Amthor tensile	2:1
Amthor stretch	1:2

The ratio of the bursting strength to the G. E. puncture on 42-lb. D.F.B.S. Fourdrinier kraft liner was of the order of 2.7:1.

The ratio was not computed for the .009/26-lb. corrugating medium since the relatively high capacity of the G. E. puncture tester did not allow sufficient subdivision of the scale to permit distinguishing between the low values obtained with any degree of accuracy.

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APPENDIX'

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# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER

# Mill A

| •<br>• ••••                                                    |                            |                                      | *                                         |                                      |                                        |                                      |                                             |                                              |                                     |                                   | <b>.</b>                                       |                                        |                                                                                              | - 4,                       | +                          |                                  |                        | Com                                  |                                      | • • •- | • • |
|----------------------------------------------------------------|----------------------------|--------------------------------------|-------------------------------------------|--------------------------------------|----------------------------------------|--------------------------------------|---------------------------------------------|----------------------------------------------|-------------------------------------|-----------------------------------|------------------------------------------------|----------------------------------------|----------------------------------------------------------------------------------------------|----------------------------|----------------------------|----------------------------------|------------------------|--------------------------------------|--------------------------------------|--------|-----|
|                                                                |                            |                                      | Weigh                                     |                                      | ~ •                                    |                                      |                                             |                                              |                                     | _                                 | ~                                              |                                        | ursting                                                                                      | G.E.                       | Punct                      |                                  | s                      | ion, lb                              | ·                                    |        |     |
| Institute                                                      |                            | (12                                  | x 12/10                                   | 000)                                 | Cali                                   | per, 0 (                             | 001 in.                                     | Apparent<br>- Density,                       |                                     | oisture                           | , %                                            | Stren                                  | igth, points                                                                                 |                            | units                      |                                  |                        | In                                   |                                      | 1      |     |
| File No.                                                       | Roll                       | Max.                                 | Min.                                      | Αν.                                  | Max.                                   | Min.                                 | Av.                                         | ib./cu.ft.                                   |                                     | Min.                              | Av.                                            | Max.                                   | Min. Av.                                                                                     | Max.                       | Min.                       | Av.                              | Max.                   | Min.                                 | · Av.                                |        |     |
| 116372/74<br>116375/77<br>116389/91                            | 1<br>2<br>3 -              | 42 5<br>43.2<br>41.1~                |                                           | 42.1<br>42.8<br>-40.9                | 15.3                                   | 14.2                                 | 14.9<br>14.8<br>-14.2                       | 33.8<br>34.7<br>34.6                         | 9.3<br>7.8<br>- 9 8-                | 65<br>7.3<br>_9.4                 | 8.3<br>7.6<br>9.7                              | 126<br>121<br>129_                     | 72 94<br>79 99<br>79 _109                                                                    | 44<br>41<br>36             | 35<br>35<br>31             | 39<br>38<br>34                   |                        | 22.0<br>22.0<br>24.0                 | 25.7<br>27.0<br>-29.0-               |        |     |
| 116392/94<br>116402/04                                         | 4<br>5                     | 41.2<br>42.3                         | $\begin{array}{c} 40.7\\ 42.0\end{array}$ | 41.0<br>42.1                         | 14.6<br>14.9                           |                                      | $\begin{array}{c} 14.1 \\ 14.3 \end{array}$ | 34.8<br>35.3                                 | $\frac{9.3}{13.7}$                  | 92<br>12,7                        | 92<br>13.2                                     | 126<br>132                             | $\begin{array}{ccc} 90 & 110 \\ 84 & 107 \end{array}$                                        | 37<br>37                   | 32<br>33                   | 35<br>36                         | 31.0                   | $25.5 \\ 21.0$                       | 28.5<br>25.8                         |        | ,   |
| 116405/07<br>116408/10<br>116444/46<br>116447/49<br>116916/18  | 6<br>7<br>8<br>9<br>10     | 42.6<br>40.4<br>39.4<br>38.6<br>41.8 | 41.7<br>39.8<br>39.0<br>38.5<br>41 0      | 42,1<br>40.1<br>39.2<br>38 5<br>41.4 | 15 7<br>14.9<br>15.6<br>15.1<br>15.4   | 14.6<br>14.0<br>14 1<br>13.8<br>9.7  | 14.5<br>14.6<br>14.5                        | 33.4<br>33.2<br>32.2<br>31.8<br>33.5         | 11.2<br>11.9<br>9.1<br>8.2<br>8.0   | 10.4<br>11.4<br>7.9<br>7.6<br>7 5 | 10.7<br>11.7 <sup>7</sup><br>8.4<br>7.9<br>7.8 | 132<br>129<br>116<br>117<br>113        | 80 111<br>86 103<br>84 99<br>78 90<br>68 95                                                  | 39<br>37<br>               | 33<br>32<br>31<br>28<br>30 | 37<br>34<br>33<br>31<br>36       | -33.5<br>28.5<br>31.0  | 24.5<br>27.0<br>22.0<br>22.5<br>23.5 | 29.2<br>29.0<br>25.9<br>27.5<br>27.5 |        |     |
| 116919/21<br>116922/24<br>116925/27<br>117066/68<br>117069/71  | 11<br>12<br>13<br>14<br>15 | 42.1<br>41.6<br>41.8<br>41.2<br>41.6 | 40.8<br>40.8<br>40.2<br>40.4<br>41.1      | 41.4<br>41.1<br>41.2<br>40.7<br>41.3 | 16.1<br>16.0<br>15.8<br>15.7<br>15.9   | 15.0<br>14 7<br>14.6<br>14.4<br>14.4 | 15.3<br>15.3<br>15.1                        | 32.0<br>32.2<br>32.3<br>32.3<br>32.3<br>32.6 | 7.4<br>6.9<br>75<br>11.7<br>12.8    | 7.0<br>5.5<br>6.8<br>10.8<br>11.5 | 7.2<br>6.3<br>7.0<br>11.3<br>12.0              | 122<br>119<br>126<br>123<br>119        | 63       92         62       88         65       93         67       98         90       104 | 40<br>37<br>40<br>38<br>39 | 30<br>32<br>32<br>33<br>35 | 35<br>35<br>37<br>35<br>37       | 32.0<br>33.0<br>37.0   | 25.5<br>24.5<br>25.0<br>26.5<br>25 5 | 28 8<br>28.1<br>27.6<br>31.6<br>31.6 |        |     |
| 117075/77<br>117078/80<br>117140/42<br>117143/45<br>117146/48  | 16<br>17<br>18<br>19<br>20 | 40.7<br>40.1<br>42.2<br>41.6<br>42.0 | 39 4<br>38.2<br>41.7<br>40.5<br>40.8      | 40.0<br>39.1<br>41.9<br>41.2<br>41.6 | **15.2<br>15.1<br>16.0<br>15.7<br>15.9 | 13.7<br>14.9                         |                                             | 32.8<br>32.5<br>32 8<br>32.9<br>33.5         | 12.2<br>12 2<br>9.9<br>10.9<br>10.3 | 11.3<br>9.5<br>8.5<br>6 7<br>8.9  | 11.8<br>10.6<br>9.1<br>8.8<br>9.6              | 117<br>119<br>122<br>122<br>121        | 69 96<br>69 88<br>83 104<br>74 104<br>79 99                                                  | 35<br>36<br>36<br>34<br>35 | 31<br>29<br>30<br>29<br>30 | 33<br>32<br>34<br>32<br>32<br>32 | $35.0 \\ 34.5 \\ 33.0$ | 27.5<br>26.0<br>26.5<br>24.5<br>26.0 | 31.5<br>30.0<br>29.8<br>28.4<br>31.2 | ,      |     |
| 117149/51<br>117290/92<br>117293/95<br>117296/98<br>117299/301 | 21<br>22<br>23<br>24<br>25 | 41:3<br>42.7<br>40.8<br>43.5<br>40.7 | 41.0<br>42.6<br>39.9<br>43.0<br>40 3      | 41.2<br>42 7<br>40.4<br>43.3<br>40.6 | 15.2<br>15.3<br>15.4<br>15.8<br>15.3   | 13.9<br>14.5                         | 14.9<br>14.8<br>15.1                        | 33.4<br>34.3<br>32.7<br>34.4<br>32.4         | 8.7<br>11.0<br>9.5<br>10 6<br>9.0   | 7.8<br>8.4<br>5.3<br>9.3<br>8 5   | 8.1'<br>9.9<br>7.9<br>10.1<br>8.7              | 124<br>122<br>121<br>121<br>121<br>120 | 80 101<br>80 100<br>69 95<br>74 98<br>67 94                                                  | 34<br>38<br>38<br>40<br>37 | 28<br>32<br>30<br>35<br>32 | 32<br>36<br>33<br>37<br>34       | 30.0.<br>34.0<br>30.0  | 26.0<br>25.0<br>26.0<br>25.0<br>24.0 | 29.2<br>27.6<br>29.4<br>27.7<br>27.1 |        |     |
| 117302/04<br>117741/43<br>117744/46                            | 26<br>27<br>·28            | 42.4<br>41.2<br>40.1                 | 41.6<br>40.0<br>40.0                      |                                      |                                        |                                      | 15.3<br>14.8<br>14.6                        | 32.9<br>32.8<br>32.8                         | 9:0<br>8.3<br>7,1                   | 7.5<br>7.1<br>4.3                 | 8.4<br>7.6<br>6.0                              | 134<br>112<br>125                      | 73 103<br>80 95<br>73 99                                                                     | · 39<br>36<br>35           | 33<br>30<br>30-            | 37<br>33<br>33                   | 30.0                   | 24.5<br>260<br>23.5                  | 28.8<br>28.2<br>27.5                 |        |     |
| Average                                                        | *                          |                                      |                                           | 41.1                                 |                                        |                                      | 14.8                                        | 33.2                                         |                                     |                                   | 9.1                                            |                                        | 99                                                                                           |                            | i.                         | 35                               |                        |                                      | 28.5                                 |        |     |

TABLE LXII

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER

Mill B

|                                                               |                            | Basic                                                                 | s Weigl                                                             | ht lb '                                                             |                                        | •                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |                                       |                                      |                                     |                                  |                                  | в                               | urstin                     | <i>a</i>                       | C F                        | Punct                      |                             |                                       | le Com<br>sion, lb                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                        |
|---------------------------------------------------------------|----------------------------|-----------------------------------------------------------------------|---------------------------------------------------------------------|---------------------------------------------------------------------|----------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------|--------------------------------------|-------------------------------------|----------------------------------|----------------------------------|---------------------------------|----------------------------|--------------------------------|----------------------------|----------------------------|-----------------------------|---------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------|
| Institute                                                     |                            |                                                                       | x 12/10                                                             |                                                                     | Calip                                  | er, 0.0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 01 in.                                |                                      | Mo                                  | oisture,                         | %                                |                                 | gth, p                     |                                |                            | units                      | uie,                        |                                       | In                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                        |
| File No.                                                      | Roll                       | Max.                                                                  | Min.                                                                | Av.                                                                 | Max.                                   | Min.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | Av.                                   | Density,<br>lb./cu.ft.               | Max.                                | Min.                             | Av.                              | Max.                            | Min.                       | Av.                            | Max.                       | Min.                       | Av.                         | Max.                                  | Min.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | Av.                                    |
| 116426/28<br>116429/31<br>116432/34<br>116726/28<br>116729/31 | 1<br>2<br>3<br>4<br>5      | $\begin{array}{r} 43 \ 2 \\ 44.8 \\ 44.4 \\ 43.3 \\ 41.3 \end{array}$ | $\begin{array}{r} 41.4 \\ 44.6 \\ 43.6 \\ 42.6 \\ 40.8 \end{array}$ | 42.2<br>44.7<br>44.1<br>42.9<br>41.1                                | 16.3<br>16.5<br>16.0<br>14.0<br>14.1   | 14.9<br>15.4<br>14.8<br>12.5<br>13.4                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 15.7<br>15.9<br>15.5<br>13.5<br>13.8  | 32.2<br>33.7<br>34.1<br>38.1<br>35.6 | 9.5<br>8.8<br>9.3<br>8 2<br>8.7     | 8.6<br>8.1<br>8.2<br>8.2<br>8.1  | 9.0<br>8.4<br>8.9<br>8.2<br>8.4  | 117<br>124<br>126<br>128<br>119 | 78<br>67<br>88<br>78<br>70 | 101<br>106<br>105<br>102<br>92 | 37<br>42<br>38<br>40<br>40 | 32<br>36<br>34<br>35<br>32 | 34<br>39<br>36<br>37<br>35  | 35.0<br>34.0<br>33.5<br>36.0<br>33.5  | 25.0<br>28.0<br>25 0<br>28 0<br>23.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 29.7<br>30.2<br>28.7<br>31.3<br>27.5   |
| 116735/37<br>116949/51<br>116952/54<br>116955/57<br>117753/55 | 6<br>7<br>8<br>9<br>10     | 43.0<br>42.3<br>42.6<br>44.0<br>45.7                                  | 41.7<br>41 4<br>41.6<br>40.6<br>44.0                                | 42.4<br>42.0<br>42.2<br>42.7<br>45.0                                | 16.4<br>16.5<br>15.9<br>16.7<br>16.8   | 15.5<br>15.1<br>14.6<br>14.8<br>15.8                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 16.0<br>15.7<br>15.3<br>15.9<br>16.4  | 31.8<br>32.0<br>33.0<br>32 2<br>32.9 | 9.7<br>7.1<br>6.9<br>7.7<br>11.3    | 9.3<br>6.3<br>5.1<br>5.8<br>10.2 | 9.6<br>6.8<br>6.0<br>6.8<br>10.8 | 130<br>112<br>120<br>110<br>119 | 72<br>71<br>76<br>66<br>84 | 104<br>94<br>96<br>91<br>104   | 40<br>37<br>37<br>42<br>42 | 32<br>30<br>32<br>35<br>37 | 37<br>34<br>35<br>39<br>40- | 37.0<br>38.0<br>37.5<br>32 5<br>33 5  | $26.5 \\ 30.0 \\ 28.0 \\ 26.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 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\\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ 28.0 \\ $ | $30.0 \\ 34.0 \\ 33.9 \\ 29.3 \\ 31.1$ |
| 117756/58<br>117759/61<br>117762/64<br>117765/67<br>117768/70 | 11<br>12<br>13<br>14<br>15 | 43.6<br>45.2<br>43.2<br>44.0<br>46.1                                  | 42.0<br>44.8<br>42.4<br>42.8<br>45.1                                | $\begin{array}{r} 42.7 \\ 45.0 \\ 42.8 \\ 43.5 \\ 45.7 \end{array}$ | $16.5 \\ 16.8 \\ 16.0 \\ 16.2 \\ 16.4$ | 15.0<br>15.7<br>15.0<br>15.0<br>14.7                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 15.9<br>16.2<br>15.6<br>15.7<br>15.6  | 32.2<br>33.3<br>32.9<br>33.2<br>35.2 | 10.2<br>10.3<br>11.4<br>10.3<br>8.9 | 9.3<br>9,2<br>10.9<br>9.2<br>7.7 | 9.7<br>9.7<br>11.1<br>9.7<br>8.1 | 109<br>119<br>120<br>120<br>138 | 87                         | 91<br>103<br>103<br>106<br>112 | 40<br>44<br>47<br>42<br>41 | 34<br>38<br>35<br>35<br>37 | 37<br>40<br>38<br>39<br>40  | 34.0<br>.34.5<br>37.5<br>39.0<br>36.5 | 25.0<br>27.5<br>27.5<br>32.0<br>29.0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 29.1<br>31.6<br>32.3<br>35.2<br>32.0   |
| 118017/19<br>118020/22<br>118023/25<br>118026/28<br>118029/31 | 16<br>17<br>18<br>19<br>20 | 41.9<br>43.4<br>43.0<br>43.1<br>41.7                                  | 41.8<br>41.5<br>41.2<br>42.4<br>41.1                                | 41.8<br>42.3<br>42.3<br>42.7<br>41.3                                | 15.2.<br>15.5<br>17.0<br>15.5<br>15.3  | $14.0 \\ 14.5 \\ 15.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ 14.8 \\ $ | 14'.8<br>15.0<br>16.4<br>15.1<br>15.0 | 33.9<br>33.8<br>31.0<br>33.9<br>33.0 | 9.3<br>10.3<br>8.5<br>8.3<br>8.3    | 8.9<br>8.9<br>7.6<br>7.3<br>7.6  | 9.1<br>9.6<br>8.0<br>7.7<br>8.0  | 144<br>132<br>108<br>134<br>108 | 67<br>88<br>74<br>94<br>71 | 101<br>108<br>93<br>111<br>95  | 39<br>41<br>41<br>39<br>37 | 33<br>33<br>35<br>33<br>32 | 36<br>37<br>37<br>36<br>35  | 31.5<br>335<br>330<br>35.5<br>32.0    | 22.0<br>24.5<br>24.0<br>25 5<br>25.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 27.9<br>30.3<br>29.4<br>31.3<br>28.9   |
| 118032/34                                                     | 21                         | 41.2                                                                  | 41.1                                                                | 41.2                                                                | 15.0                                   | 14.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 14.9                                  | 33.2                                 | 9.0                                 | 7.2                              | 8.1 <sup>.</sup>                 | 124                             | 78                         | <u>98</u>                      | 38                         | 31                         | 34                          | 32.0                                  | 24.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 28.7                                   |
| Average                                                       |                            |                                                                       |                                                                     | 42.9                                                                |                                        |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 15.4                                  | 33.4                                 |                                     |                                  | 8.7'                             |                                 |                            | 101                            |                            |                            | 37                          |                                       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 30.6                                   |

# TABLE LXI ÷., .1

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

# MILL A

|            |                                      | le Com<br>sion, Ib                        |                                      | , F                                                                                                    | Elmen                               | dorf T                              | ear, g./                                                                    | sheèt                            |                                   | •<br>•-• <u>•</u> •                    | Am                                    | thor_T                               | ensile, lb.                         | /in                                    |                                      |                                    | . An                                  | 1thor S                                | Stretch.                        | - % -                            |                                               | -                          | ••• |
|------------|--------------------------------------|-------------------------------------------|--------------------------------------|--------------------------------------------------------------------------------------------------------|-------------------------------------|-------------------------------------|-----------------------------------------------------------------------------|----------------------------------|-----------------------------------|----------------------------------------|---------------------------------------|--------------------------------------|-------------------------------------|----------------------------------------|--------------------------------------|------------------------------------|---------------------------------------|----------------------------------------|---------------------------------|----------------------------------|-----------------------------------------------|----------------------------|-----|
|            | Across .                             |                                           |                                      | In                                                                                                     |                                     |                                     | Across                                                                      | _                                |                                   | . In                                   |                                       |                                      | Across                              |                                        |                                      | In                                 |                                       |                                        | Across                          | 3                                | •                                             |                            |     |
|            | Max.                                 | Mın.                                      | Av.                                  | Max.                                                                                                   | Min.                                | Av.                                 | Max.                                                                        | Min.                             | Av.                               | Max.                                   | Min.                                  | Av.                                  | Max.                                | Min.                                   | Av.                                  | Max                                | Min.                                  | Av.                                    | Max.                            | Min.                             | Av.                                           | Roll                       |     |
|            | 24.5<br>24.0<br>24 0                 | 17.0<br>15.0<br>17.0<br>-19.5<br>18.5     | 20.0                                 |                                                                                                        | 328<br>304<br>312<br>- 208 -<br>360 | 378<br>366<br>341<br>- 336 -<br>387 | 520<br>448                                                                  | 352<br>352<br>368<br>376-<br>384 | 401<br>414<br>406<br>412 -<br>415 | 91.4<br>93.1<br>91-4-                  | 71.1<br>67.7<br>76.2<br>76:2-<br>64.3 | 83.7<br>84.6                         | 43 7<br>41 0<br>40:8                | 31 8<br>31 3<br>29 0<br>-33-0-<br>31 3 | 38.8<br>35 9<br>• 37-,4              | 3.0<br>3.3                         |                                       | 2.2<br>2.7<br>-2.9-                    | 41<br>48                        | 2.2<br>2.1<br>1.9<br>-2-5<br>1.9 | $\begin{array}{c} 3 & 3 \\ 3 & 7 \end{array}$ | $-\frac{1}{2}$             |     |
| <b>~</b> - | 25.5<br>25.0<br>22.5<br>23.0         | 18.5                                      | 23.4<br>22.1<br>20.2<br>21.2<br>21.5 | $ \begin{array}{r}     432 \\     \underline{\cdot 400} \\     360 \\     392 \\     400 \end{array} $ | 304<br>288                          | 363<br>351<br>310<br>334<br>350     | 464                                                                         | 376<br>352                       | 417<br>396<br>370<br>366<br>398   | 96.5<br>                               | 62 6                                  | 85.9                                 | 42.7<br>- 43.2<br>- 41.6<br>- 39.1. | 31.8                                   |                                      | 2.9<br>2.9<br>2.2<br>· -2 6<br>2 4 | 1.3                                   | 2.4<br>2.5-<br>1.7<br>1.9<br>2.0       | 3.4                             | -2.3<br>1.6<br>2.0               | - 3 4<br>2 6<br>2.8                           | 6<br>7<br>8<br>9,<br>10    |     |
|            | 25 5                                 | 18.0<br>17.5<br>20.0                      | 22 3<br>21.5<br>22.0<br>22.9<br>22.3 | 464<br>392<br>432<br>400<br>424                                                                        | 320<br>272<br>304<br>312<br>320     | 384<br>349<br>377<br>355<br>357     | <ul> <li>448</li> <li>480</li> <li>480</li> <li>424</li> <li>448</li> </ul> | 352<br>336<br>344<br>336<br>336  | 407<br>398<br>418<br>382<br>394   | · 91.4<br>93.1<br>91.4<br>79.2<br>77.9 | 66.0<br>69 4<br>72.8<br>59.8<br>59.6  | 82.5<br>81.7<br>82.2<br>70.7<br>74.0 |                                     | 31.2<br>30.8<br>32.5<br>27.3<br>30.3   | 35.2<br>34.6<br>36.0<br>35.4<br>33.5 | $3.5 \\ 2.2$                       |                                       |                                        | 5.1<br>4.4<br>3.9<br>5.5<br>4 9 | $2.3 \\ 2.0 \\ 1.4$              |                                               | 11<br>12<br>13<br>14<br>15 |     |
|            | 23.5<br>25.0<br>28.5<br>27.0<br>25.0 | $\begin{array}{c} 21.5\\ 23.0\end{array}$ | 24.4                                 | 400<br>376<br>424<br>400<br>368                                                                        | 296<br>296<br>288<br>296<br>264     | 350<br>333<br>339<br>336<br>319     | 488<br>440<br>480<br>464<br>432                                             | 320<br>328<br>352<br>336<br>336  | 380<br>371<br>404<br>382<br>373   | 77.5<br>80.6<br>93.1<br>96.5<br>91.4   | 62.5<br>61 5<br>69.4<br>72.8<br>72.8  | 69.4<br>69.4<br>80.5<br>86.0<br>84.3 |                                     | 29 1<br>28 4<br>31 5<br>32 2<br>30 8   | 35.1<br>33.9<br>36.9<br>36.2<br>35.0 |                                    | 1 7<br>1 3<br>1 7<br>1 9<br>1 8       | 2.2<br>2.1<br>2.0<br>2.2<br>2.2<br>2.2 | 5.7<br>5.0<br>5.2<br>4.9<br>4.6 | 2.0<br>2.0                       |                                               | 16<br>17<br>18<br>19<br>20 |     |
|            | 26.0<br>24.0<br>25.5<br>26.0<br>27.0 | 18.520.521.020.018.5                      |                                      | 352<br>352<br>384<br>376<br>376                                                                        | 248<br>280<br>248<br>296<br>312     | 313<br>321<br>316<br>331<br>339     | 400<br>416<br>408<br>456<br>392                                             | 352<br>344<br>336<br>352<br>320  | 375<br>370<br>370<br>404<br>357   | 94.8<br>85.5<br>88.0<br>83.8<br>80.9   | 72.8<br>70.3<br>72.8<br>62.1<br>66 0  | 81 2<br>77 1<br>80 7<br>74 7<br>70 6 | 38.1                                | 26.2<br>31.5<br>27.4<br>32.8<br>29.6   | 35.7<br>35.2<br>33.1<br>36.1<br>37.1 |                                    | $\begin{array}{c}1.4\\1.6\end{array}$ | 2.0                                    | 4.1<br>4.4<br>4.7<br>4 4<br>3.8 | $\frac{1.8}{2.0}$                | 3.5                                           | 21<br>22<br>23<br>24<br>25 |     |
|            |                                      | 22.0<br>18.5<br>18.0                      | 23.5<br>21.4<br>21.5                 | 376<br>368<br>368                                                                                      |                                     | 326<br>325<br>320                   | 432<br>416<br>432                                                           | 368<br>344<br>344                | 404<br>373<br>385                 | 91.4<br>80.9<br>83 8                   | 67.7<br>69.2<br>69.6                  | 76.9<br>74.9<br>77.3                 | $42.0 \\ 40.8 \\ 41.1$              | 24.7<br>33.0<br>31.2                   | 37 0<br>37.4<br>37.5                 | 3.7                                | 1.9<br>1.6<br>1.7                     | 2.3<br>2.1<br>2.0                      | $3.8 \\ 4.0 \\ 4.3$             | 2.2                              | 3.3<br>3.4<br>——                              | 26<br>27<br>28             | •   |
|            |                                      |                                           | 22.1                                 |                                                                                                        | - 1                                 | 343                                 | ,                                                                           |                                  | 391                               |                                        | •                                     | 78.5                                 |                                     |                                        | 36.2                                 | F                                  |                                       | 2.2                                    |                                 |                                  | 3.4                                           |                            |     |

# TABLE LXII

# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

# Mill B

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| Riehle Compres-<br>sion, lb.                                                                                                                                                                       | Elmendorf 7                                                             | Fear, g./sheet                                                                                                                                                                      | Amthor Te                                                                                                                                                              | nsile, lb./in.                                                              | Amthor S                                             |                                                      |                            |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|----------------------------|
| Across                                                                                                                                                                                             | In                                                                      | Across                                                                                                                                                                              | In                                                                                                                                                                     | Across                                                                      | In                                                   | Across                                               |                            |
| Max. Min' Av.                                                                                                                                                                                      | Max. Min. Av.                                                           | Max. Min. Av.                                                                                                                                                                       | Max. Min. Av.                                                                                                                                                          | Max Min. Av.                                                                | Max. Min. Av.                                        | Max. Min. Av.                                        | Roll                       |
| 28       5       19.0       22.6         28.5       21.5       25.2         25.5       19.5       22.6         29.0       23.0       25.5         27       5       17.5       23.3                 | 408 288 337<br>424 344 394<br>392 312 356<br>456 368 415<br>432 360 402 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                                | 93.1 74.2 83.6<br>101.6 81.3 90.0<br>84.5 59.1 77 6<br>78.7 59.3 71 3<br>79.6 59.6 70.0                                                                                | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                        | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | 1<br>2<br>3<br>4<br>5      |
| 26.0         18.5         22.4           26.5         22.0         24.4           29.0         22.0         25.0           27.0         18.0         23.8           25.5         19.5         22.5 | 440 328 368<br>400 304 346<br>432 320 365<br>456 328 391<br>400 312 365 | 496 392 428<br>448 328 377<br>440 344 397<br>472 360 418<br>448 344 416                                                                                                             | 98.2       77.9       89.2         84.7       70.6       81.4         88.0       72.8       83.1         91.4       66.0       78.0         99.9       77.9       89.3 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                        | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 6<br>7<br>8<br>9<br>10     |
| 25.5 19.5 22.9<br>27.5 21.5 ,24.2<br>28.0 21.0 23.8<br>27.0 22.0 25.2<br>29.0 21.0 25.5                                                                                                            | 376 288 329<br>424 320 373<br>392 304 352<br>384 304 345<br>432 352 389 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                                | 93.1 69.4 79 9<br>96.5 77.9 90.1<br>99.9 67.7 85.7<br>99.9 83.0 91 4<br>96.5 71.1 89 6                                                                                 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                        | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 11<br>12<br>13<br>14<br>15 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                    | 424         328         379           424         344         389           408         312         380           416         352         381           408         328         371 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                   | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                        | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 16<br>17<br>18<br>19<br>20 |
| $\frac{25.0  18.5  21.7}{23.7}$                                                                                                                                                                    | $344  264  \frac{304}{353}$                                             | $\frac{424}{328}  \frac{366}{397}$                                                                                                                                                  | 91.4 72.8 <u>83 9</u><br>. <u>84.1</u>                                                                                                                                 | $   \begin{array}{r} 39.1 & 28.6 & 34.8 \\ \hline 38.1 & 38.1 \end{array} $ | 2.6  1.7  2  2<br>2.2                                | 5.6 2.0 $\frac{4}{3}$ $\frac{3}{3.8}$                | 21                         |

TABLE LXHI

 $\cdot$   $z_{i} z_{i} z_{i} z_{i}$ 

5**6/3**007;----3

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PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

MILL C

|   |                                     | -          | Basis        | Woigh        | nt lb               | -     | -            |               |                        |            |                  |                         | R                       | ursting  | (*       | · G.E.   | Punc       | ture.           |                | le Com<br>sion, lb |              |
|---|-------------------------------------|------------|--------------|--------------|---------------------|-------|--------------|---------------|------------------------|------------|------------------|-------------------------|-------------------------|----------|----------|----------|------------|-----------------|----------------|--------------------|--------------|
|   | <b>T</b> ( <b>1</b> )               |            |              | x 12/10      |                     | Calip | er, 0.0      | 01 in.        | Apparent               | Ma         | oisture,         | %                       |                         | gth, po  |          |          | units      |                 |                | In                 |              |
|   | Institute<br>File No.               | Roll       | Max.         | Min.         | Av.                 | Max.  | Min.         | Av.           | Density,<br>lb./cu.ft. | Max.       | Min.             | Av.                     | Max.                    | Min.     | Av.      | Max.     | Min.       | Av.             | Max.           | Min.               | Av.          |
| 1 | 116360/62                           | 1          | 44.6         |              | 43.7                | 14.0  | 13.4         | 13.7          | 38.2                   | 8.0        | 7.5              | 7.7                     | 122                     | 79       | 98       | 41       | 34         | 37              | 34.0           | 22.0               | 28.0         |
|   | 116363/65                           | 2          | 43.6         | 42.1         | 42.8                | 13.8  | 12.8         | 13.4          | 38.3                   | 8.2        | 7.3              | 7.8                     | 119                     | 76       | 98       | 38       | 33         | 35              | 37.0           | 22.5               | 29.4         |
|   | 116366/68<br>116960/62              | - 5        | 45.2<br>42.1 | 42.9<br>41.2 | $\frac{44.0}{41.7}$ | 14.3  | 13 5<br>13.9 | 14.0          | 37.7<br>35.2 _         | 8.2<br>8.7 | 7.3              | 7.7                     | 129<br>107              | 90<br>75 | 109<br>  | 40       | 34<br>_ 33 | 38<br>_ 36_     | 36.5<br>34.5   | $27.5 \\ 29.0$     | 31.2<br>31.2 |
| - | 116963/65                           | - 5        | 43.0         | 41.2         | 42.6                | 15.1  | 14.3         |               | 33.2 _<br>34.5         | 7.8        | 6.8              | 7.4                     | 135                     |          | 104      | 50       | - 37       | - 41            | 38.5           | 28.5               | 31.6         |
|   | 116975/77                           | 6          | 42.5         | 41.9         | 42.2                |       | 14.7         | 15.0          | 33.8                   | 8.9        | 7.9              | 8.3                     | 134                     | 77       | 99       | 45       | 39         | 42              | 37.5           | 27.5               | 31.0         |
|   | 116978/80                           | 7          | 42.3         | 41.8         | 42.1                | 15.0  |              | 14.6          | 34.6                   | 8.3        | 7.2              | 7.6                     | 125                     | 80       | 101      | 45       | 38         | 41              | 36.0           | 22.0               | 29.7         |
|   | 116981/83 <sup>-</sup><br>117459/61 | - 8 ·<br>9 | 42.6         | 42.4<br>41.6 | 42.5<br>42.1        | 15.2  | 14.5<br>14.6 | -14.9<br>15.0 | $\frac{34.2}{33.7}$    | 8.5<br>5.9 | 7:9<br>5.0       | 8.2 <sup>-</sup><br>5.5 | 118 <sup>-</sup><br>124 | 80<br>65 | 99<br>99 | 43<br>42 | 37<br>38   | $\frac{41}{40}$ | - 37.0<br>35.5 | $27.5 \\ 26.5$     | 32.8<br>29.9 |
|   | 117462/64                           | 10         | 42.6         | 41.0         | 42.1                | 15.4  | 14.0         | 14.7          | 34.5                   | 5.9<br>6.6 | <sup>-</sup> 4.9 | 5.8                     | 142                     |          | 103      | 43       | 36         | 40              | 32.5           | 25.5               | 28.9         |
|   | 117977/79                           | 11         | 44.9         | 42.8         | 43.8                | 14.5  | 13.0         | 13.9          | 37.8                   | 6.9        | 3.9              | 5.6                     | 124                     | 80       | 102      | 41       | 35         | 38              | 33.0           | 26.0               | 30.3         |
|   | 117980/82                           | 12         | 42.1         | 41.6         | 41.8                | 15.2  | 14.5         | 15.0          | 33.4                   | 7.5        | 5.6              | 6.6                     | 120                     | 78       | 99       | 40       | 35         | 38              | 33.5           | 25.5               | 28.3         |
|   | 117983/85                           | 13         | 42.7         |              |                     | 15.4  |              | 14.9          | 34.4                   | 6.5        | 5.3              | 6.1                     | 113                     | 63       | 93       | 41       | 35         | 38              | 29.5           | 25.0               | 27.3         |
|   | 117986/88                           | 14         | 42.7         |              | 42.5                | 15.4  | 14.6         |               | 34.0                   | 6.8        | 54               | 6.3                     | 133                     | 78       | 97       | 42       | 34         | 38              | 32.0           | 24.0               | 27.6         |
|   | 117989/91                           | 15         | 44.5         | 43.6         | 44.0                | 15.0  | 14.2         | 14.7          | 35.9                   | 7.8        | 6.6              | 7.1                     | 131                     | 87       | 109      | 44       | 37         | 41              | 35.0           | 24.5               | 30.5         |
|   | Average                             |            |              |              | 42.7                |       |              | 14.5          | 35.3                   |            |                  | 7.1                     |                         |          | 100      |          |            | 39              |                |                    | 29.8         |
|   | Average ,                           |            |              |              | 76.1                | . '   |              | 14.0          | 00.0                   |            | •                | ,.1                     |                         |          | 1,00     |          |            |                 |                |                    |              |

#### TABLE LXIV.

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B S. FOURDRINIER KRAFT LINER

Mill D

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|                                                               |                            | n + 117 + 1                                                                                                     | , n                                  | - ,                                                                                                             |                                      |                                      |                                    |                                    |                                   | 'n                                     | <b>4</b> *                                                                                                      | C F                        | D                          |                            |                                      | le Com<br>ion, lb                    |                                      |
|---------------------------------------------------------------|----------------------------|-----------------------------------------------------------------------------------------------------------------|--------------------------------------|-----------------------------------------------------------------------------------------------------------------|--------------------------------------|--------------------------------------|------------------------------------|------------------------------------|-----------------------------------|----------------------------------------|-----------------------------------------------------------------------------------------------------------------|----------------------------|----------------------------|----------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| <b>T</b> 114 4                                                |                            | Basis Weigh<br>(12 x 12/10                                                                                      |                                      | Caliper, 0.0                                                                                                    | 01 in.                               | Apparent                             | Mo                                 | isture,                            | %                                 |                                        | arsting<br>gth, points                                                                                          |                            | Punct:<br>units            | ure,                       |                                      | In                                   |                                      |
| Institute<br>File No.                                         | Roll                       | Max. Min.                                                                                                       | Λv.                                  | Max. Min.                                                                                                       | Av.                                  | Density,<br>lb./cu.ft.               | Max.                               | Min.                               | Av.                               | Max.                                   | Min. Av.                                                                                                        | Max.                       | Min.                       | Av.                        | Max.                                 | Min.                                 | Av.                                  |
| 117006/08<br>117009/11<br>117012/14<br>117015/17<br>117018/20 | 1<br>2<br>3<br>4<br>5      | 41.1 40.3<br>41.8 40.4<br>41.8 40.2<br>40.3 40.3<br>45.4 42.9                                                   | 40.8<br>40.9<br>41.0<br>40.3<br>43.9 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                            | 14.7<br>14.7<br>14.8<br>14.9<br>16.7 | 33.3<br>33.4<br>33.2<br>32.4<br>31.5 | 8,9<br>8,7<br>9,1<br>8,2<br>8,6    | 8.3<br>6.8<br>6.9<br>6.3<br>6.7    | 8.6<br>7.9<br>7.9<br>7.1<br>7.7   | 110<br>118<br>118<br>118<br>118<br>126 | 80         94           82         102           63         93           63         84           69         100 | 40<br>39<br>40<br>38<br>47 | 33<br>35<br>35<br>31<br>40 | 38<br>37<br>37<br>36<br>44 | 33.5<br>33.0<br>29.5<br>29.5<br>31.0 | 24.0<br>24.0<br>22.0<br>20.0<br>25.0 | 28.3<br>28.6<br>25.8<br>24.4<br>27.4 |
| 117021/23<br>117054/56<br>117060/62<br>117063/65<br>117090/92 | 6<br>7<br>8<br>9<br>10     | 46.444.642.941.541.039.842.841.838.938.8                                                                        | 45.4<br>42.4<br>40.4<br>42.3<br>38.8 | $\begin{array}{rrrrr} 17.7 & 16.0 \\ 15.9 & 14.8 \\ 14.9 & 13.8 \\ 16.8 & 15.4 \\ 13.7 & 12.7 \end{array}$      | 16.6<br>15.3<br>14.4<br>16.0<br>13.3 | 32.8<br>33.2<br>33.6<br>31.7<br>34.9 | 7.9<br>11.5<br>14.1<br>12.8<br>5.8 | 6.5<br>7.6<br>11.0-<br>10.5<br>3.1 | 7.4<br>9.4<br>12.4<br>11.7<br>4.2 | 133-<br>117<br>123<br>120<br>124       | 75 100<br>73 97<br>79 102<br>79 101<br>70 91                                                                    | 48<br>40<br>39<br>40<br>32 | 41<br>32<br>32<br>34<br>28 | 44<br>36<br>34<br>37<br>30 | 35 5<br>33.5<br>36.5<br>34.0<br>33.5 | 23.0<br>25.0<br>25.5<br>26.0<br>27.0 | 28.8<br>29.9<br>29.4<br>30.1<br>31.4 |
| 117093/95<br>117111/13<br>117114/16<br>117123/25<br>117167/69 | 11<br>12<br>13<br>14<br>15 | $\begin{array}{cccc} 40.3 & 38.9 \\ 42.0 & 40.8 \\ 40.3 & 39.2 \\ 41.6 & 40.4 \\ 43.0 & 41.8 \end{array}$       | 39.6<br>41.6<br>39.7<br>40.8<br>42.5 | 13.512.414.814.013.512.315.513.915.014.5                                                                        | 13.0<br>14.3<br>12.8<br>14.3<br>14.7 | 36.5<br>34.8<br>37.2<br>34.2<br>34.7 | 5.3<br>7.7<br>7.8<br>8.6<br>6.2    | 3.6<br>6.3<br>7.0<br>7.1<br>5.7    | 4.3<br>70<br>7.4<br>8.0<br>6.0    | 120<br>111<br>121<br>114<br>125        | $\begin{array}{cccc} 71 & 95 \\ 68 & 94 \\ 89 & 104 \\ 80 & 95 \\ 82 & 102 \end{array}$                         | 33<br>37<br>33<br>37<br>38 | 28<br>30<br>29<br>30<br>31 | 30<br>33<br>32<br>33<br>35 | 36.5<br>29.5<br>30.5<br>30.0<br>30.5 | 27.0<br>24.5<br>24.0<br>22.0<br>25.5 | 31.3<br>27.0<br>27.0<br>26.1<br>27.8 |
| 117170/72<br>117173/75<br>117176/78<br>117260/62<br>117266/68 | 16<br>17<br>18<br>19<br>20 | 44.6       41.6         42.2       41.4         43.2       40.4         43.7       42.7         41.2       40.8 | 43.4<br>41.9<br>41.9<br>43.3<br>41.0 | 15.8       14.4         14.9       14.1         17.9       15.4         15.1       14.0         15.4       14.5 | 14.9<br>14.5<br>16.8<br>14.6<br>15.1 | 34.9<br>34.6<br>29.9<br>35.6<br>32.6 | 7.1<br>7.6<br>9.0<br>7.5<br>5.7    | 5.6<br>5.5<br>6.1<br>5.7<br>5.1    | 6.3<br>6.6<br>8.0<br>6.7<br>5.5   | 130<br>131<br>104<br>147<br>108        | $\begin{array}{cccc} 69 & 105 \\ 85 & 105 \\ 64 & 86 \\ 78 & 110 \\ 72 & 93 \end{array}$                        | 39<br>37<br>38<br>37<br>39 | 31<br>32<br>32<br>33<br>33 | 35<br>34<br>35<br>36<br>36 | 35.0<br>30.0<br>29.0<br>35.0<br>33.0 | 26.5<br>23.0<br>21.5<br>23.0<br>24.0 | 31.1<br>26.9<br>25.9<br>28.2<br>27.8 |
| 117269/71<br>Average                                          | 21                         | 43.0 42.6                                                                                                       | $\frac{42.8}{41.7}$                  | 15.1 14.3                                                                                                       | 14.8<br>14.8                         | $\frac{34.7}{33.8}$                  | 8.2                                | 4.6                                | 6.2<br>7.4                        | 122                                    | $\frac{76}{98}$                                                                                                 | 41                         | 35                         | $\frac{38}{36}$            | 29.0                                 | 23.0                                 | $\frac{25.9}{28.1}$                  |

TABLE LXHI

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

MILL C

| Riehle Compres-<br>sion, lb.                                                                                                                                             | Elmendorf Tear, g./sheet                             | Amthor Tensile, lb                                                                                                                                                                                                                                                    | ./in.                                                | Amthor Stretch, %                                                                                                                                                                                                                                                                                                                                                                         |                            |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------|
| Across                                                                                                                                                                   | In Across                                            | · In                                                                                                                                                                                                                                                                  | Across                                               | In Across                                                                                                                                                                                                                                                                                                                                                                                 |                            |
| Max. Min. Av.                                                                                                                                                            | Max. Min. Av. Max. Min. Av.                          | Max. Min. Av. Max                                                                                                                                                                                                                                                     | Min. Av.                                             | Max. Min. Av. Max. Min. Av.                                                                                                                                                                                                                                                                                                                                                               | Roll                       |
| 10.5       19.0       23.1         16.5       18.5       23.3         18.5       21.5       24.5         16.5       20.0       22.8         17.0       -20.5       -23.5 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 93 1 67.7 81.6 48.8<br>94.8 71.1 82.7 47.2<br>93.1 77.9 86.4 51.3<br>81.1 65.2 76.6- 41.6<br>103.3 77.9 87.2 41.1                                                                                                                                                     | 37 2 43.0<br>37.6 45.0<br>34.7 38.8                  | 2.6       1.8       2.2       8.1       2.6       5.0         2.4       1.7       2.1       6.5       2.5       4         2.6       1.8       2.2       6.3       2.3       4.7         2.4       1.17       5.5       6       3       2.4       4.7         2.4       1.17       1.5       -5.6       -3       2       4.3         2.0       1.2       1.7       5.5       2.3       3.8 |                            |
| 4.0       18.5       21.4         4.5       16.0       21.3         6.0       18.5       22.8         3.0       18.0       21.1         5.0       19.5       22.0        | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 88.0         69.4         82.4         42.3           98.2         72.8         87.6         41.8           96.5         77.9         89.8         42.3           101.6         76.2         92.0         40.0           101.6         64.3         85.2         40.1 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                      | 6<br>- 7<br>8<br>9<br>10   |
| 8.0       20.5       24.6         3.5       18.0       20.6         3.0       18.5       20.4         22.0       17.5       19.7         25.0       18.0       22.3      | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | 96.5         69.4         84.7         51.6           98.2         67.7         86.6         41.0           94.8         69.9         84.8         42.3           94.8         72.8         86.1         40.8           106.7         74.5         94.8         42.3  | 27.1 36.5<br>31.2 36.8                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                      | 11<br>12<br>13<br>14<br>15 |
| 22.2                                                                                                                                                                     | 364 405                                              | 85.9                                                                                                                                                                                                                                                                  | 38.9                                                 | 1.9 4.1                                                                                                                                                                                                                                                                                                                                                                                   |                            |

TABLE LXIV PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

| М | ۱L | L | D |  |
|---|----|---|---|--|
|   |    |   |   |  |

| Richle Compres-<br>sion, lb.                         | Elmendorf Tear, g./s                                        | sheet                         | Amthor Ter                                                                                                                                                             | nsile, lb./in.                                                                                                                                                                     | Amthor                                               | Stretch, %                                           |
|------------------------------------------------------|-------------------------------------------------------------|-------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|
| Across                                               | In Ac                                                       | Cross                         | In                                                                                                                                                                     | Across                                                                                                                                                                             | In                                                   | Across                                               |
| Max. Min. Av.                                        | Max. Min. Av. Max. M                                        | Min. Av.                      | Max. Min. Av.                                                                                                                                                          | Max. Min. Av.                                                                                                                                                                      | Max. Min. Av.                                        | Max. Min. Av.                                        |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 392 296 336 424 3<br>424 328 383 408 3<br>416 328 375 384 3 | 344 392<br>320 349<br>304 347 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                   | 49.9       27.8       41.9         41.6       24       7       36.0         47.4       35       6       42.0         51.1       29.8       41.3         44.0       27.6       39.8 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 440 320 384 456 3<br>376 312 344 424 3<br>536 288 369 456 3 | 320 366<br>312 373<br>336 406 | 82.4 58.2 72.7<br>80.1 58.1 68.5<br>82.6 64.8 71.5<br>80.6 58.1 70.9<br>82.4 63.5 74.0                                                                                 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 424 336 378 376 3<br>368 280 332 368 2<br>352 280 310 416 3 | 320 345<br>288 335<br>304 361 | 84.3       64.0       76.2         67.4       53.5       61.5         83.0       57.6       70.4         78.7       63.7       70.8         84.7       62.6       75.5 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 400 328 357 424 3<br>416 328 370 464 3<br>392 328 360 440 3 | 344 382<br>336 387<br>360 402 | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                               | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 26.0 21.0 22.7                                       | 400 320 362 424 3                                           | 360 398                       | 84.7 66.0 74.3                                                                                                                                                         | 42.3 30.0 37.3                                                                                                                                                                     | 2.6 1.9 2.3                                          | 4.9 1.8 3.8                                          |
| 22.5                                                 | 360                                                         | 378                           | 70.4                                                                                                                                                                   | 39.5                                                                                                                                                                               | 2.0                                                  | 3.5                                                  |

## TABLE LXV

PHVSICAL CHARACTERISTICS OF 42-LB, D.F.B.S. FOURDRINIER KRAFT LINER

Mill E

|                                                                      |                           | Racie                                                               | Weigł                                | ht llh               |                                       |                                      |                                        | • •                                   |                                   | •                                |                                   | נד                                  |                            |                                     | C P                         | <b>D</b>                      |                             | s                                     | le Com<br>ion, lb                      |                                        |   |   |
|----------------------------------------------------------------------|---------------------------|---------------------------------------------------------------------|--------------------------------------|----------------------|---------------------------------------|--------------------------------------|----------------------------------------|---------------------------------------|-----------------------------------|----------------------------------|-----------------------------------|-------------------------------------|----------------------------|-------------------------------------|-----------------------------|-------------------------------|-----------------------------|---------------------------------------|----------------------------------------|----------------------------------------|---|---|
| Institute                                                            |                           |                                                                     | x 12/1                               |                      | Ċalip                                 | er, 0.0                              | 01 in.                                 | Apparent<br>Density,                  | М                                 | oisture,                         | %                                 | Strer                               | urstin<br>1gth, p          | g<br>oints'                         | G.E.                        | Punct<br>units                |                             |                                       | În                                     |                                        |   |   |
| File No.                                                             | Roll                      | Max.                                                                | Min.                                 | Av.                  | Max.                                  | Mın.                                 | Av.                                    |                                       | Max.                              | Min.                             | Av.                               | Max.                                | Min.                       | Av.                                 | Max.                        | Min.                          | Av.                         | Max.                                  | Min.                                   | Av.                                    |   |   |
| <br>117084/86<br>117087/89<br>117126/28<br>117399/401<br>- 117402/04 | 1<br>2<br>3<br>4<br>5     | 45.1<br>452<br>430<br>44.5<br>-44.0-                                | 44 7<br>43.9<br>41.4<br>43.0<br>42 3 |                      | 18.2<br>18.7<br>14.8<br>16.8<br>17-0- | 16 4<br>13.0<br>15.5                 | 17.3<br>17.8<br>14.0<br>16.1<br>- 16-0 | 31.1<br>30.1<br>36.4<br>32.6<br>32-2  | 13.4<br>5.4<br>9.0<br>10.2<br>7-4 | 6.1<br>5.0<br>8.2<br>8.3<br>6:1- | 9.0<br>5.2<br>8.5<br>9.0<br>- 6.9 | 63<br>72<br>119<br>110<br>          | 42<br>41<br>66<br>81<br>66 | 52<br>58<br>92<br>97<br>92          | 29<br>32<br>34<br>38<br>38- | 26<br>24<br>29<br>32<br>- 31  | 28<br>28<br>31<br>36<br>-35 | 25.0<br>27.5<br>32.0<br>35.5<br>35:0- | 19.5<br>21.5<br>22.0<br>24.5<br>-26:0- | 22.0<br>24.3<br>25.0<br>29.7<br>-30:4- | · | • |
| <br>117405/07<br>117408/10<br>117411/13<br>117592/94<br>117595/97_   | 6<br>7<br>-8<br>-9<br>-10 | $\begin{array}{r} 44.2 \\ 45.0 \\ 42.9 \\ 43.0 \\ 44.1 \end{array}$ | 43.2                                 | 44.2<br>41.7<br>42.9 | $-\frac{16.0}{16.2}$                  | 15 0<br>14.8<br>15.0<br>13.5<br>14.4 | 15.5                                   | 32.7<br>34.2<br>32.5_<br>36.0<br>34.4 | 8.9<br>7.7<br>8.1                 | 6.2<br>5.8<br>6.2                | 7.5<br>6.8<br>                    | 119<br>128<br>- 122<br>126<br>- 126 | 76<br>84<br>               | 98<br>105<br>-104 _<br>106<br>103 . | 38<br>42<br>39<br>46<br>41  | 32<br>34<br>- 33_<br>37<br>35 | 34<br>38<br>36<br>39<br>39  | 36.0<br>32.0_                         | 25.0<br>26.0<br>.24.0<br>24.0<br>20.5  | 28 7<br>30.9<br>28.8<br>28.5<br>26.4   |   | - |
| 117598/600<br>Average                                                | 11                        | 43.1                                                                | 41.6                                 | $\frac{42.4}{43.4}$  | .15.8                                 | 15.0                                 | $\frac{15.3}{15.7}$                    | $\frac{33.3}{33.2}$                   |                                   | -                                | 7.5                               | 120                                 | 81                         | <u>96</u><br>91                     | 41                          | 35                            | $\frac{37}{35}$             | 29.5                                  | 24.0                                   | $\frac{27.5}{27.5}$                    |   |   |

#### TABLE LXVI

# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

#### MILL F

|                                                               |                                                                                                                     | Racie                                                                 | weigh                                                               | st 11s                               |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | ,                                    |                                      |                                          |                                     |                                   |                                     | ` TA                          |                            | -                          | C F                          | D                          |                                          | Riehl                                | e Com<br>ion, lb                     | pres-                                |
|---------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------|---------------------------------------------------------------------|--------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------|--------------------------------------|------------------------------------------|-------------------------------------|-----------------------------------|-------------------------------------|-------------------------------|----------------------------|----------------------------|------------------------------|----------------------------|------------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Institute                                                     |                                                                                                                     |                                                                       | x 12/10                                                             |                                      | Calip                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | er, 0.00                             | 01 in.                               | Apparent                                 | Mo                                  | isture,                           | %                                   |                               | ursting<br>gth, pi         |                            |                              | Punct<br>units             | ure,                                     |                                      | In                                   |                                      |
| File No.                                                      | Roll                                                                                                                | Max.                                                                  | Min.                                                                | Av.                                  | Max.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | Min.                                 | Av.                                  | · Density,<br>lb./cu.ft.                 | Max.                                | Min.                              | Av.                                 | Max.                          | Min.                       | Av.                        | Max.                         | Min.                       | Av.                                      | Max.                                 | Min.                                 | Av.                                  |
| 118066/68<br>118069/71<br>118072/74<br>118075/77<br>118108/10 | $     \begin{array}{c}       1 \\       2' \\       3 \\       4 \\       5 \\       5 \\       .     \end{array} $ | $\begin{array}{r} 41.5 \\ 42.9 \\ 38.5 \\ 42.8 \\ 40.1 \end{array}$   | $\begin{array}{c} 40.5 \\ 41.3 \\ 36.0 \\ 40.8 \\ 38.7 \end{array}$ | 41.1<br>42.4<br>37.5<br>41.6<br>39.3 | 14.1<br>14.7<br>14.0<br>14.0<br>13.6                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 11.8<br>12.1<br>12.2<br>12.7<br>12.3 | 13.5<br>13.9<br>13.1<br>13.5<br>13.0 | 36 5<br>36.6<br>34.3<br>. 37.0<br>. 36.3 | 11.8<br>12.9<br>93<br>12.0<br>11.8  | 9.9<br>10.3<br>7.7<br>10.2<br>8.8 | 10.7<br>11.4<br>8.7<br>11.1<br>10.3 | 117<br>119<br>93<br>96<br>109 | 80<br>66<br>55<br>57<br>68 | 98<br>96<br>76<br>75<br>83 | 48<br>39<br>32<br>41<br>32   | 35<br>34<br>24<br>28<br>26 | 39 <sup>.</sup><br>37<br>28<br>32.<br>29 | 28.5<br>26.0<br>25.5<br>24.0<br>26.5 | 18.5<br>17.5<br>20.0<br>19 0<br>19.0 | 24.3<br>21.5<br>22.3<br>21.6<br>23.7 |
| 118111/13<br>118114/16<br>118117/19<br>118120/22<br>118123/25 | 6<br>7<br>8<br>9<br>10                                                                                              | $\begin{array}{r} 40.0 \\ 38 & 0 \\ 40.5 \\ 41.1 \\ 39:1 \end{array}$ | 39_0<br>36_2<br>39_3<br>39_9<br>37_3                                | 39.4<br>36.9<br>40.0<br>40.5<br>38.4 | $13.8 \\ 13.1 \\ 14.1 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ 14.0 \\ $ | 12.5<br>12.0<br>13.0<br>11.6<br>13.1 | 13.4<br>12.6<br>13.7<br>13.5<br>13.5 | 35.3<br>35.1<br>35.0<br>36.0<br>34.1     | 8.1<br>12.6<br>11.5<br>11.4<br>10.5 | 7.5<br>7.2<br>9.3<br>9.7<br>8.5   | 78<br>95<br>105<br>106<br>95        | 97<br>93<br>118<br>116<br>94  | 58<br>58<br>79<br>75<br>57 | 78<br>76<br>97<br>95<br>74 | 34<br>30,<br>41<br>46.<br>33 | 25<br>26<br>32<br>26<br>23 | 31<br>28<br>37<br>37<br>29               | 25.5<br>25.5<br>28.0<br>29.5<br>25.5 | 20.0<br>21.0<br>21.0<br>24.0<br>18.5 | 23.2<br>23.3<br>23.4<br>26.9<br>22.6 |
| Average                                                       |                                                                                                                     |                                                                       |                                                                     | 39.7                                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                                      | 13.4                                 | 35.6                                     |                                     |                                   | 10.0                                |                               |                            | 85                         |                              |                            | $\overrightarrow{33}$                    |                                      |                                      | 23.3                                 |

#### TABLE LXVII

## PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

#### MILL G

|           |                   |                |                    |          |       |           |        |            |      | •        |      |            |                  |       |      |                |      |        | le Com<br>sion, lb |      |
|-----------|-------------------|----------------|--------------------|----------|-------|-----------|--------|------------|------|----------|------|------------|------------------|-------|------|----------------|------|--------|--------------------|------|
|           |                   |                | s Weigl<br>x 12/10 |          | Calir | er, 0.0   | 01 in. | Apparent   | Me   | oisture, | %    | B<br>Stren | urstir<br>øth. r |       |      | Punct<br>units | ure, |        | <br>In             |      |
| Institute |                   | · · · · ·      | ·                  |          |       | · · · · · |        | - Density, |      | -51411)  | 70   |            | , r              |       |      |                |      |        |                    |      |
| File No.  | Roll              | Max            | Min.               | Av.      | Max.  | Min.      | Av.    |            | Max. | Min.     | Av.  | Max.       | Min              | . Av. | Max. | Min.           | Av.  | Max.   | Min.               | Av.  |
| 117245/47 | 1                 | 42,9           | 42.0               | 42.6     | 16.1  | 14.9      | 15.5   | 33 0       | 7.7  | 6.8      | 7.3  | 114        | 66               | 93    | 40   | 34             | 37   | 30.5   | 22.0               | 27.4 |
| 117248/50 | 2                 | 42.9           | 42.1               | 42.5     | 16.2  | 15.5      | 15.9   | 32.1       | 5.5  | 4.4      | 4.9  | 109        | 55               | 87    | 45   | 35             | 38   | 30.5   | 23 0               | 26.7 |
| 117251/53 | 3                 | 42.1           | 41.9               | $42 \ 0$ | 16.1  | 15.3      | 158    | 31.9       | 7.8  | 7.1      | 7.4  | 107        | 72               | 88    | 39   | 34             | 37   | 28.0   | 22 5               | 25.7 |
| 117254/56 | 4                 | 42-4           | 41.0               | 417      | 16.1  | 15.3      | 15.7   | 31.9.      | 7.2  | 63       | 6.8  | 114        | 69               | 85    | 39   | 34             | 37   | 29.0   | 24.5               | 26.1 |
| 117257/59 | 5                 | 42 8           | 41.8               | 42.2     | 16.2  | 154       | 15.9   | 31.8       | 8.7  | 7.3      | 8.1  | 109        | 65               | 92    | 40   | 35             | 38   | 30.0   | 21.0               | 25 5 |
| 117263/65 | 6                 | 41.4           | 40 9               | 41.2     | 16.5  | 15.6      | 16.1   | 30.7       | 7.2  | 4.3      | 5.8  | 107        | 63               | 89    | 43 . | 33             | 36   | 33.5   | 24.5               | 28 8 |
| 117272/74 | 7                 | 41°.9          | 41.5               | 41.7     | 16 8  | 15.9      | 16.2   | 30.9       | 84   | 6.3      | 7.0  | 113        | . 72             | 92    | 42   | 36             | 38   | 32 5-  | 25.0.              | 28.1 |
| 117320/22 | 8                 | 42 6           | 41.5               | 42.0     | 15.6  | 14.1      | 15.0   | 33.6       | 10.8 | 10.3     | 10 5 | 129        | 84               | 106   | 40   | 36             | 38   | 32 0   | 26 0               | 28.8 |
| 117393/95 | 9                 | 417            | 41.3               | 41 5     | 16.2  | 15.0      | 15 5   | 32.1       | 8.4  | 7.9`     | 8.2  | 127        | 61               | 97    | 39 ' | 33             | 36   | 34:5   | 25.0               | 28.9 |
| 117396/98 | 10                | $42.4^{\circ}$ | 41.3               | 41 7     | 16.0  | 14.8      | 15.2   | 32.9       | 8.0  | .4.0     | 63   | 122        | 60               | 95    | 38   | 32             | 35   | 38.0   | 23.5               | 27.9 |
| 117480/82 | 11                | 44.0           | 42 7               | 43.3     | 15 9  | 14.6      | 15.3   | 34.0       | 7.5  | 65       | 6.9  | 120        | 65               | 88    | 47   | 41             | 44   | 35.0   | 22 5               | 27.4 |
| 117483/85 | 12                | 40.4           | 39.8               | 40.2     | 16.0  | 14.8      | 15.3   | 31.5       | 63   | 5.2      | 5.8  | 122        | 68               | 91    | 42   | 35             | 39   | . 33 0 | 25.0               | 28.1 |
| 117486/88 | 13                | 42 0           | 41.3               | 41.6     | 15,9  | 14.9      | 15.3   | 32 6       | 68   | 4.0      | 5.5  | 101        | 49               | 79    | 41   | - 36           | 39   | 29.0   | 23.0               | 25.6 |
| 117489/91 | 14                | 43 2           | 41.7               | 42.6     | 16.3  | 15.6      | 16.0   | 31.9       | 8.3  | 6.1      | 7.3  | 103        | 72               | 88    | 42   | 33             | 36   | 32.0   | 25.5               | 28.8 |
| 117492/94 | 15 <sup>.</sup> , | 42.0           | 40 3               | 41.0     | 15.5  | , 14.5    | 15.0   | 32.8       | 8.8  | 6 6      | 79   | 114        | 78               | 94    | 38   | 34             | 37   | 29.5   | 24.0               | 26.6 |
| Average   |                   |                |                    | 41.9     |       | •         | 15.6   | 32 2       |      |          | 7.0  |            |                  | 01    |      |                | 38   |        |                    | 27 4 |

## TABLE LXV PHYSICAL CHARACTERISTICS OF 42-LB, D.F.B.S. FOURDRINIER KRAFT LINER

| Mill E |
|--------|
|--------|

,

| Richle Compres-<br>sion, lb.                         | Elmendorf 7                                           | Fear, g./sheet                                       | Amthor Te                                                                                                                   | nsile, lb./in.                                       | Amthor S                                             | stretch; %                      |                                                                                                |
|------------------------------------------------------|-------------------------------------------------------|------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|---------------------------------|------------------------------------------------------------------------------------------------|
| Across                                               | In                                                    | Across                                               | In                                                                                                                          | Across                                               | In                                                   | Across                          |                                                                                                |
| Max. Min. Av.                                        | Max. Min. Av.                                         | Max. Min. Av.                                        | Max. Min. Av.                                                                                                               | Max Mm. Av.                                          | Max. Min. Av.                                        | Max. Min. Av.                   | Roll                                                                                           |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 94.8 65.7 82.3<br>98.2 76.2 88.0<br>96.5 69.4 84.3.<br>96.5 79.6 89.9<br>88.0 68.2 78.9<br>91.4 64 3 76.7<br>84.7 62.6 72.7 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $5.2 1.9 4.0 \\ 5.2 2.9 3.8 \\$ | $ \begin{array}{c} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7$ |
| 20.6                                                 | 324                                                   | 365                                                  | . 77.1                                                                                                                      | 34.3                                                 | • 1.8                                                | -3.6                            | ,                                                                                              |

TABLE LXVI

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

## MILL F

|                                | Compres<br>., lb.                                                                                          |                                 | Elmen      | dorf I                          | fear, g.,                         | /sheet                          |                                 | ,                                    | Amt                                  | hor Ter                              | isile, lb.,                          | /in.                                 |                                      |                                 | . Am                            | thor S                          | tretch,                           | %                               |                               |                        |
|--------------------------------|------------------------------------------------------------------------------------------------------------|---------------------------------|------------|---------------------------------|-----------------------------------|---------------------------------|---------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------|---------------------------------|---------------------------------|-----------------------------------|---------------------------------|-------------------------------|------------------------|
| Aci                            | ross                                                                                                       |                                 | In         | ······                          |                                   | Across                          |                                 |                                      | In                                   |                                      |                                      | Across                               |                                      |                                 | In                              |                                 |                                   | Across                          |                               |                        |
| Max. M                         | lin. Av.                                                                                                   | Max.                            | Min:       | Av.                             | Max.                              | Min.                            | Av.                             | Max.                                 | Min.                                 | Av.                                  | Max.                                 | Min.                                 | Av.                                  | Max.                            | Min.                            | Av.                             | Max.                              | Min.                            | Av.                           | Roll                   |
| 26.0 15<br>21.0 13<br>20.5 15  | 4.0' 18.4<br>5.0 18.9<br>3.5 16.5<br>5.0 18.0<br>7.0 19.8                                                  | 400<br>416<br>304<br>320<br>352 |            | 338<br>335<br>270<br>283<br>279 | 440<br>• 408<br>352<br>384<br>368 | 368<br>304<br>272<br>272<br>280 | 404<br>370<br>310<br>334<br>325 | 78.7<br>79.6<br>70.6<br>71.6<br>69.4 | 59.1                                 | 71.2<br>71.4<br>63.9<br>67.0<br>63 6 | 42.3<br>42.8<br>30.1<br>31.8<br>36.4 | 33.7<br>25.7<br>23.7<br>26.9<br>26.6 | 38.7<br>35.9<br>27.5<br>29.5<br>32.8 | 2.3<br>2.2<br>2.0<br>2.2<br>2.4 | 1.5<br>1.3<br>1.4               | 2.0<br>2.0<br>1.7<br>1.8<br>2.0 | 3.9<br>4.7<br>4.2<br>3.6<br>4.2   | 2.5<br>1.4<br>2.6<br>2.6<br>1.8 | 2.9<br>3.4<br>3.1             | 1<br>2<br>3<br>4<br>5  |
| 21 0 .17<br>22.5 17<br>22.5 15 | 3.0       19.7         7.0       19.9         7.5       19.9         5.5       19.8         2.0       16.0 | 328<br>296<br>384<br>400<br>320 | 296<br>288 | 292<br>262<br>338<br>348<br>276 | 368<br>336<br>416<br>432<br>376   | 336<br>336                      | 320<br>285<br>379<br>369<br>333 | 67.6<br>68.1<br>80.8<br>83.5<br>67.4 | 53.0<br>52.3<br>63.3<br>64.2<br>50.8 | 60.3<br>72.0<br>74.0<br>62.3         | 37.8<br>38.1<br>39.1<br>40.5<br>31.0 | 30 5<br>28.8<br>28.4<br>32.0<br>22.5 | 33 3<br>35.2<br>36.0<br>26.9         | 2.4<br>2.3<br>2.4<br>2.5<br>2.1 | 1.6<br>1.4<br>1.3<br>1.5<br>1.5 | 1.9<br>2.0<br>2.0<br>1.9        | $3.8 \\ 3.7 \\ 4.0 \\ 4.0 \\ 3.8$ | 2.0                             | $3.0 \\ 3.0 \\ 3.1 \\ 3.0 \\$ | 6<br>7<br>8<br>9<br>10 |
|                                | 18.7                                                                                                       |                                 |            | 302                             |                                   |                                 | 343                             |                                      | •                                    | 66.7                                 |                                      |                                      | 33.0'                                |                                 |                                 | 1.9                             |                                   |                                 | 3.1                           |                        |

TABLE LXVII

# PHYSICAL CHARACTERISTICS OF 42-LB. D F.B.S. FOURDRINIER KRAFT LINER

MILL G

| Riehle Compres<br>sion, lb.                                                                                                                                                                                                                                                                                                                                                                                                                                                          | Elmendorf Tear, g /sheet                             | Amthor Tens                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | sile, lb./in.                                        | Amthor S                                             | Stretch, %                                           |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|
| Across                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | In Across                                            | , ln                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | Across                                               | [n                                                   | Across                                               |
| Max. Min. Av                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | Max. Min. Av. Max. Min. Av.                          | Max. Min. Av.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | Max. Min. Av.                                        | Max. Min. Av.                                        | Max. Min. Av. Roll                                   |
| 29.0         19.5         23.           26.0         22.0         23.           24.0         20.0         22.           24.5         18.5         22.           24.5         18.5         22.           24.5         18.5         22.           24.5         18.5         22.           24.5         18.5         22.           24.0         18.5         21.           27.0         21.0         23.           28.0         23.5         25           28.5         24.0         25. | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 82.3       56       5       70.0       .         83.5       61.3       73.9       .       .       .         81.9       60.3       70       8       .       .       .         81.8       56.4       69.7       .       .       .       .       .         83.0       62.6       70.3       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       .       . | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| 23.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 380 405                                              | 72.3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 41.8                                                 | 1.7                                                  | 3.6                                                  |

TABLE LXVIII

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill H

| <br>                                                               |                        |                                     |                        |                                                                                         |                              | ···- ·                                |                       | ;                                                                                                          |                               |                                  |                                  | <b>∽</b> υ                      | ,<br>Bursting        | - I-                                         | ~, G E:                                                                               | Duine                                           | ·                              |                                                                            | e Com                                  |                                      | <b>~ -</b> - | - |
|--------------------------------------------------------------------|------------------------|-------------------------------------|------------------------|-----------------------------------------------------------------------------------------|------------------------------|---------------------------------------|-----------------------|------------------------------------------------------------------------------------------------------------|-------------------------------|----------------------------------|----------------------------------|---------------------------------|----------------------|----------------------------------------------|---------------------------------------------------------------------------------------|-------------------------------------------------|--------------------------------|----------------------------------------------------------------------------|----------------------------------------|--------------------------------------|--------------|---|
|                                                                    |                        |                                     | Weigh<br>x 12/10       |                                                                                         | Calip                        | er, 0 0                               | 01 in.                |                                                                                                            | м                             | oisture,                         | %                                |                                 | ngth, p              |                                              | , G.D.                                                                                | units                                           |                                |                                                                            | In                                     | ,                                    |              |   |
| Institute<br>File No.                                              | Roll                   | Max.                                | Min.                   | Av.                                                                                     | Max.                         | Min.                                  | Av.                   | • Density,<br>lb./cu.ft.                                                                                   | Max.                          | Min.                             | Av.                              | Max.                            | Min.                 | Av.                                          | Max.                                                                                  | Min.                                            | Av.                            | Max.                                                                       | Min.                                   | Av.                                  |              |   |
| <br>116396/98<br>116399/401<br>117039/41<br>117042/44<br>117045/47 | 3<br>4                 | 45.0<br>457<br>42.6<br>41.9<br>42.7 | 43,7<br>41,6<br>_41,0- | 44 6                                                                                    | 16.9<br>15.6<br>15.6-        | 15 0<br>15 9<br>14 5<br>-14 8<br>15.6 | 16.5<br>15.2<br>-15.2 | $     \begin{array}{r}       34.0 \\       32.4 \\       33.2 \\      32.8 \\       30.9     \end{array} $ | 95<br>97<br>8.3<br>9.4<br>8.3 | 8.3<br>8 7<br>7.7<br>8.5-<br>5.6 | 8.8<br>9.4<br>8.1<br>9.0.<br>7.1 | 131<br>122<br>129<br>130<br>129 | 73<br>91<br>72_      | 112<br>96<br>107<br>103-<br>108              | 45<br>46<br>38<br>                                                                    | 39<br>38<br>36<br>32<br>31                      | - 42<br>42<br>37<br>35<br>35   | 30.5<br>35.0<br>_370                                                       | 25.0<br>25 0<br>29.5<br>-24.5<br>-31.0 | _29.7                                | +            | , |
| <br>117048/50<br>117051/53<br>117607/09<br>117610/12<br>117613/15  | 6<br>7                 | 42.3<br>43.3<br>42.4<br>42.8        | 41.2                   | $\begin{array}{r} 41 & 6 \\ 42 & 4 \\ 42 & 0 \\ 42 & 3 \\ 42 & 3 \\ 42 & 7 \end{array}$ | 16.5<br>                     |                                       | 16.4<br>161<br>15.6   | $ \begin{array}{r} 31 & 4 \\ 31 & 0 \\ 31.3 \\ 32.5 \\ 32.4 \end{array} $                                  | 85<br>75<br>7.2<br>9.9<br>9.8 | 7.2<br>5.2<br>5.7<br>8.3<br>7.9  | 7.7<br>6.7<br>63<br>8.9<br>8.8   | 122<br>124<br>136<br>133<br>143 | 90                   | 105<br>101<br>110 <sup>-</sup><br>115<br>111 | $ \begin{array}{r}     44 \\     - \frac{40}{38} \\     - \frac{38}{41} \end{array} $ | $33 \\ -33 \\ -33 \\ -32 \\ -33 \\ -33 \\ -33 $ | 36<br>-37<br>-36<br>-35<br>-38 | $   \begin{array}{r}     36 & 0 \\     31.5 \\     33.0 \\   \end{array} $ | 28 0<br>29 0<br>26.5<br>28 0<br>26.5   | 31.3<br>32.1<br>28.6<br>30.9<br>30.2 |              | - |
| 117616/18<br>117619/21<br>117622/24<br>117625/27                   | 11 ·<br>12<br>13<br>14 | 43 6<br>43 2                        | 42 5<br>41.9<br>41.5   | 42 9<br>42.8<br>41.9<br>42.3                                                            | 16.3<br>16.4<br>16.2<br>16.0 | 15 6<br>15 6<br>15 5                  | 15.9                  | 32.4<br>31.9<br>31.6<br>32.5                                                                               | 9.1<br>9 8<br>8.9<br>8.5      | 7.4                              | 8.5<br>7.8<br>8.1<br>7.4         | 128<br>148<br>123<br>135        | 81<br>80<br>86<br>82 | 108<br>107<br>108<br>114                     | 41<br>42<br>41<br>38                                                                  | 35<br>35<br>33<br>33                            | 38<br>38<br>37<br>36           | $35.0 \\ 33.5 \\ 33.0 \\ 34.5$                                             | 26.0<br>29.0<br>27.5<br>27.0           | 30,5<br>30,8<br>30,1<br>31,1         |              |   |
| Average                                                            |                        |                                     |                        | 42.6                                                                                    |                              |                                       | 15.9                  | 32.2                                                                                                       |                               |                                  | 8.0                              |                                 |                      | 108                                          |                                                                                       |                                                 | 37                             |                                                                            |                                        | 30.7                                 |              |   |
|                                                                    |                        |                                     |                        |                                                                                         |                              |                                       |                       |                                                                                                            |                               |                                  |                                  |                                 |                      |                                              |                                                                                       | •                                               |                                |                                                                            |                                        |                                      |              |   |

TABLE LXIX PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill I

|                                                                |                            |                                                                     | •                                                                   |                                                                     |                                           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                                      |                                        |                                     |                                   |                                  | n                               |                            | _                               | C F                        | Punci                                  |                             |                                                                     | e Com<br>ion, lb                     |                                      |
|----------------------------------------------------------------|----------------------------|---------------------------------------------------------------------|---------------------------------------------------------------------|---------------------------------------------------------------------|-------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------|----------------------------------------|-------------------------------------|-----------------------------------|----------------------------------|---------------------------------|----------------------------|---------------------------------|----------------------------|----------------------------------------|-----------------------------|---------------------------------------------------------------------|--------------------------------------|--------------------------------------|
|                                                                | •                          |                                                                     | ; Weigh<br>x 12/10                                                  |                                                                     | Calip                                     | er, 0.0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 01 in.                               | Apparent                               | Mo                                  | oisture,                          | %                                |                                 | urstin<br>Igth, p          |                                 |                            | units                                  | ure,                        |                                                                     | In                                   |                                      |
| Institute<br>File No.                                          | ' Roll                     | Max.                                                                | Min.                                                                | Av                                                                  | Max.                                      | Min.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | Av.                                  | Density,<br>lb./cu.ft.                 | Max.                                | Min.                              | Av.                              | Max.                            | Min.                       | Av.                             | Max.                       | Min.                                   | Av.                         | Max.                                                                | Min.                                 | Av.                                  |
| 116732/34<br>116738/40<br>116741/43<br>116910/12<br>116913/15  | 1<br>2<br>3<br>4<br>5      | $\begin{array}{r} 43.0 \\ 43.4 \\ 43.1 \\ 44.6 \\ 44.2 \end{array}$ | $\begin{array}{r} 41.8 \\ 41.8 \\ 41.0 \\ 42.9 \\ 42.6 \end{array}$ | 42.5<br>42.7<br>42.5<br>43.9<br>43.5                                | 15.9<br>15 9<br>15 9<br>15.7<br>15.8      | 14 9<br>14.7<br>14.4<br>14.6<br>14.3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 15.3<br>15.1<br>15.3<br>15.1<br>15.2 | 33.3<br>33.9<br>33.3<br>. 34.9<br>34.3 | 9.1<br>9.4<br>8.7<br>7.5<br>7.7     | 8,3<br>8,2<br>8,4<br>6,6<br>6,1   | 8.7<br>8.9<br>8.5<br>7.0<br>7.1  | 128<br>137<br>147<br>130<br>124 | 93<br>90<br>85<br>84<br>86 | 111<br>107<br>109<br>106<br>105 | 42<br>45<br>45<br>45<br>45 | 37<br>40<br>40<br>37<br>37             | 40<br>42<br>42<br>40<br>41  | 33.5<br>33.0<br>31.5<br>34.0<br>31.5                                | 23.5<br>23.0<br>26.0<br>23.5<br>21.5 | 30.5<br>28.7<br>28.7<br>29.0<br>26.7 |
| 116928/30<br>116943/45<br>116946/48<br>117423/25<br>117426/28  | 6<br>7<br>8<br>9<br>10     | $\begin{array}{r} 43.4 \\ 44.2 \\ 42.6 \\ 43.8 \\ 43.7 \end{array}$ | 42.4<br>42.6<br>41 3<br>42.7<br>42.7                                | 43.1<br>43.5<br>42.1<br>43.4<br>43.2                                | 15.9<br>16.1<br>15.8<br>16 1<br>16.0      | 14.9<br>14.8<br>14 4<br>15.0<br>15.0                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 15.5<br>15.5<br>15.2<br>15.5<br>15.5 | 33.4<br>33.7<br>33.2<br>33.6<br>33.4   | 7.1<br>7.5<br>7.0<br>10.3<br>9.9    | $6.4 \\ 6.3 \\ 6.0 \\ 9.8 \\ 8.3$ | 6.9<br>7.0<br>6.5<br>10.0<br>8.9 | 133<br>129<br>129<br>132<br>133 | 81<br>80<br>76<br>83<br>82 | 108<br>104<br>102<br>106<br>109 | 45<br>45<br>42<br>43<br>44 | 37<br>37<br>37<br>37<br>37<br>38       | 41<br>41<br>39<br>40<br>40  | $\begin{array}{r} 33.0 \\ 35 0 \\ 32.0 \\ 34.0 \\ 34.5 \end{array}$ | 25.0<br>25.5<br>26.0<br>25.5<br>26.0 | 29.5<br>30.0<br>29.2<br>29.9<br>29.8 |
| 117429/31<br>117432/34<br>117435/37<br>117471/73<br>117474/76  | 11<br>12<br>13<br>14<br>15 | $\begin{array}{r} 44.6 \\ 44.4 \\ 44.0 \\ 43.5 \\ 45.9 \end{array}$ | 42.7<br>43.1<br>42.5<br>42.2<br>45.1                                | $\begin{array}{r} 43.6 \\ 43.8 \\ 43.3 \\ 42.8 \\ 45.4 \end{array}$ | 15.9<br>16.1<br>16.7<br>15.1<br>15.9      | 13 8<br>15.1<br>15.1<br>13.9<br>14.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 15.3<br>15.7<br>15.9<br>14.7<br>15.1 | 34.2<br>33.5<br>32.7<br>34.9<br>36.1   | 9 0<br>10.1<br>10.5<br>10.5<br>11.5 | 8.5<br>9.2<br>8.0<br>8.8<br>9 7   | 8.8<br>9.6<br>9.4<br>9.7<br>10.8 | 131<br>129<br>126<br>139<br>147 | 96<br>95<br>77<br>91<br>94 | 114<br>109<br>100<br>119<br>121 | 43<br>42<br>45<br>43<br>46 | 38<br>37<br>38<br>37<br>39             | 41<br>40<br>41<br>39<br>42  | . 35.0<br>34.5<br>33.0<br>33.5<br>39.0                              | 27.0<br>27.5<br>26.0<br>29.0<br>27.0 | 31.0<br>30.0<br>29.7<br>31.2<br>32.3 |
| 117477/79<br>117495/97<br>117498/500<br>117501/03<br>117504/06 | 16<br>17<br>18<br>19<br>20 | $46.0 \\ 42.7 \\ 45.1 \\ 43.7 \\ 44.0$                              | 44.5<br>42.4<br>44.1<br>42.6<br>43.8                                | 45.0<br>42.6<br>44.5<br>43.3<br>43.9                                | 15.7<br>15 6<br>15.6<br>15.2<br>15.9      | $14.6 \\ 14.4 \\ 14.1 \\ 14.1 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ 14.7 \\ $ | 15.3<br>15.0<br>14.9<br>14.9<br>15.3 | $35.3 \\ 34.1 \\ 35.8 \\ 34.9 \\ 34.4$ | 11.9<br>9.0<br>7.7<br>6.7<br>8.6    | 10.9<br>7.6<br>6.5<br>6.3<br>7 8  | 11.4<br>8.2<br>7.3<br>6.6<br>8.1 | 128<br>120<br>133<br>142<br>124 | 71<br>67<br>82<br>91<br>88 | 112<br>104<br>110<br>107<br>110 | 45<br>42<br>46<br>47<br>48 | 38<br>35<br>40<br>38<br>39             | 42<br>38.<br>42<br>42<br>43 | 35.0<br>35.0<br>39.0<br>42.0<br>41.0                                |                                      | 32.1<br>32 1<br>35.5<br>34.5<br>33.6 |
| 117507/09<br>117510/12                                         | 21<br>22·                  | $45.6 \\ 44.8 \\ .$                                                 | 44.0<br>43.6                                                        | 45.0 <sup>7</sup><br>44.1                                           | $\begin{array}{c} 16 \\ 16.1 \end{array}$ | $\begin{array}{c} 15.0\\ 14.8\end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 15.6<br>15.6                         | 34,6<br>33,9                           | 8.5<br>9.7                          | 6.4<br>7.5                        | 7.6<br>8.4                       | 143<br>+ 141                    | 85<br>81                   | 108<br>110                      | 46<br>49                   | $\begin{array}{c} 40\\ 41 \end{array}$ | $\frac{43}{44}$             | $\begin{array}{c} 40.0\\ 37.0 \end{array}$                          | 30.0<br>25.0                         | 34.5<br>30.3                         |
| Average                                                        |                            |                                                                     |                                                                     | 43,5                                                                |                                           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 15.3                                 | 34.2                                   |                                     |                                   | 8.4                              |                                 |                            | 109                             |                            |                                        | 41                          |                                                                     |                                      | 30 9                                 |

#### TABLE LXVIII

الموجود المجتمع المتدرية المحمر . الأجهادة المحمد المتدرية الم

PHYSICAL CHARACTERISTICS OF 42-LB. D.F B.S. FOURDRINTER KRAFT LINER

## MILL H

|                                      | le Corr<br>ion, lb                   |                                      |                                  | Elmer                            | ulorf T                           | 'ear, g.,                         | /sheet                           |                                  |                                      | ٨m                                   | thor Te                              | nsile, lb                             | /in.                                 |                                      | -                                            | Am                                      | thor S                          | stretch,                          | %                                       |                                 |                        | +- |
|--------------------------------------|--------------------------------------|--------------------------------------|----------------------------------|----------------------------------|-----------------------------------|-----------------------------------|----------------------------------|----------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------------|--------------------------------------|--------------------------------------|----------------------------------------------|-----------------------------------------|---------------------------------|-----------------------------------|-----------------------------------------|---------------------------------|------------------------|----|
|                                      | Across                               | <u></u>                              |                                  | In                               |                                   |                                   | Across                           |                                  |                                      | İn                                   |                                      |                                       | Across                               |                                      |                                              | ĺn                                      |                                 |                                   | Across                                  | 5                               |                        |    |
| Max.                                 | Min.                                 | Av.                                  | Max.                             | Min.                             | Av.                               | Max.                              | Min.                             | Av.                              | Max.                                 | Min.                                 | Av.                                  | Max.                                  | Min.                                 | Av.                                  | Max.                                         | Min.                                    | Av.                             | Max.                              | Min                                     | Av.                             | Roll                   |    |
| 27.5<br>27.0<br>32.0<br>29.0<br>29.5 | 20.5<br>20.5<br>21.0<br>23.5<br>23.5 | 25.4<br>24.5<br>25.7<br>25.4<br>26.1 | 536<br>528<br>424<br>-432<br>384 | 400<br>424<br>352<br>-352<br>304 | 449<br>481<br>390<br>397 -<br>340 | 504<br>512<br>472<br>- 424<br>472 | 392<br>360<br>352<br>344-<br>352 | 452<br>427<br>400<br>371<br>405  | 88.0<br>71.1<br>91.4<br>73:0<br>93.1 | 60.9<br>54.2<br>57.4<br>54.0<br>69.4 | 73.5<br>62.7<br>69.2<br>6319<br>80.0 | 56.5<br>58.7<br>53.5<br>58.7<br>48.4  | 28.1<br>33.4<br>36.9<br>41.6<br>36.1 | 47.8<br>50.3<br>45.7<br>49.7<br>42.5 | 2.9<br>3.9<br>3.3<br>2.7<br>2.5              | 2.0<br>1.6<br>1.4<br>1.5<br>1.2         | 2.5<br>2.3<br>2.0<br>2.0<br>2.1 | 5.8                               | 2.1                                     | 3.8<br>4.4<br>4.4<br>4.5<br>3.7 | 1<br>                  |    |
| 25.5<br>25.0<br>26.0<br>26.5<br>26.0 | 19.0<br>18.0<br>20.5<br>21.5<br>20.0 | 22.7<br>23.9<br>24.4                 | 392<br>400<br>416<br>384<br>432  | 320                              | 339<br>346<br>373<br>360<br>378   |                                   | 320<br>360<br>336<br>344<br>352  | 391<br>405<br>389<br>393.<br>400 | 96.5<br>84.3<br>93.1<br>96.5<br>93.1 | 63.1<br>67.0<br>67.7<br>66.0<br>69.4 | 79.5<br>75.9<br>80.5<br>80.9<br>80.8 | 45.4<br>41.8-<br>48.9<br>48.1<br>45.7 |                                      | 39.1<br>37.7<br>40.9<br>41.7<br>39.2 | 2.7<br>2 <del>.</del> 6<br>2.5<br>2.7<br>2.8 | 1.3<br>1.5<br>1.6<br>1.9<br>1.8         | 2.1<br>1.9<br>2.3<br>2.4<br>2.4 | 5.0<br>- 4.6<br>5.7<br>5.4<br>5.7 |                                         | $3.6 \\ 3.9 \\ 4.3$             | 6<br>7<br>8<br>9<br>10 |    |
| 26.5<br>28.5<br>28.0<br>27.0         | 21.0<br>23.0<br>22.0<br>23.5         | 23.7<br>24.8                         | 424<br>408<br>424<br>464         | 352<br>312<br>336                | 391<br>375<br>380<br>406          | 464<br>448<br>512<br>472          | 352<br>360                       | 409<br>406<br>• 431<br>420       | 96.5<br>93.1<br>94.8<br>91.4         | 57.6<br>71.1<br>67.7<br>49.1         | 80.0<br>82.1<br>79.1<br>73.7         | 46.0<br>45.4<br>47.4<br>45.5          | 34.5<br>32.2<br>32.2<br>29.8         | 41.0<br>40.2<br>41.3<br>40.3         | 2.8<br>2.7<br>2.7<br>2.9                     | $\begin{array}{c} 2.0\\ 1.7\end{array}$ | 2.3<br>2.4<br>2.3<br>2.3        | 5.8<br>5.4<br>5.5<br>6.0          | $\begin{array}{c} 2.1\\ 2.5\end{array}$ | $\frac{3.8}{4.4}$               | 11<br>12<br>13<br>14   |    |
|                                      |                                      | 24.5                                 |                                  |                                  | 386                               |                                   |                                  | 407                              |                                      |                                      | 75.8                                 |                                       |                                      | 42.7                                 |                                              |                                         | 2.2                             |                                   |                                         | 4.1                             |                        |    |

## TABLE LXIX PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

#### MILL I

| Richle Compres-<br>sion, lb.                                                                                                                                                                                                                | Elmendorf Tear, j                                                                                                                                                                                                                          | g./sheet                                                                                     | Amthor Te                                                                                | nsile, lb./in.                                                                         | Amthor                                               | Stretch, %                                                                        |                            |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|------------------------------------------------------|-----------------------------------------------------------------------------------|----------------------------|
| Across                                                                                                                                                                                                                                      | In                                                                                                                                                                                                                                         | Across                                                                                       | In                                                                                       | Across                                                                                 | In                                                   | Across                                                                            |                            |
| Max, Min. Av.                                                                                                                                                                                                                               | Max. Min. Av. Ma:                                                                                                                                                                                                                          | x. Min. Av.                                                                                  | Max. Min. Av.                                                                            | Max. Min. Av.                                                                          | Max. Min. Av.                                        | Mxa. Min. Av.                                                                     | Roll                       |
| 26.5       17.5       22.4         26.5       16.0       21.2         23.5       17.5       20.6         25.5       17.0       20.8         24.0       15.0       20.3                                                                      | 464       360       418       56         480       392       428       59         496       368       422       62         512       392       434       49         464       360       411       54                                       | 2 416 473<br>4 448 506<br>6 448 470                                                          | 103.3 79.6 90.9<br>98.2 72.8 88.2<br>98.2 77.9 88.4<br>98.2 72.8 88.5<br>101.6 76.2 86.3 | 41.8 29.1 36.6<br>42.8 28.8 37.9<br>41.3 32.0 37.7<br>40.8 33.0 37.1<br>41.0 27.1 35.8 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                              | 1<br>2<br>3<br>4<br>5      |
| 24.0         13.0         20.3           24.5         19.5         22.5           25.5         18.0         20.4           24.5         17.0         21.5           25.0         20.0         21.9           23.0         16.5         20.4 | 456         360         401         56           456         368         408         57           456         376         407         48           520         352         411         52           448         360         405         53 | 0 400 462<br>6 424 487<br>8 408 443<br>0 368 442                                             | 94.8 74.5 85.3<br>96.5 77.9 87.5<br>85.3 67.4 78.6<br>91.4 69.4 81.9<br>93.1 72.8 83.9   | 44.2 33.5 38.0<br>41.1 31.5 35.3<br>42.0 30.5 36.6<br>41.8 30.5 37.1<br>41.6 29.6 36.5 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                              | 6<br>7<br>8<br>9<br>10     |
| 27.0 20.5 23.7<br>25.0 20.0 22.3<br>26.5 21.0 23.6<br>24.0 20.0 22.1<br>26.5 18.0 22.2                                                                                                                                                      | 424         352         390         53           496         352         422         59           472         336         390         48           432         328         394         52           488         392         431         54 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                         | 91.4 76.2 85.5<br>88.0 67.7 80.5<br>86 3 69.4 78.4<br>93 1 72.8 83.5<br>91.4 72.8 84.2   | 41.1 33.5 37.2<br>44.4 30.3 37.0<br>40.3 29.5 35.3<br>42.3 27.6 36.3<br>42.8 28.8 37.8 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                              | 11<br>12<br>13<br>14<br>15 |
| 24.0 17.0 21.9<br>21.0 15.0 18.6<br>24.0 19.5 21.9<br>24.5 19.5 22.1<br>28.5 20.0 22.0                                                                                                                                                      | 480 320 416 54<br>440 304 366 46<br>464 336 391 50<br>488 352 416 50<br>464 368 412 48                                                                                                                                                     | 14 440 491<br>54 368 430<br>54 400 453<br>54 416 451                                         | 94.8 52.5 85.6<br>94.8 66.0 82.5<br>99.9 76.2 89.6<br>98.2 79.6 86.9<br>98.2 71.1 87.0   | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                              | 16<br>17<br>18<br>19<br>20 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                       | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                                                                                                                                                                       | $ \begin{array}{r} 44 & 408 & 443 \\ 76 & 400 & 469 \\ \hline  & 465 \\ \hline \end{array} $ | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$                                    | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{r} 6.0 & 2.4 & 4.4 \\ 6.3 & 1.9 & 4.6 \\ \hline 4.5 \end{array} $ | 21<br>22                   |

#### TABLE LXX

PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

Mill J

|   |                                                                  |                            | Basis                | Weigl                                                               | ht, lb.              |                                       |                                      |                                         |                                      |                                    | _                               | _                                | F                                | Burstir                      |                                 | C F                          | Pune                             | ture;                          | 5                                    | le Com<br>sion, lb                   |                                      |
|---|------------------------------------------------------------------|----------------------------|----------------------|---------------------------------------------------------------------|----------------------|---------------------------------------|--------------------------------------|-----------------------------------------|--------------------------------------|------------------------------------|---------------------------------|----------------------------------|----------------------------------|------------------------------|---------------------------------|------------------------------|----------------------------------|--------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
|   | Institute                                                        |                            |                      | x 12/1                                                              |                      | Cali                                  | per, 0.0                             | 01 in.                                  | Apparent<br>Density,                 | M                                  | oisture,                        |                                  | Strer                            | igth, μ                      | oints                           | 0.17                         | units                            |                                |                                      | In                                   |                                      |
|   |                                                                  | Roll                       | Max.                 | Min.                                                                | Av.                  | Max.                                  | Min.                                 | Av.                                     |                                      | Max.                               | Min.                            | Av.                              | Max.                             | Min.                         | Av.                             | Max.                         | Min.                             | Av.                            | Max.                                 | Min.                                 | Av.                                  |
| - | 116857/59<br>116860/62<br>116863/65<br>116866/68<br>116869/71    | 1<br>2<br>3<br>4<br>5 -    | 43.6<br>42.2         | 39.4<br>43.1<br>41.4<br>40.9<br>40.4                                |                      | 15.6<br>14.8<br>16.0<br>15.9<br>-15.4 | $11.8 \\ 15.0$                       | 14.9<br>13.3<br>15.4<br>15.3<br>1476    | 32.0<br>39.2<br>32.6<br>32.5<br>33.8 | 11.1.<br>96<br>8.2<br>9.7<br>8.6   | 64<br>7.0<br>6.7<br>6.9<br>7.7  | 8.7<br>8.6<br>7.6<br>8.4<br>8.1  | 98<br>107<br>113<br>121<br>- 112 | 62<br>65<br>72<br>81<br>64   | 77<br>88<br>97<br>99<br>*82     | 35<br>32,<br>37<br>35<br>32  | 29<br>28<br>32<br>30<br>25       | 31<br>31<br>34<br>             | 32.0<br>35.0<br>32.5<br>33.5<br>36.5 | 25.0<br>21.5<br>25.0<br>25.5<br>25.0 | 28.2<br>27.9<br>28.9<br>29.5<br>30.2 |
|   | 116984/86<br>116987/89<br>116999/7001<br>117096/98<br>117099/101 | 6<br>7<br>8<br>9<br>10     | 41 5<br>41 0<br>42 2 | 41.3<br>41.1<br>39.9<br>41.0<br>40.4                                |                      | 16.0<br>15.3<br>14.3<br>14.9<br>15.1  | 13.6<br>13.4<br>14.1                 | 15.2<br>14.6<br>14 0-<br>14.5<br>- 14.7 | 32.7<br>33.9<br>34.7<br>34.5<br>33.1 | $9.1 \\ 8.1 \\ 11.5 \\ 6.2 \\ 4.9$ | 7.1<br>7.7<br>6.5<br>4.9<br>4.4 | 8.4<br>8.0<br>9.1-<br>5.7<br>4.6 | 100<br>110<br>- 94<br>98<br>97   | 68<br>69<br>- 64<br>63<br>66 | 78<br>83<br>82<br>79<br>78      | 31<br>33<br>- 32<br>31<br>31 | 25<br>29<br>27<br>27<br>27<br>25 | 28<br>31<br>- 30 -<br>29<br>28 | 35.0<br>36.0<br>35.0<br>35.0<br>33.0 | 27.0<br>30.0<br>26.5<br>29.5<br>25.0 | 30.0<br>32.9<br>30.4<br>32.2<br>29.0 |
|   | 117129/31<br>117152/54<br>117155/57<br>117158/60<br>117161/63    | 11<br>12<br>13<br>14<br>15 | 42.6<br>42.0<br>41.6 | 41.8<br>41.2<br>41.8<br>41.4<br>41.0                                | 42.1<br>41.9<br>41.5 | 16.0<br>15.7<br>15.5<br>15.5<br>15.5  | 14.6<br>14.5<br>14.7<br>14.4<br>14.5 | 15.2<br>15.2<br>15.1<br>14.9<br>14.9    | 33.1<br>33.2<br>33.3<br>33.4<br>33.6 | 8.8<br>7.1<br>8.2<br>6.6<br>8.9    | 6.8<br>5.2<br>6.7<br>6.0<br>7.7 | 7.7<br>6.0<br>7.5<br>6.2<br>8.2  | 124<br>101<br>106<br>103<br>121  | 72<br>63<br>80<br>64<br>75   | 96<br>83<br>92<br>87<br>100     | 37<br>33<br>32<br>32<br>33   | 31<br>27<br>27<br>27<br>30       | 34<br>30<br>30<br>30<br>31     | 36.0<br>33.0<br>33.5<br>34.0<br>37.0 | 26.5<br>27.0<br>29.5<br>24.5<br>30.5 | 30.6<br>29.9<br>31.7<br>29.4<br>33.4 |
|   | 117164/66<br>117305/07<br>117308/10<br>117311/13<br>117314/16    | 16<br>17<br>18<br>19<br>20 | 42.8<br>43.0<br>42.5 | $\begin{array}{r} 41.0 \\ 42.6 \\ 42.5 \\ 41.7 \\ 41.8 \end{array}$ | 42.7<br>42.8<br>42.2 | 15.2<br>14.9<br>14.8<br>14.6<br>14.3  | 14.2<br>14.0<br>13.6                 | 14.9<br>14.6<br>14.5<br>14.1<br>14.0    | 33.2<br>35.1<br>35.4<br>35.9<br>36.3 | 8.4<br>9:4<br>8.6<br>9.7<br>9.3    | 6.0<br>7.5<br>5.1<br>9.2<br>4.0 | 7.4<br>8.4<br>6.5<br>9.4<br>7.2  | 122<br>124<br>130<br>140<br>147  | 86<br>68<br>90<br>85<br>67   | 103<br>106<br>111<br>109<br>105 | 33<br>46<br>41<br>41<br>42   | 28<br>37<br>34<br>35<br>34       | 30<br>39<br>38<br>38<br>38     | 35.5<br>36.0<br>34.5<br>38.5<br>34.0 | 29.0<br>28.0<br>28.0<br>25.0<br>24.0 | 31.7<br>31.2<br>31.1<br>30.5<br>30.0 |
|   | 117317/19<br>Average                                             | 21                         | 42.6                 | 41.8                                                                | $\frac{42.2}{41.7}$  | 14.6                                  | 13.7                                 | $\frac{14.1}{14.7}$                     | $\frac{35.9}{34.2}$                  | 11.4                               | 8.5                             | $\frac{10.2}{7.7}$               | 123                              | 83                           | $\frac{108}{93}$                | 42                           | 34                               | $\frac{38}{32}$                | 38.5                                 | 25.5                                 | $\frac{30.3}{30.4}$                  |

TABLE LXXI

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

### MILL S

|                                                               |                        | Basis                                | Weigi                                | ht. lb.                              |                                      |                                   |                                      |                                                   |                                       |                                   |                                   | D                          | urstir                     |                            | CF                         | Punc                       | 61.00                      |                                      | le Con<br>ion, lb                    |                                      |
|---------------------------------------------------------------|------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|-----------------------------------|--------------------------------------|---------------------------------------------------|---------------------------------------|-----------------------------------|-----------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Institute                                                     |                        |                                      | x 12/1                               |                                      | Calip                                | er, 0 0                           | 01 in.                               | Apparent                                          | Mo                                    | oisture,                          | %                                 |                            |                            | oints                      |                            | units                      | ture,                      |                                      | In                                   |                                      |
| File No.                                                      | Roll                   | Max.                                 | Min.                                 | Av.                                  | Max.                                 | Min.                              | Av.                                  | <ul> <li>Density,<br/>lb./cu.ft.</li> </ul>       | Max.                                  | Min.                              | Av.                               | Max.                       | Min                        | . Av.                      | Max.                       | Min.                       | Av.                        | Max.                                 | Min.                                 | Av.                                  |
| 117275/77<br>117278/80<br>117281/83<br>117323/25<br>117326/28 | 1<br>2<br>3<br>4<br>5  | 28.0<br>28.1<br>28.0<br>27.6<br>27.6 | 27.0<br>27.2<br>27.0<br>26.6<br>26.8 | 27.5<br>27.8<br>27.6<br>27.1<br>27.3 | 10.0<br>10.2<br>10.1<br>10.9<br>10.8 | 9.0<br>9.4<br>9.4<br>10.0<br>9.9  | 9.6<br>9.9<br>9.7<br>10:5<br>10.3    | 34.4<br>33.7<br>34.1<br>31.0<br>31.8              | 5.3<br>7.2<br>7.0<br>12.0<br>11.0     | 1.6<br>5.2<br>6.1<br>11.1<br>8.3  | 3.4<br>6.2<br>6.4<br>11.5<br>9.6  | 96<br>85<br>78<br>95<br>99 | 49<br>46<br>44<br>54<br>55 | 72<br>66<br>64<br>71<br>69 | 23<br>22<br>21<br>23<br>23 | 18<br>19<br>18<br>19<br>19 | 21<br>20<br>20<br>21<br>21 | 22.0<br>26.0<br>22.5<br>26.0<br>24.5 | 16.0<br>17.0<br>17.0<br>14.5<br>16.0 | 19.5<br>21.2<br>19.7<br>19.7<br>19.8 |
| 117329/31<br>117332/34<br>117335/37<br>117414/16<br>117417/19 | 6<br>7<br>8<br>9<br>10 | 28.0<br>27.2<br>27.6<br>27.9<br>27.2 | 26.2<br>26.8<br>26.6<br>27.5<br>26.4 | 27.1<br>27.0<br>27.2<br>27.7<br>26.8 | 10.7<br>10.7<br>10.6<br>10.8<br>10.5 | 9.4<br>10.1<br>10.1<br>9.8<br>9.8 | 10-1<br>10.3<br>10.4<br>10.3<br>10.1 | 32.2<br>31.5<br>31.4<br>32 <sup>.</sup> 3<br>31.8 | $10.7 \\ 13.5 \\ 12.0 \\ 9.1 \\ 10.0$ | 8.9<br>11.1<br>11.8<br>2.5<br>7.3 | 9.8<br>12.3<br>11.9<br>4.9<br>8.5 | 95<br>85<br>86<br>84<br>84 | 43<br>43<br>45<br>52<br>50 | 71<br>64<br>70<br>69<br>67 | 23<br>23<br>21<br>23<br>21 | 19<br>19<br>18<br>19<br>18 | 21<br>21<br>19<br>21<br>19 | 22.0<br>21.0<br>21.5<br>22.5<br>20.5 | 16.0<br>17.5<br>17.0<br>17.0<br>16.0 | 18.5<br>19.0<br>19.4<br>19.4<br>18.4 |
| Average                                                       |                        |                                      |                                      | 27.3                                 |                                      |                                   | 10.1                                 | 32.4                                              |                                       |                                   | 8.5                               |                            |                            | 68                         |                            |                            | 20                         |                                      |                                      | 19.5                                 |

# TABLE LXX

# PHYSICAL CHARACTERISTICS OF 42-LB. D.F.B.S. FOURDRINIER KRAFT LINER

## MILL J

| Acr     | oss    |      | Īn       | *     |      | Acros |       |                |                     |      | nsile, lb |        | <u> </u>     |                   |      |                   | Stretch, | 70    | -                 |          |
|---------|--------|------|----------|-------|------|-------|-------|----------------|---------------------|------|-----------|--------|--------------|-------------------|------|-------------------|----------|-------|-------------------|----------|
|         |        |      | <u> </u> |       | _    | ACIUS |       | <u> </u>       | In                  |      | <b>_</b>  | Across | s<br>        |                   | In   |                   |          | Acros | s                 |          |
| fax. Mi | n. Av. | Max. | Min      | . Av. | Max. | Min   | . Av. | Max.           | Min.                | Av.  | Max.      | Min.   | Av.          | Max.              | Min. | Av.               | Max.     | Min.  | . Λv.             | Rol      |
| 7.0 23. |        | 384  | 256      | 320   | 384  | 280   | 339 - | 67.0           | 51.1                | 59.1 | 45.2      | 30.8   | 38.3         | 2.0               | 1.0  | 1.0               |          |       |                   |          |
| 5.0 18. |        | 376  | 248      | 288   | 400  | 288   | 344   | 78.7           | 58.7                | 70.6 | 37 2      | 31.5   | 34.3         | $\frac{2.9}{2.6}$ | 1.2  | 1.9               | 4.7      | 1.6   | 3.1               | 1        |
| 6.5 19. |        | 408  | 240      | 319   | 456  | 320   | 378   | 83.3           | 69.1                | 76.5 | 42.3      | 33.9   | 38.2         | 2.0               | 1.1  | 1.7               | 3.6      | 2.0   | 2.8               | 2        |
| 7.5 22. |        | 392  | 256      | 324   | 408  | 320   | 368   | 83.5           | 63.5                | 75.5 | 42.8      | 35.6   | 38.2         |                   | 1.6  | $\frac{2.0}{2.0}$ | 4.0      | 1.9   | 2.8               | 3        |
| 5.0 20. | 5-22.4 | 320  | - 232    | -277  | 384* | 288   | -334  | 75.3           | 60.9                | 68.8 | 38.1      | 30.8   | 34.4         | 2.4<br>2.5        | 1.2  | 2.0               |          | 2.0   | 2.7-              | 4        |
| 3.5 21. | 0 24.1 | 296  | 184      | 247   | 344  | 240   | 294   |                |                     |      |           |        |              | 4.5               | 1.2  | 1.6               | 3.0      | 1.7   | 2.4               | 5        |
| 5.0 20. |        | 336  | 232      | 288   | 384  | 240   | 324   | 69.4           | 55 9                | 64.2 | 37.4      | 26 6   | 33.5         | 2.9               | 1.7  | 2.1               | 3.0      | 1.0   | 2.4               | 6        |
| 7.5 19. |        | 320  |          | 274   | -368 | 272   |       | 78.0           | 62.6                | 69.2 | 34.5      | 27.9   | 32.0         | 2.4               | 1.3  | 2 0               | 3.8      | 2.0   | 3.0               | 7        |
| 5.0 20. |        | 272  | 208      | 236   | 360  | 256   | 291   | · 77.7<br>74.0 | $\frac{58.4}{59.4}$ | 68.5 | 36.9      | 29.6   | 33.1         | 2.5               | 1.3  | 2.1               | 4.6      | 2.6   | 3.3               | 8        |
| 9.5 22. |        | 256  | 168      | 214   | 304  | 240   | 276   | 74.0           |                     | 68.2 | 36.7      | 30.6   | 33.6         | 2.3               | 1.5  | 1.9               | 4.2      | 2.0   | 3.1               | - 9      |
| E E 10  |        |      |          |       |      |       |       |                | 58.4                | 66.8 | 39.3      | 27.1   | 34.1         | 2.3               | 1.6  | 2.0               | 3.4      | 1.8   | 2.5               | 10       |
| 5.5 19. |        | 328  | 248      | 290   | 400  | 328   | 370   | 84.7           | 63.8                | 75.7 | 38.4      | 30.5   | 34.3         | 2.4               | 1.4  | 2.0               | 3.8      | 1.8   | 3.0               |          |
| 3.5 20. |        | 352  | 256      | 301   | 408  | 296   | 352   | 79.6           | 60.4                | 68.6 | 38.4      | 30.8   | 34.7         |                   | 1.6  | 2.0               | 3.3      | 1.6   | 2.3               | 11<br>12 |
| 5.5 24. |        | 352  | 256      | 298   | 352  | 304   | 331   | 76.9           | 57.6                | 67.5 | 43.3      | 35.7   | 38.6         | 2,3               | 1.5  | 2.0               | 3.7      | 2.3   | $\frac{2.3}{3.0}$ | 13       |
| .5 22.  |        | 352  | 224      | 302   | 384  | 296   | 339   | 76.0           | 59.8                | 69.2 | 40.6      | 31.0   | 36.6         | 2.1               | 1.5  | 1.8               | 3.7      | 2.0   | 2.9               |          |
| 5.5 22. | 5 24.4 | 352  | 280      | 318   | 448  | 352   | 381   | 86.3           | 67.7                | 77.8 | 41.3      | 33.9   | 36.9         | 2.6               | 1.7  | 2.3               | 4.5      | 1.8   | 3.2               | 14<br>15 |
| 5.5 22. |        | 360  | 264      | 318   | 416  | 328   | 361   | 94.8           | 71.1                | 80.0 | 39.6      | 33.0   |              |                   |      |                   |          |       |                   |          |
| 1.0 21. |        | 392  | 328      | 362   | 456  | 392   | 423   | 99.9           | 79.6                | 92.2 | 45.0      | 33.0   | 36.2         | 2.6               | 1.8  | 2.2               |          | 1.9   | 3.1               | - 16     |
| 5.0 21. |        | 368  | 320      | 338   | 456  | 352   | 403   | 99.9           | 76.2                | 92.0 | 40.6      | 34.0   | 37.2         |                   | 1.9  | 2.4               |          | 3.5   | 4.3               | 17       |
| .5 18.  |        | 368  | 296      | 331   | 424  | 384   | 400   | 93.1           | 66.0                | 84 3 | 40.0      | 30.5   | 37.8<br>36.4 |                   | 1.9  | 2.3               |          | 3.5   | 4.4               | 18       |
| .5 20.  | 5 24.8 | 400  | 304      | 344   | 456  | 352   | 412   | 96.5           | 62.6                | 85.8 | 40.8      | 31.3   | 30.4<br>36.1 |                   | 1.8  | 2.2               |          | 1.9   | 4.2               | - 19     |
| .0 21.  | 0 23.5 | 384  | 304      | 338   | 440  |       |       |                |                     |      |           |        |              | 3.1               | 1.4  | 2.3               | 5.2      | 2.8   | 4.3               | 20       |
|         |        | 304  | 304      | 330   | 448  | 376   | 412   | 101.6          | 67.7                | 90.8 | 41.8      | 34.5   | 39.3         | 2.6               | 1.4  | 2.2               | 5.5      | 2.9   | 4.1               | 21       |
|         | 23.7   |      |          | 301   |      |       | 255   |                |                     |      |           |        | •            |                   |      | —                 |          | ,     |                   |          |
|         |        |      |          | 301   |      |       | 355   |                |                     | 74.8 |           |        | 35.9         |                   |      | 2.0               |          |       | 3.2               |          |

TABLE LXXI PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

MILL S

| Across         II           Max. Min. Av.         Max. M           16.5         11.5         14.8         284         22           19.0         13.5         15.6         294         22           16.5         11.0         14.3         278         22           18.0         12.0         14.4         306         25           19.0         13.0         15.2         328         26           19.0         12.5         15.9         282         24           18.0         13.5         15.6         348         25 |                                                                      | Ac                                                                                                                                                                                    |                                                                                                         |                                                                              |                                                                                                    |                              |                      | ./in.  |                                                                                      |                          | - An | athor !                                                                 | stretch,                                      | %                                                    |                     |                                                 |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|------------------------------|----------------------|--------|--------------------------------------------------------------------------------------|--------------------------|------|-------------------------------------------------------------------------|-----------------------------------------------|------------------------------------------------------|---------------------|-------------------------------------------------|
| $            \begin{array}{ccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                                                                      |                                                                                                                                                                                       | ross                                                                                                    |                                                                              | Jn                                                                                                 |                              |                      | Across | <br>;                                                                                | <u> </u>                 |      |                                                                         |                                               | Across                                               |                     |                                                 |
| 19.0       13.5       15.6       294       22         16.5       11.0       14.3       278       22         18.0       12.0       14.4       306       25         19.0       13.0       15.2       328       26         19.0       12.5       15.9       282       24                                                                                                                                                                                                                                                    | in. Av.                                                              | Max. N                                                                                                                                                                                | lin. Av.                                                                                                | Max.                                                                         | Min.                                                                                               | Av.                          | Max.                 | Min.   | Av.                                                                                  | Max.                     | Min. | . Av.                                                                   | Max.                                          | <u> </u>                                             |                     | Roll                                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 6 253<br>6 250<br>2 281<br>0 288<br>0 265<br>6 279<br>2 287<br>2 265 | 288         2           288         2           286         2           340         2           364         2           356         2           332         2           308         2 | 44 268<br>54 270<br>48 269<br>46 269<br>40 282<br>52 286<br>72 300<br>56 285<br>44 269<br>34 261<br>276 | 63.5<br>64.3<br>67.4<br>66.0<br>58.9<br>62.5<br>56.7<br>57.1<br>60.1<br>60.9 | $\begin{array}{r} 41.6\\ 49.1\\ 41.1\\ 41.5\\ 38.1\\ 41.5\\ 39.6\\ 41.6\\ 40.6\\ 46.2 \end{array}$ | 57.2<br>53.9<br>49.7<br>50.0 | 32.2<br>32.5<br>34.7 | -010   | 27.9<br>28.9<br>28.5<br>30.1<br>29.5<br>30.7<br>31.6<br>31.0<br>33.4<br>31.9<br>30.4 | 2.4<br>2.3<br>1.8<br>1.8 |      | $1.7 \\ 1.8 \\ 1.7 \\ 1.6 \\ 1.5 \\ 1.6 \\ 1.5 \\ 1.5 \\ 1.5 \\ 1.7 \\$ | 6.2<br>7.7<br>6.3<br>7.0<br>6.4<br>6.6<br>6.5 | 4.0<br>2.9<br>2.6<br>2.0<br>2.6<br>2.6<br>3.0<br>2.6 | $5.1 \\ 4.8 \\ 4.6$ | 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10 |

## TABLE LXXH

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

, myste

· Y27 4

## Mill T

|                     |      | Basis | -Weig}<br>x 12/10 |        | ,    | er, 0.0 | <br>01 in | Apparent | · - · | <br>visture, | -<br>07. |               | urstin |    |      | Punc          | ture,          |      | le Com<br>sion, lb | ·<br> |
|---------------------|------|-------|-------------------|--------|------|---------|-----------|----------|-------|--------------|----------|---------------|--------|----|------|---------------|----------------|------|--------------------|-------|
| istitute<br>ile No. | Roll | Max.  | ·····             | ,      | Max  |         | Av.       | Density, |       |              |          | Stren<br>Max. |        |    | Max. | units<br>Min. | Av.            | Max. | In<br>Min.         | Av.   |
| 3078/80             | 1    | 30 9  | 28.0              | 29.5   | 11.9 | 10.7    | 11.2      | 31.6     | 11.6  | 9.4          | 10.8     | 60            | 36     | 47 | 24   | 19            | 22             | 16 0 | 11.5               | 14.2  |
| 081/83              | 2    | 30.0  | 29.2              | 29.5   | 13.1 | 10.7    | 11.8      | 30.0     | 13.8  | 10.8         | 12.5     | 68            | 31     | 43 | 26   | 18            | $\frac{1}{23}$ | 15.5 | 11.5               | 13.7  |
| 084/86              | 3    | 26.3  | 25.2              |        | 10.2 | 8.9     | 9.5       | 32.7     | 14.4  | 12.4         | 13.3     | 74            | 43     | 61 | 22   | 17            | 20             | 22.0 | 14.0               | 18.1  |
| )87/89              | 4    | 26.8  | 26.4              | 26.6   | 10.1 | _9.2    | 9.5       | _33.6    | 14.2  | 11.2         | 12.9     | 76            | 43_    | 63 | 23   | 17            | 20             | 19.5 | 14.0               | 16.9  |
| 90/92               | 5    | 27.7  | 26.0              | 26.6   | 10.2 | -9.4    | 9.8       | 32.6     | 13.0  | 11.8         | 12.5     |               | 42     | 59 | 22   | 17            | 19             | 21.0 | 13.0               | 16.7  |
| 93/95               | 6    | 27.0  | 25.8              | 26.4   | 10.0 | 9.0     | 9.7       | 32.7     | 12.9  | 11.9         | 12.6     | 75            | 51     | 63 | 23   | 18            | 19             | 22 5 | 13.0               | 15 5  |
| 196/98              | 7    | 28.3  | 26.3              | 27.1   | 10.4 | 9.4     | 9.9       | 32.8     | 13 8  | 9.1          | 10.8     | 76            | 41     | 55 | 20   | 14            | 18.            | 21.0 | 13.0               | 17.1  |
| 199/101             | - 8- | 27.2- | 25.2              | 26.4 - | 10.0 | 8.7     | - 9.3     | 34.1 -   | 13:1  | - 9.6        | 11.4     | 78            | - 47   | 62 | 22   | 17            | 19             | 19.0 | 11.0               | 15.3  |
| 102/04              | 9    |       | 24 4              | 25.9   | 10.4 | 9.0     | 9.7       | 32.0     | 12.1  | 9.5          | 10.9     | 74            | 32     | 58 | 23   | 17            | 20             | 20.0 | 11.0               | 15.9  |
| 105/07              | 10   | 27.4  | 25.3              | 26.4   | 10.0 | 9.1     | 9.5       | 33.3     | 11.6  | 10.0         | 10.7     | 73            | 49     | 60 | 20   | 15            | 18             | 22.5 | 11.0               | 15.8  |
|                     |      |       |                   | 27 0   |      |         | 40.0      |          |       |              |          |               |        |    |      |               | —              |      |                    |       |
| erage               |      |       |                   | 27.0   |      |         | 10.0      | 32.5     |       |              | 11.8     |               |        | 57 |      |               | 20             |      |                    | 15.9  |

#### TABLE LXXIII

## PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

Mill U

|                              |                                             |                            | Basis                                        | ; Weigh                                | ıt, lb.                              |                                      |                                     |                                                                     |                                      |                                    |                                       |                                   | в                          | urstin                     | œ                          | СF                         | Punci                      | 1170                       |                                      | le Com<br>sion, lb                   |                                      |
|------------------------------|---------------------------------------------|----------------------------|----------------------------------------------|----------------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|---------------------------------------------------------------------|--------------------------------------|------------------------------------|---------------------------------------|-----------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Inst                         | itute                                       |                            |                                              | x 12/10                                |                                      | Caliı                                | er, 0.00                            | D1 in.                                                              | Apparent<br>Density,                 | Mo                                 | oisture,                              | %                                 |                            | gth, p                     |                            |                            | units                      | cure,                      |                                      | In                                   |                                      |
|                              | No.                                         | Roll                       | Max.                                         | Min.                                   | Av.                                  | Max.                                 | Min.                                | Av.                                                                 | lb./cu.ft.                           | Max.                               | Min.                                  | Av.                               | Max.                       | Min.                       | Av.                        | Max.                       | Min.                       | Av.                        | Max.                                 | Min.                                 | Av.                                  |
| 1163<br>1170<br>1170         | 81/83<br>84/86<br>24/26<br>27/29<br>30/32   | 1<br>2<br>3<br>4<br>5      | 26.5<br>25.4<br>27.5<br>27.5<br>27.5<br>28.0 | $26.2 \\ 24.5 \\ 26.3 \\ 26.4 \\ 26.7$ | 26.3<br>25.0<br>26.9<br>26.9<br>27.4 | 11.4<br>11.5<br>11.9<br>10 1<br>10.3 | 99<br>9.1<br>10.7<br>9.4<br>9.7     | 10.7<br>9.7<br>11.4<br>9.9<br>10.0                                  | 29.5<br>30.9<br>28 3<br>32.6<br>32.9 | 12.1<br>12.0<br>9.2<br>9.6<br>11.2 | $11 \ 0 \\ 10.5 \\ 8.0 \\ 8.1 \\ 6.6$ | 11.6<br>11.3<br>8.7<br>9.0<br>8.3 | 88<br>90<br>75<br>71<br>83 | 65<br>52<br>55<br>54<br>46 | 74<br>70<br>62<br>63<br>61 | 22<br>19<br>22<br>23<br>26 | 18<br>17<br>17<br>20<br>18 | 21<br>18<br>20<br>22<br>22 | 20.0<br>20.5<br>23.0<br>24.5<br>22.0 | 13.0<br>12.5<br>14.5<br>18.0<br>14.0 | 16.8<br>16.6<br>19.9<br>20.1<br>18.6 |
| 1170<br>1175<br>1175         | 33/35<br>36/38<br>13/15<br>16/18<br>19/21   | 6<br>7<br>8<br>9<br>10     | 27.8<br>26.5<br>26.8<br>27.7<br>27.7         | 26.8<br>25.7<br>24 7<br>26.2<br>26.6   | 27.2<br>26.2<br>26.0<br>27.2<br>27.1 | 12.2<br>9.9<br>10.8<br>11 5<br>11.5  | 10 7<br>9.0<br>9.5<br>10.1<br>9.9   | 11.5<br>9.4<br>10.1<br>10.7<br>10.4                                 | 28.4<br>33.4<br>30.9<br>30.5<br>31.3 | 11.8<br>9.5<br>94<br>8.3<br>100    | 8.1<br>8.9<br>7.9<br>7.0<br>9.0       | 9.7<br>9.1<br>8.8<br>7.7<br>9.4   | 74<br>70<br>85<br>87<br>84 | 54<br>45<br>19<br>55<br>55 | 64<br>59<br>65<br>68<br>68 | 23<br>22<br>20<br>21<br>22 | 18<br>17<br>17<br>18<br>16 | 21<br>19<br>19<br>20<br>19 | 27.0<br>24.0<br>22.5<br>26.5<br>24.0 | 16.5<br>17.5<br>17.0<br>20.5<br>19.5 | 21.5<br>21.6<br>19.3<br>23.4<br>22.0 |
| 1175)<br>1177)<br>1177)      | 25/27<br>22/24<br>80/82<br>83/85<br>86/88   | 11<br>12<br>13<br>14<br>15 | 28.8<br>28.8<br>26.0<br>28.6<br>28.6<br>28.4 | 26.0<br>27.9<br>24.0<br>27.2<br>27.6   | 27.6<br>28.5<br>25.1<br>27.8<br>28.1 | 11.8<br>12.0<br>11.4<br>11.5<br>11.4 | 10.4<br>11.1<br>9.9<br>10.3<br>10.7 | $\begin{array}{c} 11.2 \\ 11.6 \\ 10.5 \\ 10.9 \\ 11.0 \end{array}$ | 29.6<br>29.5<br>28.7<br>30.6<br>30.6 | 8.4<br>11.0<br>6.4<br>7.9<br>6.1   | 8.1<br>7.8<br>6.1<br>5.5<br>5.3       | 8.3<br>9.5<br>6.3<br>6.7<br>5.8   | 89<br>89<br>97<br>76<br>93 | 55<br>49<br>42<br>42<br>48 | 70<br>66<br>59<br>61<br>67 | 21<br>23<br>20<br>23<br>22 | 17<br>19<br>15<br>18<br>17 | 19<br>21<br>17<br>20<br>21 | 25.529 023.524.023.5                 | 15.5<br>15.5<br>15.5<br>18.5<br>14.5 | 20.9<br>21.1<br>19.4<br>20.5<br>19.1 |
| 1177<br>1177<br>1179<br>1179 | 89/91<br>92/94<br>95/97<br>95/97<br>98/8000 |                            | 27.5<br>28.0<br>26.2<br>26.9<br>28.0         | 26.4<br>27.2<br>26.0<br>25.4<br>27.1   | 26.8<br>27.6<br>26.1<br>26.3<br>27.5 | 10.8<br>11.6<br>11.2<br>12.3<br>12.8 | 99<br>10.6<br>9.9<br>9.8<br>10.9    | 10.4<br>11.0<br>10.3<br>10.9<br>11.6                                | 30.9<br>30.1<br>30.4<br>28.9<br>28.4 | 8.0<br>9 2<br>8.7<br>6.3<br>8.4    | 6.5<br>8.1<br>6.1<br>4.9<br>7.3       | 7.4<br>8.7<br>7.6<br>5.5<br>7.7   | 83<br>73<br>70<br>94<br>86 | 23<br>38<br>43<br>59<br>57 | 64<br>59<br>54<br>74<br>68 | 25<br>23<br>21<br>19<br>22 | 18<br>18<br>17<br>15<br>18 | 20<br>22<br>19<br>17<br>20 | 21.0<br>22.0<br>22 0<br>22.5<br>19.5 | 15.0<br>16.5<br>14.0<br>18.0<br>13 0 | 18.2<br>18.8<br>18.1<br>20.8<br>17.8 |
| Aver                         | 01/03<br>age                                | 21                         | 27.6                                         | 26.8                                   | $\frac{27.3}{26.9}$                  | 12.0                                 | 10,5                                | $\frac{11.4}{10.7}$                                                 | $\frac{28.7}{30.2}$                  | 9,1                                | 7.9                                   | 8.7                               | 86                         | 50                         | $\frac{69}{65}$            | 23                         | 18                         | $\frac{20}{20}$            | 21.5                                 | 15.0                                 | $\frac{18.4}{19.7}$                  |

TABLE LXXII

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

· MILL T

|     | Riehle Compres-<br>sion, lb. |                                             |                                                                                 |                            | Elmer                    | ndorf I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 'ear, g                   | /sheet                    |                                                                                                     | **<br>                        | Λm                           | thor Te                        | nsile, lb, | /in                          | ,<br>                   |                    | , An                                      | thor S                    | tretch,                   | % -   |                           | ••• - ·                                                                                                |       |
|-----|------------------------------|---------------------------------------------|---------------------------------------------------------------------------------|----------------------------|--------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------|---------------------------|-----------------------------------------------------------------------------------------------------|-------------------------------|------------------------------|--------------------------------|------------|------------------------------|-------------------------|--------------------|-------------------------------------------|---------------------------|---------------------------|-------|---------------------------|--------------------------------------------------------------------------------------------------------|-------|
| • • |                              | Across                                      |                                                                                 |                            | In                       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                           | Across                    |                                                                                                     | ,                             | In                           |                                |            | Across                       |                         |                    | In                                        |                           | .1                        | Cross | ,                         |                                                                                                        |       |
|     | Max.                         | Min.                                        | Av.                                                                             | Max                        | Min.                     | . Av.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | Max.                      | Min.                      | Av.                                                                                                 | Max.                          | Min.                         | Av.                            | Max.       | Min.                         | Av.                     | Max.               | Min                                       | Av.                       | Max.                      | Min   | Av.                       | Roll                                                                                                   |       |
|     | 14.0                         | 10 0<br>9.0<br>12.0<br>10.0<br>10.5<br>11 0 | 11.2<br>13.8<br>12.2<br>12.6                                                    |                            | 240<br>210<br>202<br>206 | 292<br>284<br>225<br>_224<br>226<br>211                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 252<br>260_               | 272<br>216<br>_216<br>236 | 326<br>304<br>231<br>238<br>266<br>248                                                              | 43.7<br>57.4<br>-55.9<br>52.5 |                              | 37.1<br>46.0<br>-48.7-<br>45.9 |            | 20-3                         | 19.2<br>24.9<br>-25.6 - | 2.0<br>2-2-<br>2.3 | 1 4.<br>1.2<br>1 0<br>-1-3-<br>1.6<br>1 5 | 1.6<br>1.5<br>-1-7<br>2.0 | 3.9<br>5 0<br>5-2-<br>5 3 | 2:3-  | 2.6<br>3.9<br>-3.8<br>4.0 | $     \begin{array}{c}       1 \\       2 \\       3 \\      4 \\       5 \\       6     \end{array} $ | •<br> |
| -   | 16.5<br>                     |                                             | $ \begin{array}{r} 13.6 \\ 14.1 \\ 12.9 \\ 13.0 \\ \hline 12.8 \\ \end{array} $ | 256<br>284<br>256<br>- 242 | ··· 204 ·<br>180         | $     \begin{array}{r}       242 \\       229 \\       214 \\       220 \\       \overline{} \\       \overline{ } \\       \overline{ } \\       \overline{ } \\$ | 284<br>258-<br>276<br>274 | 226<br>206<br>224         | $   \begin{array}{r}     259 \\     244 \\     246 \\     245 \\     \hline     261   \end{array} $ | 49 9                          | 35.4<br>39.6<br>32.3<br>39.3 |                                |            | 21.0<br>19.8<br>19.8<br>20.1 |                         |                    | 1.5<br>1.6<br>1.4<br>1.5                  | 1.8                       | 55.     51     4.6        | 2.1.  |                           | 7<br>8<br>-9<br>10                                                                                     | R     |

TABLE LXXIII

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

MILL U

.

| Riehle Compres-<br>sion, lb.                         | Elmendorf Tear, g./shcet                                                                   | Amthor Tensile, lb /in.                               | Amthor St                                                      | retch, %                                             |                            |
|------------------------------------------------------|--------------------------------------------------------------------------------------------|-------------------------------------------------------|----------------------------------------------------------------|------------------------------------------------------|----------------------------|
| Across                                               | In Across                                                                                  | · In Across                                           | In                                                             | Across                                               |                            |
| Max. Min. Av.                                        | Max. Min. Av. Max. Min. Av.                                                                | Max. Min. Av Max. Min. Av.                            | 'Max. Min. Av.                                                 | Max. Min. Av.                                        | Roll                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 278250264310264291272206225284220239240206224294244272300244276308254280294240264308250268 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1<br>2<br>3<br>4<br>5      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                       | $            \begin{array}{ccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 6<br>7<br>8<br>9<br>10     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                       | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 11<br>12<br>13<br>14<br>15 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                       | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 16<br>17<br>18<br>19<br>20 |
| $15.5  10.5  \underline{12.7} \\ 13.5 $              | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                       | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $\begin{array}{c} 2.2 & 1.3 & 1.8 \\ \hline & 2.0 \end{array}$ | $6.4 \ 2.8 \ \frac{4.6}{4.8}$                        | 21                         |

## TABLE LXXIV PHYSICAL CHARACTERISTICS OF .009/26-LB. BOGUS CORRUGATING MEDIUM

Mill V

| -+ + |                                                               |                            |                                       | • •                       |                      | • •-                                 |                    |                                  |                                       |                                    | · ++                                | • • •                                      |                             |                               | •                            | ,<br>م سببہ بھر             |                                   |                             |                                             | le Com<br>sion, lb                                                  |              |
|------|---------------------------------------------------------------|----------------------------|---------------------------------------|---------------------------|----------------------|--------------------------------------|--------------------|----------------------------------|---------------------------------------|------------------------------------|-------------------------------------|--------------------------------------------|-----------------------------|-------------------------------|------------------------------|-----------------------------|-----------------------------------|-----------------------------|---------------------------------------------|---------------------------------------------------------------------|--------------|
|      | <b>T</b>                                                      |                            |                                       | s Weigh<br>x 12/10        |                      | Calip                                | oer, 0.0           | 01 in.                           | Apparent                              | M                                  | oisture,                            | %                                          |                             | lurstin<br>Igth, p            |                              | G.E.                        | . Punc<br>units                   |                             |                                             | In                                                                  |              |
|      | Institute<br>File No.                                         | Roll                       | Max                                   | Min.                      | Av.                  | · Max.                               | Min.               | Av.                              | Density,<br>lb./cu.ft.                | Max.                               | Min.                                | Av.                                        | Max.                        | Min.                          | Av.                          | Max.                        | Min.                              | Av.                         | Max.                                        | Min.                                                                | Av.          |
|      | 116369/71                                                     | 1                          | 26.5                                  |                           | 26.0                 | 10.8                                 | 10.2               | 10.4                             | 30.0                                  | 9.2                                | 7.3                                 | 8.4                                        | 39<br>49                    | 26<br>· 29                    | 31<br>39                     | 9<br>14                     | 7                                 | 8                           | 15.5                                        |                                                                     | 12.9         |
|      | 116378/80<br>116673/75                                        | 23                         | $\frac{28}{26.6}$                     | $\frac{26.4}{26.1}$       | $27.3 \\ 26.4$       | 9.8<br>10.4                          | 8.9<br>9.6         | 9.4<br>10.0                      | $\frac{34.8}{31.7}$                   | 9.1<br>11.7                        | 7.7<br>7.9                          | $\begin{array}{c} 8.4 \\ 10.0 \end{array}$ | 39                          | 25                            | 39<br>31                     | 14                          | 10<br>8                           | 12<br>10                    | $\begin{array}{c} 16.0 \\ 14.0 \end{array}$ |                                                                     | 13.1<br>12 9 |
|      | 116676/78<br>116679/81                                        | 4<br>5                     | 24.6<br>25.9                          |                           |                      | 10.5<br>10.7                         | 9.6<br>10.0        | .9.9<br>10.4                     | 29.4<br>29.7                          | -12.3<br>10.5                      | -1171<br>9.7                        | 1177<br>10.1                               | 35 <sup></sup>              | 20<br>25                      |                              | 15<br>15                    | <u>8</u><br>10                    | 11<br>12                    | 13 <sup>-0-</sup><br>16.0                   | 10.0 <sup>-</sup><br>12.0                                           |              |
|      | 116682/84<br>116685/87<br>116966/68<br>116969/71<br>116972/74 | 6<br>7<br>- 8<br>- 9<br>10 | 26.8<br>-26.6<br>27.3<br>25.7<br>25.6 | 25:6-<br>26.6<br>24.9     | 26 1 -               | 10.1<br>10 7-<br>9.9<br>10.2<br>10.6 | 9.1<br>9.8         | 99<br>103<br>9.5<br>10.1<br>10.3 | 31.6<br>30.4<br>34.0<br>-30.0<br>29.1 | 10 7<br>-10.2<br>6.5<br>6.4<br>8.1 | 9.0<br>- 7:0<br>5.2<br>- 5 0<br>7.3 | 10.0<br>- 8.5<br>5.9<br>5.5<br>7.6         | 45<br>40-<br>41<br>35<br>39 | 31<br>-23<br>-26<br>-26<br>26 | 36<br>31<br>33<br>31 -<br>30 | 15<br>15-<br>13<br>15<br>13 | 10<br>- 10<br>- 10<br>- 10<br>- 9 | 11<br>13-<br>12<br>12<br>11 | 17.5<br>14.0-<br>17.0<br>13.5<br>17.5       | 10:0<br>12.5<br>10.5                                                |              |
|      | 117338/40<br>117341/43<br>117992/94                           | 11<br>12<br>13             | 26.3<br>25.6<br>27.1                  | $25.1 \\ 23.7 \\ 25.7 \\$ | 25.5<br>24.4<br>26 3 | $10.8 \\ 10.6 \\ 10.8$               | 10.1<br>9.7<br>9.8 | 10.5<br>10.1<br>10.3             | 29.1<br>29.0<br>30.6                  | 10.5<br>18.0<br>8.4                | 8.8<br>13.5<br>7.0                  | 9.8<br>15.5<br>7.9                         | 40<br>44<br>32              | 22<br>31<br>20                | 34<br>38<br>26               | 15<br>16<br>12              | 12<br>12<br>7                     | 13<br>13<br>10              | $15.0 \\ 15.5 \\ 14.5$                      | $   \begin{array}{r}     10.0 \\     9.5 \\     9.5   \end{array} $ |              |
|      | Åverage                                                       |                            |                                       |                           | 25.8                 |                                      |                    | 10.1                             | 30.7                                  |                                    |                                     | 9.2                                        |                             |                               | 32                           | •                           |                                   | 11                          |                                             |                                                                     | 12.9         |

## TABLE LXXV

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

## MILL W

|           |      | п .  | 1117-2-1         | 11.  |       |         |        |                      |      |          |                | п     |                  |      | G.E. | Dura  |      |      | e Com<br>ion, Ib |         |
|-----------|------|------|------------------|------|-------|---------|--------|----------------------|------|----------|----------------|-------|------------------|------|------|-------|------|------|------------------|---------|
| Institute |      |      | weigh<br>x 12/10 |      | Calir | er, 0.0 | 01 in. | Apparent<br>Density, | Mo   | oisture, | %              | Stren | urstin<br>gth, p |      |      | units | ure, |      | In               |         |
| File No.  | Roll | Max. | Min.             | Av.  | Max.  | Min.    | Av.    | lb./cu.ft.           | Max. | Min.     | Av.            | Max.  | Min.             | Av.  | Max. | Min.  | Av.  | Max. | Min.             | Av.     |
| 116411/13 | 1    | 28.6 | 27.1             | 28.0 | 10.2  | 9.5     | 10.0   | . 33.6               | 12.6 | 11.4     | 12.0           | 95    | 56               | 77   | 22   | 17    | 20   | 23.0 | 12.5             | 18.7    |
| 116414/16 | 2    | 28.3 | 27.7             | 28.0 | 10,9  | 10.1    | 10.5   | 32 0                 | 11.8 | 10.9     | 11.4           | 89    | 52               | 70   | 22   | 18    | 20   | 24 0 | 14.0             | 18 3    |
| 116417/19 | 3    | 27.6 | 27.3             | 27.5 | 10.5  | 9.7     | 10.2   | 32.4                 | 12.1 | 9.9      | 11.2           | 90    | 58               | 74   | 21   | 18    | 19   | 21.5 | 14.0             | 18.2    |
| 116420/22 | 4    | 28.0 | 26.9             | 27.4 | 11.3  | 10.5    | 11.0   | 29.9                 | 11.0 | 10.2     | 10.7           | 81    | 57               | 67   | 23   | 18    | 21   | 21.0 | 12.5             | 16.4    |
| 116423/25 | 5    | 28.3 | 27.1             | 27.6 | 12.3  | 10.1    | 10.9   | 30.4                 | 13.2 | 12.1     | 12.5           | 91    | 41               | 68   | 24   | 18    | 21   | 24.0 | 15.5             | 19.7    |
| 116435/37 | 6    | 26.3 | 25.5             | 25.9 | 9.3   | 8.8     | 9.0    | 34.5                 | 13.9 | 12.8     | 13.2           | 100   | 62               | 74   | 20   | 17    | 18   | 20.0 | 13.0             | 16.0    |
| 116438/40 | 7    | 25.7 | 25.1             | 25.4 | 9.4   | 8.8     | 9.1    | 33.5                 | 12.4 | 12.0     | 12.2           | 91    | 53               | 71   | 19   | 16    | 18   | 19.0 | 12.5             | 15.8    |
| 116441/43 | 8    | 26.4 | 25.0             | 25.7 | 9.3   | 8.7     | 9.1    | 33.9                 | 10.8 | 9.0      | 10.0           | 95    | 51               | 69 · | 20   | 16    | 18   | 21.0 | 14.0             | 17.3    |
| 117057/59 | 9    | 27.6 | 26.9             | 27.4 | 10,9  | 10.1    | 10.4   | 31.6                 | 14.5 | 11.7     | $13.5^{\circ}$ | 82    | 53               | 66   | 22   | 18    | 20   | 22.5 | 16.0             | 18.9    |
| 117072/74 | 10   | 26.8 | 25.5             | 26.2 | 10.9  | 9.8     | 10.4   | 30.2                 | 15.0 | 13.0     | 14.3           | 93    | 47               | 62   | 22   | 16    | 19   | 24.0 | 14.5             | 20.3    |
| 117081/83 | 11   | 26.7 | 25.6             | 26.0 | 9.9   | 8.9     | 9.4    | 33.2                 | 12.9 | 9.3      | 11.0           | 90    | 46               | 65   | 21   | 17    | 18   | 22.0 | 15.5             | 18.3    |
| 117747/49 | 12   | 27.7 | 26.8             | 27.2 | 11.3  | 9.9     | 10.6   | 30.8                 | 6.5  | 5.8      | 6.1            | 89    | 49               | 65   | 22   | 17    | 20   | 17.5 | 11.5             | 14.9    |
| 117750/52 | 13   | 27.7 | 25.8             | 26.5 | 11.0  | 9.0     | 10.2   | 31.2                 | 7.4  | 4.9      | 6.2            | 73    | 49               | 63   | 20   | 17    | 18   | 20.5 | 13.5             | 16.7    |
|           |      |      |                  |      |       |         |        |                      |      |          |                |       |                  |      |      |       |      |      |                  | 4 77 77 |
| Average   |      |      |                  | 26.8 |       |         | 10.1   | 31.8                 |      |          | 11,1           |       |                  | 69   |      |       | 19   |      |                  | 17.7    |

# TABLE LXXIV

# PHYSICAL CHARACTERISTICS OF .009/26-LB. BOGUS CORRUGATING MEDIUM

Mill V

n. . . . . . .

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| sion, lb.       | Elmendorf Tear  | r, g./sheet     | Amthor Ten       | sile, lb./in.  | Amthor St     | retch, %      |      |
|-----------------|-----------------|-----------------|------------------|----------------|---------------|---------------|------|
| Across          | In              | Across          | În               | Across         | In            | Across        |      |
| Max. Min. Av.   | Max. Min. Av. M | lax. Min. Av.   | Max. Min. Av.    | Max. Min. Av.  | Max. Min. Av. | Max. Min. Av. | Roll |
| 11.5 8.5 10.0   | 112 80 95 1     | 130 98 112      | 33.0 26.6 30.3   | 16.8 13.0 15.2 | 1.6 1.1 1.4   | 2.6 1.2 1.9   | 1    |
| 12.0 8.5 10.1   | 158 128 143 1   | 184 116 165     | 43.7 33.9 37.6   | 22.7 15.7 18.0 | 2.6 1.4 1.8   | 3.8 1.9 2.6   | 2    |
| . 11.0 7.0 9.3. | 154, 100 _1231  | 142_ 116_ 128 - | 34.2 27.9 . 30.3 |                | 1.8-1.1-1-5   |               | - 3  |
| 10.0 8.0 9.0    | 110 94 101 1    | 138 106 123     | 30.6 22.3 28.2   | 16.6 12.9 14.1 | 1.7 1.0 1.4   | 3.2 1 6 2 6   | 4    |
| 12.0 7.5 10.1   | 132 102 113 1   | 42 110 125      | 36.1 27.6 31.0   | 19.3 15.1 17.0 | 1.6 0.8 1.3   | 2.8 1.6 2.2   | 5    |
| 13.0 10.0 11.4  | 142 116 128 2   | 208 130 159     | 41.1 33.0 36.1   | 22.0 17.3 20.0 | 2.0 1.2 1.5   | 3.0 1 7 2.5   | 6    |
| 12.5** 875 10.3 | 136 100 115 1   | 164 108 129     | 36.4 25.7 31.4   | 19.8 14.6 18.0 | 1.7 0.5 1.2   | 3.2 1.6 2.4   | ž    |
| 11.5 6.5 9.9    | 150 118 133 1   | 194 136 157     | 40.0 29.6 35.5   | 17.6 14.4 16.4 | 1.2 0.8 1.0   | 3.9 1.8 2.5   | 8    |
| 15.0 11.0 12.6  | 170 120 146 1   | 152 106 132     | 27.3 21.7 24.3   | 26.6 19.0 23.8 | 1.6 1.0 1.3   | 3.4 1.4 2.7   | ğ    |
| 11.0 7.5 9.5    |                 | 152 116 127     | 37.9 25.6 31.8   | 16.9 11.2 14.4 | 1.6 0.9 1.3   | 3.8 1.8 2.2   | 1Ó.  |
| 12.5 10.0 11.2  | 162 112 133 1   | 160 124 144     | 32.2 23.7 28.8   | 20.3 16.4 17.8 | 2.0 1.1 1.6   | 2.9 1.2 2.2   | 11   |
| 12.5 9.0 10.9   | 180 116 141 1   | 60 120 140      | 32.2 28.8 30.9   | 20.8 15.4 18.2 | 2.2 1.4 1.8   | 3.0 1.6 2.3   | 12   |
| 11.0 7.0 9.3    | 102 74 89 1     | 112 90 100      | 30.8 22.5 27.1   | 15.7 12.4 13.7 | 1.6 1.0 1.4   | 2.5 1.6 2.1   | 13   |
|                 |                 |                 |                  |                |               |               |      |
| 10-3            | 121             | 134             | 31.0             | 17.2           | 1.4           | 2.4           |      |

## TABLE LXXV PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

#### MILL W

.

|      | le Con<br>sion, lb |      |      | Elmer | ndorf '  | Tear, g. | /sheet |     |      | Am   | thor Te | ensile, lb. | ./in. |      |          | An   | 1thor | Stretch, | %     |     |    |
|------|--------------------|------|------|-------|----------|----------|--------|-----|------|------|---------|-------------|-------|------|----------|------|-------|----------|-------|-----|----|
|      | Across             |      |      | In    |          |          | Across | ;   |      | In   |         |             | Acros | 5    | <u> </u> | In   |       |          | Acros | 5   | •  |
| Max. | Min.               | Av.  | Max. | Min.  | Av.      | Max.     | Min.   | Av. | Max. | Min. | Av.     | Max.        | Min.  | Av.  | Max.     | Min. | Av.   | Max.     | Min.  | Av. | Ro |
| 15.0 | 10.0               | 12.4 | 276  | 218   | 240      | 356      | 270    | 315 | 74.5 | 57.6 | 64.4    | 28.8        | 19.8  | 23.6 | 2.8      | 2.0  | 2.4   | 4.7      | 2.4   | 3.7 | 1  |
| 15.5 | 10.0               | 12:0 | 250  | 224   | 236      | 350      | 274    | 316 | 69,4 | 49.1 | 61.1    | 26.9        | 17.3  | 22.1 | 2.6      | 2.0  | 2.3   | 4.6      | 1.8   | 3.4 | 2  |
| 14.0 | 10.0               | 12.1 | 250  | 206   | 229      | 370      | 286    | 323 | 64.3 | 55.9 | 60.2    | 26.4        | 17.4  | 22.3 | 2.9      | 1.8  | 2.3   | 4.4      | 2.6   | 3.5 | 3  |
| 14.0 | 8.5                | 10.9 | 296  | 242   | 260      | 364      | 276    | 371 | 62.3 | 46.7 | 54.0    | 24.4        | 16.8  | 20.5 | 2.3      | 1.5  | 1.9   | 4.5      | 2.4   | 3.2 | 4  |
| 15.0 | 10.0               | 12.5 | 288  | 218   | 249      | 354      | 274    | 301 | 64.5 | 37.1 | 51.4    | 24.4        | 17.4  | 20.8 | 2.6      | 1.4  | 2.1   | 5.3      | 3.0   | 4.1 | 5  |
| 14.0 | 8.0                | 11.5 | 238  | 202   | 214      | 330      | 256    | 293 | 67.7 | 45.4 | 59.6    | 26.2        | 17.9  | 22.4 | 2.9      | 2.2  | 2.5   | 4.9      | 3.3   | 4.1 | 6  |
| 13.0 | 7.0                | 10.3 | 232  | 194   | 213      | 338      | 262    | 292 | 67.0 | 50.3 | 56.5    | 23.2        | 19.1  | 20.9 | 2.7      | 1.8  | 2.2   | 4.9      | 2.5   | 3.6 | 7  |
| 13.0 | 7.5                | 10.7 | 254  | 200   | 226      | 372      | 270    | 310 | 68.7 | 46.6 | 55.5    | 27.3        | 19.5  | 22.6 | 3.1      | 2.1  | 2.5   | 5.1      | 2.7   | 3.7 | 8  |
| 14.5 | 10.0               | 11.9 | 238  | 190   | 215      | 336      | 274    | 300 | 59.3 | 42.7 | 52.9    | 25.7        | 18.6  | 22.2 | 1.5      | 0.7  | 1.2   | 5.9      | 2.5   | 3.9 | 9  |
| 12.5 | 10.0               | 11.7 | 242  | 202   | 221      | 346      | 264    | 304 | 63.7 | 40.8 | 54.2    | 24.4        | 17.6  | 20.9 | 2.4      | 1.1  | 1.9   | 3.6      | 2.2   | 3.0 | 10 |
| 15.0 | 9.0                | 11.7 | 264  | 184   | 214      | 304      | 244    | 269 | 62.8 | 45.5 | 54.8    | 25.1        | 17.6  | 22.0 | 2.4      | 1.6  | 1.9   | 6.2      | 2.9   | 4.5 | 11 |
| 12.5 | 7.5                | 10.3 | 272  | 204   | 231      | 308      | 234    | 277 | 64.7 | 42.8 | 55.3    | 24.5        | 17.3  | 21.6 | 2.2      | 1.4  | 1.9   | 6.8      | 2.6   | 4.1 | 12 |
| 14.0 | 8.5                | 11.7 | 234  | 192   | 212      | 304      | 248    | 276 | 65.0 | 48.9 | 55.8    | 24.5        | 18.6  | 21.8 | 2.4      | 1.8  | 2.1   | 5.8      | 2.9   | 4.3 | 13 |
|      |                    |      |      |       | <u> </u> |          |        |     |      |      |         |             |       |      |          |      |       |          |       | —   |    |
|      |                    | 11.5 |      |       | 228      |          |        | 300 |      |      | 56.6    |             |       | 21.8 |          |      | 2.1   |          |       | 3.8 |    |

## TABLE LXXVI

PHVSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

### MILL X

| <b>•</b> •• - |        | Racio | Weig              | nt, lb.+- | <b>.</b> . |         |            | p                    |        |          |      | •• р  | urstin | 2    | CE   | Punct |      |       | le Com<br>sion, lb. |      | - |
|---------------|--------|-------|-------------------|-----------|------------|---------|------------|----------------------|--------|----------|------|-------|--------|------|------|-------|------|-------|---------------------|------|---|
| Institute     |        |       | $x \frac{12}{10}$ |           | Calip      | er, 0.0 | 01 in.     | Apparent<br>Density, |        | oisture, | %    | Stren |        |      |      | units | ure, |       | In                  |      |   |
| File No -     | Roll . | Max.  | Min.              | Av.       | Max.       | Min.    | Av.        |                      |        |          | Av.  | Max.  | Min.   | Av.  | Max. | Min.  | Av.  | Max.  | Min.                | Av.  |   |
| . 117117/19   | 1      | 26.8  | 25.8              |           | 9.5        | 9.0     | 9.3        | 33.9                 | 6.4    | 3.9      | 5.5  | 81    | 49     | 64   | 19   | 16    | 18   | 20.0  | 15.5                | 17.8 |   |
| 117120/22     | 2      | 28.4  | 26.2              | 27.1      | 9,9        | 9.1     | 9.5        | 34.2                 | 7.5    | 6.3      | 6.7  | 83    | 52     | 67   | 21   | 17    | 19   | 23.0  | 13.0                | 18.1 |   |
| 117284/86     | 3      | 26.5  | 25.6              | 26.0      | 9.6        | 8.9     | 9.2        | 33.9                 | 6.6    | 3.8      | 5.1  | 94    | 53     | 71   | 20   | 17    | 18   | 21.5  | 15.5                | 18.1 |   |
| 117287/89     | 4      | _27.1 | .25.3.            | 26.4      | 9.9        | . 8.9.  | .9.3.      |                      | . 6.2  | . 4.3    | 5.3. | 89+ - | 44     | 70 - | 21   | -17 - | - 19 | 21.0- |                     | 18.7 |   |
| 118051/53     | 5      | 28.4  | 26.6              | 27.4      | 11.2       | 10.2    | 10.7       | 30.7                 | 8.4    | 7.5      | 7.8  | 101   | 49     | 66   | 23   | 18    | 21   | 20.0  | 15.0                | 17.7 |   |
| 118054/56     | 6      | 29.3  | 26.2              |           | 12.0       | 10.2    | 10.7       | 30 6                 | 10.8   | 6.9      | 9.0  | 86    | 52     | 68   | 25   | 18    | 21   |       | 14.5                | 17.5 |   |
| 118057/59     | 7      | 29.2  | 26.2              | 27.3      | 9.6        | 8.9     | 9.1        | 36.0                 | 9.4    | 7.5      | 8.6  | 88    | 57     | 68   | 23   | 18    | 20_  | 20.0  | 15.5                | 17.2 |   |
| 118060/62     | 8"     | 29.3  | 2879              | 29.1      | -10.6      | 9.0     | 10.1       | 34.6                 | 9.8    | 8.4      | 9.1  | 75    | 48     | 63   | 26   | 21    | 24   | 18.0  | 13.0                | 15.7 |   |
| 118063/65     | 9      | 28.4  | 27.7              | 28.1      | 10.6       | 9.1     | 9.9        | 34.1                 | 8.7    | 7.5      | 8.2  | 94    | 57     | 68   | 25   | 20    | 23   | 19.0  | 13.0                | 16.2 |   |
| 118127/29     | 10     | 28.5  | 27.1              | 27.7      | 10.5       | 9.3     | 10.0       | 33.2                 | 12.8   | 11.5     | 12.0 | 79    | 47     | 67   | 24   | 18    | 21   | 18.5  | 13.0                | 14.7 |   |
| 118130/32     | 11 -   | 28 4  | 27.4              | 27.8      | 10.0       | 9.2     | 9.8        | 34.0                 | · 11.8 | 10:4     | 11.2 | 79    | 46     | 64   | 23   | 18    | 20   | 23.0  | 14.0                | 17.4 |   |
| 118133/35     | 12     | 29.5  | 26.8              | 28.1      | 10.3       | 9.0     | 10.0       | 33.7                 | 11.3   | 10.7     | 11.0 | 97    | 57     | 75   | 23   | 19    | 22   | 19.0  | 15.0                | 16.8 |   |
| 118136/38     | 13     | 29.5  | 27.8              | 28.5      | 9.9        | 9.0     | 9.5        | 36.0                 | 11.9   | 10.4     | 11.2 | 93    | 53     | 70   | 23   | 18    | 21   | 23.0  | 16.0                | 18.8 |   |
| 118139/41     | 14     | 28.3  | 25.0              | 26.7      | 10.7       | 9.2     | <u>9.9</u> | 32.4                 | 11.3   | 10.7     | 11.1 | 86    | 58     | 68   | 24   | 20    | 22   | 20.5  | 12.5                | 15.3 |   |
| Average       |        |       |                   | 27.4      |            | . 4     | 9.8        | 33.7                 |        |          | 8.7  |       |        | 68   |      |       | 21   |       |                     | 17.1 |   |
|               |        |       |                   |           |            |         |            |                      |        |          |      |       |        |      |      |       |      |       |                     |      |   |

## TABLE LXXVII

## PHYSICAL CHARACTERISTICS OF 009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

### Mill Y

1

|                                                               |                        | Basis                                | s Weigl                              | nt. Ib.                              |                                  |                                 |                                 | 1                                    |                                      |                                     |                                      | . в                        | urstin                     | a                          | C F                        | Punci                            | tura                       |                                      | le Com<br>ion, lb                    |                                      |
|---------------------------------------------------------------|------------------------|--------------------------------------|--------------------------------------|--------------------------------------|----------------------------------|---------------------------------|---------------------------------|--------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------------|----------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| Institute                                                     |                        |                                      | x 12/1                               |                                      | Cali                             | er, 0.0                         | 01 in.                          |                                      | M                                    | oisture                             | , %                                  |                            |                            | в<br>points                | 0.17.                      | units                            |                            |                                      | In                                   |                                      |
| File No.                                                      | Roll                   | Max.                                 | Min.                                 | Av.                                  | Max.                             | Min.                            | Av.                             | Density,<br>lb./cu.ft.               | Max.                                 | Min.                                | Av.                                  | Max.                       | Min.                       | Av.                        | Max                        | Min.                             | Av.                        | Max.                                 | Min.                                 | Av.                                  |
| 116990/92<br>116993/95<br>116996/98<br>117453/55<br>117456/58 | 1<br>2<br>3<br>4<br>5  | 26.0<br>26.0<br>25.8<br>26.4<br>27 2 | 24.6<br>25.4<br>25.0<br>25.7<br>26.0 | 25.4<br>25.7<br>25.3<br>26.0<br>26.8 | 9.4<br>9.1<br>9.5<br>9.8<br>10.6 | 8.9<br>8.4<br>8.9<br>8.9<br>9.1 | 9.1<br>8.9<br>9.1<br>9.5<br>9.8 | 33.5<br>34.6<br>33.4<br>32.8<br>32.8 | 7.5<br>9.9<br>10.2<br>15.0<br>8.0    | 6.6<br>7.1<br>3.9<br>9.5<br>6.0     | 7.2<br>8.9<br>6.8<br>11.7<br>7.3     | 55<br>82<br>61<br>92<br>98 | 40<br>58<br>39<br>57<br>58 | 48<br>70<br>48<br>72<br>73 | 17<br>14<br>16<br>19<br>19 | 12<br>12<br>13<br>15<br>15       | 15<br>13<br>14<br>17<br>18 | 22.5<br>27.5<br>20.0<br>20.0<br>23.0 | 15.5<br>21.0<br>13.5<br>15.0<br>16.0 | 18.5<br>24.2<br>17.0<br>16.9<br>18.7 |
| 118204/06<br>118207/09<br>118210/12<br>118213/15<br>118216/18 | 6<br>7<br>8<br>9<br>10 | 27.5<br>27.1<br>27.6<br>26.8<br>25.3 | 26.7<br>25.2<br>26.5<br>25.5<br>24.4 | 27.0<br>26.1<br>27.1<br>26.1<br>24.9 | 10.1<br>9.8<br>8.5<br>9.5<br>9.9 | 9.4<br>9.0<br>7.9<br>9.0<br>9.1 | 9.8<br>9.4<br>8.2<br>9.2<br>9.5 | 33.1<br>33.3<br>39.6<br>34.0<br>31.5 | 10.9<br>12.3<br>12.7<br>11.8<br>11.2 | 10.2<br>10.0<br>12.2<br>10.1<br>9.2 | 10.5<br>10.8<br>12.5<br>11.1<br>10.1 | 74<br>53<br>65<br>58<br>57 | 53<br>39<br>46<br>42<br>32 | 65<br>47<br>55<br>51<br>48 | 19<br>16<br>14<br>18<br>14 | 17<br>12<br>12<br>12<br>12<br>12 | 18<br>14<br>13<br>13<br>13 | 20.0<br>19.0<br>18.5<br>19.0<br>16.5 | 14.5<br>12.5<br>13.0<br>13.5<br>12.5 | 16.8<br>15.7<br>14.9<br>16.0<br>14.3 |
| Average                                                       |                        |                                      |                                      | 26.0                                 |                                  |                                 | 9.3                             | 33.9                                 |                                      |                                     | 9.7                                  |                            |                            | 58                         |                            |                                  | 15                         |                                      |                                      | 17.3                                 |

TABLE LXXVIII

## PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

#### MILL Z

|                                                                            |                         | Rasis                                        | Weigl                                        | ht Av                                        |                                          |                                        |                                         |                                              |                                          |                                        |                                        | IJ                                  |                                  |                                    | C F                              | Dune                             | *                                |                                              | le Com<br>sion, lb                           |                                              |
|----------------------------------------------------------------------------|-------------------------|----------------------------------------------|----------------------------------------------|----------------------------------------------|------------------------------------------|----------------------------------------|-----------------------------------------|----------------------------------------------|------------------------------------------|----------------------------------------|----------------------------------------|-------------------------------------|----------------------------------|------------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------------------------------|----------------------------------------------|----------------------------------------------|
| Institute                                                                  |                         |                                              | x 12/10                                      |                                              | Calip                                    | er, 0.0                                | 01 in                                   | Apparent                                     | М                                        | oisture,                               | %                                      |                                     | urstir<br>gth, p                 | oints                              | <b>G.</b> F.                     | . Punc<br>units                  | ture,                            |                                              | In                                           |                                              |
| File No.                                                                   | Roll                    | Max.                                         | Min.                                         | Av.                                          | Max.                                     | Min.                                   | Av.                                     | · Density,<br>lb./cu.ft.                     | Max.                                     | Min.                                   | Av.                                    | Max.                                | Min.                             | Av.                                | Max.                             | Min.                             | .\v.                             | Max.                                         | Min.                                         | Av.                                          |
| 116931/33<br>116934/36<br>116937/39<br>116940/42<br>117438/40<br>117441/43 | · 2<br>3<br>4<br>5<br>6 | 26.7<br>27.9<br>28.1<br>28.1<br>27.0<br>27.2 | 26.2<br>26.2<br>26.5<br>27.5<br>25.9<br>25.9 | 26 5<br>27.3<br>27.4<br>27.9<br>26.5<br>26.5 | 9.8<br>9.4<br>10.7<br>10.3<br>9.8<br>9.6 | 8.9<br>8.6<br>9.7<br>9.0<br>8.8<br>8.7 | 9.2<br>8.9<br>10.2<br>9.5<br>9.3<br>9.1 | 34.6<br>36.8<br>32.2<br>35.2<br>34.2<br>34.9 | 9.0<br>8.1<br>8.9<br>10.1<br>8.8<br>10.1 | 8.0<br>7.5<br>8.6<br>8.3<br>6.0<br>8.8 | 8.4<br>7.8<br>8.7<br>9.1<br>7.5<br>9.5 | 89<br>105<br>77<br>104<br>99<br>102 | 55<br>56<br>50<br>43<br>50<br>36 | - 70<br>78<br>65<br>85<br>73<br>77 | 20<br>20<br>25<br>22<br>22<br>22 | 17<br>17<br>20<br>20<br>18<br>17 | 19<br>19<br>22<br>21<br>20<br>19 | 23.0<br>33.0<br>21.0<br>33.0<br>26.0<br>24.0 | 18.0<br>18.0<br>14.5<br>16.0<br>17.5<br>15.5 | 20.2<br>21.4<br>17.1<br>21.0<br>21.3<br>20.8 |
| 117444/46<br>117447/49<br>117450/52<br>117465/67<br>117468/70              | 7<br>8<br>9<br>10<br>11 | 26.8<br>26.9<br>27.0<br>26.9<br>26.5         | 25.7<br>25.5<br>25.9<br>26.4<br>26.0         | 26.4<br>26.4<br>26.6<br>26.6<br>26.3         | 9.5<br>9.5<br>9.8<br>9.9<br>10.1         | 8.7<br>8.7<br>8.6<br>9.0               | 9.0<br>9.0<br>9.0<br>9.4<br>9.4         | 35.2<br>35.2<br>35.5<br>33.9<br>33.6         | 9.6<br>10.6<br>12.5<br>10.5<br>11.7      | 8.5<br>9.5<br>9.6<br>7.3<br>9.3        | 9.1<br>9.9<br>10.9<br>8.6<br>10.8      | 98<br>96<br>98<br>84<br>92          | 60<br>62<br>48<br>56<br>49       | 79<br>75<br>78<br>74<br>73         | 22<br>21<br>22<br>22<br>22<br>23 | 17<br>17<br>18<br>17<br>18       | 19<br>19<br>19<br>19<br>19<br>20 | 24.0<br>24.0<br>25.0<br>22.0<br>21.5         | 17.0<br>16.0<br>15.5<br>15.5<br>13.0         | 20.9<br>20.1<br>20.8<br>18.5<br>17.2         |
| Average                                                                    |                         |                                              |                                              | 26 8                                         |                                          |                                        | 9.3                                     | 34.7                                         |                                          |                                        | 9.1                                    |                                     |                                  | 75.                                |                                  |                                  | 20                               |                                              |                                              | 19.9                                         |

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

| $M_{I}$ | LL | х |
|---------|----|---|
|---------|----|---|

|                                                      | ile Con<br>sion, lb                                |                                                      |                                        | Elme                                           | ndorf '                                         | ſear, g.                                      | /shee                                  | t                               | · · -        | An                                                      | thor T                       | ensile, lb   | ./in                                 | <b>.</b>                                         | p                                       | .\1                                      | nthor                                                                                             | stretch;                                  | % -                                                                                  |                                         | - +                                                                                 |   |
|------------------------------------------------------|----------------------------------------------------|------------------------------------------------------|----------------------------------------|------------------------------------------------|-------------------------------------------------|-----------------------------------------------|----------------------------------------|---------------------------------|--------------|---------------------------------------------------------|------------------------------|--------------|--------------------------------------|--------------------------------------------------|-----------------------------------------|------------------------------------------|---------------------------------------------------------------------------------------------------|-------------------------------------------|--------------------------------------------------------------------------------------|-----------------------------------------|-------------------------------------------------------------------------------------|---|
|                                                      | Across                                             |                                                      |                                        | In                                             | ••••                                            |                                               | Acros                                  | s                               |              | In                                                      |                              |              | Across                               | 5                                                |                                         | l'n                                      | ·`                                                                                                |                                           | \cross                                                                               | - <b>-</b>                              |                                                                                     |   |
| Max.                                                 | Min.                                               | Λv.                                                  | Max.                                   | Min                                            | Av.                                             | Max                                           | Min                                    | . Av.                           | Max.         | Min.                                                    | Av.                          | Max.         | Min.                                 | Av.                                              | Max                                     | Min                                      | . Av                                                                                              | Max.                                      | Min                                                                                  | Av.                                     | Roll                                                                                | 1 |
| 15.0                                                 | 12.0<br>10.5<br>10.5<br>-10.5-                     | 12:9<br>13.4                                         | 268<br>236                             | 196<br>208<br>212<br>200-                      | 231<br>236<br>221<br>-210                       | 270<br>272                                    | 208                                    | 261                             | 58.9<br>65.0 | 41.5<br>41.8                                            | 51.8<br>51.9<br>53.9<br>56:7 | 26.7<br>27.4 | 19 5<br>20.1                         | .23.3                                            | $2.3 \\ 2.3$                            | $\begin{array}{c}1 \\ 1 \\ 3\end{array}$ | $     \begin{array}{c}       2 & 0 \\       1 & 9 \\       2 & 0 \\       - 2 & 0   \end{array} $ | 56<br>68                                  | $     \begin{array}{c}       2 & 6 \\       2 & 8 \\       2 & 6     \end{array}   $ | 4.2<br>4.5                              | 1                                                                                   |   |
| 13.5                                                 | 10.0                                               | 12 6                                                 | 274                                    | 226                                            | 249                                             | 342                                           | 262                                    | 298-                            | 62.0         | 46 4                                                    | 54.8                         |              | 1975<br>19.0                         |                                                  |                                         |                                          | -2.2<br>1 9                                                                                       |                                           | 3.0<br>2.9                                                                           |                                         | 4.5                                                                                 |   |
| 16.0<br>15.5<br>15.5<br>14.5<br>16.0<br>16.0<br>16.0 | 12.0<br>13.0<br>12.5<br>7.5<br>10.5<br>9.0<br>11.0 | 13.9<br>14.1<br>13.9<br>10.8<br>13:5<br>12.4<br>13.9 | 358<br>302<br>290<br>300<br>278<br>276 | 210,<br>262<br>270<br>220<br>232<br>232<br>234 | -248<br>302<br>289.<br>256<br>261<br>250<br>250 | 306<br>394<br>346<br>334<br>312<br>326<br>306 | 274<br>286<br>260<br>272<br>260<br>266 | 310<br>300<br>295<br>297<br>288 | . 58.9.      | - 39.6.<br>35.4<br>36.9<br>38.8<br>44.7<br>44.5<br>49.1 | 56.2<br>56.4<br>58.1         | - 34.7-      | 24.7<br>25:7<br>22.7<br>19.8<br>20 7 | - 29.6 -<br>30.1<br>29 3<br>25.5<br>25.0<br>25.3 | 2:8<br>2.4<br>3.7-<br>2.6<br>2.4<br>2.6 | -1-8<br>1.6<br>1.8<br>1.6<br>1.7<br>1.4  | 2.0<br>2.2<br>2.2                                                                                 | - 6 4-<br>3.3<br>3.6<br>6 1<br>7.2<br>5.0 |                                                                                      | -4:9<br>2 4<br>2,9<br>4.7<br>5.4<br>3.8 | $ \begin{array}{c}             6 \\             -7 \\             -7 \\           $ |   |
| 14.5                                                 | 10.5                                               | $\frac{12.2}{13.1}$                                  | 316                                    | 210                                            | $\frac{245}{250}$                               | 288                                           | 242                                    | $\frac{266}{281}$               | 55.4<br>,    | 35.6                                                    | $\frac{49.1}{52.1}$          | 30.5         | 19.1<br>、                            | $\frac{25.3}{25.3}$                              |                                         | 1.2                                      |                                                                                                   | 44                                        |                                                                                      | $\frac{3}{4},\frac{7}{4}$               | 14                                                                                  |   |

#### TABLE LXXVII

PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

#### Mill Y

| Riehle Compres<br>sion, lb.                          |                                                      | Tear, g./sheet                                       | Amthor T                                             | ensile, Ib./in.                                                                                                                                                        | • • Amthor                                                              | Stretch, %                                           |                        |
|------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------|------------------------------------------------------|------------------------|
| Across                                               | In                                                   | Across                                               | In                                                   | Across                                                                                                                                                                 |                                                                         | Across                                               |                        |
| 'Max. Min. Av                                        | Max. Min. Av.                                        | Max. Min. Av.                                        | Max. Min. Av.                                        | Max.º Min. Av.                                                                                                                                                         | Max. Min Av.                                                            | Max Min. Av                                          | Roll                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1 200 136 161<br>2 198 168 183<br>7 220 174 194      | 216 170 188<br>202 160 185<br>260 226 243,           | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                   | 2.8 1.6 1.9<br>3 2 2.0 2.3<br>2.5 1 5 2 1<br>2.5 1.6 2.2<br>2.2 1.3 1.9 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1<br>2<br>3<br>4<br>5  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 31.3       21.7       26.6         22.2       17.6       19.4         25.6       20.1       22.4         24.7       19.3       22.1         21.8       17.4       20.2 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                    | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 6<br>7<br>8<br>9<br>10 |
| 12                                                   | 3 189                                                | , 219                                                | 50.7                                                 | 22.1                                                                                                                                                                   | $\frac{1}{2.0}$                                                         | 3.6                                                  |                        |

## TABLE LXXVIII

# PHYSICAL CHARACTERISTICS OF .009/26-LB. FOURDRINIER KRAFT CORRUGATING MEDIUM

## MILL Z

| Riehle Compres-<br>sion, lb.                                                   | Elmendorf                                                                                                                                                                                | Tear, g./sheet                                                                                                                                                                      | ,<br>Amthor Te                                                                                                                                                               | ensile, lb /in.                                      | Amthor                                                                   | Stretch, %                                           |                        |
|--------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|--------------------------------------------------------------------------|------------------------------------------------------|------------------------|
| Across                                                                         | In                                                                                                                                                                                       | Across                                                                                                                                                                              | In                                                                                                                                                                           | Across                                               | In                                                                       | Across                                               |                        |
| Max. Min. Av.                                                                  | Max. Min. Av.                                                                                                                                                                            | Max. Min. Av.                                                                                                                                                                       | Max. Min. Av.                                                                                                                                                                | Max. Min. Av.                                        | Max. Min. Av.                                                            | Max. Min. Av                                         | Roll                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                           | 318 228 265<br>294 226 256<br>318 256 283<br>292 236 257<br>268 232 252                                                                                                                  | 280         220         248           312         230         269           368         276         316           376         264         295           268         210         243 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                         | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                     | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 1<br>2<br>3<br>4<br>5  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$                           | 320         220         244           258         202         226           252 <sup>-</sup> 208         231           254         206         231           278         236         257 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                | 64.0       39.8       53.4         73.3       44.0       57.8         72       1       37.8       55.9         70.3       40.6       57.1         56.9       42.7       49.4 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 2.7 2.0 2.3<br>2.5, 1.7 2.1<br>2.5 1.1 2.0<br>2.4 1.3 1.9<br>2.2 1.3 1.9 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 6<br>7<br>8<br>9<br>10 |
| $   \begin{array}{r} 17.0 & 10.0 & 14.2 \\                                   $ | $   \begin{array}{r}     290 & 248 & 262 \\     \hline     251   \end{array} $                                                                                                           | $   \begin{array}{r}     282 & 234 & 260 \\     \hline     262   \end{array} $                                                                                                      | $58.4  37  2  47  3 \\ \overline{53.8}$                                                                                                                                      | $38.9 \ 28.3 \ 33.1 \ \overline{33.0}$               | $3.2 \ 1 \ 8 \ 2 \ 1 \ - 2 \ 0$                                          | 7.1 2.8 $\frac{4.8}{4.7}$                            | t't                    |