#### GEORGIA INSTITUTE OF TECHNOLOGY

#### OFFICE OF CONTRACT ADMINISTRATION

#### PROJECT ADMINISTRATION DATA SHEET

	X ORIGINAL REVISION NO.							
Project No. A-3577	GTRIAGET DATE 6/28 /83							
Project Director:Joseph C. Wyvill	XSENSON/LabTAL							
Sponsor: Perdue, Inc.								
Type Agreement: Research Agreement dtd. 6/2	1/83							
Award Period: From <u>7/1/83</u> To <u>12/31/83</u>	(Performance) (Reports)							
Sponsor Amount: This Change	Total to Date							
Estimated: S	\$ 9,622							
Funded: \$								
Cost Sharing Amount: \$	·							
Title: An Evaluation of the Noise Environmen								
Lewiston, N.C. Processing Plant								
ADMINISTRATIVE DATA OCA Contact	t John W. Burdette							
1) Sponsor Technical Contact:	2) Sponsor Admin/Contractual Matters:							
Same as (2)	Howard F. Yerges							
	Director of Engineering							
- *	Perdue, Inc.							
	P.O. Box 1537							
· •	Salisbury, MD 21801							
	Salisbuty, HD 21001							
Defense Priority Rating: N/A	Military Security Classification: N/A							
	Military Security Classification: N/A  Ompany/Industrial Proprietary: N/A							
RESTRICTIONS								
See Attached Supplemental Info	rmation Sheet for Additional Requirements.							
Travel: Foreign travel must have prior approval - Contact O	CA in each case. Domestic travel requires sponsor							
approval where total will exceed greater of \$500 or	125% of approved proposal budget category.							
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#### OFFICE OF CONTRACT ADMINISTRATION

#### SPONSORED PROJECT TERMINATION/CLOSEOUT SHEET

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#### Report

AN EVALUATION OF THE NOISE ENVIRONMENT AND TREATMENT OPTIONS FOR PERDUE POULTRY'S LEWISTON, N.C. PROCESSING PLANT

### GEORGIA INSTITUTE OF TECHNOLOGY



A Unit of the University System of Georgia Engineering Experiment Station Atlanta, Georgia 30332



#### Report

AN EVALUATION OF THE NOISE ENVIRONMENT AND TREATMENT OPTIONS FOR PERDUE POULTRY'S LEWISTON, N.C. PROCESSING PLANT

Submitted To

Perdue, Inc. P.O. Box 1537 Salisbury, Maryland

Submitted By:

The Technology Applications Laboratory Engineering Experiment Station Georgia Institute of Technology Atlanta, Georgia

Prepared By

J. Craig Wyvill October 1983

#### Introduction

On August 9, Georgia Tech initiated a three day intensive study of the noise environment in Perdue's Lewiston, N.C. Poultry Processing Plant. This report highlights both the methodology used to evaluate the noise environment together with a subsequent analysis of the severity of the noise problem and suggested methods for dealing with it.

#### Identification of the Noise Environment

To better understand the intensity and mechanics of the noise field in the Lewiston Plant, a measurement grid was laid out on 3 foot centers for use in systematically recording noise levels throughout the plant. The measurement program was confined primarily to the trim and evisceration areas of the plant because expansion activities in the cut up and pack out areas negated the usefulness of intensive studies there. The grid used is displayed in Appendix A.

Using a Type 1, B&K sound pressure level meter with slave octave filter set, readings were taken at each grid point using 5 to 15 second intervals to observe an average level. Slow meter response was selected in making these readings to allow more accurate averaging of the values. Both "A-Weighted" and linear values were recorded at most points to allow observations of possible signature changes in the frequency makeup of the field. Octave band sound level readings were also taken at select locations for use in evaluating noise control options. Dosimeters were also used to observe time weighted average levels at selected points. These values (over a three hour interval) were compared to the short interval values obtained with the sound level meter to determine how significant long term fluctuations in the

noise field affected exposure levels. Figure 1 shows both the "A-Weighted" levels observed and the resulting noise contour developed. The actual data sheets for the measurement program are in Appendix B.

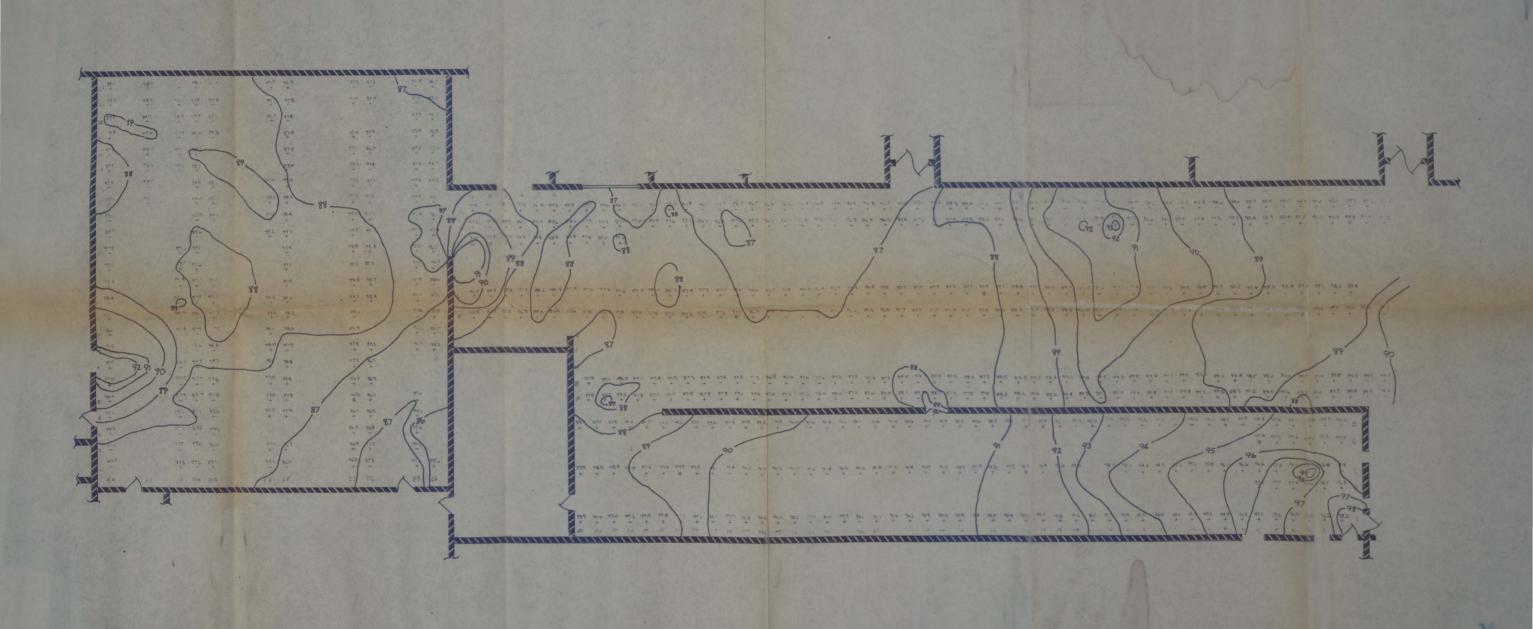
Table I shows a comparison of the short interval and long interval readings taken at selected points in the plant. Based on observations made during the measurement program, it is believed that the public address system, which was intentionally filtered out of the short interval readings, may have had a significant impact on the differences observed. The P-A system was found to be loud and in use regularly offering a potential for significantly elevating the time weighted average sound level to which employees are exposed.

With regard to the contour shown in Figure 1, it appears much of the plant is dominated by reverberant noise powered at least from five distinguishable areas:

- o The two picking rooms
- o A motor station
- o A gizzard harvestor
- o The chiller area

Ironically, levels in much of the plant are remarkably low (87-89dBA) for a poultry processing operation. However, this appears to be due more to the unusually large internal volume of the plant than to any discernable noise control effort.

While not intensively studied, readings were taken in the cut up, pack out, picking and live hang areas of the plant. The locations of these measurements are also shown in Appendix A. The values observed are shown in Appendix B and redisplayed in Table 2. The cutup and pack out areas appear similar to the trim and eviscerating areas in



 $\begin{tabular}{ll} TABLE 1 \\ \begin{tabular}{ll} Long Term vs. Short Term Sound Level Averages \\ \end{tabular}$ 

Measurement Point	Dosimeter Reading (L <sub>D</sub> ) (3 hour average)	Sound Level Meter Reading (L <sub>SLM</sub> ) (10-15 second average)	Difference (L <sub>D</sub> -L <sub>SLM</sub> )
41c	89.6dBA	89.5dBA	0.1dBA
20C	92.4dBA	91.3dBA	1.1dBA
6D	96.5dBA	95.4dBA	1.1dBA
17K	88.2dBA	87.2dBA	1.0dBA
54N	88.9dBA	88.0dBA	0.9dBA
5DD	88.0dBA	86.3dBA	1.7dBA
19KK	88.8dBA	87.5dBA	1.2dBA

"A" Weighted Sound Level Reading In Cut-Up And Pack Out Areas

TABLE 2

Mea	asurement Point	Dosimeter Reading (L <sub>D</sub> ) (1 hour average)	Sound Level Meter Reading (L <sub>SLM</sub> ) (10-15 second average)	Difference (L <sub>D</sub> -L <sub>SLM</sub> )
0	Near Giblet Wrap Tables and Chillers (DOS 1)	90.5dBA	89.3dBA	1.2dBA
0	Near Fillet Tables and Carcass Halving Machines (DOS 2)	87.1dBA	86.2dBA	0.9dBA
0	Near Wiring Cutting Table (DOS 3)	88.4dBA	87.5dBA	0.9dBA

terms of noise makeup and intensity. The sources of the noise, however, appear to differ.

#### Noise Control Assessment

Based on the data in the noise contour of Figure 1, it would appear that "A-Weighted" noise level reductions of from 3 to 5 dB would bring much of the plant below 85dBA. For the most part, this could be achieved effectively with ceiling acoustical treatment. As a goal, such treatment should strive for at least a 5dBA overall reduction in reverberant field noise levels to improve the potential for compliance with the 85dBA OSHA statue (using time weight average values typically observed to be 1 to 2 db higher than the values in Figure 1). Figure 2 shows the typical frequency spectrum for the observed reverberant field.

Even with proper ceiling treatment, however, some areas of the plant will remain in excess of this desired criteria. One such problem area is the trim room immediately after the main picking room. Here sound energy buildup in one end of the room drives levels above 90dBA. While ceiling treatment will indeed help this situation, opportunities to block or shield the room from the energy originating from the picking room would also help immensely. The same is true, to a lesser extent, in eviscerating #2 immediately outside of the smaller picking room.

With regard to the main eviscerating room, two major sources were observed. One, an electric motor in the salvage area in the northwest corner of the room, probably could be reduced using attentive maintenance. If not, a barrier wall around the unattended unit is another feasible option. The second, the gizzard harvesting area, is

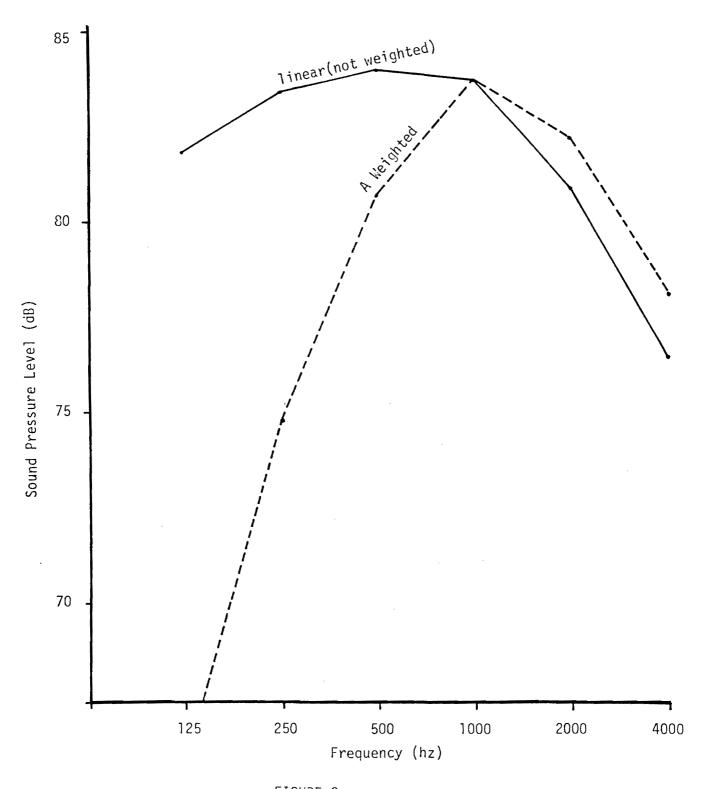


FIGURE 2

Typical Frequency Spectrum Observed for the Reverberant Field of the Plant

more difficult. Here at least one motor was observed in need of attention that could possibly help lower overall levels. But it is doubtful this alone or even with ceiling treatment can reduce levels below 85 dBA. Perhaps the best method of dealing with this area will entail ceiling treatment, attentive maintenance, and selective use of barriers. This last measure, however, should be used after the first two have been completed.

In the cut up and pack out areas, again ceiling treatment appears the best option. Ironically an earlier visit to the plant in February showed noise levels at or below 85dBA in this area. The slight escalation observed (86-87dBA) is indicative of a problem with untreated rooms. Any change in overall sound power can escalate levels throughout the room. Ceiling treatment achieving a 3 to 5 dBA drop in reverberant noise levels should greatly reduce exposure throughout cut up and pack out.

#### Commercial and Other Designs Capable of Meeting Noise Control Needs

In the previous section, noise control was discussed. This section addresses control designs that can be used to achieve noise reduction goals.

The first such design is ceiling treatment. Perhaps the most practical method of treating a room for improved absorption is to hang a series of vertical baffles in the ceiling. Such a design typically allows ready adaptation of an absorbing media to an existing room without creating problems with the accessibility of piping/wiring (as would be the case with a drop ceiling) or increasing the risk of contact with operations (as would be the case if panels were placed on the walls or floor). Many manufacturers have recognized the needs of

poultry and other food processing plants to have access to suitable absorbing materials. In researching the area at least nine companies were identified who supply a product approved for use by USDA in food processing operations. These nine were identified from inquiries to twenty-three such firms.

In selecting a product for this application, a number of items must be taken into consideration. Perhaps of upmost importance is acoustical performance. Of additional concern is the mechanical integrity of the design (or more appropriately how long will it last). Finally there is the issue of cost.

In evaluating the products potentially suited for this application we found wide variation in acoustical performance, mechanical integrity, and price. Unfortunately the acoustical performance values reported by manufacturers often differ in test methodology and panel orientation used. As a result, comparisons of values can be somewhat misleading. Nonetheless six panel designs were evaluated, using published data, with regard to determining how many would be required to lower the observe intensity of the reverberant field in the main eviscerating room 5 decibels. Table 3 displays the results of these calculations with the name of the panel's manufacturer heading each analysis. The Fiber Flex panel was found to acoustically outperform the other panel designs requiring only 400 panels in the main eviscerating room, nearly 100 less than any other. The Peabody panel, on the other extreme, needed 1100 panels to achieve this reduction.

With regard to mechanical performance, two distinct categories of panel were found:

TABLE 3

Acoustical Performance Estimates of selected Commercial Noise Baffles if used in Main Eviscerating Room (Evis #1)

ibver: Mylar c	kapisite i	IBER-FLEX	(	Est. 7	AT P	125/panel	Cover	Tyalla	r	CHILDERS	Es	+ Price	123.00	/porel
SOUND F	PRESSURE (	LEVEL ANAL	YSIS FOR		400	PANELS **	1	anuos	PRESSURE	LEVEL ANAL	YSIS FOR		# 23,00 575 PI	ANELS**
	,	EVISCERATI	ON #1							EVISCERATI	ION #1			
OCTAVE	LIN-LEV	A-ADJT	A-LEV	PNL COEF	ABSORB+	A-QUIET	ł	OCTAVE	LIN-LEV	A-ADJT	A-LEV I	PNL COEF	ABSORB+	A-QUIET
125	81.9	-16.1	65.8				1	125	81.9	-16.1	65.8			
250	83.5	-8.6	74.9	1.24	7.1	67.8		250	83 <b>. 5</b>	-8.6	74.9	<b>0.5</b> 3	<b>5.</b> 2	69.7
500	84.0	-3.2	80.8	1.29	5.4	75.4		500	84.0	-3.2	80.8	0.76	4.5	76.3
1000	83.8	0.0	83.8	1.09	6.8	77. Ø		1000	83.8	0.0	83.8	0.77	6.5	77.3
ଅପିଷ୍ଠ 4ପିଷ୍ଠ	81.0 76.6	1.2 1.0	82.2 77.6	0.80 0.46	4.5 1.1	77.7 76.5		2000 4000	81.0 76.6	1.2 1.0	82.2 77.6	0.71 0.61	5.0 2.0	77.2 75.6
OVERALL	90.2		87.9			82.9		DVERALL	90.2		87.9			82.9
Cover: Viny/				Est	Prine!	WATO I panel	Rayor	. 1 91. 4	1./	GRT LAKES	TUB ACCO	Est (	2.5.2 (2)	5.18/pane
•	,	PEABODY PA			77	11,000	cover	Polyeti	-			E3/ . /	rice. Co	2487 ANELS**
SOUN <b>D</b> F	PRESSURE I	_EVEL ANAL	YSIS FOR		1100	PANELS **		SOUND	PRESSURE	LEVEL ANAL	YSIS FOR		480 Pi	ANELS"
		EVISCERATI	ON #1				.			EVISCERAT			_	
OCTAVE	ILIN-LEV		!	D	000000		1	OCTAVE	1 7 1 7 1 7 1	A-ADJT	'	DOTE	) ABSORB+ I	0
125	81.9	-16.1	65.8	PNL COEF	HR2OKR+	A-QUIET	1	OCTAVE 125	81.9	-16.1	65.8	NL KHIE	+03URD*	H-MOIE!
250	83.5	-8.6	74.9	0.32	5.1	69.8	1	250	83.5	-8.6	74.9	4.6	5.9	69.0
500	84.0	-3.2	80.8	0.69	5.5	75.3	1	500	84.0	-3.2	80.8	8.4	4.2	76.6
1000	83.8	0.0	83.8	0.73	7.9	75.9	1	1000	83.8	0.0	83.8	10.6	6.6	77.2
2000	81.0	1.2	82.2	0.43	4.5	77.7	1	2000	81.0	1.2	82.2	10.20	5.1	77.1
4 ଉପର	76.6	1.0	77.6	0.21	0.2	77.4	1	4000	76 <b>. 6</b>	1.0	77.6	7.3	1.8	<b>75.</b> 8
OVERALL	90.2		87.9			82.9		OVERALL	90.2		87.9			82.9
Cover: Tyda	ar i	ARMSTRONG		Est	Price: §	24.50/pond	Cover	: Polye	thylene	IND NOISE	CONTROL	Est. P	rice: Con	84.95/pane
SOUND F	PRESSURE L	_EVEL ANAL	YSIS FOR		470	24.50/ponul 11,615 PANELS			•	LEVEL ANAL	YSIS FOR		480 P	#4.95/pane 23.76 ANELS**
		EVISCERATI	ON #1							EVISCERATI	ON #1			
OCTAVE	LIN-LEV		!	5tu			1	0075115	1		<u></u>		ARBORE	a hurer
125	81.9	H-HUJ! -16.1	65.8	PNL COEF	HR20KB+	A-QUIET	1	OCTAVE	!LIN-LEV			NL RATE	ABSORB+	H-GOIF!
250	83.5	-8.6	74.9	0.56	4.9	70.0	1	125	81.9	-16.1	65.8 74.0	· , <del></del>	5 0	68.9
500	84.0	-3.2	80.8	0.77	4.1	70.0 76.7	1	250 500	83.5 84.0	-8.6 -3.2	74.9 80.8	4.7 8.3	6.0 4.1	76.7
1000	83.8	0.0	83.8	0.92	6.7	77. 1		1000	83.8	-3. c 0. 0	83.8	10.6	6.6	77.2
2000	81.0	1.2	82.2	0.89	5.3	76.9	ĺ	2000	81.0	1.2	82.2	10.30	5.2	77.0
4000	. 76.6	1.0	77.6	0.71	2.1	<b>75.</b> 5		4000	76. <b>6</b>	1.0	77.6	7.4	1.8	75.8
OVERALL	90.2		87.9			82.9		OVERALL	90.2		87.9			82.9
** Estima	ted num	ber of	panels	needed	to br	ing about	G	D For G	reat L	aKes Inc	dustrial	ASSO, +1	texe nu	umbers
a 5 dec	cibel.A	-Weight	ed dro	in th	e Reve	rherant	1	are	admit	ted est	7 mates	No T	ests ha	ve been
Eiold	OVONT	l level	,ca a, o <sub> </sub>	- 111 CII	C NCVC	Derant		per	formedt	05465	tan tat	e the va	lues a	nd they
rielu	overal	i ievel			,		1	base	A accord	2000 11	2. hl ( = 1	12000	L	1 1

are therefore highly suspect.

- o Those covered in a rugged material designed to increase life and performance
- o Those using low cost polyethylene

It is doubtful long term performance will be achieved with the latter group, particularly if hot water or steam cleaning and chemical detergents are used from time to time. The designs falling into this class are those from Great Lakes Industrial Associates and Industrial Noise Control. Their main advantage is that they are relatively cheap (approximately \$5 per panel). Using the calculations shown in Table 3, (and as stated in the table some of the acoustical values are not substantiated) the main eviscerating area could be treated for around \$2500 (not including mounting hardware). This is about one-fourth the average cost of the other group of panels. But the question must be how long will they survive?

The other group of panels includes designs intended to improve mechanical performance in poultry processing environments and the like. Within this group, price and performance still vary widely. Using the values in Table 3, Fiber Flex seems to display the lowest overall total cost because of its superior acoustical performance. However, there is only a small difference between it and the Armstrong and Peabody Panels. In that calculation, the main eviscerating area was estimated to be treatable for these three for around \$10,000 to \$11,000 (not including mounting hardware). Mechanically, the cover of the Fiber Flex panel is probably the best. In studies by Georgia Tech this cover was found to have superior qualities over Tydlar for this application. The vinyl cover of the Peabody Panel while probably good mechanically, is too thick to allow proper acoustical performance.

Panel placement appears best achieved by hanging the baffles in parallel rows in the recesses of the prestressed concrete roof. For the Fiber Flex Panel, 4 foot intervals are what would be required. For hanging, it is suggested that the panels be mounted so that the bottom edge is flush or possibly even 1 foot below the bottom edge of the support strut (see Figure 3). This arrangement, however, will necessitate lowering the ceiling lights in the plant to maintain illumination standards in the plant.

With regard to source quieting, the sound energy migrating from the picking rooms, can be dealt with using a "passage absorber" installed to absorb much of the random incident sound leaking from the room. The absorber could be designed as shown in Figure 4. Approval of such a design, however, by the USDA chief inspector would be required. As an alternative, a commercial design is available from a company called Body Guard. However, the design (see Figure 5) is relatively expensive, (\$500 per 3' x 8' panel) and its performance as an absorber is not as strong as is anticipated with the Figure 4 design.

Another source quieting measure is the use of barriers. Again, the Body Guard design can be used to both block and absorb sound. However, a simple vinyl or polyethylene sheets of 1/2" to 3/4" thickness can effectively be used as a barrier to divert sound. If used in conjunction with ceiling treatment, these barriers can prove quite effective in an overall noise reduction plan.

#### Recommendation

As a basic plan of attack, Perdue is encouraged to try ceiling treatment throughout the eviscerating, trim, cut up and pack out areas.

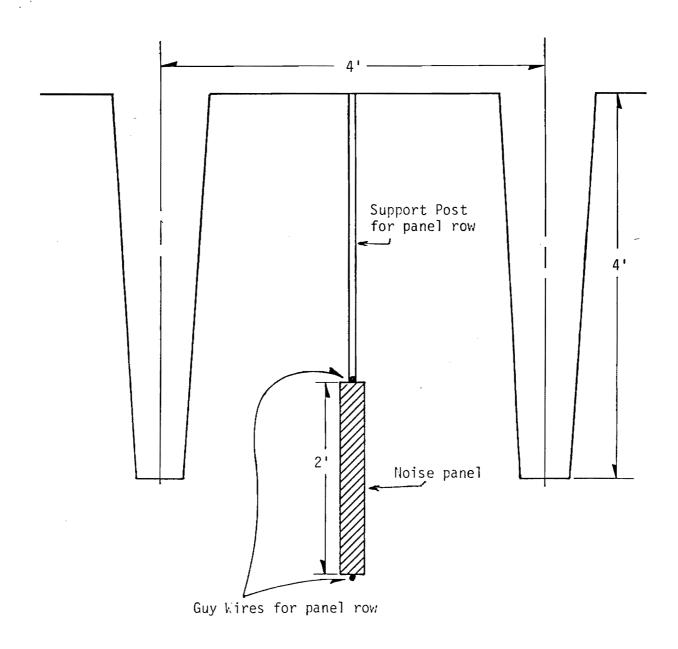


FIGURE 3
Suggested Acoustical Baffle Mounting Arrangement

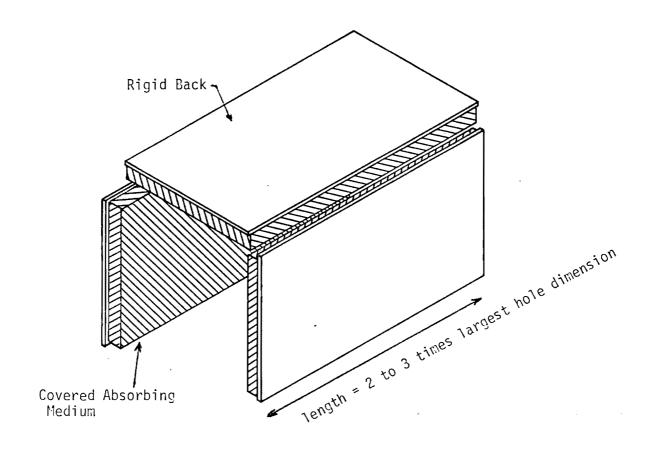


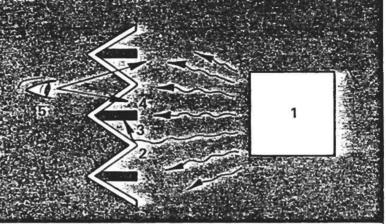
FIGURE 4
Conceptual Design of a "Passage Absorber"

100

### HOW GLEAR & QUIET " WORKS."

- the Morse Source and Science Wave
- 2. Wave strikes panel and used rected into:
- Sa Acoustical Cameveographere
- 4. Sound energy is absorbed and obssipated.
- 57. Operator is protected at incommose sould a but with this extended contact with sopera atom.

\*U.S. PATENT NO: 4,094,379



#### **SERVICES**

END CAPS — Vacuformed plastic fits over ends to provide additional strength, rigidity and moisture resistances.

DESIGN — A personal visit to your plant to measure, layout, and present an engineered proposal.

INSTALLATION — Experienced crews available for "turn-key" projects.

SUPERVISION — A skilled Body Guard lead man to direct and assist your maintenance staff in installation.

#### **GENERAL CHARACTERISTICS**

TRANSPARENCY — 87-88% Clear.

HEAT RESISTANCE — Withstands 180-200°F. Self-extinguishing foam.

IMPACT RESISTANCE — Specimen at 73°F, absorbed 39 foot pounds without failure.

SANITATION — FDA approved. Cleans easily.

CORROSION RESISTANCE — Inert to most corrosive agents.

#### ACOUSTICAL PERFORMANCE AT VARIOUS FREQUENCIES

SOUND ABSORPTION
125 Hz32% 25039% 50064% 1000110% 200092% 400092%

NOISE REDUCTION CLASS 75%

SOUND ATTENUATION	
125 Hz 22dB 250 16dB 500 20dB 31dB 35dB 4000 36dB	

SOUND TRANSMISSION CLASS 26dB

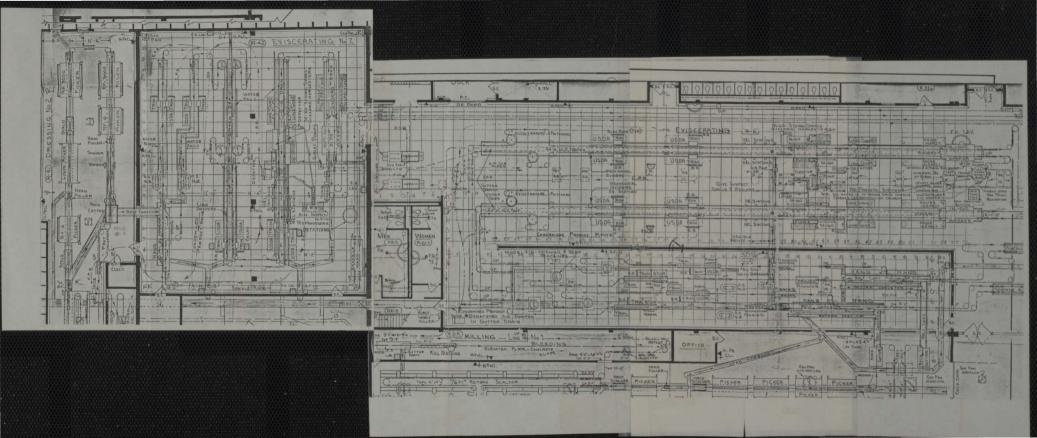
Test results certified by Riverbank Acoustical Laboratory

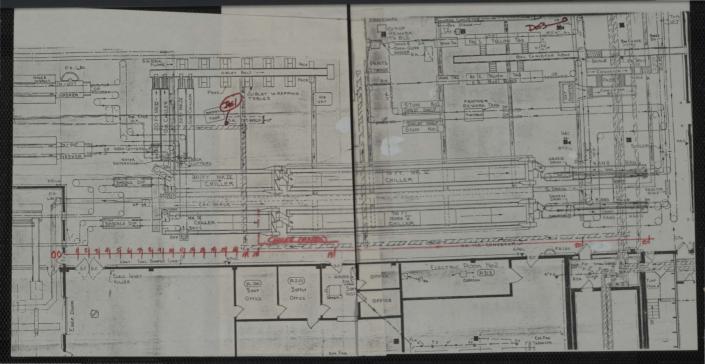
Based on rough calculations about 825 Fiber Flex panels would be needed in the eviscerating and trim areas alone. Cut up and pack out probably could require anywhere from 1000 to 2000 additional panels, the exact number depending on the reduction needed. At \$25 per panel (only a rough estimate) the cost of treating the trim and eviscerating areas would be slightly over \$20,000 (without mounting hardware and the cost of lowering the lights). The benefits of such treatment, however, should be significant. As an alternative to initially treating all of the plant, a staged introduction of panels in noisy areas and over major sources is a viable alternative. However, much of the plant will eventually require such treatment.

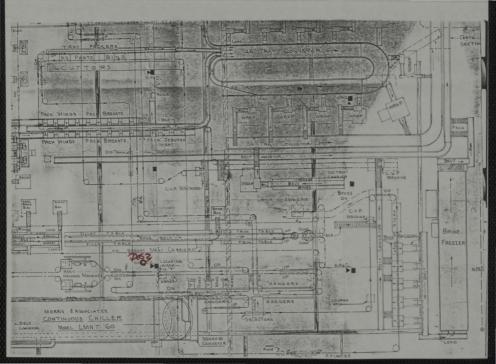
After ceiling treatment, a concerted attack on identifiable noise sources is suggested. The "passage absorber" discussed earlier would be a good focus of attention as would maintenance attention on readily identifiable "noisy" machines. Barriers are suggested only as a last resort and then only if the impact of the source is considered significant and the barrier design practical. In those areas of the plant studied, only two possibilities for barrier installation were found.

#### APPENDIX A

Plant Layouts with Measurement Positions Superimposed







#### APPENDIX B

Data Collected on Sound Levels During Measurement Program

Date 8-9-83

Reading			Soun	d Pressure	Level	-			
Position Number	0ve	rall				Octave			
Hamber	Awt.	Linear	125	250	500	1000	2000	4000	8000
A-1	97.2	101.5		-					
A-R	96.2	100.5							
A-3	96.5	100.2							
4-4	96.8	100.6							
A.5	97.6	101.0	97.0	96,2	95.0	93.0	98,5	85.4	78.0
A-6	97.5	101.5							
A.7	96.4	100.4							
A-8	95.4	99.3							
A-9	95.2	99.0							
A-10	014,4	98 b							
A-11	94.0	987							
A-12	940	93.2							
A-15	935	98.0	89.0	92.5	91.0	88.9	85.0	BIC	75.8
4-14	43,2	97,5							
A-15	92,3	97.0							
A-16	97.1	970							
A-17	91.6	97,2						_	
A-19	91.5	96.5							
A-19	91.1	96.2							
4-20	91.0	94.0							
4-21	90.8	95.6							
4-22	91.0	96.6	88.4	90.5	88.6	85,8	82.5	78.2	74.4
4-23	91.0	96.2.							
A-24	90.8	95.8	•						
H-25 H-26 H-27	10.5	95.6							
A-26	90.5	45.5		-					
	90.2	95.5							
A-29	40.3	45.6							
A-29	70.1	95.2			:			-	
A-30	90.1	951							
A-31	8.7.7	95.2							
A-32.	110.0	455							
-A-37	40.6	15.6	86.6	90.0	36.5	34.6	82.0	81.5	83.0
4-24	90.3	95.2							

Date 8/9

Reading	Sound Pressure Level											
Position Number	0ve	rall		Octave								
	Awt.	Linear	125	250	500	1000	2000	4000	8000			
A-35	90.2	95.8										
A-36	90.0	95.5										
A-37	90.0.	95,5										
A-38	89,8	15.7										
4-39	90.1	95.8										
4-40	89.3	94.5										
4-41	89.0	16.0										
4-42	88.5	95.7										
4.43	88.5	95.2										
7-44	882											
4 45	.89.0	95.0										
A 16	89.0	455										
A47	3475	965										
B47	87.4	95.8										
<b>3</b> 46	88,5	CH.1-										
<b>B</b> 46 <b>B</b> 45 <b>B</b> 44	88.4	72.5	87.5	88.0	85.8	853	50.8	76.7	75.2			
路 44	59.0	94.6										
是 4 多	39.0	91.6										
		940										
c 4b	395	94.5										
C 40	79.3	45.0										
- 39	90.1	95,6										
<u> </u>	91.9	91,6										
C 37	90.2	95.2										
36	90.0	45.8										
235	907	76.0										
c 34	11r.5	96.0 95.4										
C 33	4:2	95.4										
C 32	JC. A	95.3	87.8	90.5	37.8	554	82.0	77.8	76.5			
= 31	900	957										
C 38 C 37 C 36 C 35 C 37 C 37 C 39 C 29 C 75	900	95,6										
C 29	c/c. 4	45.5										
C 75	40 5	955										
CZ1	40.4	45.6										

Date <u>8/9</u>

Reading	Sound Pressure Level										
osition Number	0ve	rall	Octave								
Muniber	Awt.	Linear	125	250	500	1000	2000	4000	8000		
C-26	91.0	95.9									
C-25	90.5	45.8									
C-24	90.5	960			-						
C-23	70.7	96.7									
c - 22	91.2	96.5						,			
C-21	91.5	968							·		
C-7.0	915	9/0,9,									
C-19	91.5	77.0									
C-18	92,0	172									
17	13.0	97.9									
2-14	NA										
C-15	94.0	98.5									
C-14	11d. C	वर् हे									
C-13	41 =	98.6									
C-12	94,5	91.2									
C-11	957	79,5									
C-10	95.6	1000									
C-9	95.8	100.3									
C-8	96.C	KC.C.									
C - 7	46.6	16/12		\							
C-6	966	10/10									
C-5	97.6	KZ.O	- 1								
(-4	980 40,5	107.2									
53	40 <	102.5	-								
3-2	77. C	102.2. 102.5 101.0 100.5 101.0									
3-4	47.4	100.5									
3-5	97.6	101.0									
3-6	97.0	100.2									
3-71	3115	100.6						-			
3-1	91- 2	100,5									
7-4 7-3 8-5 3-6 3-7 3-1	963	100.4									
- [	95.2	100-1									
)-(	75.5	39.(.									
>- ひ	45.5	99.5									

Date\_\_\_\_\_\_

Reading			Soun	d Pressure	Level	•			
osition Number	0ve	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	8000
D-3	95.2	94 %							
D-4	95,2	99,2							
D-5	95.3	99,5							
D-6	954	99.5	41.7	45.2	92.4	90.3	86.6	83,6	772
E-1	45.0	99.7							
F-2:	95.5	99.5							
E-3	95.5	P1.4			·				
E-4	95 5	19.5							
E-5	45,2	अप इ							
E-6	900	44.2							
E-7	41.4	49.							
E-8	91.7	99.0							i
E-9	44-	986							
E-16	94.2	955				-			
E-11	458	98.C							
E-12 E-13	93.6.	984							
E - 13	पेउ न	98.0							
=-4	93,2	40							
= -15	93,71	97.5							
= - 16.	97.3	47.2							
-17	92.2	47.2							
- 18	47.1	97.2							
= -19	91.9	97.1							
=-Ze	91.5	96.8	·						
=-21	90.9	47.2							
=-27	90.9	96.5							
= 7.3	98.6	96.2		_					
= 24	90.4	96.0							
=-25	91.4	95.4				_			
1-76	air. i	95.6							
= -27	Act (	95.2 95.4							
= 1	46,0	95.4							
1-19 1-20 1-27 1-27 1-27 1-27 1-27 1-27	40.0	95 5							
= -7.0	40.1	954							

Date <u>3/9</u>

Reading			Soun	d Pressure	Level						
osition Number	0ve	rall	Octave								
	Awt.	Linear	125	250	500	1000	2000	4000	8000		
= -31	90 C	95 4									
=-32	90.4	95,4									
= - 33	90.0	95.5									
= -34	90.0	45,0									
= 74	87.9	956									
E-36 E-37	89.8	95.2							U		
	89.4	95%									
E-38	89.8	55									
E - 39	84.2	9115									
F-40	451 1	94,5									
E-41	81.0	94,5					•				
E. dre	<b>3</b> 4.9	94.0							_		
E-33	88.7	437									
E-44	88.C	935									
=-25	87.0	94.4									
E-06	87.9	94.1									
F-47	58.3	912									
F-8	87.5	季		,							
7-8	378										
= -9	89,2										
7-9	88.6		•								
<-10	88.2			-							
, -10	88.0										
- 11	87.8		-								
7-11	94.0		-								
= - 17	537										
7 - 1Z. = - 13	87.4										
<i>z</i> - 13	47.1										
i-13	97 9		,								
= - 14.	27.5										
7 - 14	イフェ						,				
- 15	×7 ×										
- 15	27.6										
- //-	47.9								· · · · · · · · · · · · · · · · · · ·		

### NOISE SURVEY DATA SHEET Perdue Poultry Processing Plant

Lewiston, N.C.

Date **5/9** 

	Sound Pressure Level										
Ov	erall		Octave								
Awt.	Linear	125	250	500	1000	2000	4000	8000			
, 874.											
7 870											
7 87.5	-										
876											
57.3											
9 976											
7 46 -				-							
7 87/2											
86.0											
× -											
87.											
2 58.5											
2 878											
3 88.C											
3 57.7											
4 87.5											
+ 511											
5 87.0							`				
87.2											
6 876											
6 51.2											
88.1											
7 88.5											
7 88.5 7 <b>98.8</b> 6 <b>99.</b> 3		abil	85								
K 29.9		0/17									
9 88.3		8/10	0/43								
9 87.0		011	/								
0 87.5											
50 37.3											
37 - 5					· ·						
1 48 -											
2 37.7	93.0	57.5	\$2.0	\$ 5,6.	35, 4	914	76.7	72.			
7 97.5			, , , , , , , , , , , , , , , , , , , ,			, , ,	110000				
3 7%.2											
1 37 1 48 2 37 7 97	7.7.5	7 73.0 5	7 93.0 87.9 5	7 93.0 87.5 \$3.0 .5	7 93.0 87.9 \$3.0 85.6 5	5	7 930 87.9 \$2.0 85.4 9/4 .5	7 93.0 87.9 \$3.0 85.6 35.4 914 76.7 5			

Date <u>\$-10</u>

Reading	Sound Pressure Level										
osition Number	0ve	rall	Octave								
, and c	Awt.	Linear	125	250	500	1000	2000	4000	8000		
9-33	88.5										
<del>34</del>	85.3										
3-34	88.5										
-35	85,5										
一35	88,5			-							
- 36	88.6										
-36	85.4										
-37	894										
1-37	39.6										
- 38	89.5	94.5									
7 - 38	900	94.2									
- 39	90.1	94.4									
3-39	84.5	4.6									
=- 40	89.4	वर्ता ।									
7-40	89.5	927									
=-41	89 =	93.7									
4-41	89.5	430									
=-17	89.8	41.0									
9-17	89.4	94.1									
-43	89.5	94,2									
3 - 43	79.11	911.0									
3 - 43 40	89.8	94,2									
A /	59.5	94.0									
-15	89.0	9412	-								
7-45	99.2	43.7									
26 5 46 = 47	995	94,0									
5 46	88.5 88.5	43,5									
= 47	88.5	44.0									
7 47	7871	93.									
- 14	84.6	936									
1/	77.5	94,0									
7 43	88	9417									
1 49	38.0	9,3,5									
: 50	89.6	49.0									

Date 5-10

Reading	Sound Pressure Level										
osition Number	0ve	rall	Octave								
	Awt.	Linear	125	250	500	1000	2000	4000	8000		
5-50	84.0	43 4							,		
-51	83.5	93.8									
1-51	89.5	73.4									
=-52	89.0	93.5									
-52	90.0	938									
- 53	89.5	94.0									
7 - 53	81E 8	93.0									
-54	39.9	93.6									
-54	895	933									
55	59, =	937									
7-55	39.5	43.3									
= - 56	39.9	44.1									
, -56	87.9	90.0									
	88 5										
	905										
_ 2	89.4										
-3	37.5										
- 3	87.5							·			
- 2	87.9										
_ 4	877										
4	86.9,										
- 5 K 5 K 6 V-1 L-7	1 88.71										
C 5	88.2 88.4										
K G	87.4		٠								
_ 6	88 9										
K-1	37.4										
L-7	×7.8										
K-5	57.5										
-8	27.5										
1-4	51.5										
1-9	47.3										
V-16	475										
(-16											
12-11	974 374										

Date 8-16

Reading	Sound Pressure Level											
osition Number	0ve	rall	Octave									
	Awt.	Linear	125	250	500	1000	2000	4000	8000			
-11	87.4											
K-12	87.5											
L-12	886											
K-13	87.2							<u> </u>				
<u>L-13</u>	88.3											
K-14-	87.6				-							
4-14	97.4											
K-15	10/:											
1-15	97.6 77.6											
K-16.		-										
1-16	87.2	42.0	81.7	85.2	83.0	82.2	80.5	77.9	73.8			
1-1-1	57.7	7210	01.1	70,00	00,0	DEVE	10013	1/19	1.5.0			
V-14	36.5											
1-18	41.6											
K-19	87.4											
L-19	86.9											
K-20	87.2											
L-20	86.8											
K-2/	87.3						٠	_				
L-21	864											
K-72	87.1											
K-22 L-22 K-23	86,9											
K-7/3	87.0											
1-23	36.7											
K-24	76.6 77.3											
1-24	37.3 37.3											
K-25 L-25	15/1.5 12/1.2											
K-76	41,4											
1-71:	877											
1-20 K-21	3/15											
1-17	51.7											
	.,,,,							L				

Date\_\_8\_10\_\_\_

Reading	Sound Pressure Level											
osition Number	0ve	rall		Octave								
-	Awt.	Linear	125	250	500	1000	2000	4000	8000			
K-28	874											
L-28	87.8											
K-29	87.5											
L-29	87.7											
K-30	87.8											
1-30	87.8											
K-31	87,4				-							
L-31	877											
K-32	57.5											
L-32	87.8	42.0	81.9	83.5	84.0	83,8	81.0	76.6	73.0			
K-33	88.0											
L-33	88./											
K-34	85.41											
L-34	88.4											
K-35	48/1											
L-35	95,00											
K-30	89.6											
L-36	842											
K-37	89.5											
1-37	89:7											
K-33	40.5											
L-35	90.5	_										
7-39	91.5	44.5										
L-40	91.3	94.5					,					
L-41	91.4	44.4	83,1	85.0	87,7	86.8	84.5	79.0	75,5			
L-47	An.A	1317				, , , , , , , , , , , , , , , , , , ,			7 3 2			
7-43	90.3	94.3				,						
L-44	91.5	44.3										
L-45	90.4	43.8										
1-39	41.1	34.3,	-									
K-640	41.8	04.5										
12-41	40 12	94-11						† — —				
K-47)	4/1.71	14 3										
K-42	761.4	14.0										
	1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	211.0		<u> </u>	.1	ļ	<u> </u>	<u> </u>				

Date 8-10

Reading Position	Sound Pressure Level									
Position Number	0ve	Overall . Octave								
	Awt.	Linear	125	250	500	1000	2000	4000	8000	
K-44	89.6	93.8								
K-45	88.7	93.5								
K-46	84.C	43,3								
1-46	81.7	43.4								
K-47	88.8	93.0		í						
1-47	89.2	93.7								
K-48	89.	47.8			·					
1-48	89.4	43.7								
K-44	₹.X.Y.	43.0								
1-49	23.4	47.6								
K-50	89.0	43 6					•			
1-50	88.4.	128								
12-51	88.4	42.4								
L-51	89.0	42.6								
1.50	29.6	47.4								
L-52	88.1	42.5								
K-53	54.8	42.8								
1-53	48,2	92.3						·		
1 K-54,	88.0	92.3								
1-54	88.8	41,8								
in/ -55	89.C	43,4	41.3	84.4	85.2	54,6	84.0	840	74.8	
L-55	NA			1						
1-56	90.2	41.8								
N-18	89.3	EDWA								
0-1	89.8	CAREY								
11-2	89.4	42.1	74.8	87.4	84.2	82.8	82.	18.5	73.3	
0 0-2	88.6	KEGO)								
M-1	91.5/	7								
M-2	99.5									
1 M-3	14413									
N-m	454,7									
0-3	43.4									
0-4	37.21									
N-1	44.									
					.1				<u> </u>	

Date <u>45-10-83</u>

Reading			~	J D	. 1 7				
osition	-	I	Soun	d Pressure	e Level			·	
Number		rall	305	T 050	T 500	Octave			_
0 1	Awt.	Linear	125	250	500	1000	2000	4000	8000
0-K	86.5								•
N-19	86.0								
0-19	84.5								
N-70	86.3								
0-20	Str. (-				<u> </u>			·	
	86.4								
0-71	86.4				·				
N-22	87.6°								
81 22	86.8								
y - 2.3	36.5								
0 - 23	57.4						·		· · · · · · · · · · · · · · · · · · · ·
N - 21	36.5								!
9 - 74	36.8								
N-25	96.8								
0-25	86.8								
N - Z6,	86.8								
$\frac{0}{V} - \frac{76}{27}$	56.7								
	87.4								
7 -27	87.C.								
V - 78 0 - 28	87.6								
0 - 28	87.0							_	
N - 27	88.0								
7-74	35.C								
V - 30	87.9		•						
0 - 30	4%3								
1 - 31	87.3								
1-31	551V								
(~ 7?	48,0								
1 - 37	88.1.								
1-33	99.0								
- 33	95,7								
1-34	84.0								
5 - 34	49.7								
1 35	90.1								

Date	<u> </u>		

	·								
Reading osition			Sound	d Pressure	Level				
osition Number	0ve	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	8000
35	90.7								
V-36	9(.1								
0-36	91.0								
11-37	918								
7-37	91.0								
¥-38	97.1								
78	91.6.								
V - 39	97,4	95.5			··				
9-34	91.1.	010,8						<u> </u>	
V - CIC	93.0	95.5							
) - 4v	910	95.2					. • .		
(-41	91.2	91.5	83,0	83,4	86.6	86.6	85.0	79.4	75,5
7-41	90.5	94.3							
1- 47.	901-	94.2							
2 42	90.6	95.7							
11-03	9C.1	910							
7 - 4-3	90 C	94.1							
1-40	89,5	93 8							
) - 44	59.9	94,1							
Y - 45	89.4	94.1							
2- 45	39,0	94.0							
V - 16-	89.3	94.8							
0 - 46	88.8	93.5							
V-47	81,2	93.2	·						
0-47	89.0	93,7				-			
V 98	88.4	93,1							
) -43	48.7	93,7							
V - 49	38.1	93.1	·						
5 - 49	88.8	93.3							
V-50	98 E	930							
7-50	34.7	93.0							
1-41	44.3	92.8							
	44.7	92.1							
カーイー	10 1	16,11	,						

Overall   Octave										
Number   N	Reading			Soun	d Pressure	Level				
Avt. Linear 125 250 500 1000 2000 4000 8000  N-53 88 9 72 0  -53 88 9 72 0  -53 88 9 72 0  -53 88 9 72 0  -53 88 9 72 0  -54 88 0 97 3 81 8 83 8 84 2 82 0 76 8 73 8  -54 88 7 92 8  -55 37 8 7 92 8  -55 37 8 7 92 8  -55 37 8 7 92 8  -56 87 7 92 8  -57 87 87 92 9  -58 98 90 9 9  -58 98 90 9 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 98 90 9  -68 90 90 9  -	osition Number	0ve	rall				Octave			
-53 88.8 97.6		Awt.		125	250	500	1000	2000	4000	8000
-53 88.1 97.5	7 -52		93.8							
- 54 88.0 97.3 81.8 83.8 84.8 84.2 82.0 76.8 73.5  - 54 887 92.4  (- 55 81.8 97.4  ) - 55 88.2 12.8  (- 55 88.2 12.8  ) - 56 88.2 12.8  A-1 85.6 91.2  B-1 87.2 91.0  B-2 86.5 90.6  B-3 85.6 90.7  B-4 88.3 91.0  B-8 86.3 91.0  B-9 86.6 90.2  A-10 88.8 90.2  B-10 87.4 91.2  A-10 88.8 90.2  B-10 87.4 91.2  A-11 87.5 90.7  A-13 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-15 87.8 90.9  B-14 86.8 90.2  B-14 86.8 90.2  B-15 87.5 90.9  B-16 87.5 90.9  B-17 88.6 91.0  B-18 86.7 90.9  B-19 86.7 90.9  B-14 86.7 90.9  B-15 87.8 90.9  B-16 87.8 90.9  B-17 88.8 90.0  B-18 86.7 90.9  B-19 86.8 90.0  B-10 87.8 90.9  B-10 88.8 90.0	Y-53	88.8	92.6		•					
- 5	> -53	88.1								
1-55 51.8 97.4 1 2.8 1 5.5 78.2 97.4 1 5.5 78.2 97.7 1 5.8 1 5.6 87.2 97.7 1 5.6 87.2 97.7 1 5.6 87.2 91.0 8.7 2 91.0 8.7 2 90.6 8 5.3 90.6 8 5.3 91.0 8.8 3 86.7 90.5 8 6.6 90.2 8 6.7 90.9 90.7 90.9 90.9 90.9 90.9 90.9 90	1 - 54			81.8	83.8	84.8	84,2	82,0	76.8	73.5
0-55 83: 12.8  1-56 34: 47.7  - 66 84: 47.7  - 66 84: 67.7  A-1 85.6 91.7  B-1 87.7 91.0  B-2 86.5 90.6  B-3 85.6 90.7  B-4 88.3 91.0  B-3 86.7 90.0  B-10 87.9 90.6  B-10 87.9 90.9	7-54	887	92.8							
1-56 84.2 97.7  -56 84.2 97.7  A-1 85.6 91.2  B-1 87.2 91.0  B-2 86.5 90.6  B-3 85.6 90.7  B-4 88 91.0  B-3 86.0 90.5  A-9 86.6 90.2  A-10 868 90.2  B-10 97.4 91.2  A-11 87.3 90.7  B-12 88.6 91.0  B-12 88.6 91.0  B-12 88.5 90.0  B-14 86.7 90.9  B-13 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-15 86.8 90.2  B-16 87.9 90.6  B-17 88.8 90.0  B-18 88.7 90.9  B-19 88.8 90.0  B-10 88.8 90.0  B-11 88.8 90.0  B-12 88.8 90.0  B-13 88.7 90.9  B-14 86.7 90.9  B-15 86.8 90.6  B-16 86.7 90.9  B-16 86.7 90.9  B-17 86.8 90.6  B-18 86.8	1-55	87.8								
A-1 85.6 91.2  B-1 87.7 91.0  B-2 86.5 90.6  B-3 85.6 90.7  B-4 88 91.0  B-8 86.3 91.0  B-9 86.6 90.2  A-10 86 90.2  B-10 87.4 91.2  A-11 87.3 90.7  B-12 88.6 91.0  B-12 88.6 91.0  B-12 88.6 91.0  B-12 88.6 91.0  B-14 86.7 90.9  B-15 86.7 90.9  B-14 86.7 90.9  B-15 87.5 90.6  B-16 87.5 90.9  B-17 88.7 90.9  B-18 86.7 90.9  B-19 86.7 90.9  B-14 86.7 90.9  B-15 87.5 90.9  B-16 86.7 90.9  B-17 86.7 90.9  B-18 86.7 90.9  B-19 86.7 90.9  B-19 86.7 90.9  B-10 87.5 90.9  B-10 87.5 90.9  B-10 87.5 90.9  B-10 88.7 90.9	0 -55		92.8							
A-1 85.6 91.2 B-1 87.2 91.0 B-2 86.5 90.6 B-3 85.6 90.7 B-4 88 91.0 B-5 81.0 90.5 A-8 86.3 91.0 B-8 86.7 90.5 A-9 86.6 90.2 A-10 868 90.2 B-10 87.4 91.2 A-11 87.3 90.7 BB 12 87.5 90.0 B 12 87.5 90.0 B 12 87.5 90.0 B 13 80.7 90.9 B 14 96.8 90.2 B 15 86.7 90.9 B 15 86.7 90.9 B 16 86.7 90.9 B 17 86.8 90.0	V- 56	8.4.2								
18-187.2 91.0 18-2 86.5 90.6 18-3 85.6 90.7 18-4 883 91.0 18-5 87.0 90.5 18-8 86.3 91.0 18-8 86.7 90.0 18-9 86.6 90.2 18-10 87.4 91.2 18-10 87.7 90.7 18-10 88.6 91.0 18-10 88.6 91.0 18-10 88.6 91.0 18-10 88.6 91.0 18-10 88.6 90.0 18-10 87.5 90.9 18-10 87.5 90.9 18-10 87.5 90.9 18-10 87.5 90.9 18-10 87.5 90.9 18-10 88.6 91.0 18-10 88.7 90.9 18-10 88.7 90.9 18-10 88.7 90.9 18-10 88.8 91.0 18-10 88.8 90.6 18-10 88.8 90.6 18-10 88.8 90.6 18-10 88.8 90.6 18-10 88.8 90.6 18-10 88.8 90.6 18-10 88.8 90.6	) - < L.	84,0								
B-2 86.5 90.6  B-3 85.6 90.7  B-4 8 B B 91.0  B-8 86.3 91.0  B-8 86.7 90.0  B-9 86.6 90.2  A-10 86.8 90.2  B-10 81.4 91.2  A-11 87.3 90.7  B-12 88.6 91.0  B-12 88.5 90.9  B-13 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-15 86.8 90.6  B-15 86.8 90.6  B-16 87.3 90.9  B-17 86.8 90.9  B-18 86.7 90.9  B-19 86.8 90.9  B-19 86.8 90.9  B-10 87.3 90.9  B-11 86.8 91.0  B-12 87.3 90.9	A-1		91.2							
B-2 86.5 90.6  B-3 85.6 90.7  B-4 8 B B 91.0  B-8 86.3 91.0  B-9 86.6 90.2  A-10 86.8 90.2  B-10 81.4 91.2  A-11 87.3 90.6  B 12 81.5 90.7  B 12 88.6 91.0  B 12 81.5 90.9  B 14 86.7 90.9  B 15 86.7 90.9  B 16 86.8 90.2  B 17 87.9 90.6  B 18 86.7 90.9	3B - 1	87.2	91,0			,		•		
B-4 86 9 91.0 B-5 87.0 90.5 B-8 86.7 90.0 B-9 86.6 90.2 B-10 87.4 91.2 B-10 87.4 91.2 B-11 87.3 90.7 BB 12 87.9 90.6 B12 88.6 91.0 B12 87.5 90.9 B13 81.5 90.9 B14 18 86.7 90.9 B15 86.7 90.9 B15 13 87.5 90.9 B15 13 87.5 90.9 B16 86.7 90.9 B17 86.7 90.9 B18 10 86.7 90.9 B18 10 86.8 90.6 B18 10 86.8 90.6 B18 10 86.8 90.6 B18 10 86.8 90.6	另-て	86.5	90.6							
B-4 86 9 91.0 B-5 87.0 90.5 B-8 86.7 90.0 B-9 86.6 90.2 B-10 87.4 91.2 B-10 87.4 91.2 B-11 87.3 90.7 BB 12 87.9 90.6 B12 88.6 91.0 B12 87.5 90.9 B13 81.5 90.9 B14 18 86.7 90.9 B15 86.7 90.9 B15 13 87.5 90.9 B15 13 87.5 90.9 B16 86.7 90.9 B17 86.7 90.9 B18 10 86.7 90.9 B18 10 86.8 90.6 B18 10 86.8 90.6 B18 10 86.8 90.6 B18 10 86.8 90.6	3B-3	85,6	90.7							
A-8 86.3 91.0  B-8 86.7 90.5  A-9 86.6 90.0  B-9 86.6 90.2  B-10 87.4 91.2  A-11 87.3 90.7  BB 11 87.9 90.6  B-12 88.6 91.0  B-13 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-14 86.8 90.6  B-15 86.8 90.6  B-16 87.3 90.6  B-17 86.8 90.6  B-18 86.8 90.7  B	3B-4	863	91.0							
A-8 86.3 91.0  B-8 86.7 90.5  A-9 86.6 90.0  B-9 86.6 90.2  B-10 87.4 91.2  A-11 87.3 90.7  BB 11 87.9 90.6  B-12 88.6 91.0  B-13 86.7 90.9  B-14 86.7 90.9  B-14 86.7 90.9  B-14 86.8 90.6  B-15 86.8 90.6  B-16 87.3 90.6  B-17 86.8 90.6  B-18 86.8 90.7  B	3B-5	87.0	90.5							
B-8 46.7 90.5 A-9 86.6 90.2 B-9 86.6 90.2 B-10 87.4 91.2 A-11 87.3 90.7 BB 11 87.9 90.6 B12 87.5 90.7 A13 86.7 90.9 B13 87.5 90.9 B14 14 86.7 90.9 B15 86.8 90.6 B15 87.3 90.8 B16 86.8 90.6 B16 86.8 90.6	7A-8	86.3								
A-9 86.6 90.2  A-10 86.8 90.2  B-10 87.4 91.2  A-11 87.3 90.7  BB 11 87.9 90.6  A 12 88.6 91.0  B 12 87.5 90.9  A-13 86.7 90.9  BA-14 86.7 90.9  BA-14 86.8 90.6  A 15 86.8 90.0  BA-15 86.8 90.6  BA-16 86.8 90.8  BA-16 86.8 90.8			90.5							
B-9 86.6 90.2  A-10 868 90.2  B-10 87.4 91.2  A-11 87.3 90.7  BB 11 87.9 90.6  A 12 88.6 91.0  B 12 87.5 90.9  A-13 86.7 90.9  B-14 86.7 90.9  B-14 96.8 90.6  A 15 86.8 91.0  B 15 87.3 90.8  B 16 86.3 90.8  B 16 86.3 90.8		86.5	90.0							
B-10 868 90.2 B-10 87.4 91.2 A-11 87.3 90.7 BB 11 87.9 90.6 B 12 88.6 91.0 B 12 87.5 90.7 A 13 86.7 90.9 BB-14 86.7 90.9 BB-14 86.7 90.9 BB-14 86.8 90.6 BB-15 86.8 90.6 BB-15 86.8 90.6 BB-15 86.8 90.6 BB-16 86.3 90.5 BB-16 86.3 90.5	B-9									
B-10 87.4 91, z A-11 87.3 90.7 B 12 88.6 91.0 B 12 87.5 90.7 A 13 86.7 90.9 B 13 87.5 90.9 B -14 86.7 90.9 B 15 86.8 91.0 B 15 87.3 90.8 A 16 86.3 90.5 B 16 86.3 90.5		86.8								
A-11 87.3 90.7 B 12 88.6 91.0 B 12 87.5 90.7 A 13 86.7 90.9 B 13 87.5 90.9 B 14 86.7 90.9 B 15 86.8 91.0 B 15 87.3 90.8 B 16 86.3 90.5 B 16 86.3 90.5	另-10	87.4	91.2							
BB 11 87.9 90.6  PA 12 88.6 91.0  B 12 87.5 90.7  A 13 86.7 90.9  BB 14 86.7 90.9  BB-14 86.8 90.6  A 15 86.8 91.0  B 16 86.3 90.8  B 16 86.3 90.8	A-11	87.3			,					
BB13 87.5 90.9 AB-14 86.7 90.9 BB-14 96.8 90.6 A 15 86.8 91.0 B 16 86.3 90.5 B 16 86.8 90.6	3B 11	87.9								
BB13 87.5 90.9 AB-14 86.7 90.9 BB-14 96.8 90.6 A 15 86.8 91.0 B 16 86.3 90.5 B 16 86.8 90.6	74 12			·						
BB13 87.5 90.9 AB-14 86.7 90.9 BB-14 96.8 90.6 A 15 86.8 91.0 B 16 86.3 90.5 B 16 86.8 90.6	, B 12	87,5	90.7							
BB13 87.5 90.9 AB-14 86.7 90.9 BB-14 96.8 90.6 A 15 86.8 91.0 B 16 86.3 90.5 B 16 86.8 90.6	AB	86.7	90.9							
A-14 86.7 90.9 3B-14 86.8 90.6 HA 15 86.8 91.0 3B 15 87.3 90.8 A 16 86.3 90.5 B 16 86.8 90.6										-
3B-14 96.8 90.6 14 15 86.8 91.0 3B 15 87.3 90.8 4 16 86.3 90.5 B 16 86.8 90.6		86.7	90.9							
15 86.8 91.0 3B 15 87.3 90.8 A 16 86.3 90.5 B 16 86.8 90.6	3B-14		90.6							
· <del>  </del>	1A 15	86.8	91.0							
· <del>  </del>	3B 15	87.3	90.8							
· <del>  </del>	A 16	8613	90.5							
· <del>  </del>	B 16	86.8								
	# 17		91.8							•
	<del></del>		11,6							

Read	ing			Soun	d Pressur	e Level				
osit Numb		0ve	rall				Octave			
		Awt.	Linear	125	250	500	1000	2000	4000	8000
B	17	37.9	91.8							
A	18	87.2	91.1							
沿溜	18	87.8	90.6							
A	19	86.5	90.5							
B	19	87.0	90,7							
A	20	87.0	91.5							
B	70	87.0	91.0			·				
BABAB	2	86.9	91.3							
B	21	87.4	9.6		<u></u>					
FA	27	88.0	91.0							
3B 1A	22	87.2	91.0							
14	23	87.0	91.5							
3B 7A	23	87.2	91.0							
7A	24	36.5								
B	24	86.4	91.2.							
		87.3	90.5							
D		86.8	90.6							
70	2	87.2	90.0							
$\overline{\mathcal{D}}$	2,	86.9	89.8							
<u>70</u>	3	36.8	90.4							
现记	3	86.8	40.6					·		
10	4	86.1	90.3							
DD	4	86.70	90.6							
10	5	8/000	90.3							,
<u> </u>	5	86.3	90.0	80.7	81.8	83.0	82.2	19.8	177.5	74.8
<u>CC</u>	6	36.8	40.0							
	6	86.7	90.5							
<u>C</u> C	- 7	86.7	90,4							
<u>UI</u>	)/	87.3	91.0						,	
PO	-8	37.2	90.8							
	D8 1	97.9	90.2							
İ	)9	88.8	91.6,							
D	10	88.6	91.4							
DI	211	88.7	915							
		3					,			

Reading			Sour	ıd Pressure	Level				
osition Number	0ve	rall	3541	,		Octave			
Number	Awt.	Linear	125	250	500	1000	2000	4000	8000
CC-11	88.4	91.2							
DD-12	88.8	41,6							
Č( -12	88.7	90.7							
CC-13	89.2	90.9							
PD-13,	89.3	91.3							
CC-14	88.4	91.0							
DD-14	88.8	91.4							
<u>(CC-15</u>	83.7	91.2							
DD-15	89,5	91.2				ာ			
(10-16	87.8	90:7							
DD-16	88.8	91:1							
(10-17)	87.8	90.8							
BD-//	87/	41.4							
(0-18	8/3	91.3							
DD-18	8/,5	91.5							
NC-19	37.4	90.3							
DD-19	88.0	90.7							
10-20	87.3	90.8							
00-20	86.7	40,4							
CC-21	87.3	90.17							
DD-21	87.0	40.7							
CC-28 DD-28 CC-23 DD-23 LC-24 D-24	NA								
DD-69	MA							_	
CC-23	87.0	90.7	•						
D-23	87.5	91.3							
10-24	87.2	90.6 90.8 90.7						_	
D-74	87.3	40,8							
EE-1	8/05/	90.1							
FF-	87.2	90.8		_					
SE-2	669	90.0							
EE-1 FF-1 SE-2 FF-0 FF-0	47.0	90.6							
EE-3	AIU								
FF B	NIX								
EE4	451.3	90.7							

Date 1-67

Reading			Soun	d Pressure	Level				
osition Number	0ve	rall	00411			Octave			
number	Awt.	Linear	125	250	500	1000	2000	4000	8000
F4	87.5	91.0							
EE 5	87.8	91.0							
F 5	87,0	90.5							
E6	87.8	90.7							
F 6	87.5	90.5							
F 7	8,08	70.4							
F 7	88.1	90.4							
E 8	87.5	90.5							
F8	80.0	91.0							
E9	88.0	91.2.							
F q	88.1	90.1							
E 10	88.2	90.5							
F 10	88.0	91.2							
EII	89.0	915							
F 11	88.2	90.8							
EIZ	89.5	91.4							
	N/A:	生态							
F13	89.1	91.5							
	A/N	(*)							
F 14	89.5	91.3							
F 14	N/A								
F 15	1 00. /	91.4							
P 15	88.2	90.9							
16	88.4	90.8						·	
- P 16	84.0	91,5							
EE 17	88.3	91.0							
F 17	89.2	91.5							
E 18	48,0	91.0							
= 1 ,8	A SIL	91.48							
19	80,0	91.0 N/A							
19	7	/Y//-							
CF 21	88.2 89.0 88.3 89.2 98.0 \$8.0 \$8.0 \$1.5 81.4 87.8	90,5							
Lt. (1	01,4	91.5							
21 20	87.8	90.4							

Date 6-10-83

Reading			Soun	d Pressure	e Level				
osition Number	0ve	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	8000
FV	88.7	91.5							
EE 23	87.8	910							
FF 23	88.2	91,0							
EE 24	86.8	91.0							
FF 24	87.5	91.0							
36-1	87.1	90.8							
44-1	87.2	90.5			·				
II - /	87.3	90.8							
GG-2	86.5	90.2							
HH-2	87.0	90.7							
エーン	87.5	90.7							
56-3	87.3	90.7			-				
44-3	875	91.0							
11-3	87.3	91.0							
GG-4	87.6	90,9							
44-4	88./	91.4							
TT-4	94:0	91.5					, , , , , , , , , , , , , , , , , , ,		
36-5	87.4	91.0							
HH-5	87.7	91.6							
11-5	57.4	an.8						يسي	242
3G-6	87.6	90.5							
44-6	975	91.0							
1-6	88.5	91.6						<del>                                     </del>	
36-7	88.3	91.4	-						<del> </del>
44-7	87.8	91.3				ſ			
##-7 II-7	88.7,	01.4	81.7	84.3	85.5	83.4	80.8	99.7	79.0
26-8	88,4	000			00.0	() () ()	$\frac{1}{2}$	1.10	77.0
76-8 14-8	886	90.8							
	88.4	91.13							
1-8 G-9 IH-9 <b>I</b> -9	87.5	91.0							
14-4	878	914							
I-9	88.4	91.6							
6-10	897								
7H-10	88.0	91.0							
11110	00.0	90.1			<u> </u>			<u> </u>	<u> </u>

Reading			Sound	d Pressure	Level				
osition Number	Ove	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	8000
I-10	88.4	91.6							
6-11	87.3	90.6							
14-11	87.8	90.8							
T-11	89.3	91.7							
6-12	87.9	91.2							
14-12	87.7	92.2							
II-12	88.4	91.1						,	
56-13	NH								
44-13	87.6	9/./							
1/-/3	87.8	91.1							
56-14,	11/1-								
14-14	88./	91.3				·			
1-14	88.3	90.8							
36-15	N/A								-
+ 17-15	87.6	90.6				·			
H-15	N/A-	(1)							
9G-16	88.4	91.0							
44-16	88.7	91.1						·	
11-16	NA								
56-11	88.2	41.6							
##-//	88.0	91.3							
#-//	88.3 <sub>c</sub>	010							
11-17 15G-18 17H-18 11-18	88.7	91.7							
74-18	88,4 N/A-	41.3							
11-18	N/#-								
56-19 HH-18 TI -14	N/A 88.7	91.2							
H# 18	80.1	91.0							
11-14	N/A								
20-14	NIA	015							
14-14	DDI	91.5							
1-10	88,2	90.4							
36-19 11-19 56-20 11-20 1-20	N/A-	13,17							
111-4	89.6	91.7							
1-W	88.1	91.2							

Date <u>8-10-83</u>

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Reading Position			Sound	d Pressure	Level				
Number	0ve	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	8000
5G-21	88.3	91.7							
44-21	88.0	91.9							
II-21	87.9	91.2				-	# (* * * * * * * * * * * * * * * * * * *		
36-22	89.3	92.0				,			-
HH-22	88.8	91.7				-			
11-22-	87.9	91.6		-					
36-23	87.8	91.1					2.5		
HH-23	87.9	91.4							4
II - 23	88.2	91:8					, , , ,		
36-24	88,4	91.4							•
44-24	88.2	91.5			~				
II-24	88.0	91.7							
JJ-24	88.5	92,0		·	:				
JJ 23	283	91.7							
II 22	48.7	91.5							
J 21	99.0	91.8							
I) 20	88,5	91.4		\$				_	
J 19	883	97.0			<del>.</del>				
J 18	83.5	91,4							
J 17	910	91.5							
KK 24	98.2	92.1							-
KK 23	88.2	92.2					·		
KK 22	89.2	92.4							
KK 21 KK 21	88,8	91,9							
KK 70	89.7 88.8 87.8 87.5	91,8							
KK 19	67.5	91,7							
KK18	87.9	91.6							-
KK17	87.8	910							
KK16	88.6	91.2							
XX16 XX15	99,5	91.0							
KK14	99,5	91.7							
KK 13	49.2	91,2							
KK12	88.4	91.2 91.0 91.2 91.2 91.2 92.5							
KKII	89.4	924							1
		<del></del>		<del></del>	1	<del></del>	اـــــــــــــــــــــــــــــــــــــ		

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Reading Position		-	Soun	d Pressure	Level				
Number	0ve	rall		_		Octave	·		
	Awt.	Linear	125	250	500	1000	2000	4000	8000
KK 10	90.1	93.0							
CK-9	90.1	92.8			·				
K8	91.0	91 4					4 J. F.	-	
KK.7	92.5	96.4							- 2
KK6	92.0	95.7							
CK 5	90.4	93.4							
KK 4	89.7	97.8			,				
KK3	883	97.11							
KKZ	87.7	91.5					1744		
<b>建</b>	不算								
KKI	87.5	91.7			-				
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Date 8/11

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Reading			Sound	d Pressure	Level				
Position Number	0ve	rall				Octave			
	Awt.	Linear	125	250	500	1000	2000	4000	<b>80</b> 00
Dos	19.3	92.6	82.1	83,8	85.4	86.7	82.6	76.2	71.4
Dos 2	86.2	90.8	53. O	84.5	83.0	80.5	78.6	74-8	71,8
Do 3	87.5	94.8	83,6	84,8	83.1	83.6.	79:5	75.0	72,0
00-1	920	4							
00-7	90.5								
-00-3	90.1								
00-4	90.2				•			•	
00-5	90.0								
00-6	900						7		
00-7	90,0						\- <u>-</u>		•
00-8	90.0				v				
00-9	90.5								
00 10	90.3			.=	<u>;</u>				
DØ 11	90.6								
00 12	91,0								
00 13	90.4								
00 14	90.5			*					
co 15	90.8				-				
00 16	90,3								
00 17	90.3								
00 18	10.0		·						
00 19	49.2								
00 70	87.8								
00 71	86.2		· ·						
Hock 1	103.2	106.0	95.8	100.8	100.0	98.6	95.6	89.0	84.7
	Figure 1								
LIVE	44.4	91.4	82.5	83.2	83,3	84.0	81,0	79.5	78,2
						7,1			
Hock 2	101.7	104,8	96.2	99.7	99.3	97.8	93.4	87,7	94.1
									<u> </u>
<u> </u>									
	.1	1	<u> </u>		<u> </u>	ļ <u>.</u>			<u></u>

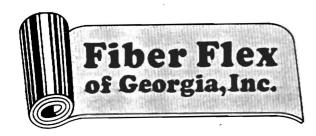
# NOISE SURVEY DATA SHEET Perdue Poultry Processing Plant Lewiston, N.C. Date 8-9 Thru 8-11

Dosimeter Reading Position Number	Sound Lev 94% 54%	Pressure  Yel  TWA-SPL  96.5dBA  97.4dBA  84.6dBA	Duration (hrs min.)  130 - 430  135 - 431  140 - 433	
0) K 17 1 N 54	30% 84% 32%	88.2 JBA	8:52 - 11:49	
DD:5 10:TT 13: 10:KK 19	29% 00/10/2 32%	88.0 dBA 88.8 dBA	1:10 - 4:10 1:12 - 4:11 1:16 - 4:12	
205 1 205 2 2053	1476   1876   1070	90.5 ABA 87. I ABA 88. 4 ABA	9:50 -10:56 10:05 - 11:03 10:15 - 10:15	
Dosimeter reading	g appears	highly mace	curate - Value suspect	
		100 pom	The control of profits	ly —
			the control of proper	

#### APPENDIX C

Selected Technical Brochures on Commercial Baffles Designed for Use In Food Processing Applications

(Note: This display in no way constitutes an endorsement of any product by Georgia Tech)



### **Testing Data for Acoustic Panels**

#### **TEST METHOD:**

The sound absorption tests were conducted in accordance with ASTM C423-81. For the A mounting a 80 square foot sample was placed directly on the Reverberation Room floor.

Hanging: the baffles were suspended six feet from the Reverberation Room floor in three rows of three each, rows were three foot on center, the baffles were placed end to end in each row to form rows 12 feet in length. The values obtained for the suspended baffles are reported in sabins per baffle. This is the amount of absorption which can be expected for each baffle of this design when placed in an array similar to that used for evaluation.

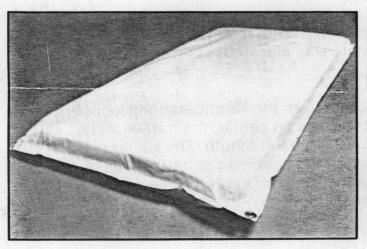
#### **RESULTS:**

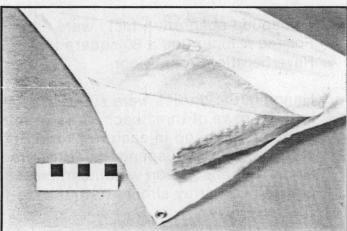
OCF Test Mounting		Sound Absorption Coefficients 1/3 Octave Band Center Frequencies, Hz.
No.	No.	125 250 500 1000 2000 4000 NRC
A48781	4	.53 1.24 1.29 1.09 .80 .46 1.10
		Sabins/Baffle 1/3 Octave Band Center Frequencies Hz.
		125 250 500 1000 2000 4000 Avg. (250-4000)
A48681	Hanging	3.06 8.22 15.00 14.03 10.37 5.85 11.90

In the preceding table, some of the measured coefficient values are shown greater than 1.00. This is a real effect which is due to the diffraction of sound waves adjacent to the test specimen. As recommended by the ASTM C-423 test method, no adjustment has been made to these coefficient values.



### **Fiberflex Acoustic Panels**





FEATURES	BENEFITS
Of Acoustic Panel	To User

Fiberglas ......High accoustical performance

Reinforced Polyester Film Covering . . . . . High accoustical transmission

Long wear life High resistance to tear

Total encapsulation ......Permanent vapor barrier protection for

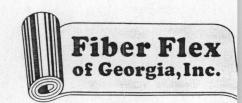
acoustical insulation

of installation

USDA Approval ......Product can be used in most food

processing applications

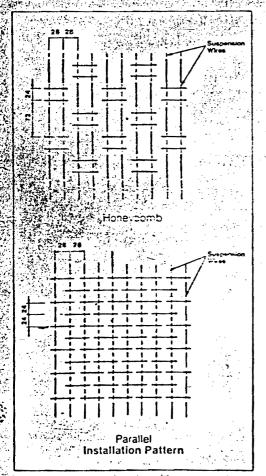


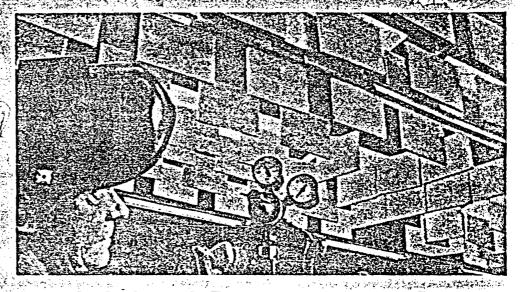


### Peabody Noise Control

### baffles

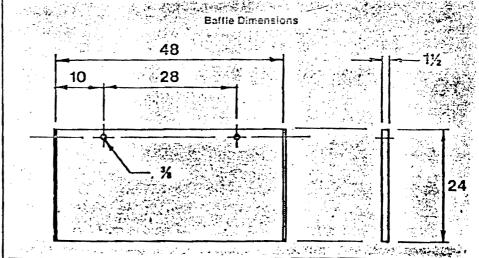
Kinetics Noise Control Baffles are used to reduce overall noise levels in industrial, recreational, or other high noise areas, and are suspended from wires or from the structure near the noise source. Kinetics Noise Control Baffles are 2.7 pcf fiberglass, 2'0" x 4'0" x 11/2" thick sealed into a 3 mil white fire retardant vinyl film cover. When tested according to UL E-84, the cover material exhibits flamespread of 15, smoke development of 45, and fuel contribution of D. The Average Absorption rating of Kinetics baffles is 10 Sabins. Actual noise reduction can be up to 10 dB, but depends on the way was configuration of the space and the absorption present before installing baffles. Baffles are packaged ten (10) per carton





Acoustical Per	Absorpt	
125 250 500 1000 2000 4000	.11 32 .69 .73 .43	2.0 5.8 12.5 13.2 7.8 3.8
A NRC	55	AV 10.0

When suspended in the Honeycomb Pattern, .42 Baffles can be installed per square foot. When suspended in the Parallel Pattern, .54 Baffles can be installed per square foot.



	n Absorption Coefficient
Terminology	Description
Hard	All (6) Surfaces Brick, Concrete, Marble, Tile, Steel
Medium Hard	(5) Surfaces Hard, (1) Surface Absorptive — Carpet,
	Acoustical Tile, Drapes, or Open to the Outside
Medium	(4) Surfaces Hard, (2) Surfaces Absorptive
Medium Soft	(3) Surfaces Hard, (3) Surfaces Absorptive
Soft	(1) or (2) Surfaces Hmz. Balance Absorptive

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#### Example:

Consider an 80' x 40' x 20' industrial plant.

Step 1 Determine surface area:

 $80 \times 20 \times 2 \text{ (walls)} = 3200$  $40 \times 20 \times 2 \text{ (walls)} = 1600$ 

 $80 \times 40 \times 1$  (ceiling) = 3200  $80 \times 40 \times 1$  (floor) = 3200

Total Surface 11200 so

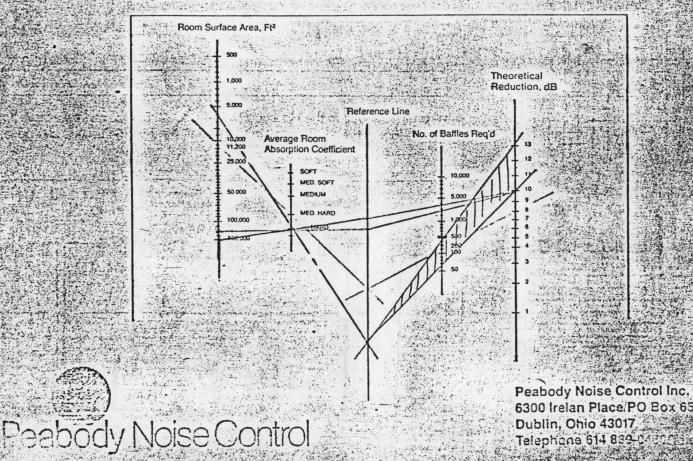
Step 2 Determine the overall acoustical character of the building.

Assume this building is medium hard since the floors and walls are hard and the ceiling is medium.

Step 3 Connect 11,200 ft.2 and medium hard on the nomogram. Extend the line to its intersection with the vertical reference line.

Step 4 If an 8 dB noise reduction is desired, connect a line between 8 on the "Reduction" scale, and the intersection point on the "Reference Line"

Step 5 Read 200 as the number of baffles required on the "Required" line



### Armstrong

### Vertical Baffle Sound Absorbers

#### **Industrial Acoustical Control**

Armstrong Vertical Baffle Sound Absorber panels are designed for overhead installation in exceptionally noisy areas such as:
industrial plants machine shops food-processing plants gymnasiums

These panels are particularly effective in all areas where reduction of excess sound, especially in the reverberant field levels, is desirable.

Made of a mineral-fiber core encased in an opaque white Tedlar\* film, the panels are unaffected by moisture or high humidity. They have excellent ultraviolet stability, capable of withstanding up to 2,000 hours of U-V exposure without any significant change in physical properties or appearance.

Easy to install, the panels are supplied fully assembled with an integral hanging system.

· Du Pont Company



Size and Detail

2'x4'x1½" (nominal) panels Mineral-fiber core, encased in Tedlar film Opaque White 8 lb/unit

Fire Data

Flame spread: 0-25 (ASTM E 84 Tunnel Test) Class A—Federal Spec. SS-S-118B, Class IV

Maintenance

The exceptionally durable Tedlar surface is easy to clean. Any regular detergent is suitable for most problems—any really tough situations may require stronger solvents—use of either will not damage the Tedlar surface.

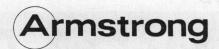
These washable baffles are acceptable by USDA for use in meat- and poultry-processing plants.

**Acoustical Data** 

Sound-absorbtion-tested according to ASTM C 423, Sound Absorbtion of Acoustical Materials in Reverberation Rooms.

Vertical baffles suspended in rows, 4' oc

Freq. (Hertz)	Sabins/Unit
125	3.6
250	4.4
500	9.5
1000	13.9
2000	13.2
4000	10.2
Four-freq. average	10.2



# Sound Absorber Lay-in Panels

#### Industrial Acoustical Control-Lay-in Panels

As a special order, these mineral-fiber shrink-wrapped panels are available as 2'x4' lay-in panels. Their physical properties are similar to those of the Armstrong Vertical Baffle Sound Absorber panels, but rather than hanging from the ceiling they may be installed directly in a conventional grid system.

They are USDA-approved for use in meatand poultry-processing plants and are easy to clean.

#### **Acoustical Data**

Sound-absorption-tested according to ASTM C 423, Sound Absorption of Acoustical Materials in Reverberation Rooms.

Lay-in units, mounting #7

Freq. (Hertz)	Absorption Coefficients
125	.37
250	.56
500	.77
1000	.92
2000	.89
4000	.71
NRC	.80

#### Installation

Baffles and Lay-in Panels

**Baffles**—are suspended from wires or cables attached to structural members of the building. This system allows for quick, easy installation or replacement.

Calculations to determine suspension cable size and anchoring should be based on a weight of 8 lbs. per baffle. Slight differences in acoustical performance are obtained by varying the pattern of installation.

**Lay-in Panels**—may be cut for border applications or for pipe or conduit perforations. Simply cut the film with a knife or razor blade to provide an overlapping flap to cover board edges, then cut the board to size. The film is resealed using a Tedlar tape such as 3M No. 838.

These panels are installed in standard grid systems.

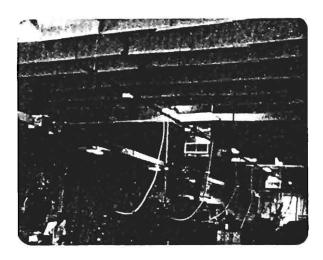
For further information on Armstrong Vertical Baffle Sound Absorbers, contact your Armstrong Representative.

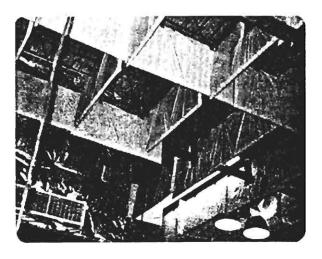


### industrial noise control, inc. CASE



A successful noise control project requires proper planning, appropriate materials, and competent installation. This report represents a factual summary of a situation where we and our customer worked together to solve a noise problem.





### The Problem:

Noise level in the press room of a manufacturer of electrical switch parts was consistently running at 95-96 dBa during punching operations. The level was considered to be hazardous for the workers.

#### Limitations:

The 18 presses, all contributing to the overall noise level in the room, were arranged close together and the operational scheme was such that enclosures or screens would be a "last resort" solution.

#### Solution:

Since the floor, walls, and "ceiling" in the  $110' \times 58' \times 20'$  high room were hard surfaces, it was decided that free hanging absorbers, hung from bar joists and perpendicular strung wires would have a substantial effect on the overall noise level with virtually no interference to the production scheme.

INC Type 24-T absorbers were hung, one per each 9.4 square foot of floor area (680 absorbers in all). They were hung in an egg-crate array to achieve proper installation density, ventilation, and appearance.

### Measured Results:

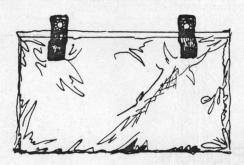
Tabulation of reduction of 12 strategic points revealed a minimum of 4 dB reduction, maximum of 7 dB. The project was considered successful; worker exposure was well within OSHA reguations

This case history, from the engineering files of INC Systems, is made available to Noisemart customers to illustrate usage of materials that have been field tested, proven, and available off the shelf from INC NOISEMART.

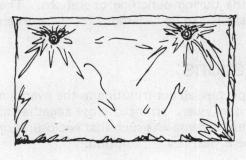


en noise pollution becomes your problem make it ours

industrial noise control, inc.



24-7



24-G

### About the Product:

The I.N.C. 24 Series absorber is a very efficient noise reducing device when used in specific situations. Those situations are generally where there are many noise sources in a factory area and much of the noise is being reflected from hard surfaces. It is generally not a good idea to hope for more than two or three dB overall reduction in a situation like this one but very often reductions are greater. In cases where four or five dB reduction would "solve the problem" it is usually practical to employ absorbers as a first step.

Free hanging absorbers are also very effective when used in conjunction with screens and partial enclosures or in just about any situation where noise is being reflected to other parts of an enclosed space.

The cost of the materials used on this particular job was approximately \$2600.00. Installation costs will vary with specific circumstances.

BAFFLES ARE AVAILABLE WITH TABS OR GROMMETS.

Color photos available upon request.

The growth of INC since 1970 has been strictly in response to the need for noise control in industry. In essence, our customers have dictated the kinds of services and products we offer.

Consequently, it is highly probable that your specific needs for noise control match our capabilities.

PLANNING . SYSTEMS . MATERIALS . INSTALLATION

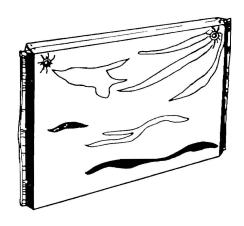
When noise pollution becomes your problem . . . make it ours®



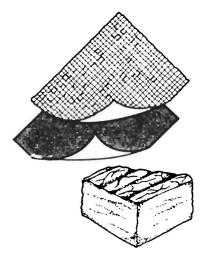
industrial noise control, inc.

#### AB-1000 NOISE ABSORBING BAFFLES

Safe, low cost baffles for industrial, commercial, school or institutional use with complete protective cover and non combustible media. Installation method and hardware for various ceiling and deck structure can be provided.

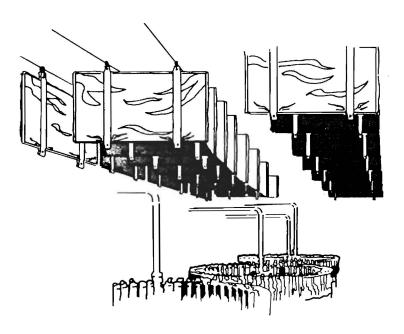


AB-1000 BAFFLE



#### TOCKING DISTRIBUTOR

omprehensive selection of bulk materials. e can help select the optimum for your application.



Food Can Fill Room

- Firm, dense, media enclosed in plastic cover maintains shape therefore retaining absorption performance and good appearance.
- Noise absorption rating of media NRC = .90

Baffle installations can produce 4 to 6 db reduction; combined with barriers 10 to 18 db reduction can be achieved. We will evaluate your potential application and recommend use only when conditions dictate success.

- Flexible, weighted, barrier vinyls. A variety of weights, colors, strengths and fire ratings.
- Quilted Fiber Glass Absorbers. Bulk or fabricated panels. Also available in a composite with barrier.
- VinyI/Foam and Lead/Foam composites.
- Damping Products: Compounds, sheets, pre-damped sheet metals for any damping application.
- · Prefabricated Acoustical Panels.
- Accessories to apply materials including adhesives.